



# Article A Threshold Line for Safe Geologic CO<sub>2</sub> Storage Based on Field Measurement of Soil CO<sub>2</sub> Flux

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Abstract: Carbon capture and storage (CCS) is an established and verified technology that can implement zero emissions on a large enough scale to limit temperature rise to below 2 °C, as stipulated in the Paris Agreement. However, leakage from CCS sites must be monitored to ensure containment performance. Surface monitoring of carbon dioxide (CO<sub>2</sub>) concentrations at onshore CCS sites is one method to locate and quantify CCS site leakage. Employing soil accumulation chambers, we have established baseline data for the natural flux of CO<sub>2</sub> as a threshold alert to detect CO<sub>2</sub> leakage flux to ensure the safety of onshore CCS sites. Within this context, we conducted on-site CO<sub>2</sub> measurements at three different locations (A, B, and C) on the INAS test field at the Ito campus, Kyushu University (Japan). Furthermore, we developed a specific measurement system based on the closed-chamber method to continuously measure CO<sub>2</sub> flux from soil and to investigate the correlation between CO<sub>2</sub> flux from the soil surface and various parameters, including environmental factors and soil sample characteristics. In addition, gas permeability and the effect of different locations on soil CO<sub>2</sub> flux are discussed in this study. Finally, we present an equation for estimating the soil CO<sub>2</sub> flux used in the INAS field site that includes environmental factors and soil characteristics. This equation assists in defining the threshold line for an alert condition related to CO<sub>2</sub> leakage at onshore CCS sites.

**Keywords:** soil  $CO_2$  flux; geologic  $CO_2$  storage; threshold line; field measurement; safety;  $CO_2$  leakage

# 1. Introduction

Carbon dioxide (CO<sub>2</sub>) emissions to the atmosphere have gradually increased, causing a global warming phenomenon over the past one to two centuries. According to the Intergovernmental Panel on Climate Change (IPCC), global CO<sub>2</sub> emissions are currently rising at approximately  $42 \pm 3$  Pg C per year [1]. Consequently, surface temperatures will be 2 °C higher than in the pre-industrial era (before 1876) in the next coming decades. Currently, a number of different approaches are being considered to mitigate CO<sub>2</sub> emissions [2], as set out in the Paris Agreement and include the following:

- 1. Improve energy efficiency and promote energy conservation.
- 2. Increase usage of low-carbon fuels, including natural gas, hydrogen, or nuclear power.
- 3. Utilize renewable energy such as solar, wind, hydropower, and bioenergy.
- 4. Apply geoengineering approaches, for example afforestation and reforestation.
- 5.  $CO_2$  capture and storage (CCS) or  $CO_2$  capture, usage, and storage (CCUS).

Of these methods, CCS can potentially achieve zero emissions on a large enough scale to decrease the forecast temperature rise to less than 2 °C. In 2019, the number of large-scale CCS facilities increased to 65, including 26 operational, three under construction, two



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**Copyright:** © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). have been suspended, 13 in advanced development, and 21 in early development [3]. The global capture and storage capacity of projects currently in operation or under construction equates to approximately 40 million tons per annum.

However, for reasons concerning health, safety, and the surrounding environment, geological  $CO_2$  storage sites need to monitor all types of  $CO_2$  leakage into the atmosphere. Monitoring methods include seismic monitoring, geo-electrical methods, temperature logs, gravity methods, remote sensing, geochemical sampling, atmospheric monitoring, tracers, soil gas, and microbiology. Of these, atmospheric monitoring methods play an important role in the detection of environmental abnormalities. In particular, the monitoring of subsurface  $CO_2$  leakage from natural fractures or tectonic faults is essential. Leakage monitoring can be conducted by continuously measuring soil  $CO_2$  flux from the soil surface to identify possible leakage sources [4–11].

A number of studies have concluded that soil, as a carbon source, can store approximately 2300 Pg C in the upper 100 cm of soil [12]. The amount of CO<sub>2</sub> flux emitted from soil to the atmosphere ranges from 280 Pg C per year [13] to 359 Pg C per year [14], which is approximately one-quarter of the total emissions in the carbon cycle. Principally, CO<sub>2</sub> gas in the soil is produced by respiration of plant roots, decomposition of soil organic matter (*SOM*), and microbial activities [15]. As the CO<sub>2</sub> concentration in the soil layer increases, a higher rate of diffusion into the atmosphere occurs at the soil surface due to the concentration gradient effect.

The emission of  $CO_2$  from the soil surface is a complicated process affected by many factors. Among these, environmental elements such as soil temperature, soil water content (moisture), and *SOM* content are the primary factors that have been investigated by several researchers [13,16–20]. A number of studies have shown that soil  $CO_2$  flux depends on soil temperature, moisture content, and oxygen concentration [21–23]. Furthermore, soil characteristics such as porosity and water saturation have also been shown to be important, because they affect the transport of gas in the soil. Although numerous studies have been conducted within this field, the flux of  $CO_2$  from soils is still not well understood due to complicated environmental and soil-related factors.

In this study, we developed an equation to estimate the threshold line to find a possibility of  $CO_2$  leakage at onshore geological  $CO_2$  storage sites. The established baseline play an essential role as a threshold alert to ensure the safety of onshore CCS sites. Once abnormal  $CO_2$  flux from soil surface is detected, it is necessary to take action immediately. In addition, the effect of various environmental factors and soil characteristics on soil  $CO_2$  flux was also investigated at the INAS test field site located on the Ito campus, Kyushu University.

## 2. Methods and Study Area

# 2.1. Study Area

Site investigations for this study were conducted at the INAS test field site (Figure 1), located on the west side of Ito campus, Kyushu University (Japan) at latitude  $33^{\circ}35'$  N and longitude  $130^{\circ}12'$  E. The test field has previously been used for various environmental studies. Based on data obtained from the official website of the Japan Meteorological Agency (JMA), the average temperature in 2017 was 17.6 °C, with minimum and maximum monthly average temperatures of 7.4 °C in January and 29.5 °C in August, respectively. A maximum precipitation of 289.5 mm was recorded in October, with a minimum of 23.5 mm recorded in November.



**Figure 1.** Map of the INAS test field study area with three different measuring locations, A, B, and C, located at Ito campus, Kyushu University, Japan. Because specific soil characteristics could influence results, the following three locations within the INAS test field were selected for our study: Location A: covered with leaf litter and several clusters of living grasses. Location B: soft soil surface covered with living grasses. Location C: hard soil with many pebbles and no grass or leaf litter.

## 2.2. Soil CO<sub>2</sub> Flux

To accurately measure soil CO<sub>2</sub> flux, the authors developed a soil CO<sub>2</sub> flux measuring system based on the closed-chamber method that includes a measuring chamber and controlling system. An airtight chamber, 0.20 m in diameter and 0.35 m in height, was used to trap emitted gas from the soil (Figure 2). In addition, a CO<sub>2</sub> gas sensor (GMP-343, VAISALA Inc., Helsinki, Finland) was used to measure CO<sub>2</sub> concentrations and calibrated using  $\pm 0.5\%$  accurate gases at 0, 200, 370, 600, 1000, 4000 ppm, and 2%. While a high butterfly valve with an automated close-open regime was located inside the chamber at 0.26 m from the soil surface, a circulated fan located at the top of the chamber was used to replace the air in the chamber with atmospheric air. Thermocouples (T-type, CHINO Inc., Tokyo, Japan) with a range from 0 to 200 °C and  $\pm 1.0$  °C or  $\pm 0.75\%$  in accuracy were set up to measure the temperature at different depths. Moisture sensors (EC-5, METTER Inc., Pullman, WA, USA) with a range from 0 to 100% were then inserted into the subsurface at a depth of 5 to 10 cm near the measuring chamber. A controlling system (Logger 308, CYBER MELON, Hyogo, Japan) was used to control and record signals from these sensors.



**Figure 2.** System for measuring soil CO<sub>2</sub> flux using a closed-chamber method including (**a**) schematic diagram of the system and (**b**) operational stages using a butterfly valve in the measurement cycle.

The following procedure was used to measure soil CO<sub>2</sub> flux:

- All measuring apparatuses and related devices were carefully prepared to ensure that they were in good working order. A power supply was set up to allow continuous measurements to be taken, while a vinyl sheet was used to cover and protect all measuring apparatuses and devices from rain. In addition, all measuring locations were cleaned and leveled to ensure measurement stability.
- The chamber was inserted vertically at the selected area to a depth of 1.5 cm to minimize interference from the surrounding atmosphere. In addition, the installation of the chamber was completed 1 to 2 h before measurements were taken to ensure precise and accurate results.

- The CO<sub>2</sub> sensor, fan, butterfly valve, thermocouples, and moisture sensors were connected to the controlling system, with one end of the thermocouple and moisture sensors inserted into the soil at a depth of 7 cm.
- The power source was connected to the controlling system with adapters, and all switches were turned on.
- The butterfly valve was opened fully, the fan was turned on for approximately one min for gas circulation, and CO<sub>2</sub> concentrations were stabilized to atmospheric levels (400–500 ppm). Next, the butterfly valve was gradually closed until completely shut. Finally, the CO<sub>2</sub> concentration inside the chamber was measured for 10 min, together with other parameters such as soil temperature and moisture content.
- Soil CO<sub>2</sub> flux was calculated using the following equation [24]:

$$J = \frac{V}{A} \cdot \frac{\partial C}{\partial t} \cdot \frac{1}{22.4 \times 10^{-3}}$$
(1)

where J (µmol·m<sup>-2</sup>·s<sup>-1</sup>) represents the soil CO<sub>2</sub> flux emitted from the soil surface,  $\frac{\partial C}{\partial t}$  (ppm·s<sup>-1</sup>) is the time gradient of CO<sub>2</sub> concentration in the chamber, V (m<sup>3</sup>) is the volume of the chamber, A (m<sup>2</sup>) is the soil area covered by the chamber, and 22.4 × 10<sup>-3</sup> (m<sup>3</sup>/mol) is the molar volume of an ideal gas at standard temperature and pressure.

The total time for a measuring cycle was 16 min, which included ten minutes for measuring, one minute for air circulation, and five minutes for opening and closing the butterfly valve. All data, including  $CO_2$  concentrations and soil temperature, were recorded every four seconds. In contrast, the time gradient of the  $CO_2$  concentration was recorded and calculated every 16 min using a data logger (Serial Ghost DB9, KEELOG, Minami, FL, USA).

#### 2.3. Measurement of Soil Moisture

In this study, soil moisture was measured with soil moisture sensors using capacitance/frequency domain technology. Principally, soil capacitance is measured by the sensor output with a range from 0 to 2500 mV, equivalent to a moisture content of 0 and 100%, respectively. Therefore, soil moisture is calculated from the correlation between output voltage and measured soil moisture. As soil moisture–capacitance is correlated to soil type, the soil moisture output must be calibrated using the sampled soil. Several soil samples were taken from locations A, B, and C at the INAS test field to verify the correlation between the output voltage from soil moisture sensors and moisture measurements in the laboratory. Using this correlation, an appropriate amount of water was added to the dried soil in the laboratory to prepare mixed soil samples with different moisture contents. Soil samples were then packed into plastic containers that matched the original volume in the field. Two soil moisture sensors were inserted into the soil samples, and sensor outputs, water saturation, volumetric water content, and gravimetric water content of soils were recorded for varying moisture contents.

Water saturation can be described as the volume of water per unit of pore volume using the following equation:

$$S_w = \frac{V_w}{V_{pore}} \cdot 100 \tag{2}$$

where  $S_w$  (%) represents water saturation,  $V_w$  (cm<sup>3</sup>) is the volume of water, and  $V_{pore}$  (cm<sup>3</sup>) is the volume of the pores in the soil. Soil water content includes gravimetric and volumetric soil water measured as mass or volume [25]. Gravimetric soil water content is the mass of water in the soil, measured as the difference between moist soil and the soil dried at 105 °C, or oven-dry weight. Notably, gravimetric soil water content is expressed per unit mass of oven-dried soil using the following equation:

$$GWC = \frac{m_1 - m_2}{m_2} \cdot 100$$
(3)

where *GWC* (%) is the gravimetric soil water content,  $m_1$  (g) is the mass of moist soil, and  $m_2$  (g) is the mass of the oven-dried soil. Measurements of soil gravimetric water content are considered destructive (oven-drying) and therefore, the soil sample was not used for further chemical analysis.

Volumetric soil water content is the volume of water per unit volume of soil expressed by the following equation:

$$VWC = \frac{V_w}{V_s} \cdot 100 \tag{4}$$

where *VWC* (%) is the volumetric soil water content,  $V_w$  (cm<sup>3</sup>) is the volume of water, and  $V_s$  (cm<sup>3</sup>) is the volume of soil.

Soil moisture data were calculated using Equations (2) to (4) together with output data from the sensors at each water weight level to investigate the correlation between output voltage and analyzed soil moisture for samples from locations A, B, and C (Figures 3–5).



Figure 3. Calibrated results of water saturation at three locations (A, B, and C) using two sensors.



**Figure 4.** Calibrated results of volumetric water content at three locations (A, B, and C) using two sensors.



**Figure 5.** Calibrated results of gravimetric water content at three locations (A, B, and C) using two sensors.

As shown in Figures 3–5, the correlation coefficient ( $\mathbb{R}^2$ ) between sensor output and water content was over 0.94 across all samples. Therefore, it is possible to use moisture sensor output data to calculate soil moisture using correlation equations. In this study, *VWC* represents soil moisture in all calculations and discussions and was calculated using the following equations:

Samples at Location A : 
$$y = 0.173 \cdot x - 57.36$$
 (5)

Samples at Location B : 
$$y = 0.174 \cdot x - 57.03$$
 (6)

Samples at Location C : 
$$y = 0.156 \cdot x - 51.28$$
 (7)

where y (%) represents the volumetric soil water content and x (mV) represents the sensor output data.

## 2.4. Measurement of Soil Organic Matter (SOM)

Soil organic matter (*SOM*) and soil moisture were analyzed in the laboratory using 1 g soil samples taken from a 2.5 cm subsurface soil layer at the INAS testing field locations. First, the weight of moisture ( $W_W$ ) was derived by subtracting the weight of the soil sample after placing it in a drying oven at 105 °C for 1 h from the weight of the initial soil sample. Next, to determine the weight of ash ( $W_C$ ), soil samples were placed in an electric furnace at 500 °C for 1 h. Then, the temperature was increased to 800 °C for 45 min and cooled down for 3 h in a vacuum canister. Subsequently,  $W_C$  was calculated by determining the difference between the sample weights before and after heating. Finally, the weight of *SOM* ( $W_O$ ) was derived by subtracting the weight of moisture and ash from the weight of the initial soil sample.

The amount of SOM rate was calculated using the following equation:

$$SOM = \frac{W_O}{W_S} \tag{8}$$

where  $W_O$  (g) refers to the weight of soil organic matter and  $W_S$  (g) is the weight of the soil sample.

The weight of SOM,  $W_O$  was calculated from the proximate analysis results of moisture and ash content in soil using the following equation:

$$W_O = W_S - W_W - W_C \tag{9}$$

where  $W_S$  (g) represents the weight of the soil sample,  $W_W$  (g) is the weight of moisture, and  $W_C$  (g) the weight of the ash.

## 2.5. Laboratory Measurement of Gas Permeability

The decrease in soil CO<sub>2</sub> flux from the soil surface after rainfall is primarily due to an increase in soil water saturation ( $S_w > 0.4$ ). This is due to a reduction in CO<sub>2</sub> gas diffusion as pores are filled by water. Therefore, in this study, the physical effect of soil water saturation was estimated from CO<sub>2</sub> gas permeability using packed soil (6.38 cm<sup>2</sup> cross-section, 21.8 cm length) from locations A and B (Figure 6). Gas permeability of soil can be correlated to the gas diffusion coefficient through soil porosity ( $\varepsilon$ ). Furthermore, based on the Kozeny-Carman equation [26], permeability *k* (mD) is expressed by a function of  $\varepsilon^n/(1 - \varepsilon)^2$ , where n = 3-4, while the gas diffusion coefficient D (m<sup>2</sup>/s) is approximately proportional to  $\varepsilon$ . Therefore, although both increase with an increase in  $\varepsilon$ , *k* is more sensitive to  $\varepsilon$  than *D*. In the laboratory-based investigations, permeability was calculated using pressure drop and CO<sub>2</sub> gas flow rate through soil packed in acrylic pipes using Darcy's equation [27].



**Figure 6.** Soil packed into an acrylic pipe for measurement of gas permeability (6.38 cm<sup>2</sup> cross-section, 21.8 cm length).

Results regarding gas permeability of soils are shown in Figure 7. As water saturation increases, CO<sub>2</sub> gas permeability decreases because of the declining porosity. The clear correlation between gas permeability and water saturation indicates that CO<sub>2</sub> diffusion is constrained by increasing water content in soil. Consequently, soil CO<sub>2</sub> flux decreased with increasing soil moisture, due to the physical effect of moisture on soil. However, in lower soil moisture ranges ( $S_w \leq 0.3$ ), the soil gas flux may be affected differently owing to enhanced biological activity in the soil. We will discuss in detail the effect in Section 3.2. In summary, our results indicate the permeability of soil at Location A to be lower than that at Location B.



**Figure 7.** Carbon dioxide (CO<sub>2</sub>) gas permeability versus water saturation ( $S_w$ ) at Locations A and B.

# 3. Results and Discussion

## 3.1. Soil Temperature at Different Depths

Soil temperature is one of the most significant parameters related to soil  $CO_2$  flux. To determine the appropriate depth at which to measure soil temperature, temperature measurements were taken on the surface and at 5, 7, and 10 cm depths. Temperature readings were carried out simultaneously with soil  $CO_2$  flux measurements.

Our results indicate that soil temperature on the surface and at a depth of 5 cm had a wide range of fluctuation, while temperatures at a depth of 7 cm were more stable and consistent and showed the highest correlation coefficient with soil  $CO_2$  flux (Figure 8). Hence, our results and discussion, we primarily focus on temperature data recorded at a depth of 7 cm.



Figure 8. Soil temperature on the surface and at three different depths, recorded at Location A (Dec 21, 2016 to Jan 2, 2017).

#### 3.2. Effect of Environmental Factors on Soil CO<sub>2</sub> Flux

Results from our study indicate a general trend of an increase in soil temperature leading to an increase in soil  $CO_2$  flux (Figure 9). Notably, a similar tendency was observed with the vertical fluctuation of soil temperature and soil  $CO_2$  flux, indicating a specific correlation between soil temperature and soil  $CO_2$  flux. Furthermore, as soil temperature fluctuated ahead of the soil  $CO_2$  flux in both increasing and decreasing soil temperature trends, we conclude that  $CO_2$  flux from soils was affected by the respiration of plant roots and soil microorganisms. As described by Pavelka [28],  $CO_2$  molecules produced by respiration diffuse to the soil surface and are then released into the atmosphere. Therefore, soil temperature is a significant environmental factor that affects  $CO_2$  flux from soils.

Together with the correlation between soil  $CO_2$  flux and soil temperature, we also investigated the effect of precipitation on  $CO_2$  flux. (Figure 10). Precipitation was recorded from Dec 14, 2016 (0:00 a.m.) to Dec 15, 2016 (0:00 a.m.), with no rain recorded from Dec 17, 2016 (0:00 a.m.) to Dec 19, 2016 (9:00 a.m.). Our results indicate a high correlation between  $CO_2$  flux from soil and soil temperature when precipitation was near zero (from Dec 17, 2016 (9:00 a.m.) to Dec 19, 2016 (9:00 a.m.)). On the other hand, during rainfall periods (from Dec 14, 2016 (0:00 a.m.) to Dec 15, 2016 (0:00 a.m.)), the correlation with soil temperature was unclear. We suggest that under saturated conditions, soil CO<sub>2</sub> is partly dissolved by water and stored in the soil pores rather than being emitted to the surface. The amount of soil CO<sub>2</sub> flux over rainy days (Dec 14–15) was substantially lower than that over dry days (Dec 17–19) by an average of 0.15  $\mu$ mol·m<sup>-2</sup>·s<sup>-1</sup>. Therefore, we can conclude that precipitation caused a reduction in CO<sub>2</sub> flux from soil.



**Figure 9.** Variation trend of soil flux and soil temperature at a depth of 7 cm, as recorded at Location A (Dec 30, 2016 to Dec 31, 2016).



**Figure 10.** Correlation between CO<sub>2</sub> flux from soils and soil temperature together with rainfall data recorded at Location A (Dec 14, 2016 to Dec 20, 2016).

Furthermore, soil  $CO_2$  flux levels declined not only on rainy days, but also for several days thereafter. We suggest that this occurred because soil pores were filled with water, leading to a lowering of gas diffusivity. Consequently,  $CO_2$  gas does could not diffuse into the atmosphere due to the displacement of  $CO_2$ -rich soil by rainwater.

To investigate the relationship between  $CO_2$  flux from soils and soil temperature, we collected long-term monitoring data at Location A, from Dec 1, 2016 to Nov 23, 2017 (Figure 11). This figure demonstrates that soil  $CO_2$  flux (*J*) increased exponentially with a rise in soil temperature (*T*) at a range of 0 to 28 °C, with a peak of 8 µmol·m<sup>-2</sup>·s<sup>-1</sup> (3.8 g·m<sup>-2</sup>·day<sup>-1</sup>). However, when soil temperatures were above 28 °C, soil  $CO_2$  flux decreased, specifically by 75% at 35 °C. This phenomenon can be explained by a long period of high soil temperatures (above 28 °C) with no rain for approximately two weeks in August, which resulted in a decrease in the activities of  $CO_2$ -producing soil microbes. Davidson used the same method with us, he reported that the natural soil  $CO_2$  flux range from 1 to 30 g  $CO_2 \cdot m^{-2} \cdot day^{-1}$  at a depth of 1 to 100 m [29]. In our study, soil  $CO_2$  flux was up to 8 µmol·m<sup>-2</sup>·s<sup>-1</sup> or 3.8 g·m<sup>-2</sup>·day<sup>-1</sup> at a depth of 7 cm.



**Figure 11.** Long-term monitoring of soil CO<sub>2</sub> flux and soil temperature at Location A (Dec 1, 2016 to Nov 23, 2017).

Our results are consistent with those of Allison [30] that indicate that a warming soil could reduce carbon-use efficiency and reduce carbon decomposition by microbes, thereby limiting the production of  $CO_2$ . Furthermore, Tang [19] indicates root and microorganism activity to be typically low under dry conditions, resulting in a low soil  $CO_2$  flux.

As a result, soil  $CO_2$  flux increased with soil moisture at a soil moisture range of 0 to 30%, but substantially decreased at soil moisture levels of above 30% (Figure 12). This, again, highlights the reduction in  $CO_2$  flux from soils at high moisture levels due to soil pores filling with water and consequently, lowering gas diffusivity from the soil to the atmosphere. Although an increase in soil moisture generally increases bio-activity in the soil, under very high soil moisture conditions, total soil  $CO_2$  flux is reduced due to the limited diffusion of oxygen and subsequent reduction in  $CO_2$  emissions [20].



**Figure 12.** Soil CO<sub>2</sub> flux (*J*) and soil temperature (*T*) across various soil moisture levels, recorded at Location A (Dec 5, 2016 to Oct 9, 2017).

Results from soil CO<sub>2</sub> flux data across various water saturation levels at Location A show the reduction in soil CO<sub>2</sub> flux not only during rain hours, but also for a specific postrain period (Figure 10). This indicates that CO<sub>2</sub> flux was directly affected by precipitation. More specifically, precipitation firstly increased the water saturation in soil porosity and secondly, increased the soil moisture content. Furthermore, our results indicate that the CO<sub>2</sub> flux reached a peak at  $S_w = 0.4$  (Figure 13). Several studies have presented a similar quadratic correlation between soil CO<sub>2</sub> flux and soil water content, with soil CO<sub>2</sub> flux reaching a peak at a certain soil water level [24,31].



**Figure 13.** Correlation between CO<sub>2</sub> flux from soil (*J*) and water saturation ( $S_w$ ), recorded at Location A (Jul 31, 2017 to Oct 9, 2017).

Under conditions where  $S_w > 0.4$ , the exchange of CO<sub>2</sub> and oxygen molecules via gaseous diffusion is reduced due to reduced porosity in the soil [32]. In addition, the diffusion of CO<sub>2</sub> in the soil matrix is limited due to pores being filled with water [33].

The correlation between soil  $CO_2$  flux and water saturation is expressed in Equation (10).

$$J(S_w, T)/J_{\text{max}} = -3.09S_w^2 + 2.77S_w + 0.37$$
(10)

However, under low water saturation levels ( $S_w < 0.4$ ), CO<sub>2</sub> gas generated by decomposing carbon from roots and plants is accelerated by moisture under sufficient oxygen molecules diffused from the surface. Overall, it can be concluded that when  $S_w = 0.4$ , soil CO<sub>2</sub> flux (*J*) reaches a peak by satisfying oxygen diffusion and enhancing carbon decomposition by microorganisms in the soil. Therefore, both extreme dry and wet conditions result in reduced CO<sub>2</sub> gas flux from the soil to the surface.

#### 3.3. Soil CO<sub>2</sub> Flux at Different Locations

To investigate the influence of different soil characteristics and environmental factors on soil  $CO_2$  flux, we compared data collected from three study locations, namely Location A (Dec 1, 2016 to Nov 26, 2017), B (Nov 1 to Dec 19, 2018), and C (Oct 25 to Nov 1, 2018).

Data on the relationship between soil  $CO_2$  flux and soil temperature at the three study locations indicate that the soil  $CO_2$  flux at Location A increased exponentially with increasing soil temperature (Figure 14). A similar trend was also recorded at Location B with a substantially higher amount of soil  $CO_2$  flux than at Location A. On the contrary, only a minimal amount of the soil  $CO_2$  flux was recorded at Location C.



**Figure 14.** Comparison of the relationship between CO<sub>2</sub> flux from soil (*J*) and soil temperature (*T*) at Location A (Dec 1, 2016 to Nov 26, 2017), B (Nov 1, to Dec 9, 2018), and C (Oct 25, to Nov, 2018).

Based on the results from Figure 14, the following three equations were obtained:

For Location A : 
$$J_{Max} = 0.487 e^{0.099T}$$
 (11)

For Location B:  $J_{Max} = 1.76e^{0.099T}$  (12)

For Location C :  $J_{Max} = 0.128e^{0.099T}$  (13)

where  $J_{Max}$  (µmol·m<sup>-2</sup>·s<sup>-1</sup>) is the soil CO<sub>2</sub> flux from the soil surface, and *T* (°C) represents soil temperature.

To investigate the difference in soil  $CO_2$  flux between the three study area locations, porosity and *SOM* were examined as characteristics related to soil  $CO_2$  flux (Figure 15). Our results indicate that Location B, covered with living grasses, had the highest *SOM* value of 0.173, while a *SOM* of 0.082 was measured at Location A, and the lowest *SOM* value of 0.036 was measured at Location C, which was covered with pebbles.



Figure 15. Soil organic matter (SOM) and porosity at three study locations (A, B, and C).

Furthermore, the larger the *SOM*, the larger the fluctuation range of soil CO<sub>2</sub> flux at the same soil temperature. For example, at a temperature of 16 °C, the soil CO<sub>2</sub> flux ranged from 0.910 to 2.583  $\mu$ mol·m<sup>-2</sup>·s<sup>-1</sup> and from 3.833 to 6.695  $\mu$ mol·m<sup>-2</sup>·s<sup>-1</sup> at Locations A and B, respectively, while less than 0.311  $\mu$ mol·m<sup>-2</sup>·s<sup>-1</sup> at Location C (Figure 14). Overall, soil CO<sub>2</sub> flux was significantly affected by the *SOM* of each soil location and the presence of plant roots and microorganisms.

Soil CO<sub>2</sub> flux measurements at 0 °C ( $C_J$ ) across different *SOM* values indicate that soil CO<sub>2</sub> flux increased exponentially with an increase in *SOM* (Figure 16). For example, the soil CO<sub>2</sub> flux was 0.128 µmol·m<sup>-2</sup>·s<sup>-1</sup> at a *SOM* of 0.036 at Location C, but showed an approximately four-fold increase at Location A and an almost fourteen-fold increase at Location B with values of 0.082 and 0.173, respectively. Overall, the larger the amount of *SOM* in the soil, the larger the soil CO<sub>2</sub> flux.



**Figure 16.** Correlation between C<sub>I</sub> and soil organic matter (*SOM*) at locations A, B, and C.

The correlation between soil  $CO_2$  flux and related factors can be expressed by the following equation:

$$T_{Max} = C_I \cdot C_s \cdot e^{\beta I} \tag{14}$$

where  $C_I$  is correlation coefficient related to *SOM*,  $C_s$  is the correlation coefficient related to water saturation, *T* represents soil temperature,  $\beta$  is the attenuation of soil CO<sub>2</sub> flux, and  $\beta$  = 0.099 for all measuring locations.

The relationship between  $C_I$  and *SOM* can be demonstrated by Equation (15).

$$C_I = 46.27SOM^2 + 2.13SOM \tag{15}$$

while the relationship between  $C_s$  and  $S_w$  is expressed in Equation (16).

1

$$C_s = -3.09S_w^2 + 2.77S_w + 0.37 \tag{16}$$

Based on Equations (14)–(16), the following comprehensive equation was developed, which includes soil temperature, water saturation, and *SOM*:

$$J_{Max} = \left(46.27SOM^2 + 2.13SOM\right) \cdot \left(-3.09S_w^2 + 2.77S_w + 0.37\right) e^{0.099T}$$
(17)

This equation represents the maximum baseline for soil CO<sub>2</sub> flux ( $J_{Max}$ ), determined from the data collected at the INAS test field site (Figure 17). This data can be used to identify CO<sub>2</sub> gas leakages from CCS onshore sites. The threshold line represents the soil CO<sub>2</sub> flux across different soil temperatures under normal conditions for the INAS field site. Hence, a CO<sub>2</sub> flux value above the limit determined from the threshold line indicates that a CO<sub>2</sub> leakage has occurred through natural fractures or tectonic faults and wide-range monitoring should be implemented to localize leakage areas on the soil surface.



Figure 17. Plots of soil CO<sub>2</sub> flux measured at Locations A, B, and C.

#### 4. Conclusions

Our investigations and field measurements at the INAS test field, Kyushu University (Japan) have been carried out. To summarize our results, we highlight the following significant points:

The threshold line for geologic CO<sub>2</sub> storage site is estimated and expressed by the following equation:

$$J_{Max} = \left(46.27SOM^2 + 2.13SOM\right) \cdot \left(-3.09S_w^2 + 2.77S_w + 0.37\right) e^{0.0997}$$

Soil  $CO_2$  flux is tightly correlated to soil temperature, soil water, and *SOM*. Therefore, these parameters must be considered before setting out the alert condition at  $CO_2$ storage sites.

The threshold line can be used for the early detection of  $CO_2$  leakage from the  $CO_2$  storage sites based on the proposed equation for the INAS field. Once abnormal  $CO_2$  flux from soil surface is detected, it is necessary to take remedial action in the case that leakage occurs.

We suggest that future work focuses on the construction of a robust and reliable soil  $CO_2$  flux monitoring system using an independent power supply such as solar or wind energy. By using this system, soil  $CO_2$  flux can be monitored at all sites, regardless of local conditions.

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