

# Supplementary Materials

## Nomenclature

$f$	Fugacity, $\text{mol m}^{-3}$
$G$	Gibbs free energy, $\text{J mol}^{-1}$
$N_{ij}$	Number of moles of component $i$ in reaction $j$
$R_{\text{const}}$	Ideal gas constant, $\text{J K}^{-1} \text{mol}^{-1}$
$T$	Temperature, K

## Greek symbols

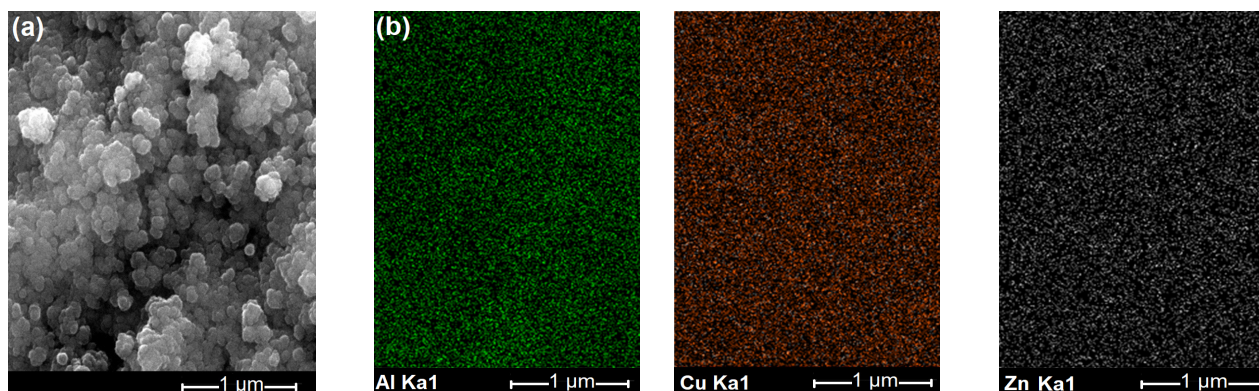
$\mu_i$	Chemical potential of component $i$ , $\text{J mol}^{-1}$
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## Superscript

$^o$	Standard state
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## 1. Scanning electron microscopy–Energy dense X-Ray spectroscopy of the Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst

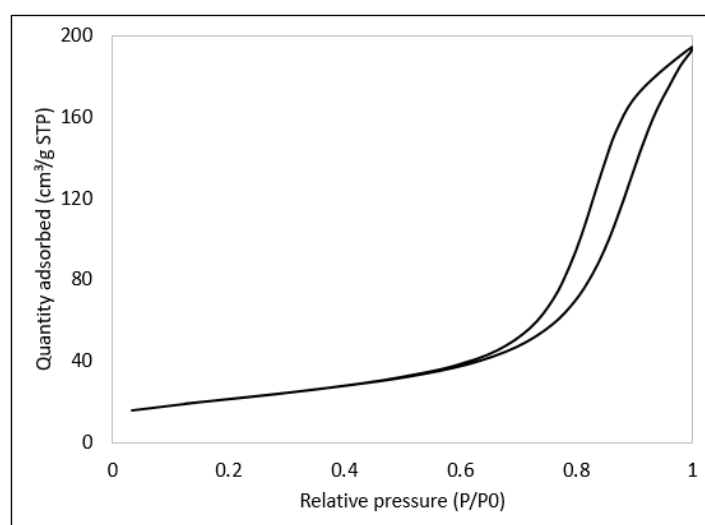
SEM-EDS results confirmed the presence of Cu, Zn, Al and O in the catalyst. The SEM micrograph (Figure S1a) shows a catalyst consisting of a large number of isolated and agglomerated globular catalyst particles. The EDS maps (Figure S1b) show a very homogeneous distribution of Cu, Zn and Al in the catalyst, which is expected to result in beneficial interactions between well-mixed and uniformly spread nanoparticles, especially Cu and ZnO.



**Figure S1.** Commercial Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst: (a) morphology displayed on the SEM micrograph and (b) EDS maps of elemental distribution: Al (green), Cu (red) and Zn (black).

## 2. N<sub>2</sub> adsorption/desorption profile of the Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst

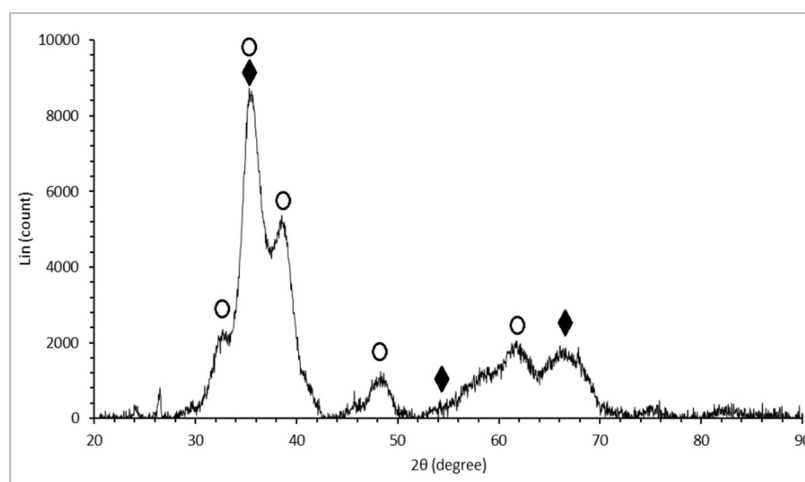
The N<sub>2</sub> adsorption/desorption profile of the catalyst corresponds to a Type IV isotherm with a H1 hysteresis loop, which is a characteristic of catalysts with a mesoporous structure [48].



**Figure S2.** Isothermal (−196 °C) linear plot of the N<sub>2</sub> adsorption/desorption on the Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst.

### 3. X-ray diffractogram of the Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst

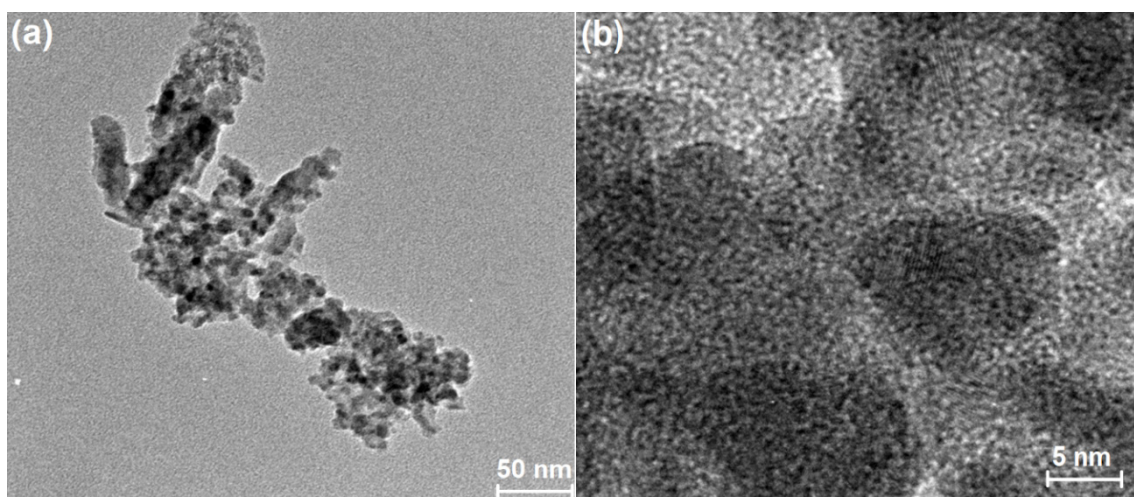
The XRD diffractogram of the catalyst (Fig S3) confirmed the presence of CuO and ZnO. Al<sub>2</sub>O<sub>3</sub> peaks were not visible, probably because of their low content or amorphous nature.



**Figure S3.** XRD diffractogram of the Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst showing typical CuO (◆) and ZnO (○) peak positions as reported in the literature [14,18,39].

### 4. Transmission electron microscopy of the Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst

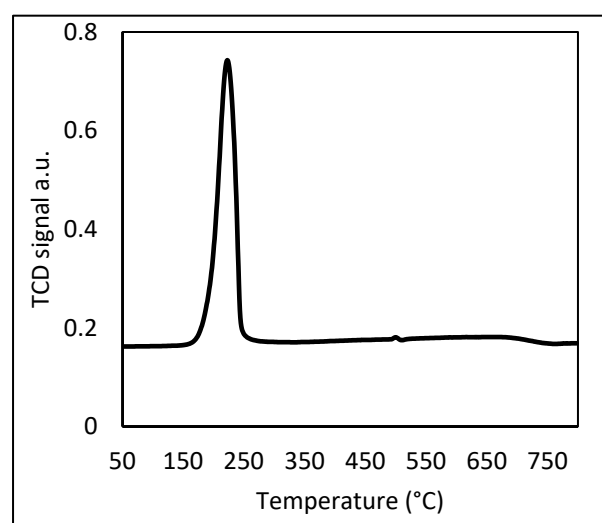
The TEM micrographs (Fig. S4) reveal that the catalyst components (Cu, ZnO and Al<sub>2</sub>O<sub>3</sub>) are hardly distinguishable. Furthermore, the fact that the particles are not well shaped can also denote a low level of crystallinity of the catalyst components [9], TEM micrographs suggest an intimate contact between Cu and ZnO particles. This has been reported to enhance the catalytic performance of Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> [9,14].



**Figure S4.** Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst: (a) low-magnification and (b) high-magnification TEM micrographs.

### 5. Catalyst temperature programmed reduction profile

H<sub>2</sub> temperature programmed reduction profile (Fig. S5) was used for the determination of the Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst reduction temperature. A reduction temperature of 230 °C was used in the reduction of the catalyst prior to experiments.



**Figure S5.** H<sub>2</sub>-TPR profile of the Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst.

### 6. Equilibrium calculations

Equilibrium calculations were performed using ASPEN v8.6 Gibbs equilibrium reactor (RGibbs). In order to simulate the direct CO<sub>2</sub>-to-MeOH process, and generate the equilibrium CO<sub>2</sub> conversion and methanol selectivity curves, the feed composition was set to 75% H<sub>2</sub> and 25% CO<sub>2</sub>, and the products were set to include CO, H<sub>2</sub>O, the unreacted CO<sub>2</sub> and H<sub>2</sub>. The RGibbs works on the principle of Gibbs free energy minimisation, which is a non-stoichiometric method, assuming that a system of  $n$  components involved in  $r$  reactions is thermodynamically favoured when the change in Gibbs  $dG$  free energy is minimum [49,50].

$$dG = \sum_{i=1}^n \sum_{j=1}^r \mu_i dN_{ij} = 0.$$

In Eq. B1, the chemical potential  $\mu_i$  of component  $i$  is calculated by

$$\mu_i = R_{const} T \left[ G_i^0 + \ln \left( \frac{f_i}{f_i^0} \right) \right].$$

Neither methane nor other hydrocarbons were part of the product gas. Hence, the CO<sub>2</sub> hydrogenation to MeOH and reverse water gas shift were the only possible reactions in the system.