
Article

A Sequential Anammox Zeolite-Biofilter for the Removal of Nitrogen Compounds from Drinking Water

Stephan Eberle ¹, Hilmar Börnick ¹ and Stefan Stolte ^{1*}

¹ Institute for Water Chemistry, Technische Universität Dresden, 01062 Dresden, Germany

* stefan.stolte@tu-dresden.de, Tel. +49(0)351/463-32759

Supporting Information

S1 Inoculation of the Anammox zeolite-biofilter



Left:

90 mL sludge mixture per filter segment. Sludge from wastewater treatment plants from Rotterdam and Wansdorf.

Right:

473±1 g of zeolites per segment.



First Anammox zeolite layer. Side (left) and topdown (right) views.



Following 10 mL of sludge inoculum, a second layer of zeolites was added.

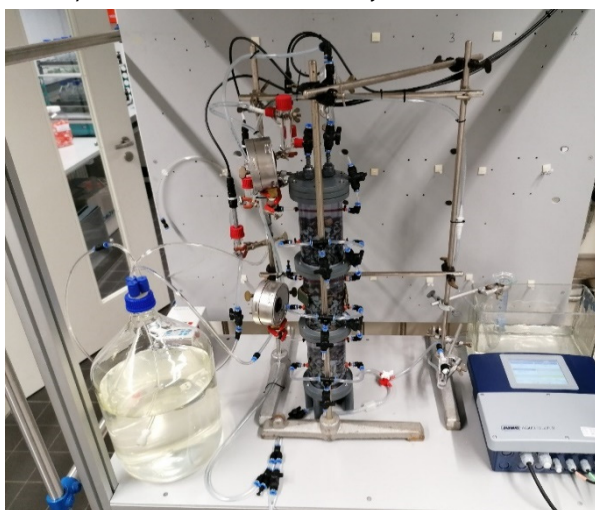


First segment completed and filled with oxygen free nutrient solution.

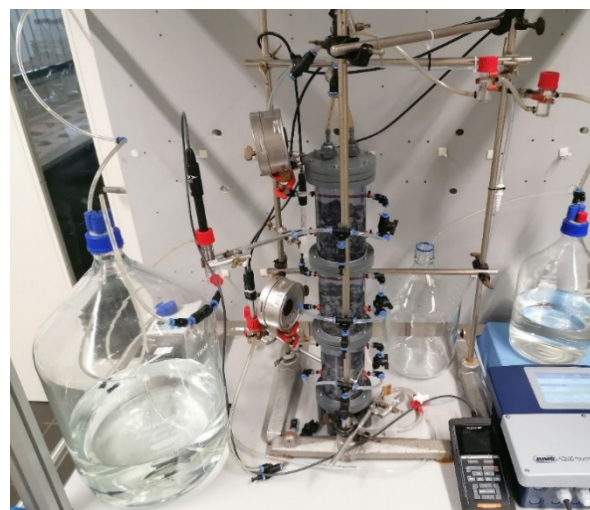
Segment 2 and 3 were completed using the same inoculation procedure.

Figure S1. Inoculation steps of the Anammox zeolite-biofilter.

S2 Completed Anammox zeolite-biofilter



(a)



(b)

Figure S2. Completed Anammox zeolite-biofilter in circular flow (a); and (b) flow through operation mode.

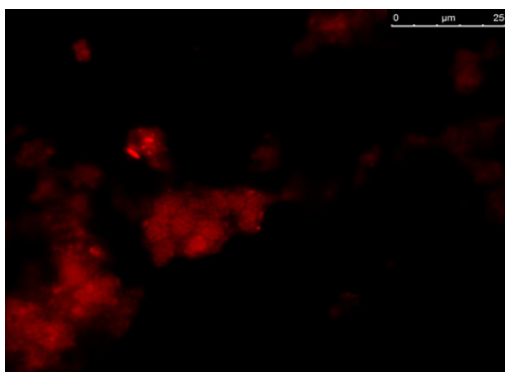


Figure S3-1. Qualitative detection of Amx in the inoculated sludge.

Table S1. Typical chemical composition of the Elbe-/tap water mixture used (1:10).

Na ⁺ (mg/L)	K ⁺ (mg/L)	Ca ²⁺ (mg/L)	Mg ²⁺ (mg/L)	NH ₄ ⁺ (mg/L)	NO ₂ ⁻ (mg/L)	NO ₃ ⁻ (mg/L)	TN (mg/L)	DOC (mg/L)	HCO ₃ ⁻ (mg/L)
10.57	1.95	17.63	8.75	4.16	5.56	2.41	5.46	2.53	77.40

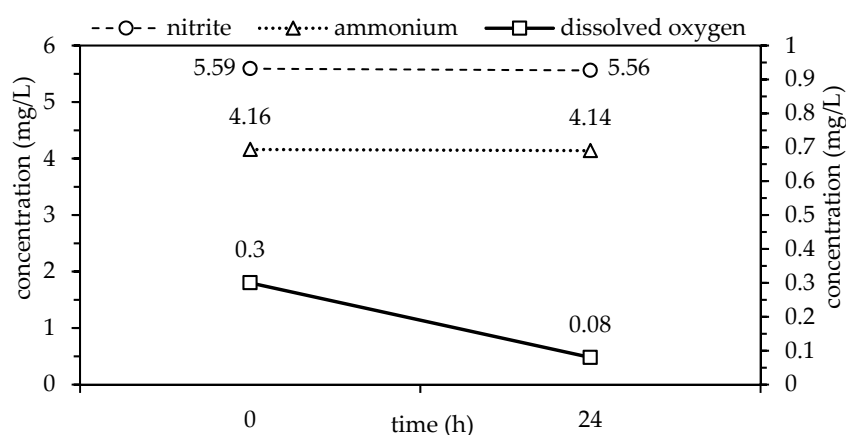


Figure S3-2. Substrate and dissolved oxygen concentrations in the receiving tank over a 24 h period.

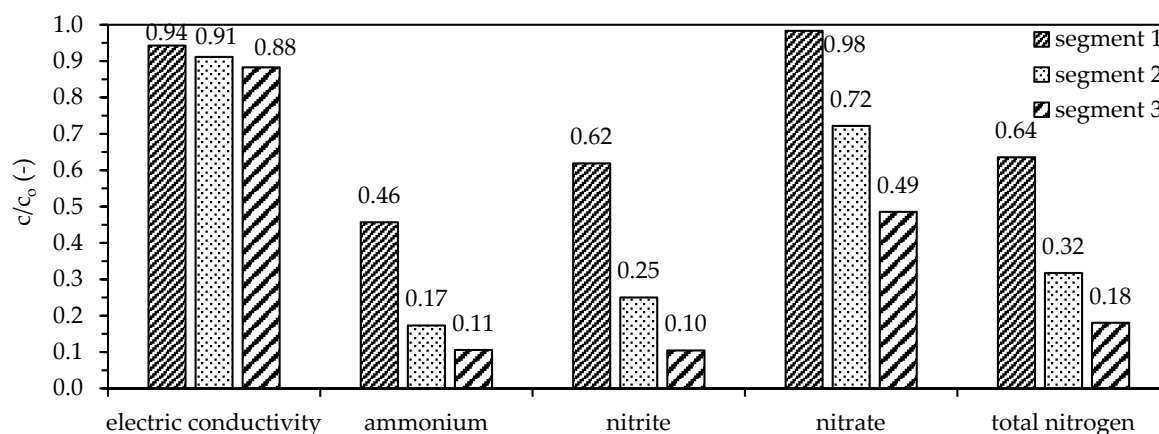


Figure S3-3. Nitrogen degradation efficiencies and decreasing electrical conductivity in each segment of the Anammox zeolite-biofilter for the first investigation after sludge inoculation at the starting point (matrix: Elbe/



tap water (1:10); $v_F = 0.032$ m/h; $c_0(\text{NH}_4^+) = 4.3$ mg/L; $c_0(\text{NO}_2^-) = 5.7$ mg/L; $c_0(\text{DOC}) = 2.5$ mg/L; pH: 7.8; $T = 22$ °C; $n = 1$).

S4 Investigations of the Nitrite/Ammonium-Ratio and Half-Life

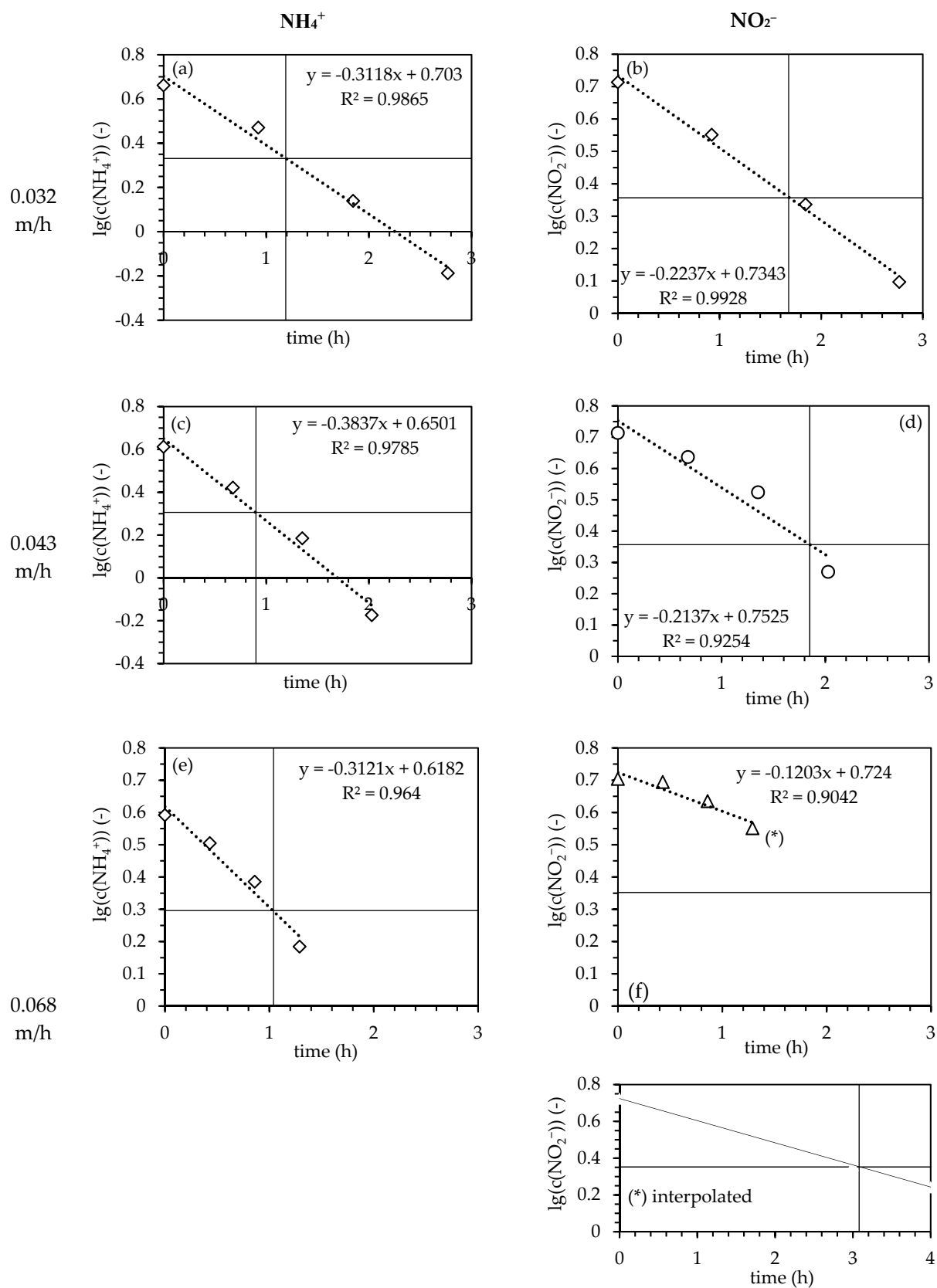


Figure S4. Determination of the half-life period of NH_4^+ and NO_2^- degradation and its dependence on filter velocity: (a), (b) for 0.032 m/h; (c), (d) for 0.043 m/h; and (e), (f) for 0.068 m/h.

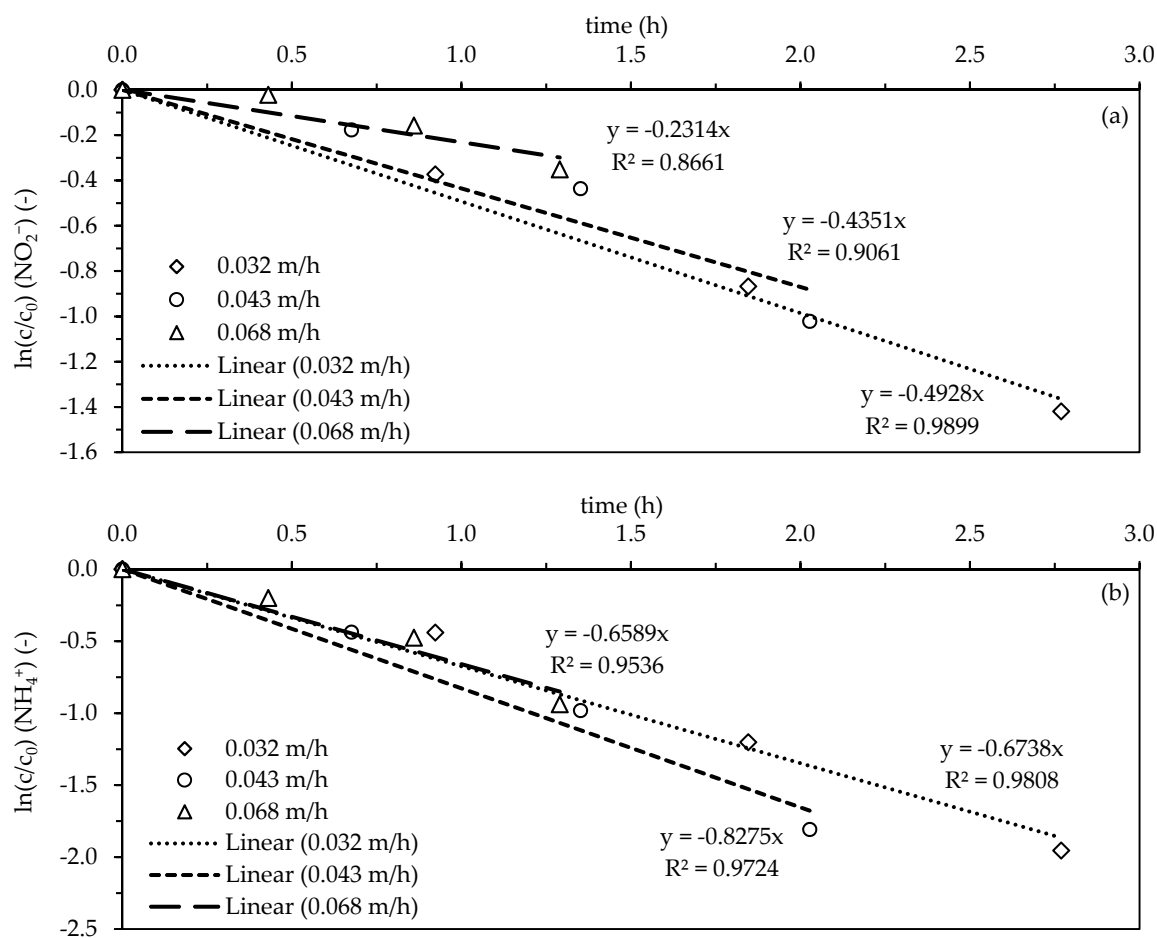
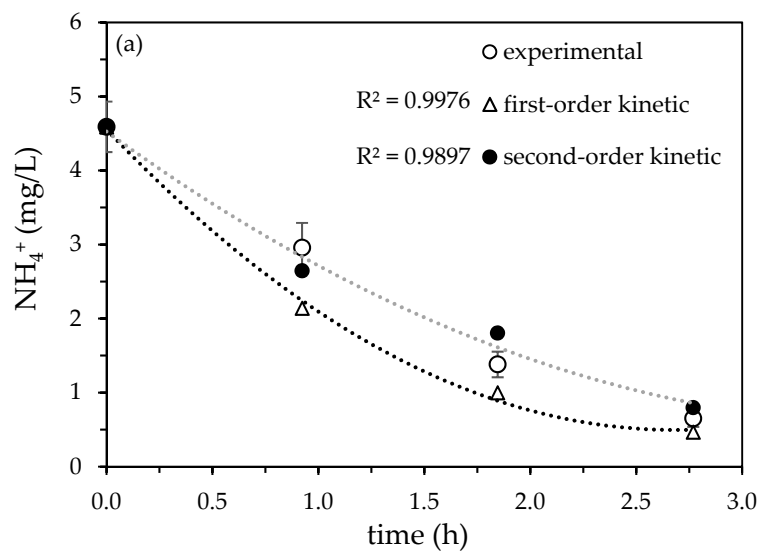
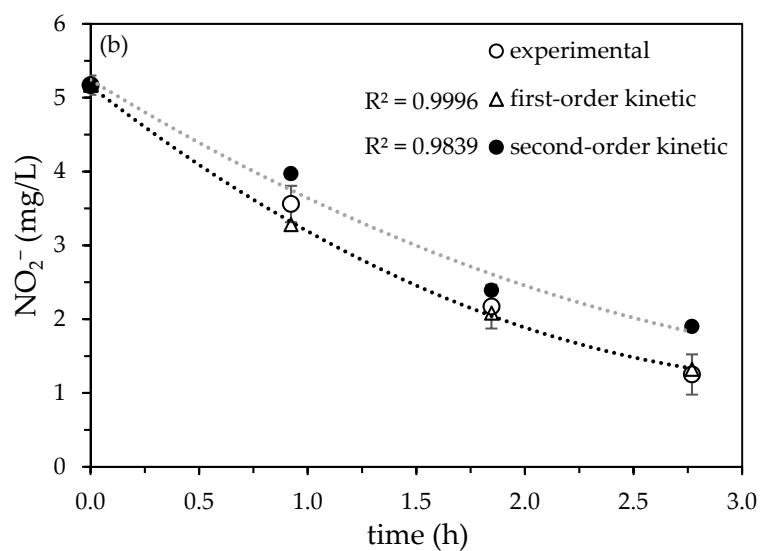
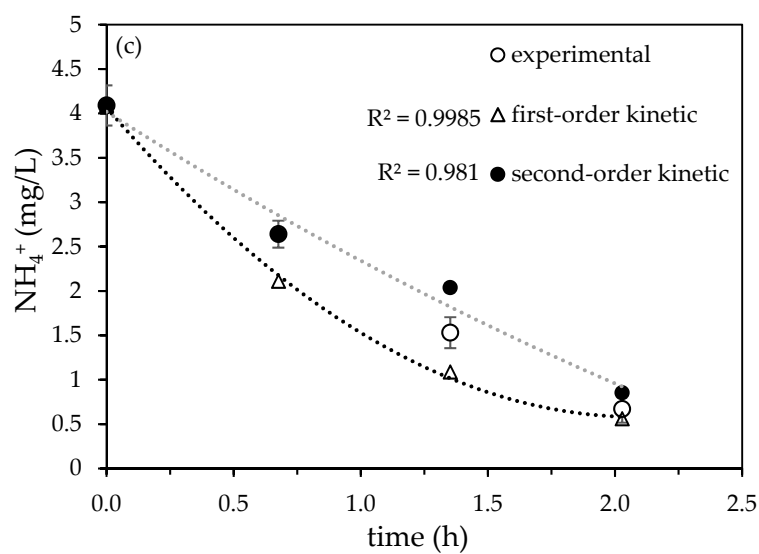


Figure S5. Determination of the reaction rate constant k for the pseudo first order. k determined by plotting the logarithm of the substrate concentration against the effective hydraulic retention time: (a) for NO_2^- ; and (b) for NH_4^+ .

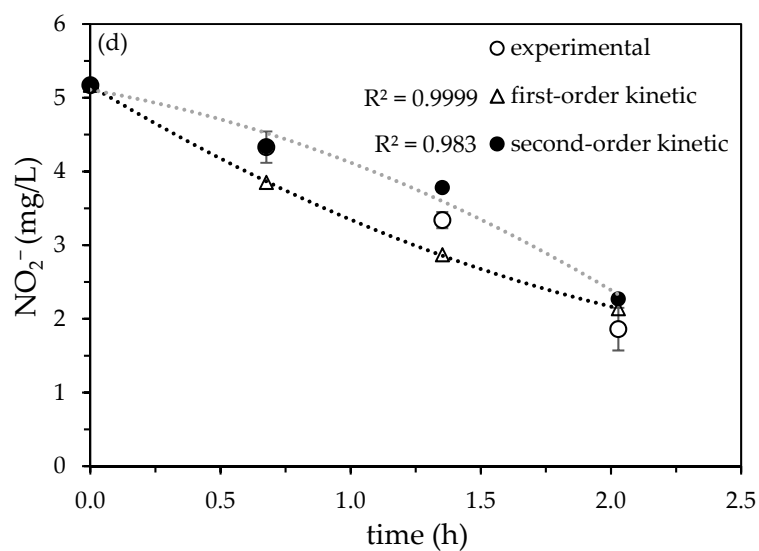


0.032 m/h

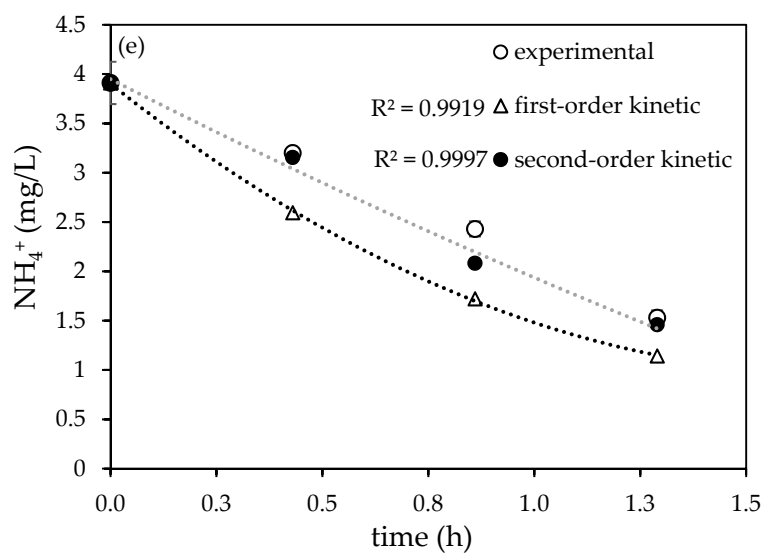




0.043 m/h



0.068 m/h



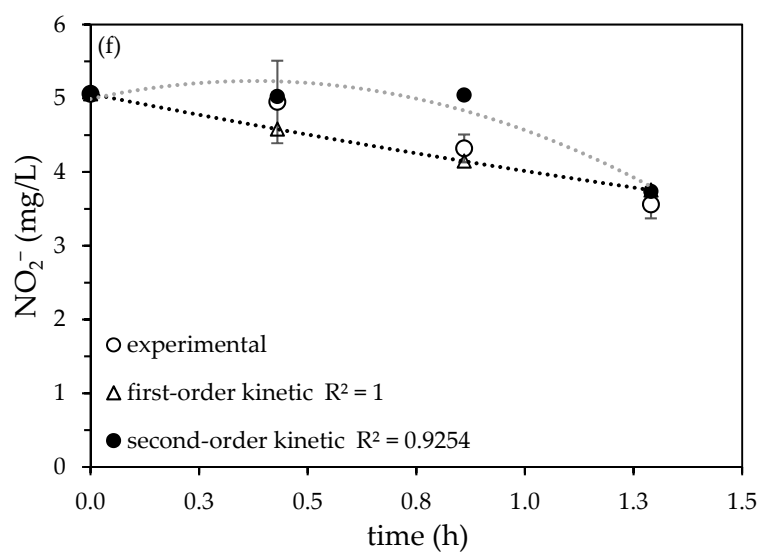
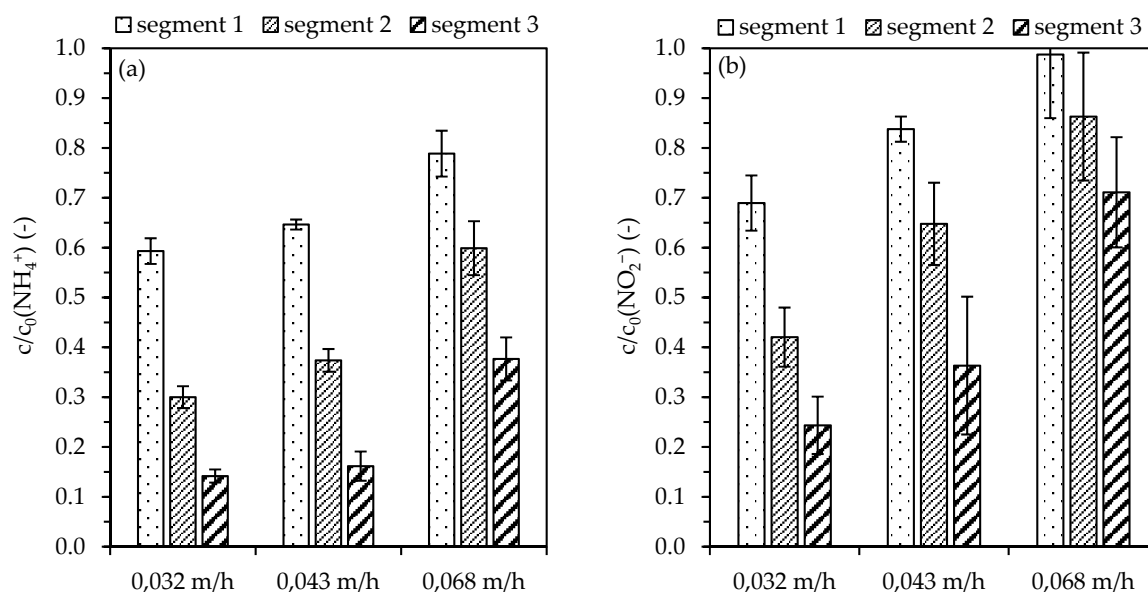


Figure S6. Calculated filter-velocity dependent reaction first-order and second-order for NH_4^+ and NO_2^- removal compared to experimental data: (a), (b) for 0.043 m/h; (c), (d) for 0.043 m/h; and (e), (f) for 0.068 m/h (matrix: Elbe-/tap water (1:10); $v_F = 0.032, 0.043, 0.068$ m/h; $c_0(\text{NH}_4^+) = 4.3$ mg/L; $c_0(\text{NO}_2^-) = 5.7$ mg/L; $c_0(\text{DOC}) = 2.5$ mg/L; pH: 7.8; $T = 22^\circ\text{C}$; $n = 3$).

S7 Degradation of Nitrogen Compounds



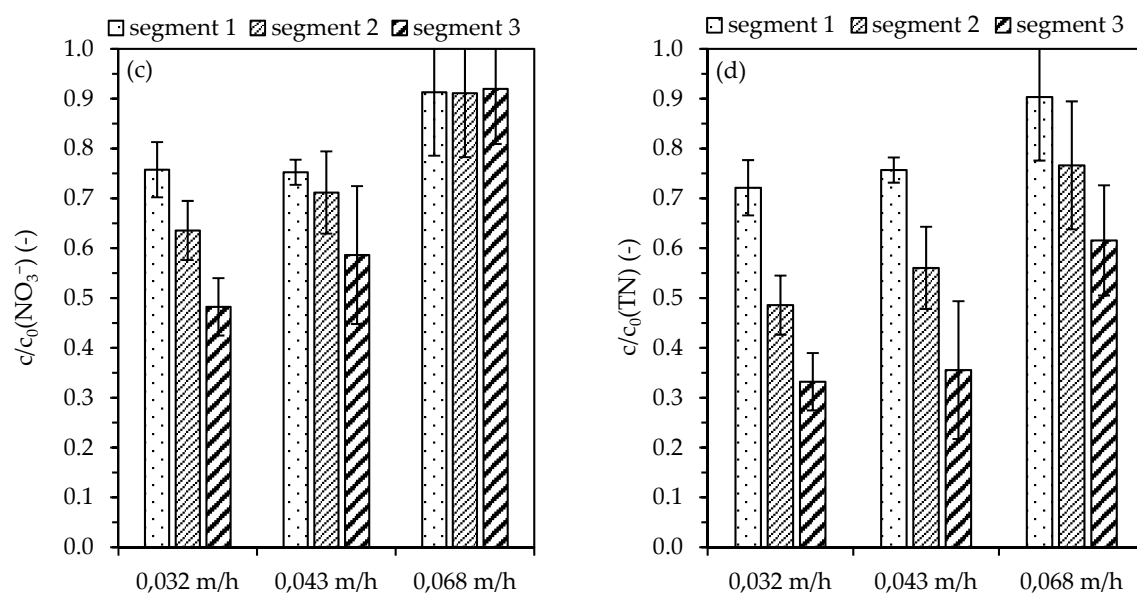


Figure S7. Degradation of nitrogen compounds depending on the filter velocity and Anammox zeolite-biofilter's height: (a) for NH_4^+ ; (b) for NO_2^- ; (c) for NO_3^- ; and (d) for TN.