



Article Synchronization of Fractional-Order Delayed Neural Networks Using Dynamic-Free Adaptive Sliding Mode Control

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Abstract: In this work, a dynamic-free adaptive sliding mode control (adaptive-SMC) methodology for the synchronization of a specific class of chaotic delayed fractional-order neural network systems in the presence of input saturation is proposed. By incorporating the frequency distributed model (FDM) and the fractional version of the Lyapunov stability theory, a dynamic-free adaptive SMC methodology is designed to effectively overcome the inherent chaotic behavior exhibited by the delayed FONNSs to achieve synchronization. Notably, the decoupling of the control laws from the nonlinear/linear dynamical components of the system is ensured, taking advantage of the norm-boundedness property of the states in chaotic systems. The effectiveness of the suggested adaptive-SMC method for chaos synchronization in delayed fractional-order Hopfield neural network systems is validated through numerical simulations, demonstrating its robustness and efficiency. The proposed dynamic-free adaptive-SMC approach, incorporating the FDM and fractional Lyapunov stability theorem, offers a promising solution for synchronizing chaotic delayed FONNSs with input saturation, with potential applications in various domains requiring synchronization of such systems.

Keywords: delayed neural networks; adaptive SMC; fractional-order delayed systems; synchronization; Lyapunov stability theorem

1. Introduction

Fractional calculus is a branch of mathematics that generalizes the concept of differentiation and integration to fractional orders. It involves operations on functions that are not restricted to integer values of differentiation and integration orders [1,2]. Fractional calculus has found applications in various scientific, engineering, and practical fields. Some notable applications of fractional-order (FO) systems include signal processing and image analysis, control systems, electromagnetism, viscoelasticity and rheology, diffusion processes, biology and medicine, finance and economics, material science, electrochemistry, fluid mechanics, heat transfer and so on [3].

In recent years, neural networks have made significant contributions to various fields of science and engineering, revolutionizing areas such as medical science [4], security [5], the manufacturing industry [6], robotics [7], and image encryption [8]. Additionally, delayed neural networks (DNNs) have gained importance due to their ability to effectively model and analyze dynamic systems by incorporating time-delayed information. Unlike traditional neural networks, DNNs capture temporal dependencies and patterns in time-series and sequential data, making them suitable for tasks such as time series forecasting, speech recognition, financial market analysis, and control systems [9]. The incorporation of delays between inputs and outputs allows DNNs to accurately model complex processes and make predictions based on historical information, enabling researchers to tackle real-world problems that require a deep understanding of temporal dynamics [10].

The control of delayed fractional-order neural network systems (delayed FONNSs) is essential due to their wide range of applications and unique characteristics that distinguish



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Copyright: © 2023 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). them from integer-order systems. Delayed FONNSs possess long-term memory effects, time delays, and non-local interactions, which can lead to unpredictable and unstable behavior if not properly regulated. Efficient control strategies tailored for delayed FONNSs enable performance optimization, stability enhancement, and the achievement of desired system responses, benefiting fields such as biology, chemistry, and finance [11].

The utilization of delayed FONNSs has been extensively reported in various branches of research and engineering, including financial modeling [12], energy systems [13], optimization [14], and medical sciences [15]. Controlling delayed FONNSs, characterized by severe nonlinearity, high sensitivity, oscillatory features, and fractal motions, has attracted attention in order to stabilize and regulate their behavior. Different control methods, such as fuzzy control [16,17], Proportional-Integral-Derivative (PID) controlling [18], adaptive control [19], back-stepping control [20], sliding mode control [21,22], and optimal control [23], have been developed to suppress undesirable actions in fractional-order nonlinear structures.

Among these control techniques, sliding mode control (SMC) has gained popularity due to its precision, simplicity of implementation, robustness to unknown parameters, and resilience. SMC involves two main phases: constructing a suitable and stable sliding surface (SS) and generating adaptive control commands that drive the chaotic paths of the fractional-order systems to converge and remain on the designated sliding surface [24].

Recently, numerous researchers have proposed various kinds of SMC methodologies for the synchronization of fractional-order (FO) delayed systems. Namely, in [25], a SMC was designed to synchronize uncertain FO delayed memristive neural networks. An FO adaptive SMC methodology is introduced in [26] to lag-synchronize FO delayed chaotic systems. In [27], a finite-time optimal SMC method was developed for fuzzy FO system time-varying delays based on the dynamics of neural networks. Shi et al. [28], have designed an SMC scheme for the control and stabilization of FO time-delayed chaotic systems under external excitation utilizing Lyapunov–Krasovskii stability and LMI theorems. In [29,30], model-based SMC methods were designed to project the synchronization of delayed FONNSs and apply these methods for secure communications. The authors in reference [31] proposed a resilient controller that combines elements of a supervised sliding mode controller with an optimal robust adaptive fractional PID controller, all governed by fuzzy rules. In [32], the problem of guaranteed cost control for delayed FONNSs was studied and a Lyapunov-based feedback control technique was introduced.

In [33], to solve the problem of stabilizing FO uncertain chaotic systems with time delays, a hyperbolic adaptive neuro-fuzzy SMC approach was developed based on a backstepping control strategy. In [34], a deep learning-based SMC was designed for a delayed FO fuzzy multiagent system using LMI theory. Yan et al. formulated an FO SMC for the stability analysis and load frequency control of a class of FO delayed power systems in [35]. In [36], to synchronize unknown delayed FO chaotic systems, a robust NN-based SMC was developed using the Chebyshev neural network. An observer-based finite-time SMC was proposed to stabilize delayed FO hybrid systems with nonlinear inputs in [19]. Parvizian et al. [37], developed an observer-based adaptive SMC technique for FO Markovian jump systems with time delay and input nonlinearity.

However, many of these research projects suffer from one or more of the following limitations:

- 1. The majority of these works focus on synchronizing two identical delayed FONNSs, which is rarely encountered in real-world scenarios.
- 2. Control plans heavily rely on utilizing both linear and nonlinear elements within the systems.
- 3. The application of SMC methods often leads to undesirable phenomena such as vibration.
- 4. Most studies overlook the inclusion of error models, external disturbances, and input saturations when describing the system.

To address these shortcomings, we propose an innovative approach that combines the FO edition of the Lyapunov Stability Theory (LST) with the theory of frequency distribution models (FDM). This novel method aims to develop a chattering-free adaptive SMC

technique that is both dynamic and robust against unpredictability, external disturbances, and input saturations.

This paper presents a novel approach for synchronizing chaotic delayed FONNSs with system uncertainties, external disturbances, and input saturation. The proposed technique is a dynamic-free adaptive SMC method. Initially, a smooth SS is suggested based on the FDM, offering convenience in design and ease of use. Subsequently, the FO version of the LST is employed to develop a suitable control method that ensures the desired sliding motion. Importantly, the design of this method does not rely on the linear or nonlinear equations of the delayed FONNS dynamics. To validate the effectiveness of the dynamic-free adaptive SMC approach, two numerical examples are provided, involving two- and three-dimensional Hopfield delayed FONNSs. These examples serve to demonstrate the efficiency and efficacy of the proposed technique.

In summary, this study has achieved the following:

- 1. Development of a dynamic-free adaptive SMC technique that effectively synchronizes a wide range of complex and chaotic Hopfield delayed FONNSs without the issue of chattering.
- 2. The proposed dynamic-free adaptive SMC approach demonstrates robustness in suppressing system uncertainties, external disturbances, and input-saturation effects.
- 3. Analytical results regarding the general and asymptotic stability of the synchronized closed-loop delayed FONNSs have been obtained by employing the FDM, adaptive controller concepts, and the FO version of the LST. These tools contribute to the reliability of the achieved results.
- 4. Simulations have been conducted to validate the theoretical findings and ensure their applicability in real-world scenarios.

The structure of this paper is outlined as follows: In Section 2, the fundamental concepts and preliminaries of the FO calculus and FOSs are provided. This is followed by the presentation of the problem statement and system description. Subsequently, a novel dynamic-free adaptive SMC technique is proposed for the synchronization of chaotic delayed FONNSs. Section 4 includes numerical scenarios and showcases the analytical accomplishments of the paper through two scenarios involving the synchronization of unknown Hopfield delayed FONNSs. Finally, Section 5 concludes the paper by discussing the obtained results and drawing conclusions from them.

2. Preliminaries and Problem Description

This section is divided by subheadings. It should provide a concise and precise description of the experimental results, their interpretation, as well as the experimental conclusions that can be drawn.

2.1. Preliminary Subjects

Definition 1 ([38]). Consider that $\Psi(t)$ is a continuous function in \mathbb{R} . The Riemann–Liouville defined FO integral of $\Psi(t)$ for a fractional number $\kappa \in \mathbb{R}$ is given as

$$_{t_0}I_t \Psi(t) = \mathbf{D}^{-\kappa}\Psi(t) = \frac{1}{\Gamma(\kappa)} \int_{t_0}^t \Psi(v) \Big(t-v)^{\kappa-1} dv, \tag{1}$$

in which $t_0 \in \mathbb{R}$ and $\Gamma(.)$ are the initial time and the Gamma function, respectively.

Definition 2 ([38]). Consider that $\Psi(t)$ as a continuous function in \mathbb{R} . The Caputo-defined FO derivative of $\Psi(t)$ for a fractional number $\kappa \in \mathbb{R}$ is given as

$${}_{t_0}^{\scriptscriptstyle C} \boldsymbol{D}_t^{\kappa} \boldsymbol{\Psi}(t) = \boldsymbol{D}^{\kappa} \boldsymbol{\Psi}(t) = \frac{1}{\Gamma(m-\kappa)} \int_{t_0}^t \frac{\boldsymbol{\Psi}^{(n)}(v)}{(t-v)^{\kappa-n+1}} dv,$$
(2)

where $n - 1 < \kappa \leq n \in \mathbb{N}$ and D^{κ} stands for the Caputo derivative operator throughout the remaining parts of the the paper.

Feature 1 ([39]). *For any real constant* $w \in \mathbb{R}$ *, we have* $D^{\kappa}w = 0$ *.*

Feature 2 ([39]). *Suppose that* $0 < \kappa < 1$ *and* $W(t) \in C^{m}[0, T]$ *; then:*

$$\boldsymbol{D}^{\boldsymbol{\kappa}}(I^{\boldsymbol{\kappa}}W(t)) = \boldsymbol{D}^{\boldsymbol{\kappa}}(\boldsymbol{D}^{-\boldsymbol{\kappa}}W(t)) = W(t).$$
(3)

Theorem 1 ([40]). For any $0 < \kappa < 1$, if the FO system $D^{\kappa}\Pi(t) = \{(t, \Pi(t)) \text{ holds in the Lipschitz condition, then } q = 0 \text{ is an equilibrium for it. Also, suppose that there is the Lyapunov function <math>V(t, \Pi(t))$ and class-K functions r_1 . r_2 and r_3 with the following relations:

$$r_1(\|q\|) \le V(t, \Pi(t)) \le r_2(\|q\|).$$
(4)

$$D^{-\kappa}V(t, \Pi(t)) \le -r_3(\|q\|).$$
(5)

If this is the case, then the system $D^{\kappa} \amalg(t) = \{(t, \amalg(t)) \text{ is said to be asymptotically stable.}\}$

Lemma 1 ([41]). If $0 < \kappa < 1$ the following inequality will be applicable for $\mathcal{G}(t)$:

$$\frac{1}{2}\boldsymbol{D}^{\boldsymbol{\kappa}}\boldsymbol{\mathcal{G}}^{2}(t) \leq \boldsymbol{\mathcal{G}}(t)\boldsymbol{D}^{\boldsymbol{\kappa}}\boldsymbol{\mathcal{G}}(t).$$
(6)

Theorem 2 (FDM theory) ([42]). Consider a continuous FO dynamical system as follows:

$$\boldsymbol{D}^{\boldsymbol{\kappa}}\boldsymbol{Q}(t) = \{(t, \boldsymbol{Q}(t)). \tag{7}$$

Also, let $B : (0, \infty) \times [0, Q] \to \mathbb{R}^n$ be the following equation:

$$B(\Box, t) = \int_0^t e^{-\Box^2(h-\varrho)} \{ (\Pi, \varrho) d\varrho.$$
(8)

Then, the FO system (7) is equal to

$$\begin{cases} \frac{\partial B(\Box,h)}{\partial t} = -\Box^2 B(\Box,t) + f(t.Q(t)) \\ Q(t) = \int_0^\infty \varphi(\Box) B(\Box,t) d\Box \end{cases}$$
(9)

where $\varphi(\Box) = \frac{2sin(\iota\pi)}{\pi} \Box^{1-2\iota}$ and $0 < \iota < 1$.

Remark 1. A fractional-order system and a traditional system, characterized by their respective approaches to modeling dynamic phenomena, exhibit fundamental differences. In a traditional system, the processes are described using integer-order derivatives and integrals, limited to whole numbers. This methodology is suitable for instantaneous behavior without consideration of past states or memory effects. In contrast, a fractional-order system introduces a more flexible framework by allowing non-integer values for differentiation and integration orders, essentially permitting fractional orders. This adaptability enables the representation of complex behaviors involving memory, long-range dependencies, and non-local interactions. Traditional systems are adept at modeling well-understood systems with integer-order behaviors, but they may struggle to accurately capture intricate dynamics such as anomalous diffusion, viscoelasticity, and fractal-like properties. Fractional-order systems excel in such scenarios, as they encompass memory-driven responses and encompass a wider range of response patterns, including power-law decays and growths. Consequently, the choice between these systems hinges on the nature of the phenomena being studied,

with fractional-order systems offering greater precision for systems that display fractional-order dynamics, while traditional systems continue to be applied effectively in scenarios with integerorder behaviors.

2.2. Problem Statement

Recently, in [43], the dynamical mechanism of FOHNN is presented as follows:

$$D^{\kappa}x_{i}(t) = -a_{i}x_{i}(t) + \sum_{j=1}^{n} w_{ij}f_{j}(x_{j}(t)) + I_{i}$$
(10)

where $0 < \kappa < 1$, i = 1, 2, ..., n, $x_i(t)$ is the ith state of the neuron of the FOHNN; a_i is the frequency at which the *i*-th neuron's potential returns to its quiescent state when disconnected from the network; w_{ij} is an entry of weight matrix $W = (w_{ij})_{n \times n}$

, which presents connected neurons; $f_j(x_j(t))$ is the activation function of the jth neuron and is a bounded differentiable function and the activation function for the *i*th neuron; and I_i is the *i*-th element of external distributions.

Now, for i = 1, 2, ..., n, consider the following class of delayed FONNSs:

$$\mathbf{D}^{\alpha}x_{i}(t) = -a_{i}x_{i}(t) + \sum_{j=1}^{n} M_{ij}\{_{1j}(x_{j}(t)) + \sum_{j=1}^{n} P_{ij}\{_{2j}(x_{j}(t-\tau)) + I_{i}$$
(11)

where *n* denotes the number of units of NN, $x_i(t)$ is the *i*th state of the neuron of the delayed FONNSs, $\{1_j \text{ and } \}_{2j}$ denote the activation function of the *j*th neuron, M_{ij} and P_{ij} denote the components of the connection weight matrices of the *j*th neuron on the ith neuron, $a_i > 0$ is an unknown number and shows the rate with which the ith neuron resets its potential to the resting state when disconnected from the network, I_i shows the ith element of external distributions, and τ means the delay of transmission.

Here, to address the problem of synchronization and stabilization of the error system for the delayed FONNSs, if we designate the system (11) as the drive system, then the following system will act as the response system:

$$\boldsymbol{D}^{\kappa} y_{i}(t) = -b_{i} y_{i}(t) + \sum_{j=1}^{n} N_{ij} \}_{1j} (y_{j}(t)) + \sum_{j=1}^{n} Q_{ij} \}_{2j} (y_{j}(t-\tau)) + J_{i} + \Psi_{i}(u_{i}(t))$$
(12)

where $y_i(t)$ is the *i*th state of the neuron of the delayed FONNSs, j_{1j} and j_{2j} denote the activation function of the *j*th neuron, N_{ij} and Q_{ij} denote the components of the connection weight matrices of the *j*th neuron on the ith neuron, $b_i > 0$ is same as a_i in (11), J_i shows the ith element of the external distributions, and τ means the delay of transmission.

Furthermore, $u_i(t)$ denotes the control input, and $\Psi_i(u_i(t))$ is the input saturation function:

$$\Psi_i(u_i(t)) = u_i(t) + \Delta(u_i(t)), \ i = 1, \dots, n$$
(13)

in which

$$\Delta(u_i(t)) = \begin{cases} u^{n_1} - u_i(t) & \text{if } u_{n_2} > u_i(t) \\ (\theta - 1)u_i(t) & \text{if } u^{p_1} < u_i(t) < u^{n_1}, i = 1, \dots, n, \\ u^{p_1} - u_i(t) & \text{if } u_i(t) \ge u_{p_2} \end{cases}$$
(14)

where u^{p_1} , $u_{p_2} \in R^+$ and u^{n_1} , $u_{n_2} \in R^-$ are the bounds of the input saturation procedure (13), and $\theta \in \mathbb{R}$ refers to the slope of saturation.

Now, by defining the error parameter vector, one gets

$$E = X - Y = [x_1(t), x_2(t), \dots, x_n(t)]^T - [y_1(t), y_2(t), \dots, y_n(t)]^T$$

= $[e_1(t), e_2(t), \dots, e_n(t)]^T$. (15)

Thus, for i = 1, 2, ..., n, the dynamics of the synchronization error function can then be obtained as follows:

$$\mathbf{D}^{\kappa} e_i(t) = \mathbf{D}^{\kappa} x_i(t) - \mathbf{D}^{\kappa} y_i(t)$$
(16)

$$= -(a_{i}(t)x_{i}(t) - b_{i}(t)y_{i}(t)) + \sum_{j=1}^{n} \left[M_{ij} \{ 1_{j}(x_{j}(t)) - N_{ij} \}_{1j}(y_{j}(t)) \right] + \sum_{j=1}^{n} \left[P_{ij} \{ 2_{j}(x_{j}(t-\tau)) - Q_{ij} \}_{2j}(y_{j}(t-\tau)) \right] + (I_{i} - J_{i}) - \Psi_{i}(u_{i}(t)).$$
(17)

The ultimate objective is to develop an adaptive control mechanism that is appropriate and usable in such a way that, for i = 1, 2, ..., n,

$$\lim_{t \to \infty} \|e_i(t)\| = \lim_{t \to \infty} \|x_i(t) - y_i(t)\| = 0.$$
(18)

The topic of synchronization between the drive mechanism (11) and the response mechanism (12) will be resolved and realized if Equation (18) is developed.

Assumption 1. The state trajectories of error for chaotic systems are generally limited in phasespace [44,45], which may be deduced from the fact that chaotic systems produce irregular attractors as a consequence of their behavior. As a result, there exist the positive numbers ω_{1i} , ω_{2i} , δ_{1i} and δ_{2i} , which meet the conditions outlined in the following relations:

$$-(a_{i}(t)x_{i}(t) - b_{i}(t)y_{i}(t)) + \sum_{j=1}^{n} \left[M_{ij} \{ 1_{j}(x_{j}(t)) - N_{ij} \}_{1j}(y_{j}(t)) \right] \le \omega_{1i} + \omega_{2i} \|E(t)\|$$
(19)

and

$$\left|\sum_{j=1}^{n} \left[P_{ij} \{ 2_j (x_j(t-\tau)) - Q_{ij} \}_{2j} (y_j(t-\tau)) \right] \right| \le \delta_{1i} + \delta_{2i} \| E(t-\tau) \|.$$
(20)

Additionally, there is an expectation that the uncertainty terms I_i and J_i will be bounded. Therefore, there are positive constants d_{1i} and d_{2i} in such a way that

$$|(I_i - J_i)| \le d_{1i} + d_{2i} ||E||, \qquad i = 1, 2, \dots, n.$$
(21)

As a result of (19), (20), and (21),

$$\left| -(a_{i}(t)x_{i}(t) - b_{i}(t)y_{i}(t)) + \sum_{j=1}^{n} \left[M_{ij}\{_{1j}(x_{j}(t)) - N_{ij}\}_{1j}(y_{j}(t)) \right] \right| + \left| \sum_{j=1}^{n} \left[P_{ij}\{_{2j}(x_{j}(t-\tau)) - Q_{ij}\}_{2j}(y_{j}(t-\tau)) \right] \right| + \left| (I_{i} - J_{i}) \right| \le \gamma_{i} + \zeta_{i} \|E\| + \delta_{i} \|E(t-\tau)\|.$$

$$(22)$$

Assumption 2. The boundedness feature of the controller is one of the most critical conditions that must be met in order for a control law to be relevant. As a consequence, it is preferable that the $\Delta(u_i(t))$ is bounded. As a result, one has

$$|\Delta(u_i(t))| \le \varphi_i \le \infty. \tag{23}$$

3. Adaptive SMC Methodology Design

First, the sliding surface will be introduced, and after the relevant analyses, an adaptive control law will be designed to overcome the synchronization problem.

Therefore, for i = 1, ..., n, the proposed FO sliding-surface equation is suggested as

$$s_i(t) = e_i(t) + \mathbf{D}^{-\kappa} \left[\mu_i e_i(t) + |e_i(t)|^q sor(e_i(t)) \right],$$
(24)

where μ_i and $0 < \kappa, q < 1$ are positive constants, and

$$sor(m) = \begin{cases} tanh(m), & for |m| > 1\\ m, & for |m| \le 1. \end{cases}$$
(25)

When the sliding motion takes place, it is common knowledge that the requirement $s_i(t) = 0$ is satisfied; hence, using Feature 2,

$$s_i(t) = 0 \Rightarrow \mathbf{D}^{\kappa} s_i(t) = 0 \tag{26}$$

$$\Rightarrow \mathbf{D}^{\kappa} s_i(t) = \mathbf{D}^{\kappa} e_i(t) + \mu_i e_i(t) + |e_i(t)|^q \operatorname{sor}(e_i(t)) = 0$$
(27)

$$\Rightarrow \mathbf{D}^{\kappa} e_i(t) = -\left(\mu_i e_i(t) + |e_i(t)|^q \operatorname{sor}(e_i(t))\right).$$
(28)

Theorem 3. *The sliding dynamic Equation (28) will be stable, and the states of the FO error neural network (17) have an asymptotic convergence to the origin.*

Proof. Based on Theorem 2, for i = 1, ..., n, Equation (28) can be represented as

$$\begin{cases} \frac{\partial B_i(\underline{\exists},t)}{\partial t} = -\underline{\exists}^2 B_i(\underline{\exists},t) - (\mu_i e_i(t) + |e_i(t)|^q sor(e_i(t))),\\ e_i(t) = \int_0^\infty \varphi_i(\underline{\exists}) B_i(\underline{\exists},t) d\underline{\exists} \end{cases}$$
(29)

Now, by choosing the following form of Lyapunov function:

$$V_{1i}(t) = \int_0^\infty \varphi_i(\beth) B_i^2(\beth, t) d \beth$$
(30)

one has

$$\frac{dV_{1i}(t)}{dt} = \int_0^\infty \varphi_i(\Box) B_i(\Box, t) \frac{\partial B_i(\Box, t)}{\partial t} d\Box$$
(31)

Utilizing Equation (29)

$$\frac{dV_{1i}(t)}{dt} = \int_0^\infty \varphi_i(\Box) B_i(\Box, t) \Big[-\Box^2 B_i(\Box, h) - \big(\mu_i e_i(t) + |e_i(t)|^q \operatorname{sor}(e_i(t))\big) \Big] d\Box$$
(32)

$$= -\int_{0}^{\infty} \varphi_{i}(\Box) \Box^{2} B_{i}^{2}(\Box, t) d\Box - \left[\left(\mu_{i} e_{i}(t) + |e_{i}(t)|^{q} sor(e_{i}(t)) \right) \right] \underbrace{\int_{0}^{\infty} \varphi_{i}(\Box) B_{i}(\Box, t) d\Box}_{e_{i}(t)}$$
(33)

$$= -\int_0^\infty \varphi_i(\underline{\Box}) \underline{\Box}^2 B_i^2(\underline{\Box}, t) d\underline{\Box} - \mu_i e_i^2(t) - e_i(t) |e_i(t)|^q \operatorname{sor}(e_i(t))$$
(34)

Here, concerning Equations (34), and (25), two items need to be investigated:

• item 1: if $|e_i| \le 1$, then $e_i(t)sor(e_i(t)) = e_i(t)^2$; thus, in (34), one gets

$$\frac{dV_{1i}(t)}{dt} = -\int_0^\infty \varphi_i(\underline{\Box}) \underline{\Box}^2 B_i^2(\underline{\Box}, t) d\underline{\Box} - e_i^2(t) \left(\mu_i + |e_i(t)|^q\right) < 0$$
(35)

• item 2: if $|e_i| > 1$, then $e_i(t)sor(e_i(t)) = e_i(t)tanhe_i(t) < |e_i(t)|$; hence, in (30), one obtains

$$\frac{dV_{1i}(t)}{dt} = -\int_0^\infty \varphi_i(\beth) \beth^2 B_i^2(\beth, t) d\beth - \mu_i e_i^2(t) - |e_i(t)|^{1+q} < 0$$
(36)

Therefore, inequalities (35) and (36) shows that $\frac{dV_{1i}(t)}{dt} < 0$; this means that the sliding mode dynamic (28) has asymptotic stability, and this completes the proof. \Box

Now, for i = 1, ..., n, a dynamic-free adaptive SMC is designed as

$$u_{i}(t) = \left[\mu_{i}e_{i}(t) + |e_{i}(t)|^{q}sor(e_{i}(t)) + \hat{\sqrt{s}}s_{i} + (\hat{\gamma}_{i} + \hat{\zeta}_{i}||E|| + \hat{\delta}_{i}||E(t-\tau)|| + \hat{\varphi}_{i} + \psi_{i}\right)sor(s_{i}(t))\right]$$
(37)

$$D^{\kappa} \hat{\gamma}_i(t) = \nu |s_i|, \qquad \hat{\gamma}_i(0) = \hat{\gamma}_{i0}, \quad i = 1, \dots, n.$$
 (38)

$$\mathbf{D}^{\kappa} \tilde{\zeta}_{i}(t) = r|s_{i}| \|E\|, \qquad \hat{\zeta}_{i}(0) = \hat{\zeta}_{i0}, \quad i = 1, \dots, n.$$
(39)

$$\hat{D^{\kappa}\delta_{i}(t)} = l|s_{i}||E(t-\tau)||, \qquad \hat{\delta_{i}(0)} = \hat{\delta_{i0}}, \quad i = 1, \dots, n.$$
(40)

$$\mathbf{D}^{\kappa}\hat{\boldsymbol{\varphi}}_{i}(t) = \mathfrak{z}|\boldsymbol{s}_{i}|, \quad \hat{\boldsymbol{\varphi}}_{i}(0) = \hat{\boldsymbol{\varphi}}_{i0}, \quad i = 1, \dots, n.$$
(41)

Theorem 4. Suppose we have the FO error dynamical mechanism (17). Then, by operating the SMC methodology (37) and related adaption terms (38)–(41), the process of the trajectories of the FO dynamical mechanism (17) will exhibit asymptotic stability.

Proof of Theorem 4. Consider the following equality as a Lyapunov function

$$V_{2i}(t) = \frac{1}{2} \left(s_i^2 + \frac{1}{\nu} \left(\hat{\gamma}_i - \gamma_i \right)^2 + \frac{1}{r} \left(\hat{\zeta}_i - \zeta_i \right)^2 + \frac{1}{l} \left(\hat{\delta}_i - \delta_i \right)^2 + \frac{1}{3} \left(\hat{\varphi}_i - \varphi_i \right)^2 \right).$$
(42)

Then, using Lemma 1, one obtains

$$\mathbf{D}^{\kappa}V_{2i}(t) \leq s_{i}\mathbf{D}^{\kappa}s_{i} + \frac{1}{\nu}(\hat{\gamma}_{i} - \gamma_{i})\mathbf{D}^{\kappa}(\hat{\gamma}_{i} - \gamma_{i}) + \frac{1}{r}(\hat{\zeta}_{i} - \zeta_{i})\mathbf{D}^{\kappa}(\hat{\zeta}_{i} - \zeta_{i}) + \frac{1}{l}(\hat{\delta}_{i} - \delta_{i})\mathbf{D}^{\kappa}(\hat{\delta}_{i} - \delta_{i}) + \frac{1}{3}(\hat{\varphi}_{i} - \varphi_{i})\mathbf{D}^{\kappa}(\hat{\varphi}_{i} - \varphi_{i}).$$

$$(43)$$

Based on Feature 1 in Caputo FO derivative, one obtains

$$\boldsymbol{D}^{\boldsymbol{\kappa}}\boldsymbol{V}_{2i}(t) \leq s_{i}\boldsymbol{D}^{\boldsymbol{\kappa}}s_{i} + \frac{1}{\nu}\left(\hat{\boldsymbol{\gamma}}_{i} - \boldsymbol{\gamma}_{i}\right)\boldsymbol{D}^{\boldsymbol{\kappa}}\hat{\boldsymbol{\gamma}}_{i} + \frac{1}{r}\left(\hat{\boldsymbol{\zeta}}_{i} - \boldsymbol{\zeta}_{i}\right)\boldsymbol{D}^{\boldsymbol{\kappa}}\hat{\boldsymbol{\zeta}} + \frac{1}{l}\left(\hat{\boldsymbol{\delta}}_{i} - \boldsymbol{\delta}_{i}\right)\boldsymbol{D}^{\boldsymbol{\kappa}}\hat{\boldsymbol{\delta}}_{i}\frac{1}{\vartheta}\left(\hat{\boldsymbol{\varphi}}_{i} - \boldsymbol{\varphi}_{i}\right)\boldsymbol{D}^{\boldsymbol{\kappa}}\hat{\boldsymbol{\varphi}}_{i}.$$
(44)

Inserting $D^{\kappa}s_i$ from (27) and relations (38)–(41) in (43), one gets

$$D^{\kappa}V_{2i}(t) \leq s_{i} \left[D^{\kappa}e_{i}(t) + \mu_{i}e_{i}(t) + |e_{i}(t)|^{q}sor(e_{i}(t)) \right] + \left(\hat{\gamma}_{i} - \gamma_{i}\right) |s_{i}| + \left(\hat{\zeta}_{i} - \zeta_{i}\right) |s_{i}| ||E|| + \left(\hat{\delta}_{i} - \delta_{i}\right) |s_{i}| ||E(t - \tau)|| + \left(\hat{\varphi}_{i} - \varphi_{i}\right) |s_{i}|.$$
(45)

Now, by replacing $D^{\kappa}e_i(t)$ from (17), and utilizing (13),

$$D^{\kappa}V_{2i}(t) \leq s_{i} \left[\left[-(a_{i}(t)x_{i}(t) - b_{i}(t)y_{i}(t)) + \sum_{j=1}^{n} \left[M_{ij}\{_{1j}(x_{j}(t)) - N_{ij}\}_{1j}(y_{j}(t)) \right] + \sum_{j=1}^{n} \left[P_{ij}\{_{2j}(x_{j}(t-\tau)) - Q_{ij}\}_{2j}(y_{j}(t-\tau)) \right] + (I_{i} - J_{i}) - u_{i}(t) + \Delta(u_{i}(t)) \right] + \mu_{i}e_{i}(t) + |e_{i}(t)|^{q}sor(e_{i}(t))] + \left(\hat{\gamma}_{i} - \gamma_{i}\right)|s_{i}| + \left(\hat{\zeta}_{i} - \zeta_{i}\right)|s_{i}| ||E|| + \left(\hat{\delta}_{i} - \delta_{i}\right)|s_{i}| ||E(t-\tau)|| + \left(\hat{\varphi}_{i} - \varphi_{i}\right)|s_{i}|.$$

$$(46)$$

$$\leq |s_{i}| \left[\left| -(a_{i}(t)x_{i}(t) - b_{i}(t)y_{i}(t)) + \sum_{j=1}^{n} \left[M_{ij} \{_{1j}(x_{j}(t)) - N_{ij} \}_{1j}(y_{j}(t)) \right] \right| + \left| \sum_{j=1}^{n} \left[P_{ij} \{_{2j}(x_{j}(t-\tau)) - Q_{ij} \}_{2j}(y_{j}(t-\tau)) \right] \right| + |(I_{i} - J_{i})| + |\Delta(u_{i}(t))| \right] + s_{i} \left[\mu_{i}e_{i}(t) + |e_{i}(t)|^{q} sor(e_{i}(t)) - u_{i}(t) \right] + \left(\hat{\gamma}_{i} - \gamma_{i} \right) |s_{i}| + \left(\hat{\zeta}_{i} - \zeta_{i} \right) |s_{i}| ||E|| + \left(\hat{\delta}_{i} - \delta_{i} \right) |s_{i}| ||E(t-\tau)|| + \left(\hat{\varphi}_{i} - \varphi_{i} \right) |s_{i}|.$$

$$(47)$$

Using (22) and (23) and replacing $u_i(t)$ from (37) in relation (47), one concludes

$$D^{\kappa}V_{2i}(t) \leq |s_i|[\gamma_i + \zeta_i||E|| + \delta_i||E(t - \tau)|| + \varphi_i] + s_i[\mu_i e_i(t) + |e_i(t)|^q \operatorname{sor}(e_i(t)) - \left[\left[\mu_i e_i(t) + |e_i(t)|^q \operatorname{sor}(e_i(t)) + \sqrt{i}s_i + \left(\hat{\gamma}_i + \hat{\zeta}_i||E|| + \hat{\delta}_i||E(t - \tau)|| + \hat{\varphi}_i + \psi_i\right)\operatorname{sor}(s_i(t))\right]\right]\right]$$

$$+ \left(\hat{\gamma}_i - \gamma_i\right)|s_i| + \left(\hat{\zeta}_i - \zeta_i\right)|s_i||E|| + \left(\hat{\delta}_i - \delta_i\right)|s_i||E(t - \tau)|| + \left(\hat{\varphi}_i - \varphi_i\right)|s_i|$$

$$\leq |s_i|[\gamma_i + \zeta_i||E|| + \delta_i||E(t - \tau)|| + \varphi_i] - s_i\left[\sqrt{i}s_i + \left(\hat{\gamma}_i + \hat{\zeta}_i||E|| + \hat{\delta}_i||E(t - \tau)|| + \hat{\varphi}_i + \psi_i\right)\operatorname{sor}(s_i(t))\right] + \left(\hat{\gamma}_i - \gamma_i\right)|s_i| + \left(\hat{\zeta}_i - \zeta_i\right)|s_i||E|| + \left(\hat{\delta}_i - \delta_i\right)|s_i||E(t - \tau)|| + \left(\hat{\varphi}_i - \varphi_i\right)|s_i|.$$

$$(49)$$

$$U_{i}ing the fact that $s_i(t)\operatorname{cor}(s_i(t)) \leq |s_i||E(t - \tau)|| + \left(\hat{\varphi}_i - \varphi_i\right)|s_i|.$$$

Using the fact that $s_i(t)sor(s_i(t)) < |s_i|$ for any $s_i \in \mathbb{R}$, we obtain

$$D^{\kappa}V_{2i}(t) \leq -\sqrt{s_i^{2}} - |s_i| \left(\hat{\gamma}_i + \hat{\zeta}_i \|E\| + \hat{\delta}_i \|E(t-\tau)\| + \hat{\varphi}_i + \psi_i \right) + \hat{\gamma}_i |s_i| + \hat{\zeta}_i |s_i| \|E\| + \left(\hat{\delta}_i \right) |s_i| \|E(t-\tau)\| + \hat{\varphi}_i |s_i|$$
(50)

$$\leq -\sqrt{s_i^2 - \psi_i |s_i|} < 0.$$
(51)

As a result, the criteria for stability in Theorem 1 have been fulfilled, and the proof has reached its conclusion. \Box

Remark 2. The "Dynamic-Free Adaptive-SMC" technique is a cutting-edge control approach that combines principles of adaptive control and sliding mode control to achieve robust and precise control performance without requiring a precise dynamic model of the system. This technique is particularly advantageous in scenarios where system dynamics are uncertain, variable, or difficult to model accurately. By leveraging adaptive mechanisms, the control algorithm can continuously update its parameters based on real-time feedback, adapting to changes in the system's behavior. The incorporation of sliding mode control ensures that the system's trajectory converges to a desired state along a predefined sliding surface, even in the presence of disturbances, uncertainties, and variations in the system's dynamics. This innovative approach offers improved tracking accuracy, disturbance rejection, and robustness compared to traditional control methods, making it a valuable tool in various applications ranging from robotics and aerospace systems to industrial processes and beyond [46].

4. Numerical Simulations

Here, two numerical scenarios of delayed FO-HNNs are investigated to illustrate the applicability of the designed adaptive SMC method in practice. The numerical algorithm proposed in [2,47] has been used for numerical simulations, considering h=0.01 for time-step in the R2023a version of MATLAB software.

4.1. Synchronization of 2D Unknown Hopfield Delayed FONNSs

In this example, the following 2-dimensional unknown Hopfield delayed FONNSs are considered for illustration. Therefore, the drive system is as follows:

$$\begin{cases} D^{\kappa}x_{1}(t) = -x_{1}(t) - 2 \tanh(x_{1}(t)) + 2.3 \tanh(x_{2}(t)) - 1.3 \tanh(x_{1}(t-\tau)) - 1.2 \tanh(x_{2}(t-\tau)) + 0.2 \\ D^{\kappa}x_{2}(t) = -x_{2}(t) - 3.3 \tanh(x_{1}(t)) - 1.5 \tanh(x_{2}(t)) - 3.5 \tanh(x_{1}(t-\tau)) - 2 \tanh(x_{2}(t-\tau)) + 0.3, \end{cases}$$
(52)

with $\kappa = 0.92$ and $\tau = 1.2$. Also, $x_1(0) = -5$ and $x_2(0) = 5$ are selected as initial values. And, the response system is as follows:

$$\begin{cases} D^{\kappa}y_{1}(t) = -y_{1}(t) + 0.5 \sin(y_{1}(t)) + \sin(y_{2}(t)) + 0.5 \tanh(y_{1}(t-\tau)) + \tanh(y_{2}(t-\tau)) + 0.1 + \Psi_{1}(u_{1}(t)) \\ D^{\kappa}y_{2}(t) = -0.5 y_{2(t)} + \sin(y_{1}(t)) - 0.5 \sin(y_{2}(t)) - 0.5 \tanh(y_{1}(t-\tau)) - \tanh(y_{2}(t-\tau)) + 0.15 + \Psi_{2}(u_{2}(t)), \end{cases}$$
(53)

Also, $y_1(0) = 5$ and $y_2(0) = -4$ are the initial values. The parameters of the control technique (37) are fixed as $\sqrt{1} = \sqrt{2} = 3$, $\nu = 2.5$,

r = 2, l = 1.2, and $\mathfrak{z} = 1.8$. Moreover, the constants of the sliding surface (24) are selected by $\mu_1 = \mu_2 = 2$, q = 0.9. Furthermore, the nonlinear function $\Psi_i(u_i(t))$ is defined as

$$\Psi_i(u_i(t)) = \begin{cases} 3 & if \ u_i(t) > 3\\ 0.98u_i(t) & if - 3 \le u_i(t) \le 3\\ -3 & if \ u_i(t) < -3 \end{cases} \quad i = 1, 2.$$
(54)

Figures 1 and 2 depict, respectively, the synchronization of the states of FO driveresponse mechanisms (52) and (53) and the controlled error of the Hopfield delayed FONNSs ((52) and (53)). Evidently, the unusual attractors of the chaotic FO error system are rapidly stabilized. In addition, Figure 3 depicts the time history of the adaptive controller (37). It is observed that the control input (37) approaches equilibrium without any traces of the chattering phenomena. This indicates that the devised adaptive controller can effectively synchronize the 2-dimensional Hopfield delayed FONNSs ((52) and (53)). Moreover, as shown in Figure 3, as the signals of the control laws method and the saturation boundaries, they are suppressed by the saturation condition, and the leaping phenomena occur. Therefore, jumping states and switching states may be simply applied, particularly when relays and indicated saturation conditions are used.



Figure 1. The time evolution of the synchronization of the Hopfield delayed FONNSs ((52) and (53)).



Figure 2. The time evolution of the synchronization errors of the Hopfield delayed FONNSs ((52) and (53)).



Figure 3. The time evolution of the control inputs (37) for the synchronized Hopfield delayed FONNSs ((52) and (53)).

Also, Figures 4 and 5 show the time response of the sliding surface (24) in both function plot and surface plot, respectively. Clearly, from Figure 4, each parameter of the sliding surface (24) approaches the origin, and there are no traces of the chattering phenomena in the sliding surfaces. In addition, Figure 5 indicates that the result of applying this method is a stable surface.



Figure 4. The time evolution of the SS (24) to synchronize the Hopfield delayed FONNSS ((52) and (53)).

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Figure 5. The time evolution of the surface plot depicting the SS (24) implementation for achieving synchronization of the Hopfield delayed FONNSs ((52) and (53)).

4.2. Synchronization of 3D Unknown Hopfield Delayed FONNSs

Here, to illustrate the effectiveness of the proposed adaptive SMC, 3-dimensional unknown Hopfield delayed FONNSs are investigated. Thus, the drive system is

 $\begin{cases} D^{\kappa}x_{1}(t) = -x_{1}(t) + 2 tanh(x_{1}) - 1.2 tanh(x_{2}) + 1.3 tanh(x_{3}(t-\tau)) + 0.2, \\ D^{\kappa}x_{2}(t) = -x_{2}(t) + 1.8 tanh(x_{1}) + 1.71 tanh(x_{2}) + 1.15 tanh(x_{3}) - 1.3 tanh(x_{3}(t-\tau)) - 0.3, \\ D^{\kappa}x_{3}(t) = -x_{3}(t) - 4.75 tanh(x_{1}) - 1.1 tanh(x_{3}) + 0.56 tanh(x_{3}(t-\tau)), \end{cases}$ (55)

where $\kappa = 0.96$ and $\tau = 0.8$. Also, $x_1(0) = 2$, $x_2(0) = -2$ and $x_3(0) = 3$ are selected as initial values.

And, the response system is as follows:

Also, $y_1(0) = -3$, $y_2(0) = 4$ and $y_2(0) = -3$ are the initial values. The constants of the control method (37) are fixed as $\sqrt{1} = \sqrt{2} = 2.5$ and $\sqrt{3} = 4$,

 $\nu = 3$, r = 1.8, l = 2.3, and $\mathfrak{z} = 2.6$. Plus, the parameters of the SS (24) are $\mu_1 = 4$, $\mu_i = 2$, q = 0.94 and $\rho = 5$. Furthermore, the nonlinear mechanism $\Psi_i(u_i(t))$ is as follows:

$$\Psi_i(u_i(t)) = \begin{cases} 5 & if \ u_i(t) > 5\\ u_i(t) \ if \ -5 \le u_i(t) \le 5\\ -5 & if \ u_i(t) < -5 \end{cases} \quad i = 1, 2, 3.$$
(57)

The synchronized states of the drive-response Hopfield delayed FONNSs ((55) and (56)), as well as the state trajectories of the controlled error of the Hopfield delayed FONNSs, are shown in Figures 6 and 7, respectively. It is clear that the chaotic FO error system's peculiar attractions are fast stabilizing. In addition, the time history of the adaptive controller (37) is shown in Figure 8. It can be seen that the control input (37) is moving

closer and closer to equilibrium without exhibiting any signs of the chattering phenomenon. This indicates that the adaptive controller that was developed is capable of synchronizing the 3-dimensional unknown Hopfield delayed FONNSs ((55) and (56)) in an efficient manner. In addition, as can be seen in Figure 3 that, when the signals of the control law go close to the borders of the saturation state, the saturation condition causes them to be suppressed, which in turn causes the jumping phenomenon to take place. As a direct consequence of this, jumping states and switching states may be implemented with relative ease, in particular in situations where relays and indicated saturation conditions are used.



Figure 6. The evolution of the synchronization of the Hopfield delayed FONNSs ((55) and (56)).



Figure 7. The time evolution of the synchronization error of the Hopfield delayed FONNSs ((55) and (56)).

Furthermore, the temporal response of the SS (24), applied to synchronize the driveresponse Hopfield delayed FONNSs ((55) and (56)), is shown in both the function plot and the surface plot, shown in Figures 9 and 10, respectively. Figure 9 makes it abundantly clear that each parameter of the sliding surface (24) is getting closer and closer to the origin, and there are no indications that the chattering phenomenon is present in the sliding surfaces. In addition, the use of this approach results in a surface that is stable, as seen in Figure 10.



Figure 8. The time evolution of the control inputs (37) for the synchronized Hopfield delayed FONNSs ((55) and (56)).



Figure 9. The time evolution of the SS (27) to synchronize Hopfield delayed FONNSs ((55) and (56)).



Figure 10. The time evolution of the surface plot depicting the SS (24) implementation for achieving synchronization of the delayed FONNSs ((55) and (56)).

Now, to draw a comparison to the adaptive SMC method, we also employ another adaptive sliding mode controller, as outlined in Reference [48], for the synchronization of the FO Hopfield neural network described by Equations (55) and (56) with $\kappa = 0.99$. It is worth noting that Reference [48] deals with adaptive synchronization for a specific category of uncertain delayed fractional-order Hopfield neural networks in the presence of external disturbances. Here, we adopt the control methodology from [48] in the following manner:

$$s_i(t) = \int \left(\mathbf{D}^{\kappa} e_i(t) + p_i e_i(t) + q_i \operatorname{sign}(e_i(t)) \right) dt,$$
(58)

where p_i and q_i are positive numbers. Also, for i = 1, 2, 3:

$$u_{i}(t) = -\left(\hat{-a_{i}(t)} + p_{i}\right)e_{i}(t) - \hat{d_{i}(t)} - |s_{i}(t)| \left(\sum_{j=1}^{3} |M_{ij}|L_{j}^{f}|e_{j}(t)| + \sum_{j=1}^{3} |P_{ij}|L_{j}^{g}|e_{j}(t-\tau)|\right) - q_{i} sign(e_{i}(t)) - \varsigma_{i}^{a}s_{i}(t) - \varsigma_{i}^{b} sign(s_{i}(t)),$$
(59)

$$\hat{a}_i = -\eta_i^a s_i(t) e_i(t) \tag{60}$$

$$\hat{d}_i = \eta_i^d s_i(t), \tag{61}$$

where L_i^j , L_i^g , ζ_i^a , ζ_i^b , η_i^a and η_i^b are positive constants as control parameters.

The controller parameters are chosen as $L_1^f = L_2^f = 2.2$, $L_3^f = 2, L_1^g = L_2^g = L_3^g = 2.3$, $\zeta_1^a = \zeta_2^a = \zeta_3^a = 1.9$, $\zeta_1^b = 2.5$, $\zeta_2^b = \zeta_3^b = 3$, $\eta_1^a = \eta_2^a = \eta_3^a = 1.8$, and $\eta_1^b = 2$, $\eta_2^b = \eta_3^b = 2.5$. Moreover, for i = 1, 2, 3, $p_i = 0.9$ and $q_i = 1.1$.

Figure 11 illustrates the trajectories of controlled error states for the Hopfield delayed FONNSs described by equations (55) and (56). These systems are controlled using the proposed adaptive SMC method (37) and the SMC method (59) presented in [48]. While both methods manage to guide the error states to the origin, it is evident that the suggested adaptive SMC exhibits superior convergence compared to the SMC method (59). A detailed analysis of this comparison is consolidated in Table 1.



Figure 11. Comparison of state trajectories of the error of the FO systems ((55) and (56)), controlled with suggested adaptive SMC and SMC method in [48].

Aspects of Comparison	The Outcomes of This Research	The Outcomes of Ref. [48]
Control Approach	Dynamic-free adaptive SMC	Adaptive SMC
Controller Configuration Parameters	In total, the selection of 2n + 5 parameters is necessary.	In total, the selection of 8n parameters is necessary
System Details.	The dynamic-free adaptive SMC method does not require dynamic terms of the systems; only the states are sufficient.	The Adaptive SMC requires complete access to dynamic terms from both the drive and response systems.
Amplitude of Oscillations	Standard Range (determined by the behavior of the error system)	Beyond Range (determined by the behavior of the error system)
Conclusions	 The benefits of the suggested dynamic-free adaptive SMC are as follows: (1) Enhanced robustness; (2) Simplified controller design for practical feasibility; (3) Absence of chattering; (4) Heightened convergence precision. 	The advantages of the adaptive SMC method include: (1) A potential challenge with numerous parameters that can be complex to manage; (2) Effective operation when the system states are known; (3) Absence of chattering;

Table 1. A Comparative Analysis of the Outcomes Achieved with AMF (21) and SMC (37).

Remark 3. In Figures 4 and 8, we delve into the concept of sliding surfaces, illustrating the convergence of sliding surface states to the origin. This illustrative model is widely employed across the relevant literature. However, it is important to note that obtaining an exact depiction of the stable surfaces proves challenging due to the nature of Figures 4 and 8, which present line views of sliding surfaces (24) in Scenarios 1 and 2. To address this limitation, we have included Figures 5 and 10, which offer a surface plotting perspective to visually demonstrate the stability of sliding surface (24) in Scenarios 1 and 2. These supplementary figures provide a more comprehensive understanding of the stability concept.

Remark 4. The dynamic-free adaptive sliding mode control method, rooted in the principles of the frequency distributed model (FDM) theorem, the Lyapunov stability theorem, and norm-bounded control, presents a compelling approach for addressing the synchronization of non-identical systems, all while remaining free from explicit system dynamics. In contrast to traditional methods that often rely on explicit knowledge of system dynamics, the dynamic-free nature of this approach stands out. By capitalizing on the FDM theorem, the method estimates and counteracts disturbances without necessitating in-depth knowledge of the complex underlying dynamics of the systems. This is especially advantageous when dealing with non-identical systems, as such complexities can vary significantly. Furthermore, the inclusion of the Lyapunov stability theorem guarantees the method's convergence and stability, even in the context of non-identical systems. The controller's adaptability is further augmented by its adaptive nature, enabling it to automatically adjust control actions based on observed differences between the systems. This adaptability addresses the challenge of synchronizing non-identical systems by ensuring that the control strategy accommodates variations. The norm-bounded control aspect maintains control signals within predefined bounds, resulting in a smoother and more predictable response, which is particularly crucial when dealing with diverse system dynamics. In conclusion, this dynamic-free adaptive sliding mode control method offers a novel and potent solution for synchronizing non-identical systems. By focusing on disturbance estimation, adaptability, and stability analysis, the method overcomes the limitations of explicit system dynamics. This distinctive feature, coupled with its adaptability, positions the method as a strong contender for real-world scenarios involving non-identical systems.

Remark 5. In practical applications, particularly when dealing with complex fractional-order (FO) systems that defy accurate modeling and are plagued by inherent uncertainties, this model-free controller holds substantial promise. Furthermore, its implementation can be seamlessly achieved using readily available digital devices such as the FPGA (Field-Programmable Gate Array) or DSP (Digital Signal Processing), requiring only knowledge of the system's current state.

Remark 6. Research into the proposed dynamic-free adaptive SMC approach for synchronizing delayed fractional-order nonlinear chaotic systems (FONNS) is an evolving area with notable achievements. However, it is essential to acknowledge the existing limitations, with the anticipation of future improvements. These limitations encompass (1) constraints on the differentiation order, typically limited to the range of 0 to 1; (2) the intricate nature of analyzing and computing models for delayed systems and control methodologies, which can be challenging; (3) the reliance on trial-and-error methods for selecting optimal controller settings.

Addressing these restrictions is pivotal for advancing the efficacy and versatility of the dynamic-free adaptive SMC approach in synchronizing chaotic systems.

5. Discussion and Conclusions

This work presents a novel dynamic-free adaptive sliding mode control (adaptive SMC) methodology for achieving synchronization in a specific class of chaotic delayed fractional-order neural network systems with input saturation. By incorporating the FDM and the FO version of the Lyapunov stability theory, the proposed adaptive SMC method effectively overcomes the inherent chaotic behavior exhibited by the delayed FONNSs and ensures synchronization. One key advantage of the approach is the decoupling of control inputs from the nonlinear-linear dynamical terms of the system, leveraging the norm-boundedness property of states in chaotic systems. Through numerical simulations, the effectiveness of the adaptive SMC method has been demonstrated to achieve chaos synchronization in delayed fractional-order Hopfield neural network systems, showcasing its robustness and efficiency. The integration of the FDM and FO Lyapunov stability theorem offers a promising solution for synchronizing chaotic unknown Hopfield delayed FONNSs with input saturation. This innovative approach holds potential applications in diverse domains that require the synchronization of such systems. Therefore, the proposed dynamic-free adaptive SMC method represents a significant contribution to the field of chaotic systems control, providing a reliable and efficient means to achieve synchronization in complex neural network systems with time delays and fractional-order dynamics, even in the presence of input saturation. The findings open up new possibilities for research and applications in various areas where the stable synchronization of chaotic systems is of paramount importance.

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