



Article

The Effect of CO₂ Laser Engraving on the Surface Structure and Properties of Spruce Wood

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Abstract: This work appraises the influence of CO₂ laser irradiation on mass loss, morphology, chemical changes and discolouration of spruce wood surfaces. The amount of energy applied to the surface was expressed as the total irradiation dose, which was demonstrated to have a strong impact on increasing wood weight loss. Along with increasing mass loss, surface roughness also increased, resulting from the differences in density between the early wood and late wood. The evaluated roughness parameters increased linearly with increasing irradiation dose and mass loss. At the maximum irradiation dose, the Ra parameter value parallel to the fibre direction showed a 6-fold increase; perpendicular to the grain, the increase was as much as 33.5-fold. Similar differences were also observed for the parameter Rz. At the lowest laser power and the lowest raster density, the engraved spruce wood surface exhibited some evidence of discolouration ($\Delta E^* \cong 9$). An additional increase in the amount of supplied energy clearly resulted in a novel surface colour compared to the original ($\Delta E^* = 12$). The chemical analysis of the wood surface revealed that the discolouration was mainly caused by heat-induced cleavage of C=O groups in the lignin and hemicellulose structures. Part of these structures (so-called chromophores) are responsible for the natural colour of the wood as well as for colour changes caused by engraving. The detected dependences of the wood mass loss and colour values on the total radiation dose are the basis for achieving targeted modifications of spruce wood surfaces using a laser beam.

Keywords: CO₂ laser; spruce wood; engraving; raster density; laser power; morphology; roughness; FTIR analysis; colour



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1. Introduction

Wood surface treatment with CO_2 laser is, aside from cutting, increasingly used to attain proposed changes in wood surface properties, especially those concerning morphology and colour. The energy of the laser beam absorbed in the surface structures of the wood is converted into heat, thus inducing sublimation of the thin surface layer of the contact area between the laser beam and the wood surface. After this treatment, structural changes occur on the surface of the wood, accompanied by melting and formation of a carbonised layer. This is reflected in altered wood surface morphology, discolouration and changes in other surface properties [1–10].

The wood mass loss affects its surface geometry. However, variable results are reported by different authors. Several works [2,3,8,11] show that laser irradiation of wood can result in a reduction in surface roughness, due to melting cells down to a depth of several micrometres. In this way, ablation of the wood surface fibres released by the precedent machining can lessen roughness. On the other hand, the engraving of wood surface with a laser may exert the opposite effect, i.e., increased roughness [7,8,12–14]. The roughness is mainly attributable to non-uniform wood mass degradation within an annual ring due to differences in density between early wood and late wood [8]. The roughness is notably affected by the fibre angle under which the wood surface is treated [15]. The published

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results confirm that, via appropriate adjustment of the CO₂ laser engraving parameters, targeted changes in the wood surface morphology can be ensured [8,13,14].

The results obtained by applying Fourier transform infrared spectroscopy (FTIR), X-ray photoelectron spectroscopy (XPS) and gas chromatography (GC) imply that the energy absorbed by the wood surface during CO_2 laser irradiation causes chemical alterations in the main wood components. Proportionate to the energy amount applied, there are reduced polysaccharide amounts as a result of degradation of hemicelluloses and a certain part of the amorphous cellulose fraction [16]. Changes in the lignin structure and an increase in non-polar C–C and C–H bonds were also observed. These chemical changes are also dependent on the wood species [1–4,8,17].

The changes in morphology and chemical structure associated with wood treatment with a CO_2 laser initiate surface discolouration—manifested as darkening [4,7,8,18–21]. The degree of darkening of the engraved surfaces is dependent on the amount of energy applied, the manner of its application and the width of the engraved track formed by the laser beam passing across the wood surface [8,20,22]. A single laser beam path, aside from track discolouration, causes the removal of a narrow strip of the surface layer. At higher raster density (number of paths per one millimetre of width), the mass loss is more evident at spots where the paths overlap. There is also more apparent discolouration [6,8,23–25].

The extent of changes in surface structures of engraved wood are also dependent on the degree and method of energy supply. This energy is possible to control via adjustment of the laser power, the movement speed of the laser head, focal distance and raster density [2,4,7,8,12,19,24,26]. Apart from the energy amount, the thickness of the sublimated layer and the changes in the engraved surface structure are dependent on the wood species, and also on structural heterogeneity occurring within a single species [1–3,7,8,11,27,28].

Recognising the impact of all the aforementioned factors is necessary, not only from the viewpoint of the proposed changes to the wood surface structure, but also with regard to the intended discolouration of the modified wood surface. The wood colour is a characteristic feature of the wood. The changes in the colour coordinate values, L^* , a^* and b^* , are relatively easy to measure and, as such, they can serve as indicators of significant chemical changes—and changes in other wood properties—resulting from a specific surface treatment (IR radiation, UV radiation, thermal modification and similar) [29]. This is the main reason for the interest in this issue today [6,8,13,15,25,26,30-33].

To date, the intended colour modification of a particular wood species has mostly been achieved through practical experience. There, however, arises evidence that this could be approached by quantifying the relationship between the discolouration and the total energy amount delivered onto the wood surface. Fixing the specific laser parameters allows the determination of the total energy applied to the wood surface and its impact on discolouration [8]. As the colour spaces of the different wood species are practically disjunct, the first study phase is to recognise these relations for a particular wood species.

To achieve this goal, it is necessary to perform comprehensive studies on wood surface property modifications in individual wood species using identical methods. It has been shown that the amount of energy delivered onto the wood surface with a laser beam can be expressed through the irradiation dose, $H(J \cdot cm^{-2})$ [8]. Recognising the dependence of discolouration on the total irradiation dose provides a basis for proposed changes to the surface of individual wood species treated with a CO_2 laser.

This work aimed to evaluate the influence of a $\rm CO_2$ laser on the structure, surface morphology, chemical changes and discolouration of spruce wood. The following investigations were conducted:

- Determining the total irradiation dose under variable parameters of s CO₂ laser (laser power and density) and this dose's impact on the wood mass loss;
- The influence of the treatment method on the morphology of the wood surface quantified through roughness parameters;
- Changes in FTIR spectra and discolouration corresponding to various engraving parameters;

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Determining the functional dependence of the colour coordinates on the total irradiation dose.

2. Materials and Methods

2.1. Experimental Materials and Irradiation Conditions

The samples were prepared from spruce stems by cutting logs at a height of approx 1.3 m. The log length was 2 m, with the diameter ranging from 0.4 to 0.5 m. The logs were used for preparing radial timber which was gradually dried to 12% moisture content. From each log, one plank was selected with a 1000 mm \times 80 mm \times 20 mm size, which was used to prepare test samples with a radial surface of 100 \times 50 mm² (Figure 1). From each plank, two specimens were randomly selected and subsequently conditioned to 6% moisture content before sanding (P180 grit). The samples' oven dry density ranged from 405 to 440 kg·m $^{-3}$.

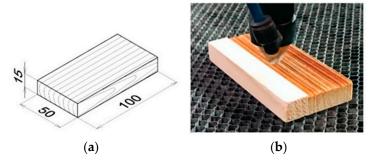


Figure 1. Wood surface engraving with a CM-1309 CO₂ laser. (a) Specimen's radial surface; (b) engraving process.

Engraving of samples followed previously described methods [8]. The samples were placed under the focus of the lens of the CO_2 laser equipment (CM-1309, Shenzhen Reliable Laser Tech, Shenzhen, China). The samples 'distance from the lens was 17 mm. The laser head moved over the samples' surface parallel to the grain. Moving speed of the laser head was 350 mm·s⁻¹ (Figure 1), and maximum laser power was $P_{\rm max} = 137.5$ W (measured on the resonator output according to the method described in previous work [8]). The amount of radiation energy varied according to laser power and raster density. From each wood species, three sample sets were prepared and engraved at laser powers of 8, 12 and 16% (assigned based on the $P_{\rm max}$).

The following raster densities were used: 2, 5, 10, 20 and 30 mm⁻¹, representing, for each wood species, 5 combinations each consisting of 4 samples (plus 4 non-engraved "reference" samples). The samples were irradiated along their entire length and width (Figure 1). The laser parameters were set based on our experience with previous measurements [34], as well as from information collected from the literary sources referenced in Section 1 (Introduction).

The amount of energy applied was expressed as the total irradiation dose, H, per unit area. The H value was, in accordance with the previous work [8], calculated using the following equation:

$$H = \frac{P_{\mathbf{e}} \cdot x \cdot n \cdot y}{A \cdot v} \tag{1}$$

where P_e is the effective power of the laser beam on the sample surface, x is the sample length, n is the raster density, y is the width of the track incised by the laser beam by one path on the wood surface, v is the speed of the laser head movement and A is the area irradiated by one laser beam path. The track width was measured with the aid of a camera (Leica EC3, Leica Microsystems, Heerbrugg, Switzerland).

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2.2. Evaluation of Weight Loss of Wood Mass

The wood mass loss resulting from CO_2 laser engraving was evaluated on the samples prepared from each particular wood type. The samples were dried to constant weight at a temperature of 103 ± 2 °C. The dry samples were removed from the drying chamber and placed in an exicator containing silica gel. After cooling, the samples were weighed on a laboratory scale (Precisa 300A, Precisa Gravimetrics AG, Dieticon, Switzerland) with a precision of 0.001 g (mass m_{01}). The prepared samples were engraved at specified laser powers and raster densities. After this process, the samples were weighed again (mass m_{02}). Then, the equation

$$m = \frac{m_{01} - m_{02}}{A_0} \cdot 100 \tag{2}$$

was used for calculating the weight loss of the wooden mass per unit area, A_0 .

2.3. Evaluation of Wood Surface Morphology

Wood surface morphology after laser treatment was evaluated from the viewpoints of anatomy and physics [34]. The roughness profiles were measured with a profilometer (Surfcom 130A, Carl Zeiss, Oberkochen, Germany) consisting of a measuring unit and an evaluation unit. The changes to the wood surface morphology induced by CO_2 laser engraving were evaluated with respect to the following roughness parameters: Ra (mean arithmetic deviation) and Rz (the maximum peak height plus the maximum depression depth within the cut-off, or sampling length).

The roughness was measured on the irradiated radial surfaces, both parallel with and perpendicular to the grain course. This measurement process started by filtering off the waviness from the basic profile, and then the roughness curve was transferred onto the basic line. The entire transverse length consisted of the run-up segment, l_r ; five sampling length (cut-off) segments, λ_c ; and the over-travel segment, l_p . The basic lines were chosen from the interval 0.025 to 8 mm, based on the preliminary measurements of the roughness parameters, Ra and Rz. For studying the structure of the engraved oak wood surfaces, a light microscope (Leica MZ 9.5, Leica Microsystems, Heerbrugg, Switzerland), camera (Leica EC3) and a digital microscope (Keyence VHX 7000, Keyence International, Mechelen, Belgium) were used. Microscopic slides of the transverse cuts were prepared according to the methods described in a previously published work [7].

2.4. Evaluation of Colour

The colorimetric values L^* , a^* and b^* on the reference and engraved surfaces were measured with a spectrophotometer (Spectro-Guide 45/0 gloss (BYK-GARDNER GmbH, Geretsried, Germany) [8]. The measurements were made at ten locations on each sample. The colour differences, ΔL^* , Δa^* and Δb^* , and the total colour difference, ΔE^* , were calculated according to the following equations:

$$\Delta L^* = L_2 - L_1 \tag{3}$$

$$\Delta a^* = a_2 - a_1 \tag{4}$$

$$\Delta b^* = b_2 - b_1 \tag{5}$$

$$\Delta E^* = \sqrt{\Delta L^{*2} + \Delta a^{*2} + \Delta b^{*2}} \tag{6}$$

where the subscript "1" represents the colour values in the reference sample (not engraved), and "2" indicates the values of the wood sample irradiated with the CO_2 laser.

2.5. Detecting Chemical Changes after Engraving

Chemical changes were examined in samples irradiated at 8% and 16% laser power (P_e) and raster density (n) with values 10, 20 and 30 mm⁻¹. For this purpose, FTIR analysis was used. FTIR spectra of the engraved surface of the samples were recorded on a Nicolet

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iS10 FTIR spectrometer (Thermo Fisher Scientific, Waltham, MA, USA), equipped with a Smart iTR diamond attenuated total reflectance (ATR) sampling accessory. The spectra were acquired by accumulating 64 scans in absorbance mode at a spectral resolution of 4 cm⁻¹ over the range 4000 to 650 cm⁻¹ with baseline correction. Each spectrum was obtained by applying a constant gauge pressure for intimate contact with the ATR crystal (internal reflection element). The diamond crystal was cleaned with ethanol between scans. The obtained data were analysed using OMNIC 9.0 software (Thermo Fisher Scientific, Waltham, MA, USA). Four replicate measurements were performed on the radial surface of each sample.

3. Results and Discussion

The interactions between the laser beam and wood surface were significantly influenced by all engraving process parameters, with important impacts on wood surface chemistry, morphology and colour alteration.

3.1. Total Irradiation Dose and Wood Mass Losses Corresponding to Different Irradiation Parameters

To avoid multifaceted evaluation of the impacts of all the tested laser parameters on the changes in structure and properties of the tested wood surface, all these parameters were replaced with a single variable—the total irradiation dose (H) determined according to Equation (1). The irradiation dose per unit surface area of the samples (at specified parameter values) were calculated according to the given equation and are summarised in Table 1. This shows that values of H ranged from 6.17 to 185.15 J·cm⁻².

Table 1. Irradiation dose supplied per surface unit area, corresponding to specific laser power and
raster density.

Power [%] 8		16
11	16.5	22
	Irradiation dose H [J·cm ⁻²]	
6.17	9.26	12.34
15.42	23.14	30.86
30.84	46.28	61.71
61.68	92.57	123.43
92.52	138.85	185.15
	6.17 15.42 30.84 61.68	11 16.5 Irradiation dose H $[J \cdot cm^{-2}]$ 6.17 9.26 15.42 23.14 30.84 46.28 61.68 92.57

Almost all energy concentrated in the laser beam and applied to the given spot on the spruce wood surface was converted to heat. Experimental measurements performed using a thermo-camera with an upper measuring limit of 1000 °C revealed that, at as low as 8% laser power (11 W), the temperature of the wood surface at the moment of impact of the laser beam was near to this limit. The high temperature concentrated within the laser beam of minuscule diameter induced instantaneous sublimation of the thin surface layer at the contact spot. A qualitatively similar phenomenon was also observed in the case of oak wood [8].

There has been a confirmed close dependence of the wood mass loss per unit area on the total irradiation dose supplied to this area (Figure 2). Due to the heterogeneous spruce wood structure, the wood mass loss corresponding to specific engraving conditions was variable across the wood surface. This fact was significantly reflected by the wood surface morphology (Figure 3).

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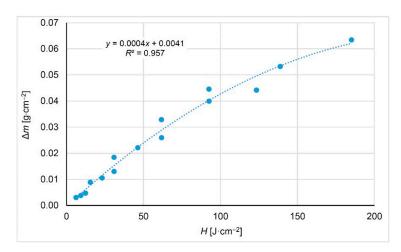


Figure 2. Wood mass loss, Δm , in dependence on the total irradiation dose, H, in spruce wood.

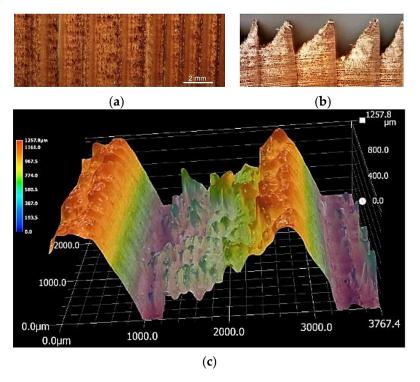


Figure 3. Spruce wood engraved with a CO_2 laser performing at a power of 8% (11 W) and a raster density of 20 mm⁻¹. (a) Radial surface, (b) transverse cut and (c) annual ring detail after engraving.

Figure 3 shows trenches resulting from engraving the spruce wood radial surface. The trenches were parallel to the grain course and, thus, they enhanced the wood roughness mainly in the direction perpendicular to the grain course. With the raster width of 0.14 mm, consequently, beginning with a raster density of $10~\rm mm^{-1}$, the trenches were overlapping. At the overlapping spots, the wood mass losses were higher and the original trenches more pronounced. These phenomena were accentuated in wood of lower density.

The most obvious variations in wood morphology were mainly observed within annual rings. In the case of spruce wood annual rings, there were distinct differences in density between early wood and late wood. The average density of early spruce wood is $300~{\rm kg\cdot m^{-3}}$, while that of late wood is $750~{\rm kg\cdot m^{-3}}$ [35]. The cited work shows that neither early nor late wood density depends on the cambial age. On the other hand, the cambial age influences the annual ring widths, and, in this way, also the proportions of the early and late wood in particular rings. With increasing cambial age, the annual rings become narrower due to the decreasing proportion of the early wood.

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At the beginning of the growing season, there is an obvious boundary between the early wood and the late wood. In its proximity, the density of the early wood is the lowest, which was also reflected in the intensive wood mass erosion. With the advancing vegetation period, the early wood was gradually transformed to late wood, the wood density increased, and the wood mass destruction declined as a result (Figure 3c).

The wood density variability, both intra- and inter-species, can be acknowledged as an important factor influencing the surface roughness in the engraving process with a CO_2 laser, in line with other work [1–3,8,28].

3.2. Roughness of Wood Surfaces Engraved with a CO₂ Laser

The surface morphology after laser engraving was evaluated on the experimentally measured roughness profiles parallel with and perpendicular to the grain course. Figure 4 illustrates roughness profiles measured using a mechanical profilometer perpendicular to the grain course before and after engraving with a $\rm CO_2$ laser performing at a laser power of 8% and a raster density of 20 mm $^{-1}$. Figure 5 displays a roughness profile measured with an optical profilometer at a laser power of 16% and a raster density of 30 mm $^{-1}$. All the measured roughness profiles were evaluated through the roughness parameters $\it Ra$ and $\it Rz$. Figures 4 and 5 show how the non-uniform wood mass erosion within the individual annual rings was reflected by (1) distinct deepening of trenches in the early wood and (2) distances between areas of profile unevenness.

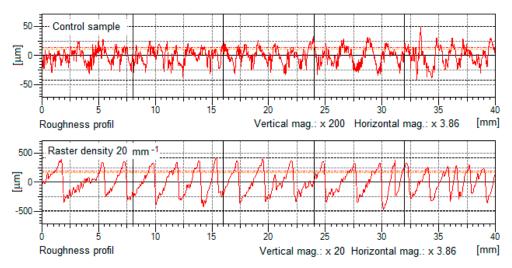


Figure 4. Roughness profile measured perpendicular to the grain course, before and after engraving with a CO_2 laser performing at a power (P_e) of 8% (11 W) and a raster density (n) of 20 mm⁻¹.

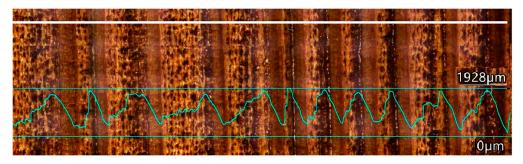


Figure 5. Roughness profile (green curve) measured perpendicular to the grain course, after engraving with a CO_2 laser performing at a P_e of 16% (22 W) and a n of 30 mm⁻¹.

Three-way variance analysis confirmed significant impacts for all the three evaluated factors (raster density, laser power and anatomical direction) and their interactions on the inspected roughness parameters. The basic statistical characteristics of the values of the

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parameters *R*a and *R*z for the given raster density range for all three laser power values and the two anatomical directions are presented in Table 2. Table 2 shows that the values of the roughness parameters *R*a and *R*z in the reference spruce wood samples exhibited the lowest roughness parameter values, both in the grain course and parallel to the grain. The reference roughness was distinctly higher perpendicular to the grain, following from the orientation of the main cell elements.

Table 2. Basic statistical characteristics for roughness parameters of spruce wood engraved with a laser performing under different irradiation conditions.

	Basic	Laser Po	ower 8%	Laser Po	ower 12%	Laser Po	wer 16%	
Raster Density [mm ⁻¹]	Statistical			Roughness	Parameters			
	Character.	Ra	Rz	Ra	Rz	Ra	Rz	
		[µm]						
				Parallel to	the Grain			
D. C	\overline{x}	7.25	50.73	7.25	50.73	7.25	50.73	
Reference	s	2.86	21.13	2.86	21.13	2.86	21.13	
2	\overline{x}	11.41	73.26	8.58	62.99	10.28	77.60	
2	s	3.27	21.34	3.86	30.40	3.58	32.59	
	\overline{x}	21.66	107.83	13.90	93.52	12.03	77.35	
5	s	8.80	38.50	5.60	40.38	4.10	20.12	
10	\overline{x}	27.67	180.31	25.02	167.35	27.23	179.07	
10	s	8.13	44.99	8.55	55.40	10.34	58.68	
20	\overline{x}	28.34	185.38	34.36	231.88	41.18	203.08	
20	s	9.74	63.07	11.70	62.20	1.89	23.51	
20	\overline{x}	36.27	231.14	37.26	243.36	44.34	245.16	
30	s	9.69	60.18	2.54	24.67	5.19	32.18	
				Perpendicula	ar to the grain			
D (\overline{x}	11.64	89.32	11.64	89.32	11.64	89.32	
Reference	s	1.58	19.20	1.58	19.20	1.58	19.20	
	\overline{x}	37.85	214.36	40.84	230.39	45.15	241.00	
2	s	1.34	16.32	2.27	17.22	2.01	15.14	
-	\overline{x}	44.34	229.59	42.29	239.17	46.52	254.77	
5	s	2.17	22.33	2.23	23.31	2.68	27.13	
10	\overline{x}	103.72	497.03	117.57	532.06	170.12	766.84	
10	s	18.18	76.13	20.86	56.64	18.24	46.68	
20	\overline{x}	210.73	903.06	283.62	1074.25	310.24	1122.00	
20	s	34.97	103.13	9.91	31.93	5.80	18.73	
20	\overline{x}	273.03	1132.5	320.25	1245.48	389.88	1433.28	
30	S	17.56	70.12	8.27	37.69	7.26	46.22	

The values of arithmetic mean, \bar{x} , and standard deviation, s, were each calculated based on 60 measurements. The "Reference" is an untreated surface.

The results confirm that the wood surface engraving with a CO_2 laser resulted in significant increases in roughness parameter values, which is in accordance with other research [8,12,14,15,19]. A more significant roughness increase was obtained by increasing n than by increasing the P_e (Figure 6).

We conclude that the *R*a and *R*z grew linearly with wood mass loss (Figure 7). At the maximum wood mass loss, the roughness parameter increase in the grain course was several times more than that of the reference value, while perpendicular to the grain, the increase represented even more than one order.

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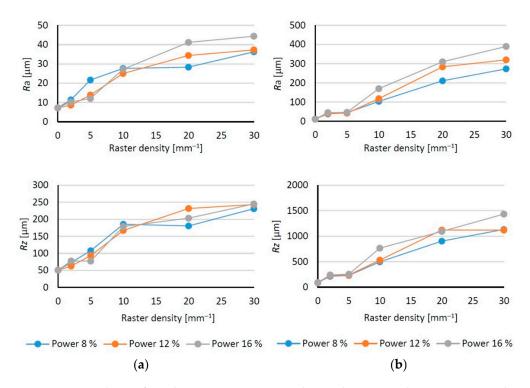


Figure 6. Dependence of roughness parameters *R*a and *R*z on laser raster density in engraved wood surfaces at laser power vales of 8, 12 and 16%. (a) Parallel to the grain; (b) perpendicular to the grain.

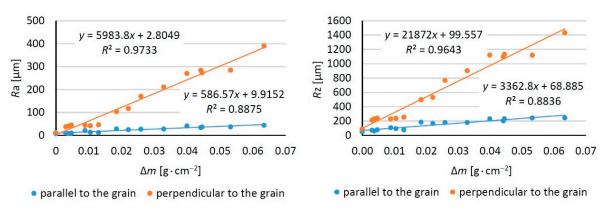


Figure 7. Dependence of roughness parameters Ra and Rz on wood mass loss.

Many early-wood and late-wood tracheids on the engraved spruce wood surface were carbonised. This phenomenon was mostly observed at higher raster densities (20 and 30 mm⁻¹) and at laser power values exceeding 16 W. In the case when the surface layer consisted exclusively of early-wood tracheids, their cell walls were often disturbed due to burn-through by the laser beam, and due to the removal of the very unstable carbonised layer (Figure 8a,b). The radial surfaces also exhibited the occurrence of melted mass, largely due to the resin outflow (Figure 8c). This phenomenon, on the other hand, was more frequent at lower values of raster density and laser power.

3.3. Changes in the FTIR Spectra

FTIR spectra were examined by applying the ATR technique on the wood surface before and after CO₂ laser engraving. The absorption band with a peak at 3350 cm⁻¹ (O–H vibrations in the lignin structure, in hemicelluloses and in cellulose) [16,36], showed apparent variations at all levels of raster density and laser power. Absorbance increase was mainly evident at lower raster densities, while density increase was, contrarily, associated with decreasing absorbance. The reduction of O–H groups was accompanied by

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condensation of lignin and oxidation to C=O groups [37]. The area from 2950 to 2850 cm⁻¹ (asymmetric and symmetric C-H stretching vibrations in aliphatic compounds) [38] manifested similar patterns. The range from 1800 to 800 cm⁻¹, typical for the stretching and deformation vibrations of all wood components, exhibited more conspicuous variations in the absorbances. The treated samples generally showed increasing absorbance in proximity to 1730 cm⁻¹ (stretching vibrations in unconjugated C=O groups) with increasing raster density of the engraving laser (Figures 9 and 10).

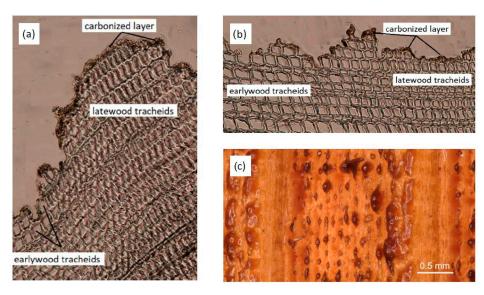


Figure 8. Microscopic spruce wood slides. (a) and (b) Transversal cuts; (c) radial surface.

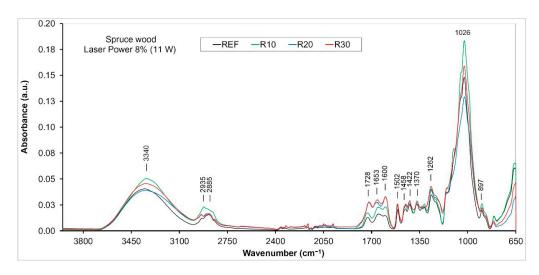


Figure 9. FTIR spectra of spruce wood surface engraved with CO₂ laser at 11 W power.

At higher raster densities, a shift in the band 's maximum towards lower wavenumbers (from 1728 to 1712 cm⁻¹) was also recorded, possibly caused by carbonyl group conjugation with other double bonds in alkenes, supported by thermo-oxidation reactions [39]. These facts point to the changes in several functional groups in lignin and in hemicelluloses [40,41]. The growth of the absorbance value of the band (belonging to the non-conjugated C=O groups) indicates increasing amounts of carbonyl and carboxyl groups in lignin and in polysaccharides, formed in oxidation processes [39], which is optically reflected in wood surface darkening [42]. The band decrease can be primarily due to deacetylation of hemicelluloses during exposure of the wood surface structure to heat [4]. A similar trend was also recorded near to the 1650 cm⁻¹ band (conjugated C-O in quinones, coupled with C=O stretching in various groups in lignin) [43,44]. The band increase is

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thought to be due to removal of acetyl groups from hemicelluloses and lignin, splitting β -alkyl-aryl-etheric bonds, while the decrease is induced by the removal of acetyl groups from hemicelluloses and by the release of acetic acid, accelerating the depolymerisation of saccharides and condensation reactions in lignin [45,46].

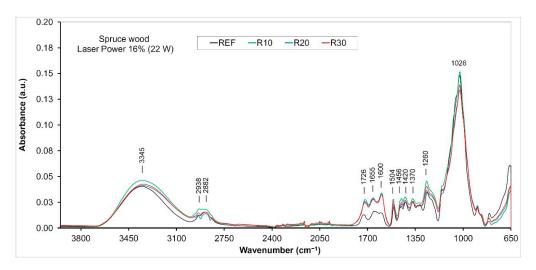


Figure 10. FTIR spectra of spruce wood surface engraved with CO₂ laser at 22 W power.

Chemical changes in the functional groups present in lignin and in hemicelluloses, primarily the increase in C=O bonds, result in forming of and changes to the chromophore structures. These substances underlie the natural colour of wood, and wood discolouration is induced by various forms of energy. The band close to 1600 cm⁻¹ (C=C stretching vibration conjugated with aromatic ring in lignin, benzene derivatives assigned to ring vibrations) effectively copies the behaviour of the band associated with carbonyl groups. The absorbance value at 1500 cm⁻¹ (C=C stretching vibration and aromatic skeleton vibration) shows only moderate alterations, providing evidence of the relatively good thermal stability in this part of the aromatic structure [46,47]. At higher temperatures, condensation reactions occur in lignin [45].

Moderate absorbance changes, primarily dependent on the raster density, were also observed at 1460 cm⁻¹ (CH₃ asymmetric bending) and at 1420 cm⁻¹ (CH₂ symmetric bending), related to groups in hemicelluloses and lignin [48], and at 1370 cm⁻¹ (C–H deformation) related to the phenolic hydroxyl groups [49,50]. These changes, triggered by heat, support the theory of splitting the aryl–alkyl–ether bonds in lignin and elimination of methanol during the formation of conjugated ethylene bonds [46,51]. The increased band at 1260 cm⁻¹ (C–O stretching vibrations) indicates the formation of novel guaiacyl units [47].

The range between 1200 and 900 cm $^{-1}$ is characterised by different overlapping bands typical for all the main wood components [48]. The band with the highest absorption was close to 1026 cm $^{-1}$ (C-O deformation vibrations). The intensity varied mainly at low laser power values (Figures 9 and 10), which indicated degradation of the structure of cellulose, hemicelluloses and methoxyl groups of lignin [52,53]. This fact may be related to the partial demethoxylation of lignin and to gradual cross-linking of the lignin [46]. Similar changes in the main components of wood engraved with CO $_2$ laser were also indicated in oak wood [8].

3.4. Spruce Wood Surface Discolouration Related to Engraving

The phenomena occurring on spruce wood surface during engraving with a CO_2 laser, and the related chemical changes, also caused obvious wood surface discolouration. The basic statistical characteristics of the variables, L^* , a^* and b^* , obtained for spruce wood over the whole raster density range and all three laser power levels are listed in Table 3.

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Table 3. Basic statistical characteristics of L^* , a^* and b^* in engraved spruce wood surfaces with a CO₂ laser.

Colour Coordinate	Basic Statistical Character			Powe	er 8%		
				Raster Den	sity [mm ⁻¹]		
		Reference	2	5	10	20	30
L*	\overline{x}	84.93	78.14	68.03	65.93	54.99	48.48
	S	0.98	0.96	1.04	1.82	2.43	1.48
a*	\overline{x}	3.23	4.79	8.19	8.23	9.84	10.19
	S	0.39	0.34	0.31	0.61	0.51	0.45
b*	\overline{x}	19.53	25.02	32.37	33.54	32.00	30.45
	S	0.99	0.61	0.83	0.91	1.64	0.63

Visualisation of discolouration of specimens



				Powe	er 12%		
		Raster density [mm ⁻¹]					
		Reference	2	5	10	20	30
 L*	\overline{x}	84.93	77.22	66.40	59.99	49.57	44.00
	S	0.98	1.45	1.17	3.72	2.55	2.06
a*	$\frac{\overline{x}}{s}$	3.23 0.39	4.86 0.31	8.29 0.22	9.25 0.76	10.33 0.45	9.31 0.52
b*	\overline{x} s	19.53 0.99	24.84 0.37	31.43 0.41	33.24 0.98	30.83 1.43	27.18 1.60

Visualisation of discolouration of specimens



				Power 16%			
		Raster density [mm ⁻¹]					
		Reference	2	5	10	20	30
	\overline{x}	84.93	74.84	62.52	59.09	46.54	41.27
L"	S	0.98	0.66	3.79	3.38	2.32	2.15
*	\overline{x}	3.23	5.33	8.78	9.29	9.98	9.45
a*	S	0.39	0.37	0.45	0.35	0.56	0.29
b*	\overline{x}	19.53	25.53	31.46	33.22	29.66	26.84
<i>0</i> **	s	0.99	0.61	1.05	0.98	1.52	0.97

Visualisation of discolouration of specimens



The results of two-way variance analysis confirmed that both studied parameters and their interactions had significant impacts on the discolouration in the engraved wood surfaces. The discolouration of the spruce wood surface was more influenced by the raster density than by the laser power on its own.

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The highest lightness, L^* , values were measured in the case of spruce wood reference samples (before engraving), as shown in Table 3. With increasing raster density, lightness decreased significantly. The steepest decrease in lightness associated with increasing raster density (61.3%) was recorded at the lowest laser power.

Similar lightness values corresponding to the identical engraving parameters were observed in beech wood and in oak wood [7,8]. In comparison with these two species, the lightness decrease in spruce was the lowest. These differences corresponded to the differences in the physical structure and chemical composition between the respective species. The discolouration was also considerably influenced by the lightness differences between the species before engraving.

With the variation in the parameters of the laser used in engraving, the colour values a^* and b^* also varied (Table 3). The influence of raster density and CO_2 laser power on the colour differences, ΔL^* , Δa^* and Δb^* , and on the total colour difference, ΔE^* , are shown in Figure 11. In all cases, the a^* values before engraving ranged within the red colour zone, near to the achromatic colour. At all used laser powers, this colour values gradually shifted to more saturated red. The b^* values moved within the yellow zone, with the saturation in engraved surfaces significantly increasing up to a raster density of 10 mm⁻¹, but decreasing progressively as raster density increased further, as a result of the moderate shift towards the achromatic colour.

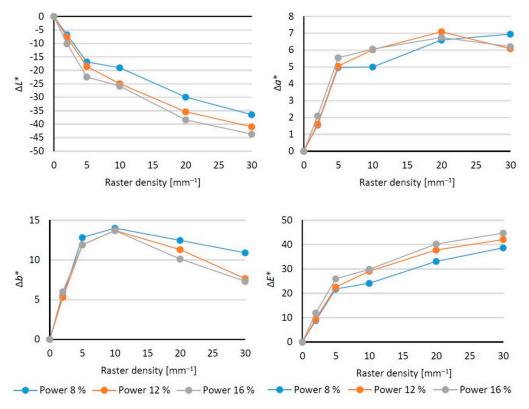


Figure 11. CO₂ laser power and raster density influencing colour differences, ΔL^* , Δa^* , Δb and ΔE^* , in spruce wood.

The total colour difference, ΔE^* (Figure 11), reached values from 10 to 12 at the lowest laser power (8%) and raster density (2 mm⁻¹). These values are between the degrees 5 and 6 of the six-degree colour scale [54] and, as such, represent an obvious discolouration compared to the original colour. With the continued increase in laser power and raster density, ΔE^* values were far beyond 12, indicating a novel colour compared to the original.

The discolouration of the engraved spruce wood surfaces is also illustrated in the figures embedded in Table 3. These figures show clearly that the engraved surfaces, step-by-step, turned dark brown with increasing raster density. These colour modifications corre-

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sponded to the changes in spruce wood chemical structure, discussed in the previous chapter. These qualitative changes are in line with those previously reported [4,7,8,19–24,33]. Our results quantitatively differ from the earlier results, given the different wood species examined and the different laser parameters set. As all the laser parameters may be expressed together through the unique variable, total irradiation dose (Equation (1)), our study examined the dependence of wood discolouration on the total irradiation dose. The dependence of colour differences, and the total colour difference, on the total irradiation dose applied is illustrated in Figure 12. The results confirmed the close correlation of the colour coordinate values with the total irradiation dose.

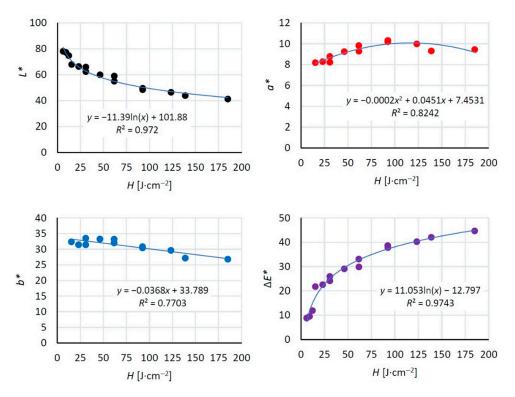


Figure 12. Dependence of the colour values, L^* , a^* , b^* and ΔE^* , in spruce wood on the total irradiation dose, H, applied.

Knowledge about the close dependence of wood mass loss and wood colour coordinates on the total irradiation dose offers better and more objective conditions for targeted colour modification of spruce wood surface treated with a CO_2 laser. There are also novel possibilities in creating patterns with higher quality, specifically concerning the plasticity and colourfulness.

4. Conclusions

The results of analysis of spruce wood engraving with a CO₂ laser allow us to state the following conclusions:

The investigated engraving parameters have significant effects on mass loss, surface morphology, chemical composition and discolouration of the spruce wood surface.

All the irradiation parameters can be amalgamated into a single variable—the total irradiation dose, *H*.

During engraving of the radial spruce wood surfaces, immediate destruction and sublimation of thin surface layers occurred. A close correlation was recognised between the wood mass loss and the total irradiation dose.

The wood mass loss varied across the treated surface as a result of density differences between the early and late spruce wood, and this was also reflected in the enhanced surface roughness.

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The roughness both parallel with and (mainly) perpendicular to the grain course significantly increased with increasing laser power and raster density. The values of the roughness parameters, *R*a and *Rz*, increased linearly with increasing wood mass loss.

Wood surface treatment with a CO_2 laser caused its obvious discolouration. Perceptible discolouration was just discernible at the lowest laser power and raster density. The spruce wood surface was dark-brown-coloured. By further increasing the laser parameters, the spruce wood became even darker and the altered surface colour was recognised as novel in comparison to the original hue. The results confirmed a close dependence of the colour coordinates, and the total colour difference, on the total irradiation dose.

The main factors underlying the discolouration were heat-induced processes associated with degradation of the carbonyl groups in lignin and in polysaccharides; the splitting of the C=O bonds influenced the chromophore content responsible for the natural wood colour, in addition to the colour modification related to engraving.

The identified dependence of wood mass loss and of colour changes on the total irradiation dose can be exploited by setting laser parameters precisely to achieve targeted wood surface discolouration, and to ensure a higher quality of patterns created on the wood surface.

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References

- 1. Wust, H.; Haller, P.; Wiedemann, G. Experimental Study of the Effect of a Laser Beam on the Morphology of Wood Surfaces. In Proceedings of the Second European Conference on Wood Modification, Göttingen, Germany, 6–7 October 2005.
- 2. Haller, P.; Beyer, E.; Wiedemann, G.; Panzner, M.; Wust, H. Experimental Study of the Effect of a Laser Beam on the Morphology of Wood Surfaces. In Proceedings of the First International Conference of the European Society for Wood Mechanics, Lausanne, Switzerland, 19–21 April 2001; p. 459.
- Dolan, J.A. Characterization of Laser Modified Surfaces for Wood Adhesion. Master's Thesis, The Faculty of Virginia Polytechnic Institute, Blacksburg, VA, USA, 2014; 100p.
- 4. Kubovský, I.; Kačík, F. Colour and Chemical Changes of the Lime Wood Surface Due to CO₂ Laser Thermal Modification. *Appl. Surf. Sci.* **2014**, *321*, 261–267. [CrossRef]
- 5. Li, R.; He, C.; Wang, X. Effects of Processing Parameters on Mass Loss and Coating Properties of Poplar Plywood During CO₂ Laser Modification. *Eur. J. Wood Wood Prod.* **2022**, *4*, 899–906. [CrossRef]
- Li, R.; He, C.; Xu, W.; Wang, X.A. Prediction of Surface Roughness of CO₂ Laser Modified PoplarWood Via Response Surface Methodology. *Maderas. Ciencia y Tecnología* 2022, 24, 1–12. [CrossRef]
- Kúdela, J.; Kubovský, I.; Andrejko, M. Surface Properties of Beech Wood after CO₂ Laser Engraving. Coatings 2020, 10, 77.
 [CrossRef]
- 8. Kúdela, J.; Kubovský, I.; Andrejko, M. Influence of irradiation parameters on structure and properties of oak wood surface engraved with a CO₂ laser. *Materials* **2022**, *15*, 8384. [CrossRef]
- 9. Liu, H.; Hu, Q.; Guo, H.; Wu, R.; Zhang, C. Glaze layer induced by femtosecond laser. Surf. Interfaces 2023, 37, 102716. [CrossRef]

Coatings **2023**, 13, 2006 16 of 17

10. Kim, Y.W.; Song, S.H. Efficient Laser Image Engraving by Work Area Sectioning and Multi-laser Head Cooperation: A Conceptual Study. *Int. J. Precis. Eng. Manuf.* **2023**, 24, 1813–1820. [CrossRef]

- 11. Guo, Q.; Wu, Z.; Zhang, C.; Yang, C.; Ma, Y.; Xu, F.; Cao, Z. Study on a New Clean Machining Method Instead of Sanding Technology for Wood. *Alex. Eng. J.* **2021**, *60*, 2369–2380. [CrossRef]
- 12. Gurău, L.; Petru, A.; Varodi, A.; Timar, M.C. The Influence of CO₂ Laser Beam Power Output and Scanning Speed on Surface Roughness and Colour Changes of Beech (*Fagus sylvatica*). *BioResources* **2017**, 12, 7395–7412. [CrossRef]
- 13. Gurău, L.; Coşereanu, C.; Paiu, I. Comparative Surface Quality of Larch (*Larix decidua* Mill.) Fretwork Patterns Cut through by CNC Routing and by Laser. *Appl. Sci.* **2021**, *11*, 6875. [CrossRef]
- 14. Gurău, L.; Petru, A. The Influence of CO₂ Laser Beam Power Output and Scanning Speed on Surface Quality of Norway Maple (*Acer platanoides*). *BioResources* **2018**, *13*, 8168–8183. [CrossRef]
- Gurău, L.; Coșereanu, C.; Timar, M.C.; Lungu, A.; Condoroţeanu, C.D. Comparative Surface Quality of Maple (Acer pseudoplatanus)
 Cut through by CNC Routing and by CO₂ Laser at Different Angles as Related to the Wood Grain. Coatings 2022, 12, 1982.
 [CrossRef]
- 16. Kamperidou, V. Chemical and Structural Characterization of Poplar and Black Pine Wood Exposed to Short Thermal Modification. Drv. Ind. 2021, 72, 155–167. [CrossRef]
- 17. Kačík, F.; Kubovský, I. Chemical Changes of Beech Wood Due to CO₂ Laser Irradiation. *J. Photochem. Photobiol. A* **2011**, 222, 105–110. [CrossRef]
- 18. Petutschnigg, A.; Stöckler, M.; Steinwendner, F.; Schnepps, J.; Gütler, H.; Blinzer, J.; Holzer, H.; Schnabel, T. Laser Treatment of Wood Surfaces for Ski Cores: An Experimental Parameter Study. *Adv. Mater. Sci. Eng.* **2013**, 2013, 123085. [CrossRef]
- 19. Li, R.; Xu, W.; Wang, X.; Wang, C. Modeling and Predicting of the Color Changes of Wood Surface During CO₂ Laser Modification. *J. Clean. Prod.* **2018**, *183*, 818–823. [CrossRef]
- 20. Gochev, Z.; Vitchev, P. Colour modifications in plywood by different modes of CO₂ laser engraving. *Acta Fac. Xylologiae Zvolen* **2022**, *64*, 77–86. [CrossRef]
- 21. Chernykh, M.; Zykova, M.; Stollmann, V.; Gilfanov, M. Influence effect of wood laser engraving mode on aesthetic perception of images. *Acta Fac. Xylologiae Zvolen* **2022**, *64*, 87–96. [CrossRef]
- 22. Li, R.; He, C.; Chen, Y.; Wang, X. Effects of Laser Parameters on the Width of Color Change Area of Poplar Wood Surface During a Single Irradiation. *Eur. J. Wood Wood Prod.* **2021**, *79*, 1109–1116. [CrossRef]
- 23. Panzner, M.; Wiedemann, G.; Henneberg, K.; Fischer, R.; Wittke, T.; Dietsch, R. Experimental Investigation of the Laser Ablation Process on Wood Surfaces. *Appl. Surf. Sci.* **1998**, 127–129, 787–792. [CrossRef]
- 24. Lin, C.J.; Wang, Y.C.; Lin, L.D.; Chiou, C.R.; Wang, Y.N.; Tsai, M.J. Effects of Feed Speed Ratio and Laser Power on Engraved Depth and Color Difference of Moso Bamboo Lamina. *J. Mater. Process. Technol.* **2008**, 198, 419–425. [CrossRef]
- 25. Nath, S.; Waugh, D.G.; Ormondroyd, G.A.; Spear, M.J.; Pitman, A.J.; Sahoo, S.; Mason, P. CO₂ Laser Interactions with Wood Tissues During Single Pulse Laser-incision. *Opt. Laser Technol.* **2020**, *126*, 106069. [CrossRef]
- 26. Li, R.; He, C.; Wang, X. Evaluation and Modeling of Processability of Laser Removal Technique for Bamboo Outer Layer. *JOM* **2021**, 73, 2423–2430. [CrossRef]
- 27. Arai, I.; Kawasumi, H. Thermal analysis of laser machining in wood III. J. Jpn. Wood Res. Soc. Mokuzai Gakkaishi 1980, 26, 773–782.
- 28. Barcikowski, S.; Koch, G.; Odermatt, J. Characterisation and modification of the heat affected zone during laser material processing of wood and wood composites. *Holz Roh Werkst.* **2006**, *64*, 94–103. [CrossRef]
- 29. Kučerová, V.; Lagaňa, R.; Hýrošová, T. Changes in chemical and optical properties of silver fir (*Abies alba* L.) wood due to thermal treatment. *J. Wood Sci.* 2019, 65, 21–31. [CrossRef]
- 30. Yang, C.; Jiang, T.; Yu, Y.; Bai, Y.; Song, M.; Miao, Q.; Ma, Y.; Liu, J. Water-jet Assisted Nanosecond Laser Microcutting of Northeast China Ash Wood. Experimental Study. *BioResources* **2019**, *14*, 128–138. [CrossRef]
- 31. Jurek, M.; Wagnerová, R. Laser Beam Calibration for Wood Surface Colour Treatment. Eur. J. Wood Wood Prod. 2021, 79, 1097–1107. [CrossRef]
- 32. Reinprecht, L.; Vidholdová, Z. The Impact of a CO₂ Laser on the Adhesion and Mold Resistance of a Synthetic Polymer Layer on a Wood Surface. *Forests* **2021**, *12*, 242. [CrossRef]
- 33. Lungu, A.; Timar, M.C.; Beldean, E.C.; Georgescu, S.V.; Co¸sereanu, C. Adding Value to Maple (*Acer pseudoplatanus*) Wood Furniture Surfaces by Different Methods of Transposing Motifs from Textile Heritage. *Coatings* **2022**, *12*, 1393. [CrossRef]
- 34. Kúdela, J.; Andrejko, M.; Mišíková, O. Wood Surface Morphology Alteration Induced by Engraving with CO₂ Laser Under Different Raster Density Values. *Acta Fac. Xylologiae Zvolen* **2021**, *63*, 35–47. [CrossRef]
- 35. Moliński, W.; Roszyk, E.; Jabloński, A.; Puszyński, J.; Cegiela, J. Mechanical parameters of thermally modified ash wood determined by compression in radial direction. *Maderas. Cienc. Tecnol.* **2016**, *18*, 577–586. [CrossRef]
- 36. Kubovský, I.; Kačíková, D.; Kačík, F. Structural Changes of Oak Wood Main Components Caused by Thermal Modification. *Polymers* **2020**, *12*, 485. [CrossRef] [PubMed]
- 37. Nada, A.M.A.; Youssef, M.A.; Sha_ei, K.A.; Aalah, A.M. Infrared spectroscopy of some treated lignins. *Polym. Degrad. Stabil.* **1998**, 62, 157–163. [CrossRef]
- 38. Nguila Inari, G.; Pétrissans, M.; Gerardin, P. Chemical reactivity of heat-treated wood. Wood Sci. Technol. 2006, 41, 157. [CrossRef]
- 39. Esteves, B.; Marques, A.V.; Domingos, I.; Pereira, H. Chemical changes of heat treated pine and eucalypt wood monitored by FTIR. *Maderas*. *Ciencia y Tecnología* **2013**, *15*, 245–258. [CrossRef]

Coatings **2023**, 13, 2006 17 of 17

40. Colom, X.; Carrillo, F.; Nogués, F.; Garriga, P. Structural analysis of photodegraded wood by means of FTIR spectroscopy. *Polym. Degrad. Stabil.* **2003**, *80*, 543–549. [CrossRef]

- 41. Lagaňa, R.; Csiha, C.; Horváth, N.; Tolvaj, L.; Andor, T.; Kúdela, J.; Németh, R.; Kačík, F.; Ďurkovič, J. Surface properties of thermally treated European beech wood studied by PeakForce Tapping atomic force microscopy and Fourier-transform infrared spectroscopy. *Holzforschung* **2021**, *75*, 56–64. [CrossRef]
- 42. Chen, Y.; Gao, J.; Fan, Y.; Tshabalala, M.A.; Stark, N.M. Heat-induced chemical and color changes of extractive-free black locust (*Robinia pseudoacacia*) wood. *BioResources* **2012**, 7, 2236–2248. [CrossRef]
- González-Peña, M.M.; Curling, S.F.; Hale, M.D. On the e_ect of heat on the chemical composition and dimensions of thermally-modified wood. *Polym. Degrad. Stabil.* 2009, 94, 2184–2193. [CrossRef]
- 44. Bhagia, S.; Ďurkovič, J.; Lagaňa, R.; Kardošová, M.; Kačík, F.; Cernescu, A.; Schäfer, P.; Yoo, C.G.; Ragauskas, A.J. Nanoscale FTIR and Mechanical Mapping of Plant Cell Walls for Understanding Biomass Deconstruction. *ACS Sustain. Chem. Eng.* **2022**, 10, 3016–3026. [CrossRef]
- 45. Popescu, M.C.; Froidevaux, J.; Navi, P.; Popescu, C.M. Structural modifications of Tilia cordata wood during heat treatment investigated by FT-IR and 2D IR correlation spectroscopy. *J. Mol. Struct.* **2013**, *1033*, 176–186. [CrossRef]
- 46. Kačík, F.; Luptáková, J.; Šmíra, P.; Nasswettrová, A.; Kačíková, D.; Vacek, V. Chemical alterations of pine wood lignin during heat sterilization. *BioResources* **2016**, *11*, 3442–3452. [CrossRef]
- 47. Zhang, P.; Wie, Y.; Liu, Y.; Gao, J.; Chen, Y.; Fan, Y. Heat-Induced Discoloration of Chromophore Structures 402 in Eucalyptus Lignin. *Materials* **2018**, *11*, 1686. [CrossRef] [PubMed]
- 48. Boukir, A.; Fellak, S.; Doumenq, P. Structural characterization of Argania spinosa Moroccan wooden artifacts during natural degradation progress using infrared spectroscopy (ATR-FTIR) and X-Ray diffraction (XRD). *Heliyon* **2019**, *5*, E02477. [CrossRef] [PubMed]
- 49. Weiland, J.J.; Guyonnet, R. Study of chemical modifications and fungi degradation of thermally modified wood using DRIFT spectroscopy. *Holz Roh Werkst.* **2003**, *61*, 216–220. [CrossRef]
- 50. Popescu, M.C.; Gazacu, G.; Singurel, G.; Vasile, C. Study of the process of the water desorption from lignins. *Rom. J. Phys.* **2006**, *51*, 277–283. Available online: https://www.academia.edu/4749147/Study_of_the_process_of_the_water_desorption_from_lignins (accessed on 24 July 2022).
- 51. Bourgois, J.; Bartholin, M.C.; Guyonnet, R. Thermal treatment of wood: Analysis of the obtained product. *Wood Sci. Technol.* **1989**, 23, 303–310. [CrossRef]
- 52. Faix, O. Fourier transform infrared spectroscopy. In *Methods in Lignin Chemistry*; Lin, S.Y., Dence, C.W., Eds.; Springer: Berlin, Germany, 1992; pp. 83–109.
- 53. Ciolacu, D.; Ciolacu, F.; Popa, V.I. Amorphous cellulose-structure and characterization. *Cell. Chem. Technol.* **2011**, 45, 13–21. Available online: https://www.researchgate.net/publication/279897864_Amorphous_cellulose_-_Structure_and_characterization (accessed on 16 March 2020).
- 54. Allegretti, O.; Travan, L.; Cividini, R. Drying Techniques to Obtain White Beech. In Proceedings of the Wood EDG Conference, Bled, Slovenia, 23 April 2009. Available online: http://timberdry.net/downloads/EDG-SeminarBled/Presentation/EDG (accessed on 25 May 2022).

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