



1. Estimation of excess Ga and Al accumulated during QW growth under different Me-rich conditions.

During the growth of MQW structures under Me-rich conditions with various Ga/N₂* flux ratio the following typical growth parameters were used. MQW-2.2-S structure was grown at the growth fluxes of $Ga=1.00$ ML/s, $N_2^*=0.464$ ML/s and the duration of the growth of QW with a nominal thickness of 1.5ML $t_{QW}=3.2\text{s}$. Substrate temperature was $T_s=691^\circ\text{C}$ and in accordance with [1] the equilibrium Ga desorption flux at this temperature was estimated as $Ga^{DE} = 0.22\text{ML/s}$. These fluxes provided the strong Ga-rich growth conditions of GaN: $(Ga - N_2^*) > Ga^{DE}$ and the effective Ga-desorption flux $Ga^D = Ga^{DE}$. Thus, the excess Ga accumulated during the QW growth equals

$$E^{Ga} = (Ga - Ga^D - N_2^*) \cdot t_{QW} = 1.0\text{ML} \quad (S1)$$

MQW-1.1-S structure was grown at the growth fluxes of $Ga = 0.50$ ML/s, $N_2^* = 0.450\text{ML/s}$ and the duration of the growth of QW with a nominal thickness of 1.5ML $t_{QW}=3.1\text{s}$. At the same substrate temperature (691°C), the fluxes used ensured the weak Ga-rich conditions $(Ga - N_2^*) < Ga^{DE}$, at which the Ga desorption flux was equal to $Ga^D = (Ga - N_2^*) = 0.5 - 0.45 = 0.05$ ML/s and excess Ga did not accumulate.

2. Calculation of the stress in the $400\times\{\text{GaN}_{1.5}/\text{AlN}_{16}\}$ MQW structure coherently grown on AlN layer

An average Al-content (x) in the $400\times\{\text{GaN}_{1.5}/\text{AlN}_{16}\}$ MQW structure was calculated by the equation $x=d_{BL}/(d_{QW} + d_{BL})$, which at the used thicknesses $d_{GaN}=1.5\text{ML}$ and $d_{AlN}=16$ gave the value $x=0.91$. Vegard's law was used for the calculations of the a-lattice constant of the equivalent ternary alloy as $a_{\text{AlGaN}}=a_{\text{AlN}} \cdot x + a_{\text{GaN}} \cdot (1-x)=3.118 \text{ \AA}$, where a-lattice constants for binary alloys were $a_{\text{AlN}} = 3.111 \text{ \AA}$, $a_{\text{GaN}} = 3.189 \text{ \AA}$ [2]. Using these data, the biaxial strain in the coherently grown $\text{Al}_x\text{Ga}_{1-x}\text{N}/\text{AlN}$ heterostructure was estimated as $\epsilon_{xx} = (a_{\text{AlN}} - a_{\text{AlGaN}})/a_{\text{AlGaN}} = -0.00221$. In the same way, the biaxial elastic modulus of $\text{Al}_x\text{Ga}_{1-x}\text{N}$ (was calculated as $M_{\text{AlGaN}} = M_{\text{AlN}}x + M_{\text{GaN}}(1-x) = 472 \text{ GPa}$ with the following reference data for biaxial elastic modulus AlN and GaN: and $M_{\text{AlN}} = 471 \text{ GPa}$ [3], $M_{\text{GaN}} = 479 \text{ GPa}$ [4], which was used to estimate the biaxial stress in this coherently grown heterostructure as $\sigma_{xx} = M_{\text{AlGaN}} \times \epsilon_{xx} = 1.0 \text{ GPa}$.

3. The SEM image of this structure with clearly visible cracks

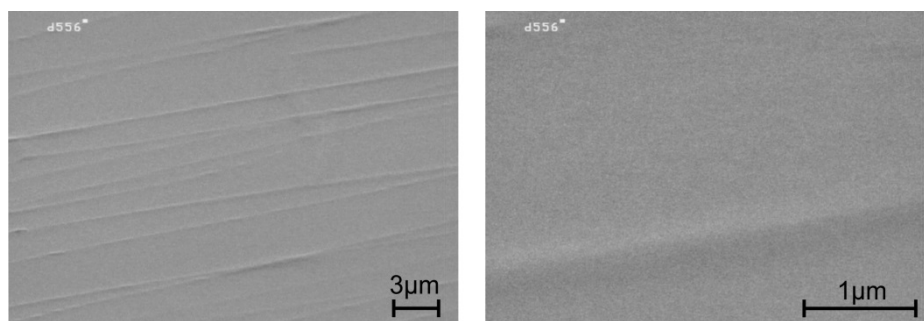


Figure S1. SEM images of structure MQW-2.2-D₁ obtained at various magnifications.

4. The (105) RSMs of $\{\text{GaN}_{1.5}/\text{AlN}_{16}\}$ ($N=50,100$) MQW structures grown at various Ga/N_2^* flux ratio

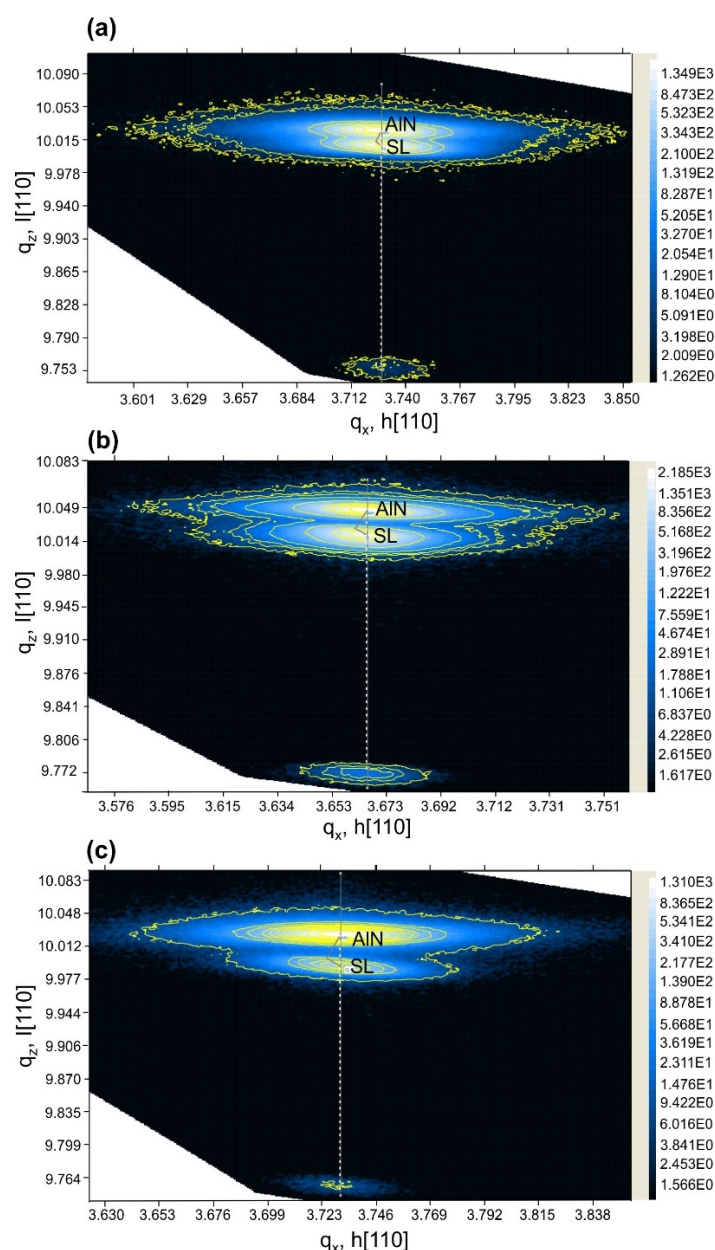


Figure S2. The (105) RSMs of $N \times \{\text{GaN}_{1.5}/\text{AlN}_{16}\}$ structures (a) 400×QW-1.5-1.1-S grown under $\text{Ga}/\text{N}_2^* = 1.1$; (b) 400×QW-1.5-2.2-S (c) 400×QW-1.5-2.2-S (both (b) and (c) were grown under $\text{Ga}/\text{N}_2^* = 2.2$).

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