

# Supplementary Materials: On the Laser Fragmentation for the Synthesis of Ligand-Free Ultra-Small Iron Nanoparticles in Various Liquid Environments

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- Estimation of laser fluence, roughly considering a beam's free propagation, and calculation of the full evaporation fluence threshold.
- Supporting DLS graphs of supernatant and sediment for all the samples.
- SAED diffraction data displaying the crystallographic families corresponding to the specific type of Fe-based crystals.
- Supporting figure displaying the TEM images of all the samples on a bigger scale than the one reported in the main text, and supporting EDX line scanning graphs of the individual nanoparticles in different solvents.
- The raw ICP-OES data confirming the presence of iron.

The calculation of the laser fluence was determined according to the following set of standard formulas:

$$P = 7.0 \text{ W (measured average power)} \quad (1)$$

$$N = 2000 \text{ (number of pulses)} \quad (2)$$

$$E = \frac{P}{N} \text{ (energy per pulse)} \quad (3)$$

$$E = 3.5 \text{ mJ} \quad (4)$$

$$f = 35 \text{ mm (local length of plano – convex focusing lens)} \quad (5)$$

$$s = 12 \text{ mm (measured diameter of unfocused beam)} \quad (6)$$

$$\lambda = 527 \text{ nm (laser's central wavelength)} \quad (7)$$

$$d = \frac{2 \cdot 1.22 \cdot \lambda \cdot \frac{f}{s}}{\sqrt{2 \cdot \ln(2)}} \text{ (diameter of focused beam)} \quad (8)$$

$$d = 3.19 \cdot 10^{-4} \text{ cm} \quad (9)$$

$$S = \pi \cdot \left(\frac{d}{2}\right)^2 \text{ (area of focused laser beam)} \quad (10)$$

$$S = 8 \cdot 10^{-8} \text{ cm}^2 \quad (11)$$

$$J = \frac{E}{S} \text{ (laser fluence)} \quad (12)$$

$$J = 4.3 \cdot 10^4 \text{ J/cm}^2 \quad (13)$$

The calculation of the fluence threshold for heating-melting-evaporation model was determined according to the following set of formulas:

$$E_{abs} = \frac{E_0}{S_0} \cdot \sigma_{abs} = \Psi \cdot \sigma_{abs} \quad (14)$$

where  $E_0$  represents the energy of a single pulse,  $S_0$  the laser beam cross-section (the area of light that is perpendicular to the beam direction),  $\Psi = E_0/S_0$  the laser fluence and  $\sigma_{abs}$  the particle absorption cross-section, which describes the energy absorbed by the irradiated particle.

$$\Psi \cdot \sigma_{abs} = m_p \cdot \int_{T_0}^T c_p(T) \cdot dT \quad (15)$$

where  $m_p = \rho_p \pi d_p^3 / 6$  is the particle mass,  $\rho_p$  is the density of the particle,  $d_p$  is the diameter of the particle and  $T_0$  is the initial temperature of the particle and  $T$  is the final temperature of the particle.

$$\Psi \cdot \sigma_{abs} = m_p \cdot \int_{T_0}^{T_m} c_p^s(T) \cdot dT + m_p \cdot \Delta H_m + m_p \cdot \int_{T_m}^{T_b} c_p^l(T) \cdot dT + m_p \cdot \Delta H_{ev} \quad (16)$$

Here,  $c_p^s$  represents the heat capacity of the material in the solid state,  $c_p^l$  the heat capacity in the liquid state,  $T_m$  the melting temperature,  $T_b$  the boiling temperature and as previously mentioned,  $\Delta H_m$  the enthalpy of the melting and  $\Delta H_{ev}$  the enthalpy of the evaporation.

$$\Psi \cdot \sigma_{abs} = m_p \cdot [(H_{T_m} - H_{T_0}) + \Delta H_m + (H_{T_b} - H_{T_m}) + \Delta H_{ev}] \quad (17)$$

where  $H_{T_m} - H_{T_0}$  represents the relative enthalpy to reach the melting point and  $H_{T_b} - H_{T_m}$  the relative enthalpy to reach the boiling point.

$$\sigma_{abs}(d_p) \cdot \mathbf{d}(\Psi) = \Delta H_{ev} \cdot \mathbf{d}(m_p) \quad (18)$$

which after the substitution of  $m_p$  and the editing takes the following form

$$\mathbf{d}(\Psi) = \frac{\pi}{2} \cdot \rho_p \cdot \Delta H_{ev} \cdot \frac{d_p^2 \cdot \mathbf{d}(d_p)}{\sigma_{abs}(d_p)} \quad (19)$$

Then, the final equation that enables to calculate the required fluence to fully evaporate micro particles will be

$$\begin{aligned} \Psi = & \frac{\pi \cdot d_p^3 \cdot \rho_p}{6 \cdot \sigma_{abs}} \cdot [(H_{T_m} - H_{T_0}) + \Delta H_m + (H_{T_b} - H_{T_m})] + \\ & \frac{\pi \cdot \rho_p}{2} \cdot \Delta H_{ev} \cdot \left( \int_{d_p}^0 \frac{d_p^2}{\sigma_{abs}(d_p)} \cdot \mathbf{d}(d_p) \right) \end{aligned} \quad (20)$$

Note, the particle cross-section was calculated by Mie-theory calculator [1] and the required values of the quantities were taken from the database [2].

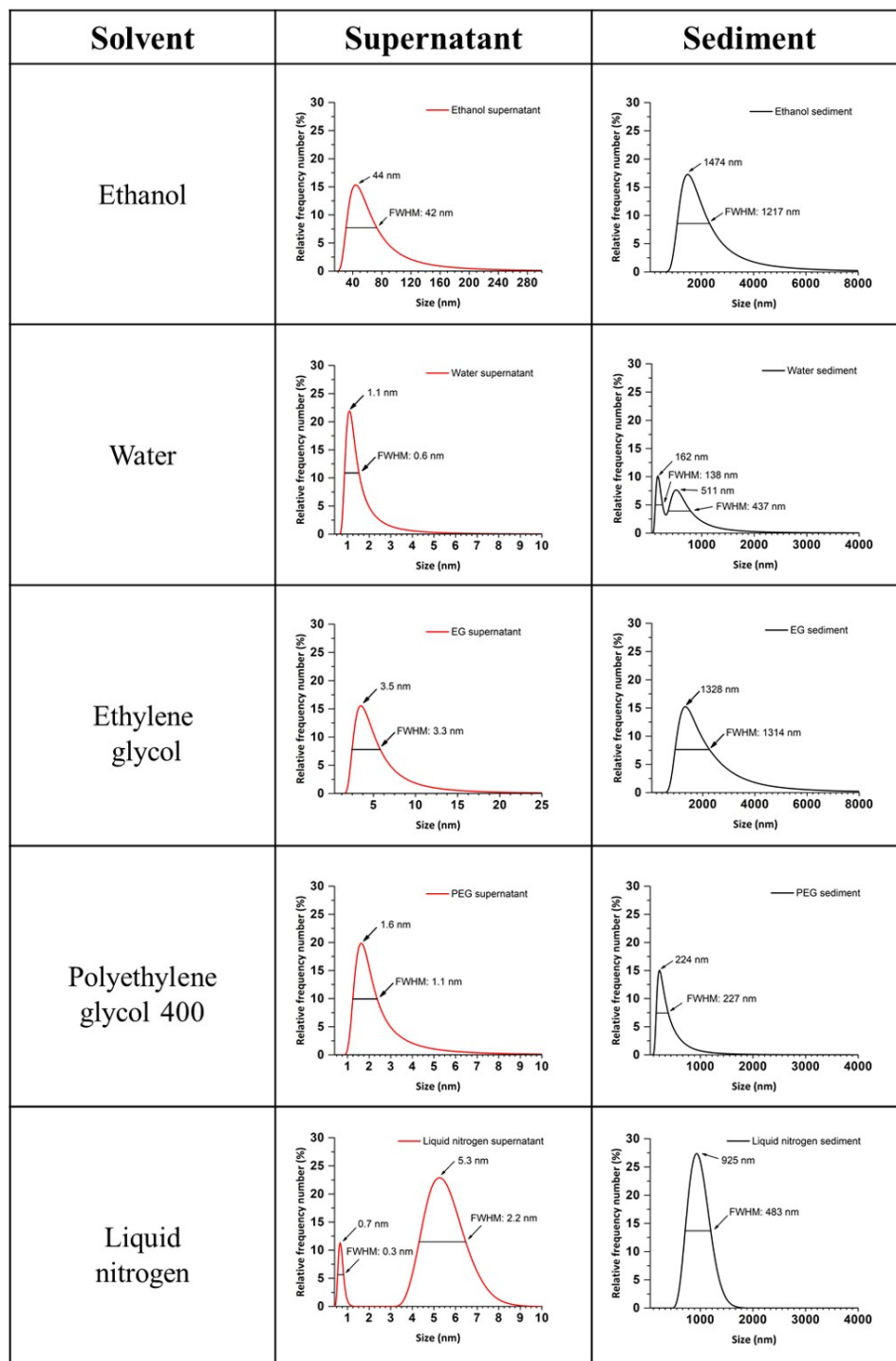
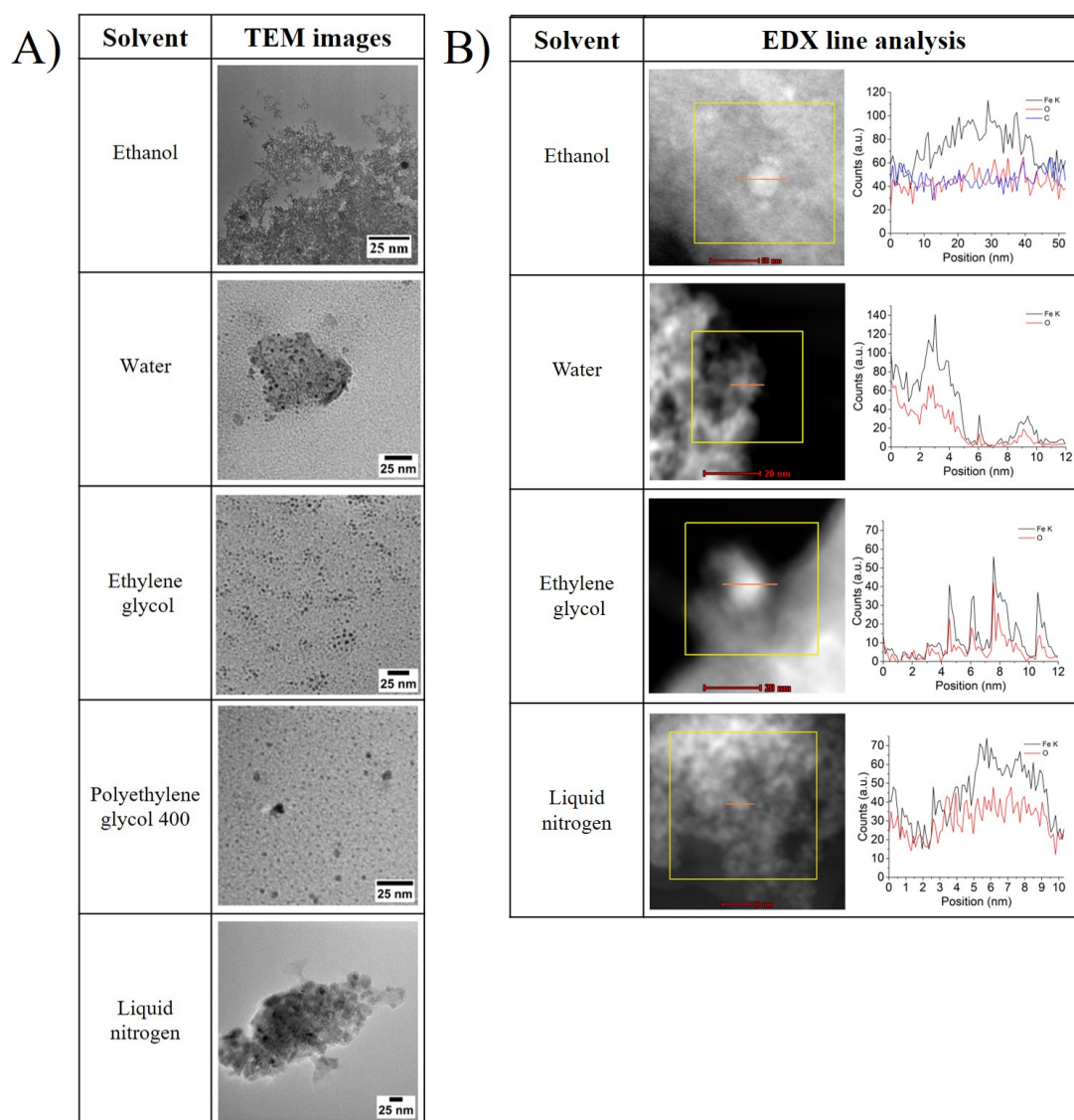


Figure S.1. Representative DLS images of sediment and supernatant samples.

**Table S1.** SAED parameters of samples corresponding to the specific crystallographic families in Fe-based crystals. Tetragonal Fe<sub>2</sub>O<sub>3</sub> crystal (ICDD file: 65-390), cubic Fe<sub>3</sub>O<sub>4</sub> crystal (ICDD file: 65-3107), hexagonal Fe crystal (ICDD files: 34-529), and the monoclinic Fe<sub>5</sub>C<sub>2</sub> crystal (ICDD file: 20-508)

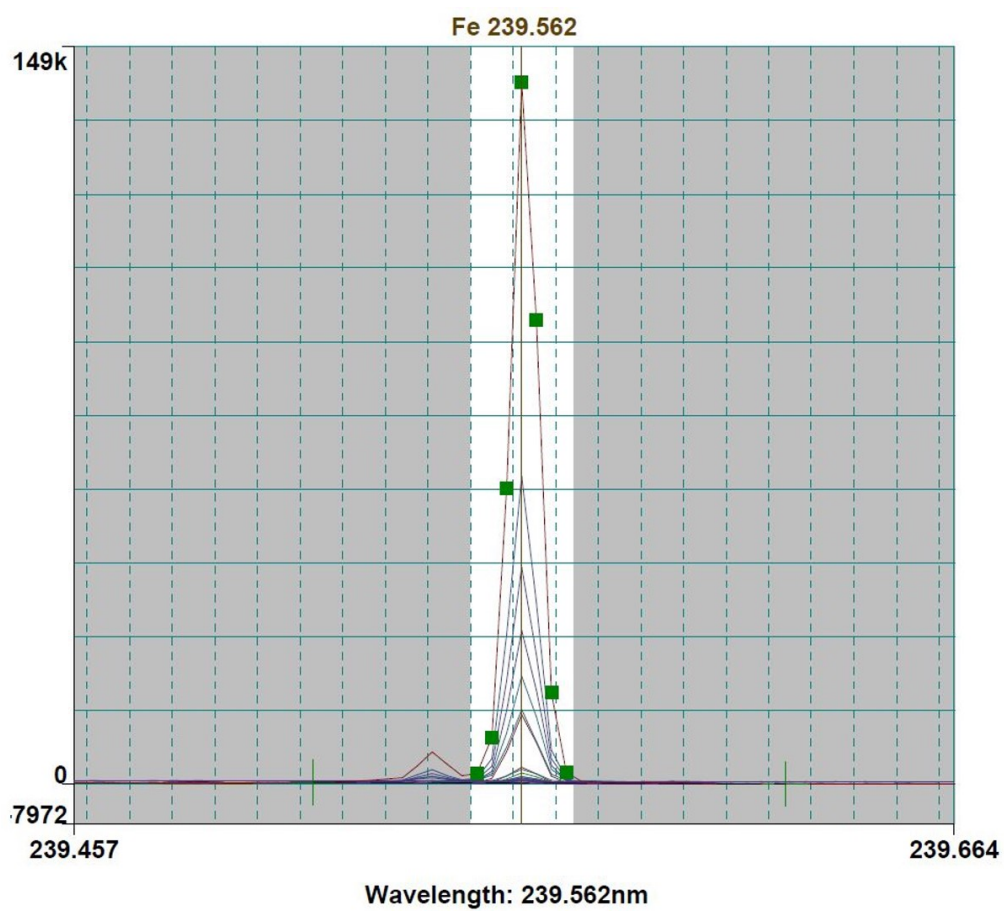
Ethanol				Crystal type	Water				Crystal type
No	1/2r (nm <sup>-1</sup> )	d-spacing (Å)	hkl		No	1/2r (nm <sup>-1</sup> )	d-spacing (Å)	hkl	
1	6.741	2.967	(220)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>	1	7.830	2.554	(311)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>
2	8.001	2.500	(311)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>	2	11.719	1.707	(422)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>
3	9.544	2.096	(400)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>	3	13.780	1.451	(440)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>
4	10.970	1.823	(101) / (312)	Fe / Fe <sub>5</sub> C <sub>2</sub>	4				
5	13.455	1.486	(440)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>	5				
Ethylene glycol				Crystal type	Liquid nitrogen				Crystal type
No	1/2r (nm <sup>-1</sup> )	d-spacing (Å)	hkl		No	1/2r (nm <sup>-1</sup> )	d-spacing (Å)	hkl	
1	6.816	2.934	(220)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>	1	7.957	2.514	(311)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>
2	7.966	2.511	(311)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>	2	9.652	2.072	(400)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>
3	9.511	2.103	(400)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>	3	13.608	1.470	(101)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>
4	13.597	1.471	(440)	Fe <sub>2</sub> O <sub>3</sub> / Fe <sub>3</sub> O <sub>4</sub>	4				



**Figure S.2.** A) Representative TEM images of the different samples where the bar scale is 25 nm. In these images, it is possible to appreciate the oxide matrices containing the iron-based particles synthesized in ethanol, and the agglomerates of the sample synthesized in liquid nitrogen and further redispersed in ethanol. B) Representative EDX line scans of the individual ultra-small NPs found in the samples' supernatant.

[1] [https://omlc.org/calc/mie\\_calc.html](https://omlc.org/calc/mie_calc.html) [online 21-04-2021]

[2] <https://www.webelements.com/iron/thermochemistry.html> [online 25-04-2021]



**Figure S.3.** Details from ICP-OES measurements. The main iron peak was measured at 239.56 nm, and is possible to observe smaller peak at 239.54 nm, also belonging to the iron.