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Sensor Fault-Tolerant Control Design for Mini Motion Package Electro-Hydraulic Actuator

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Abstract: With the rapid development of computer science and information and communication technology (ICT), increasingly intelligent, and complex systems have been applied to industries as well as human life. Fault-tolerant control (FTC) has, therefore, become one of the most important topics attracting attention from both engineers and researchers to maintain system performances when faults occur. The ultimate goal of this study was to develop a sensor fault-tolerant control (SFTC) to enhance the robust position tracking control of a class of electro-hydraulic actuators called mini motion packages (MMPs), which are widely used for applications requiring large force-displacement ratios. First, a mathematical model of the MMP system is presented, which is then applied in the position control process of the MMP system. Here, a well-known proportional, integrated and derivative (PID) control algorithm is employed to ensure the positional response to the reference position. Second, an unknown input observer (UIO) is designed to estimate the state vector and sensor faults using a linear matrix inequality (LMI) optimization algorithm. Then an SFTC is used to deal with sensor faults of the MMP system. The SFTC is formed of the fault detection and the fault compensation with the goal of determining the location, time of occurrence, and magnitude of the faults in the fault signal compensation process. Finally, numerical simulations were run to demonstrate the superior performance of the proposed approach compared to traditional tracking control.

Keywords: unknown input observer; fault-tolerant control; fault compensation

1. Introduction

In modern industries, valve-driven hydraulic actuators (VHAs) have been used extensively due to their advantageous features such as simplicity and high-precision control for linear as well as nonlinear systems [1–4]. However, these actuators have some limitations, including low energy efficiency due to leakage through the valve of the hydraulic pump, and throttle losses. Electric motor-pump-driven hydraulic actuators, tagged as electro-hydraulic actuators (EHAs), have been recently introduced as an alternative to provide high output power at great energy efficiency [5,6]. A representative configuration of an EHA is depicted in Figure 1. Here, the position of the hydraulic cylinder is adjusted directly by the bidirectional pump, with the support of two pilot-operated check valves and two pressure relief valves [5,6]. Because of their advantages, various types of EHAs have been commercialized and are widely used in different industrial applications, including active vibration isolation of machine tools [7] and wing control and landing gear control in aircraft [8–10]. Among these, a class of compact EHAs from Kayaba Industrial Company, known as mini motion packages (MMPs), is considered one of the most feasible solutions for applications requiring short operating ranges and high output power.

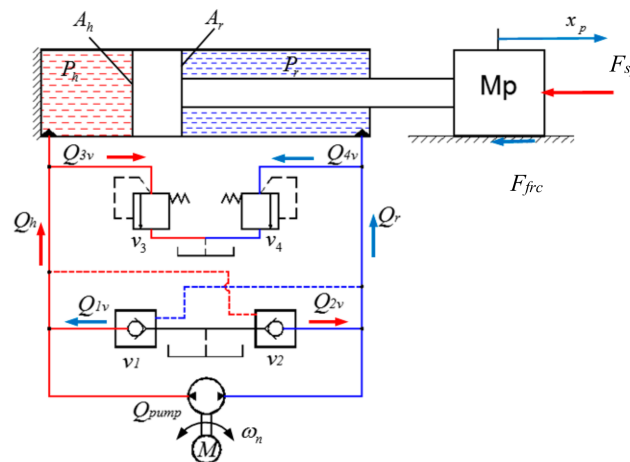


Figure 1. Schematic of an electro-hydraulic actuator (EHA) system.

However, when working in a disturbed environment, system nonlinearities with large uncertainties become critical challenges in utilizing EHAs to obtain high-precision positioning (or force) tracking control. The traditional linear control approaches derived for VHAs are therefore not suitable for this type of application due to the large control error [11], and the nonlinear schemes for EHA tracking control have attracted considerable attention from researchers and engineers to solve faults or failures of EHAs. Faults or failures arise from components of the EHA system such as failures in the electrical machine of the pump, the leakage faults of the pump and cylinder, aging and cable break faults of the sensor, and the others as polluted oil, etc. To address this issue, the fault-tolerant control (FTC) technique for EHAs was introduced. This technique handles the impacts of actuator faults (AFs) and sensor faults (SFs) [12–18], and sensor fault-tolerant control (SFTC) techniques are also used to solve the problems of SFs [19,20]. With the rapid development of mechatronics technology, increasingly intelligent and complex systems using the FTC technique have been applied to both industries and human life. Applications with EHAs also face new control challenges to maintain the system stability when a fault or failure occurs. In general, FTC is a complex combination of three major research fields, fault detection and isolation (FDI), robust control, and reconfigurable control. The FDI and the reconfigurable controller need to be robust against uncertainties and disturbances as in [21,22]. By using FTC techniques, the system still works as normal instead of stopping under the impacts of AFs and SFs [12–18]. Thus, the FTC plays a key role to improve the performance of systems prone to faults or failures. However, actuator failures cannot be handled [21]. In recent decades, various fault detection and diagnosis (FDD) and FTC techniques have been developed by researchers, such as the FDD schemes that use an extended Kalman filter (EKF) algorithm for isolating either the SF or the AF of the system [14,20,23]. In [23], the author applies FDI based on multiple hybrid Kalman filters to detect the fault process. Furthermore, the FTC technique in [14] utilizes Kalman filter reconfiguration, which helps ignore the feedback signal from the sensor when a sensor fault occurs. Especially in the FTC function [20], if a sensor fault appears, the feedback signal is formed from the estimation state of an unknown input observer (UIO). In contrast, this feedback signal will be the data transferred directly from the sensor. The systems described in these articles perform fault detection and isolation without removing the faults.

However, a recently developed FTC compensation technique removes the faults that come from the SFs or the AFs [19]. This technique has been successfully designed and applied in linear and nonlinear systems and is attracting several researchers. The two main tasks of this technology are to determine the estimated fault and to perform fault compensation. To obtain the estimated fault, some advanced observer methods are proposed, such as the sliding mode observer [15,24], the augmented observer [12,16–18,25–28], and sensor fault reconstruction [29,30]. In particular, a UIO of the system variable reconstruction has the benefits of not only estimating the state vector, but also the fault

estimation, as shown in [18,29,30]. The estimations of the state and the fault are implemented by the augmented observer, based on a UIO of the system variable reconstruction and an LMI optimization algorithm. This method has advantages in the AF estimation and the SF estimation are performed by an LMI optimization algorithm so that the UIO to be asymptotically stable [29]. However, in [18], decoupling the unknown input disturbance created difficulty in practical applications. Therefore, the SFTC technology developed in this paper is based on a combination of the error calculation method described in [18] and the UIO of the system variable reconstruction with the LMI optimization algorithm given in [31]. We can clearly see the effects of using FTC technique compared with traditional tracking control in [31,32].

In this paper, an advanced SFTC technology is proposed for robust position tracking control of an MMP system under fault conditions. The classic PID control algorithm is employed to enhance the system tracking performance. First, the mathematical model of the MMP system is developed to simplify the control process of the EHA system, which is different from the methods in [5,6]. Second, a UIO is built from robust, observer-based reconstruction for the linear and nonlinear discrete-time system with an unknown input disturbance and SF. Here, the state estimation and the fault estimation are applied to the UIO of the system variable reconstruction, which is different from the approaches in [28–30]. Lyapunov's stability condition and an LMI optimization algorithm are utilized for the asymptotical stability of the proposed state observer. Then an SFTC compensation technique is designed for the MMP system. According to this technique, the magnitude of the compensation signals is received from the fault estimation process of the UIO. The fault compensation decision is made based on the residual signal. Finally, numerical simulations are run to demonstrate the superior performance of the proposed approach compared with traditional tracking control.

The important contributions of this paper are summarized as follows:

- The piston position equation of the MMP system is established using the derivative of the dynamic system. This equation is transformed in the form of the nonlinear system or the nonlinear discrete-time system in state space. The main task of this step is to simplify the piston position control process of the MMP model. Additionally, the new control equations of the valves are successfully applied to the position control using the PID controller.
- To achieve asymptotic stability of the state observer, the UIO utilizing the optimization algorithm (LMI) for the linear and nonlinear discrete-time system is proposed. Our approach is described and validated by Lyapunov's stability based on the error conditions. Finally, the matrix inequality is obtained to apply the LMI optimization algorithm.

This paper is organized as follows. In Section 2, a mathematical model of the MMP system is addressed to simplify the control process of the EHA system and the numerical simulation process. In Section 3, a UIO-based sensor fault estimation using a reconstruction approach for systems is implemented, and necessary and sufficient conditions for the existence of a robust UIO are provided. LMI techniques are described for the discrete-time Lipschitz nonlinear systems. In Section 4, simulations with the MMP model using the proposed FTC technique are carried out and the results are discussed. Final conclusions are drawn in Section 5.

2. EHA Model

Referencing the schematic of the EHA system shown in Figure 1, the dynamics of the piston position can be written as [20]:

$$m_p \ddot{x}_p + B_v \dot{x}_p + F_{sp} + F_{frc} + d = A_h P_h - A_r P_r \quad (1)$$

where m_p is the equivalent mass of the object M_p , x_p is the piston position, \ddot{x}_p and \dot{x}_p are the acceleration and piston velocity, respectively, P_h and P_r are the pressure in two chambers, respectively, A_h and A_r are the piston area in two chambers, respectively, F_{sp} is the external load force on the cylinder, d is the disturbance, B_v is the viscosity damping coefficient, and F_{frc} is the friction force.

The spring force F_{sp} can be computed as:

$$F_{sp} = K_{sp}x_p \quad (2)$$

where K_{sp} is stiffness of the spring.

The friction force F_{frc} can be presented as [33]:

$$F_{frc} = \sqrt{2e}(F_{brk} - F_C)e^{-(\frac{v_p}{v_{st}})^2} \frac{v_p}{v_{st}} + F_C \tanh\left(\frac{v_p}{v_{st}}\right) \quad (3)$$

where F_{brk} and F_C are breakaway friction and Coulomb friction, respectively. v_p , v_{st} , and B_v are position velocity, Stribeck velocity threshold, and viscous friction coefficient, respectively.

The hydraulic continuity equations of the EHA system can be expressed as [5]:

$$\dot{P}_h = \Delta_1(Q_h - Q_i - \dot{x}_p A_h) \quad (4)$$

$$\dot{P}_r = \Delta_2(Q_r + Q_i + \dot{x}_p A_r) \quad (5)$$

where

$$\Delta_1 = \beta_e / (V_{ch} + x_p A_h); \Delta_2 = \beta_e / (V_{cr} - x_p A_r); Q_{13i} = Q_{1v} - Q_{3v} - Q_i \text{ and } Q_{24i} = Q_{2v} - Q_{4v} + Q_i.$$

β_e is the effective bulk modulus in each chamber, and V_{ch} , and V_{cr} are the initial control volumes of the two chambers.

The internal leakage flow rate of the cylinder Q_i is described as [5]:

$$Q_i = C_{leak}(P_h - P_r) \quad (6)$$

where C_{leak} is the coefficient of the internal leakage of the cylinder.

The flow rates into the two chambers of the cylinder are computed as [5]:

$$Q_h = Q_{pump} + Q_{1v} - Q_{3v} \quad (7)$$

$$Q_r = -Q_{pump} + Q_{2v} - Q_{4v} \quad (8)$$

where Q_{1v} and Q_{2v} are the flow rate through of the pilot-operated check valve on the left, and the pilot-operated check valve on the right, respectively. Q_{3v} and Q_{4v} are the flow rate through the pressure relief valve on the left and the pressure relief valve on the right in Figure 1.

The pump flow rate Q_{pump} can be presented as [5]:

$$Q_{pump} = D_p \omega \quad (9)$$

where D_p is displacement of the pump, and ω is the speed of the servo pump system.

The left pilot-operated check valve (v_1) is described as [34]:

$$Q_{1v} = C_d A_{1p} \sqrt{\frac{2}{\rho}} \frac{p_1}{(p_1^2 + p_{crack}^2)^{1/4}} \quad (10)$$

where

$$A_{1p} = \begin{cases} A_{leak} & \text{if } p_{1e} < p_{crack} \\ A_{leak} + k \cdot (p_{1e} - p_{crack}) & \text{if } p_{crack} < p_{1e} < p_{max} \\ A_{max} & \text{if } p_{1e} \geq p_{max} \end{cases},$$

$$p_{1e} = k_{pv}P_r - P_h; k = \frac{A_{\max} - A_{leak}}{p_{\max} - p_{crack}}; p_1 = -P_h.$$

P_{crack} , P_{max} , are the valve cracking pressure and the pressure needed to fully open the valve, respectively. A_{pmax} and A_{leak} , are the maximum valve opening area and the closed valve leakage area, respectively. C_d and K_{pc} are the valve coefficient and valve constant, respectively.

Similarly, the right pilot-operated check valve (v_2) can be calculated as (10).

The flow rate through the pressure relief valve (v_3) is determined according to the following Equations [34]:

$$Q_{3v} = C_{dp} A_{3p} \sqrt{\frac{2}{\rho} \frac{p_3}{(p_3^2 + P_{3cr}^2)^{1/4}}} \quad (11)$$

where

$$A_{3p} = \begin{cases} A_{leak} & \text{if } p_3 < p_{set} \\ A_{leak} + k \cdot (p_3 - p_{set}) & \text{if } p_{set} < p_3 < p_{\max} \\ A_{\max} & \text{if } p_3 \geq p_{\max} \end{cases},$$

$$k = (A_{\max} - A_{leak}) / p_{reg}; p_3 = P_h.$$

The minimum pressure for turbulent flow p_{3cr} is calculated according to the transition from a laminar to a turbulent regime, as defined by the following equation:

$$p_{3cr} = (P_3/2 + P_{atm})(1 - B_{lam}),$$

where P_{atm} , and B_{lam} are the atmospheric pressure and the pressure ratio at the transition between the laminar and turbulent regimes, respectively.

Similarly, the pressure relief valve (v_4) can be calculated as (11).

Moreover, taking the derivative of (1) leads to:

$$m_p \ddot{x}_p + \Theta \dot{x}_p + K_{sp} \dot{x}_p + \Gamma \ddot{x}_p = A_h \dot{P}_h - A_r \dot{P}_r \quad (12)$$

where

$$\Theta = B_v + F_C / v_{cl}$$

$$\Gamma = -\frac{F_C}{v_{cl}} \tanh\left(\frac{\dot{x}_p}{v_{cl}}\right)^2 + \frac{\sqrt{2e}(F_{brk} - F_C)e^{-(\frac{\dot{x}_p}{v_{st}})^2}}{v_{st}} - \frac{2\sqrt{2e}\dot{x}_p^2(F_{brk} - F_C)e^{-(\frac{\dot{x}_p}{v_{st}})^2}}{v_{st}^3}.$$

Substituting (4) and (5) into (12), we obtain:

$$\begin{aligned} m_p \ddot{x}_p + \Theta \dot{x}_p + K_{sp} \dot{x}_p + \Gamma \ddot{x}_p &= A_h \dot{P}_h - A_r \dot{P}_r \\ &= (A_h \Delta_1 + A_r \Delta_2) Q_{pump} - (A_h^2 \Delta_1 + A_r^2 \Delta_2) \dot{x}_p + \Omega \end{aligned} \quad (13)$$

where

$$\Omega = A_h \Delta_1 Q_{13i} - A_r \Delta_2 Q_{24i}.$$

Finally, (13) can be rewritten as:

$$\ddot{x}_p = -\gamma_1 \ddot{x}_p - \gamma_2 \dot{x}_p + g(x, u) \quad (14)$$

where

$$\begin{aligned} g(x, u) &= -(\Gamma/m_p) \ddot{x}_p + \Omega/m_p + \gamma_4 u - \gamma_3 \dot{x}_p \\ \gamma_1 &= \Theta/m_p; \gamma_2 = K_{sp}/m_p; u = \omega. \end{aligned}$$

Equation (14) can be built in form as:

$$\dot{x} = Ax + f(x, u) \quad (15)$$

where

$$\begin{cases} x_1 = x_p; \\ \dot{x}_1 = x_2 = \dot{x}_p; \\ \dot{x}_2 = x_3 = \ddot{x}_p \\ \dot{x}_3 = -\gamma_1 x_3 - \gamma_2 x_2 + g(x, u) \end{cases} ; x = \begin{bmatrix} x_1^T & x_2^T & x_3^T \end{bmatrix}^T \text{ and } f(x, u) = \begin{bmatrix} 0 & 0 & g^T(x, u) \end{bmatrix}^T.$$

The matrix A shown in (15) is the constant matrix. It can be expressed in a nonlinear discrete-time state space model as:

$$x_{k+1} = A_k x_k + \phi_{x_k, u_k} \quad (16)$$

where

$$x_k = \begin{bmatrix} x_1^T(k) & x_2^T(k) & x_3^T(k) \end{bmatrix}^T$$

$$A_k = \begin{bmatrix} 1 & T_s & 0 \\ 0 & 1 & T_s \\ 0 & -T_s \gamma_2 & (1 - T_s \gamma_1) \end{bmatrix}, \text{ and } \phi_{x_k, u_k} = \begin{bmatrix} 0 \\ 0 \\ T_s g(x_k, u_k) \end{bmatrix}.$$

3. UIO-Based Reconstruction Approach

3.1. UIO for Linear Discrete-time System

A dynamics system with uncertainty is utilized in a linear discrete form with an additive unknown disturbance term as the following equation [18]:

$$\begin{cases} x_{k+1} = A_k x_k + B_k u_k + D_d d_k \\ y_k = C_k x_k + F_s s_k \end{cases} \quad (17)$$

where $x_k \in \mathbb{R}^n$ is the state vector, $y_k \in \mathbb{R}^p$ is the outputs vector and $d_k \in \mathbb{R}^{r_d}$ is the unknown input or disturbance vector, and $s_k \in \mathbb{R}^q$ is the sensor fault. A_k, B_k, C_k, D_d , and F_s are known constant matrices with suitable dimensions.

The system variable reconstruction of (17) can be rewritten in the following form:

$$\begin{cases} \bar{E} \bar{x}_{k+1} = \bar{A}_k \bar{x}_k + \bar{B}_k u_k + \bar{G} s_k + \bar{D}_d d_k \\ y_k = \bar{C}_k \bar{x}_k \end{cases} \quad (18)$$

where

$$\bar{A}_k = \begin{bmatrix} A_k & 0 \\ 0 & -I_p \end{bmatrix}; \bar{E} = \begin{bmatrix} I_n & 0 \\ 0 & 0_p \end{bmatrix}; \bar{B}_k = \begin{bmatrix} B_k^T & 0_p^T \end{bmatrix}^T;$$

$$\bar{C}_k = \begin{bmatrix} C_k & F_s \end{bmatrix}; \bar{D}_d = \begin{bmatrix} D_d \\ 0 \end{bmatrix}; \bar{G} = \begin{bmatrix} 0 \\ I_p \end{bmatrix}; \bar{x}_k = \begin{bmatrix} x_k \\ s_k \end{bmatrix} \in \mathbb{R}^{\bar{n}}$$

with $\bar{n} = n + p$.

Based on [18], the UIO model can be built by the influences of unknown inputs in the system (18) as:

$$\begin{cases} \bar{z}_{k+1} = F \bar{z}_k + \Sigma \bar{B}_k u_k + L y_k \\ \hat{x}_k = \bar{z}_k + H y_k \\ \hat{y}_k = \bar{C}_k \hat{x}_k \end{cases} \quad (19)$$

where $\hat{x}_k \in \mathbb{R}^{\bar{n}}$, $\hat{y}_k \in \mathbb{R}^p$, and $\bar{z}_k \in \mathbb{R}^{\bar{n}}$ are state vector estimation of \bar{x}_k , measurement output estimation vector and state vector of the observer, respectively. The observer matrices $F \in \mathbb{R}^{\bar{n} \times \bar{n}}$, $\Sigma \in \mathbb{R}^{\bar{n} \times \bar{n}}$, $H \in \mathbb{R}^{\bar{n} \times p}$, $L \in \mathbb{R}^{\bar{n} \times p}$, $L_1 \in \mathbb{R}^{\bar{n} \times p}$, and $L_2 \in \mathbb{R}^{\bar{n} \times p}$ should be designed according to the state estimation error vector.

Similarly, by using [18], the estimation error can be defined as:

$$\bar{e}_k = \bar{x}_k - \hat{x}_k \quad (20)$$

and

$$\begin{aligned} \bar{e}_{k+1} &= \bar{x}_{k+1} - \hat{x}_{k+1} \\ &= (I_{\bar{n}} - H\bar{C}_k)\bar{x}_{k+1} - \bar{z}_{k+1} \\ &= \Sigma\bar{x}_{k+1} - \bar{z}_{k+1} \end{aligned} \quad (21)$$

where

$$\Sigma = I_{\bar{n}} - H\bar{C}_k$$

Multiplying both sides of the matrix Equation (18) by the matrix Σ , Equation (18) can be rewritten as:

$$\Sigma\bar{E}\bar{x}_{k+1} = \Sigma\bar{A}_k\bar{x}_k + \Sigma\bar{B}_k u_k + \Sigma\bar{G}s_k + \Sigma\bar{D}_d d_k \quad (22)$$

and from (19), we obtain

$$\begin{aligned} \hat{x}_{k+1} &= F\bar{z}_k + \Sigma\bar{B}_k u_k + L y_k + H\bar{C}_k \bar{x}_{k+1} \\ &= F\hat{x}_k - FH y_k + \Sigma\bar{B}_k u_k + L y_k + H\bar{C}_k \bar{x}_{k+1} \\ &= F\hat{x}_k - (FH - L_2)y_k + \Sigma\bar{B}_k u_k + L_1\bar{C}_k \bar{x}_k + H\bar{C}_k \bar{x}_{k+1} \end{aligned} \quad (23)$$

where $L = L_1 + L_2$

Using (20)–(23), we have:

$$\bar{e}_{k+1} = F\bar{e}_k + [I_{\bar{n}} - (\Sigma\bar{E} + H\bar{C}_k)]\bar{x}_{k+1} + [(\Sigma\bar{A}_k - L_1\bar{C}_k) - F]\bar{x}_k + (FH - L_2)y_k + \Sigma\bar{G}s_k + \Sigma\bar{D}_d d_k \quad (24)$$

From (20), (21), and (24), the estimation error (25) can be represented as:

$$\bar{e}_{k+1} = F\bar{e}_k + \Sigma\bar{D}_d d_k \quad (25)$$

If the following conditions are satisfied

$$\left. \begin{aligned} \Sigma\bar{E} + H\bar{C}_k &= I_{\bar{n}} \\ \Sigma\bar{G} &= 0 \\ \Sigma\bar{A}_k - L_1\bar{C}_k &= F \\ FH &= L_2 \end{aligned} \right\} \quad (26)$$

without loss of generality, the matrix Σ can be defined:

$$\Sigma = \begin{bmatrix} I_n & \delta_1 \\ -C_k & \delta_2 \end{bmatrix} \quad (27)$$

where $\delta_1 \in \mathbb{R}^{n \times p}$ and $\delta_2 \in \mathbb{R}^{p \times p}$ are arbitrary matrices.

By solving (26) and (27), we obtain:

$$\Sigma = \begin{bmatrix} I_n & 0 \\ -C_k & 0 \end{bmatrix}; \delta_1 = \delta_2 = 0; H = \begin{bmatrix} 0 \\ I_p \end{bmatrix} \quad (28)$$

Lemma 1. [18] The necessary and sufficient conditions for the existence of UIO (19), if the system (18) guarantees as follows:

$$\begin{aligned} & \text{rank}(C_k D_d) = \text{rank}(D_d) \\ \text{a) } & \begin{bmatrix} A_k - I_n & D_d \\ C_k & 0 \end{bmatrix} = n + r_d, \text{ and } D_d \text{ is a full column rank} \\ \text{b) } & \begin{bmatrix} A_k - zI_n & D_d \\ C_k & 0 \end{bmatrix} = n + r_d \quad \forall z \text{ with } |z| > 1. \end{aligned}$$

Lemma 2. [29] For the equation in the following form:

$$\dot{\zeta}(t) = \Phi \zeta(t) + Y u(t) \quad (29)$$

The eigenvalues of a given matrix $\Phi \in \mathbb{R}^{n \times n}$ belong to the circular region $D(\alpha, \rho)$ with the center $\alpha + j0$ and the radius ρ if and only if there exists a symmetric positive definite matrix $P \in \mathbb{R}^{n \times n}$ such that the following condition holds:

$$\begin{bmatrix} -P & P(\Phi - \alpha I_n) \\ * & -\rho^2 P \end{bmatrix} < 0 \quad (30)$$

Theorem 1. For system (18), there exists a robust UIO in the form of (19) such that $\|e_{yk}\| \leq \gamma \|d_k\|$, and a prescribed circular region $D(\alpha, r)$, if there exists a positive-definite symmetric matrix $P_L \in \mathbb{R}^{\bar{n} \times \bar{n}}$ and matrix $Q_L \in \mathbb{R}^{\bar{n} \times p}$, and a scalar $\gamma > 0$ such that the following inequalities hold:

$$\begin{bmatrix} -P_L & 0 & (\Sigma \bar{A}_k)^T P_L - \bar{C}_k^T Q_L^T & \bar{C}_k^T \\ * & -\gamma I_d & (\Sigma \bar{D}_d)^T P_L & 0 \\ * & * & -P_L & 0 \\ * & * & * & -\gamma I_p \end{bmatrix} < 0 \quad (31)$$

and

$$\begin{bmatrix} -P_L & P_L \Sigma \bar{A}_k - Q_L \bar{C}_k - \alpha P_L \\ * & -r^2 P_L \end{bmatrix} < 0 \quad (32)$$

where $Q_L = P_L L_1$ and output estimation error $e_{yk} = \bar{C}_k \bar{e}_k$

Then the state observer (18) is asymptotically stable.

Proof of (31). Consider Lyapunov functions as $V_k = \bar{e}_k^T P_L \bar{e}_k$; then its difference between two adjacent steps $\Delta V_k = V_{k+1} - V_k$ is given as:

$$\begin{aligned} \Delta V_k &= V_{k+1} - V_k \\ &= \bar{e}_{k+1}^T P_L \bar{e}_{k+1} - \bar{e}_k^T P_L \bar{e}_k \\ &= \bar{e}_k^T F^T P_L F \bar{e}_k + \bar{e}_k^T F^T P_L \Sigma \bar{D}_d d_k - e_k^T P_L e_k + d_k^T (\Sigma \bar{D}_d)^T P_L F \bar{e}_k + d_k^T (\Sigma \bar{D}_d)^T P_L \Sigma \bar{D}_d d_k \end{aligned} \quad (33)$$

or

$$\Delta V_k = \begin{bmatrix} \bar{e}_k \\ d_k \end{bmatrix}^T \begin{bmatrix} F^T P_L F - P_L & F^T P_L \Sigma \bar{D}_d \\ * & (\Sigma \bar{D}_d)^T P_L \Sigma \bar{D}_d \end{bmatrix} \begin{bmatrix} \bar{e}_k \\ d_k \end{bmatrix}.$$

Based on the initial condition $\|e_{yk}\| \leq \gamma \|d_k\|$, the matrix J in (34) can be presented as:

$$J = \begin{bmatrix} \bar{e}_k \\ d_k \end{bmatrix}^T \begin{bmatrix} \frac{1}{\gamma} \bar{C}_k^T \bar{C}_k & 0 \\ 0 & -\gamma I_d \end{bmatrix} \begin{bmatrix} \bar{e}_k \\ d_k \end{bmatrix} \leq 0 \quad (34)$$

where $e_{yk} = \bar{C}_k \bar{e}_k$ is output estimation error.

From (33) and (34), the matrix Y can be expressed in the stable condition of system as:

$$Y = \Delta V_k + J \leq 0 \quad (35)$$

Thus, (35) can be rewritten as:

$$\begin{aligned} Y &= \begin{bmatrix} \bar{e}_k \\ d_k \end{bmatrix}^T \begin{bmatrix} F^T P_L F - P_L + \frac{1}{\gamma} \bar{C}_k^T \bar{C}_k & F^T P_L \Sigma \bar{D}_d \\ * & (\Sigma \bar{D}_d)^T P_L \Sigma \bar{D}_d - \gamma I_d \end{bmatrix} \begin{bmatrix} \bar{e}_k \\ d_k \end{bmatrix} \\ &= \chi^T \Pi \chi \end{aligned} \quad (36)$$

where

$$\begin{aligned} \chi &= \begin{bmatrix} \bar{e}_k^T & d_k^T \end{bmatrix}^T \\ \Pi &= \begin{bmatrix} -P_L + \frac{1}{\gamma} \bar{C}_k^T \bar{C}_k & 0 \\ 0 & -\gamma I_d \end{bmatrix} + \begin{bmatrix} F^T P_L F & F^T P_L \Sigma \bar{D}_d \\ * & (\Sigma \bar{D}_d)^T P_L \Sigma \bar{D}_d \end{bmatrix}. \end{aligned}$$

Using the Schur lemma [34] for the inequality (35) with $\Pi < 0$, then (31) is satisfied, once existent $J < 0$ satisfies the condition $\|e_{yk}\| \leq \gamma \|d_k\|$. \square

Proof of (32). Applying (25) to Lemma 2, then (32) is satisfied. \square

Although the linear UIO is developed here, there are still some limitations:

- Performance of the control system using the linear UIO can be inaccurate because of any unknown nonlinear terms.
- In fact, an MMP system is a nonlinear system with unknown nonlinearities and uncertainties [5,6].

To address this challenge, the nonlinear UIO is proposed and developed in the following section.

3.2. UIO for Nonlinear Discrete-time System

We consider the following nonlinear discrete-time system subject to an unknown input in the following form:

$$\begin{cases} x_{k+1} = A_k x_k + B_k u_k + \phi_{x_k, u_k} + D_d d_k \\ y_k = C_k x_k + F_s s_k \end{cases} \quad (37)$$

where $\phi_{x_k, u_k} = \phi(x_k, u_k)$ is a nonlinear function vector $\forall x_k, x_k \in \mathbb{R}^n, u_k \in \mathbb{R}^m$.

Based on [29], a Lipschitz constraint of the discrete-time nonlinear function vector ϕ_{x_k, u_k} can be expressed as

$$\|\Delta \phi_{x_k, u_k}\| \leq \zeta \|e_k\| \quad (38)$$

where $\|\Delta \phi_{x_k, u_k}\| = \|\phi_{x_k, u_k} - \phi_{\hat{x}_k, u_k}\|$ and $\|e_k\| = \|x_k - \hat{x}_k\|$.

Similar to (18), the system variable reconstruction for the nonlinear discrete-time system (37) is rewritten as:

$$\begin{cases} \bar{E} \bar{x}_{k+1} = \bar{A}_k \bar{x}_k + \bar{B}_k u_k + \bar{\phi}_{x_k, u_k} + \bar{G} s_k + \bar{D}_d d_k \\ y_k = \bar{C}_k \bar{x}_k \end{cases} \quad (39)$$

where $\bar{\phi}_{x_k, u_k} = \begin{bmatrix} \phi_{x_k, u_k} & 0 \end{bmatrix}^T \in \mathbb{R}^{\bar{n}}$.

From (38), we obtain

$$\|\Delta\bar{\phi}_{x_k, u_k}\| \leq \bar{\zeta}\|\bar{e}_k\| \quad (40)$$

where

$$\Delta\bar{\phi}_{x_k, u_k} = \bar{\phi}_{x_k, u_k} - \bar{\phi}_{\hat{x}_k, u_k} \\ \bar{e}_k = \bar{x}_k - \hat{x}_k; \quad \bar{\zeta} = \begin{bmatrix} \zeta I_n & 0 \\ 0 & 0_p \end{bmatrix} \in \mathbb{R}^{\bar{n}}.$$

The UIO is built for the nonlinear discrete-time systems (38) as:

$$\begin{cases} \bar{z}_{k+1} = F_n \bar{z}_k + \Sigma \bar{B}_k u_k + L y_k + \Sigma \bar{\phi}_{\hat{x}_k, u_k} \\ \hat{x}_k = \bar{z}_k + H y_k \end{cases} \quad (41)$$

where vector Σ and H are matrices to be designed for satisfying (28).

Furthermore, the estimation error is also computed following (20) and (21). It is easy to write (42) as:

$$\bar{e}_{k+1} = F_n \bar{e}_k + \Sigma \Delta\bar{\phi}_{x_k, u_k} + \Sigma \bar{D}_d d_k \quad (42)$$

if the following conditions are satisfied:

$$\left. \begin{aligned} \Sigma \bar{E} + H \bar{C}_k &= I_{\bar{n}} \\ \Sigma \bar{G} &= 0 \\ \Sigma \bar{A}_k - L_1 \bar{C}_k &= F_n \\ F_n H &= L_2 \end{aligned} \right\} \quad (43)$$

The matrix Λ in the inequality condition (44) can be inferred from (40) as:

$$\Lambda = \begin{bmatrix} \bar{e}_k \\ \Delta\bar{\phi}_{x_k, u_k} \end{bmatrix}^T \begin{bmatrix} -\bar{\zeta}^T \bar{\zeta} & 0 \\ 0 & I_{\bar{n}} \end{bmatrix} \begin{bmatrix} \bar{e}_k \\ \Delta\bar{\phi}_{x_k, u_k} \end{bmatrix} \leq 0 \quad (44)$$

Theorem 2. For system (39), there exists a robust UIO in the form of (41) such that the output estimation error satisfies $\|e_{yk}\| \leq \mu \|d_k\|$ and a prescribed circular region $D(\alpha, r)$ if there exists a positive-definite symmetric matrix $P_n \in \mathbb{R}^{\bar{n} \times \bar{n}}$, matrix $Q_n \in \mathbb{R}^{\bar{n} \times p}$, and positive scalars μ , and ε such that the following inequalities (41, 42) hold:

$$\begin{bmatrix} -P_n + \varepsilon \bar{\zeta}^T \bar{\zeta} & 0 & 0 & (\Sigma \bar{A}_k)^T P_n - \bar{C}_k^T Q_n^T & \bar{C}_k^T \\ * & -\varepsilon I_{\bar{n}} & 0 & \Sigma^T P_n & 0 \\ * & * & -\mu I_d & (\Sigma \bar{D}_d)^T P_n & 0 \\ * & * & * & -P_n & 0 \\ * & * & * & * & -\mu I_p \end{bmatrix} < 0 \quad (45)$$

and

$$\begin{bmatrix} -P_n & P_n \Sigma \bar{A}_k - Q_n \bar{C}_k - \alpha P_n \\ * & -r^2 P_n \end{bmatrix} < 0 \quad (46)$$

Then the state observer (41) is asymptotically stable.

Proof of (45). Consider a Lyapunov function as $V_k = \bar{e}_k^T P_n \bar{e}_k$; then its difference between two adjacent steps $\Delta V_k = V_{k+1} - V_k$ is given as:

$$\begin{aligned} \Delta V_k &= V_{k+1} - V_k \\ &= \bar{e}_{k+1}^T P_n \bar{e}_{k+1} - \bar{e}_k^T P_n \bar{e}_k \\ &= \lambda^T \begin{bmatrix} F_n^T P_n F_n - P_n & F_n^T P_n \Sigma & F_n^T P_n \Sigma \bar{D}_d \\ * & \Sigma^T P_n \Sigma & \Sigma^T P_n \Sigma \bar{D}_d \\ * & * & (\Sigma \bar{D}_d)^T P_n \Sigma \bar{D}_d \end{bmatrix} \lambda \end{aligned} \quad (47)$$

where

$$\lambda = \begin{bmatrix} \bar{e}_k^T & \Delta \bar{\phi}_{x_k, u_k}^T & d_k^T \end{bmatrix}^T.$$

Moreover, (44) can be described as:

$$\Lambda = \lambda^T \begin{bmatrix} -\bar{\zeta}^T \bar{\zeta} & 0 & 0 \\ 0 & I_{\bar{n}} & 0 \\ 0 & 0 & 0 \end{bmatrix} \lambda \leq 0 \quad (48)$$

Combining (47) and (48) leads to:

$$\begin{aligned} \Delta V_k &\leq \lambda^T \begin{bmatrix} F_n^T P_n F_n - P_n & F_n^T P_n \Sigma & F_n^T P_n \Sigma \bar{D}_d \\ * & \Sigma^T P_n \Sigma & \Sigma^T P_n \Sigma \bar{D}_d \\ * & * & (\Sigma \bar{D}_d)^T P_n \Sigma \bar{D}_d \end{bmatrix} \lambda - \varepsilon \Lambda \\ &= \lambda^T \begin{bmatrix} F_n^T P_n F_n - P_n + \varepsilon \bar{\zeta}^T \bar{\zeta} & F_n^T P_n \Sigma & F_n^T P_n \Sigma \bar{D}_d \\ * & \Sigma^T P_n \Sigma - \varepsilon I_{\bar{n}} & \Sigma^T P_n \Sigma \bar{D}_d \\ * & * & (\Sigma \bar{D}_d)^T P_n \Sigma \bar{D}_d \end{bmatrix} \lambda \end{aligned} \quad (49)$$

Based on the measurement error condition $\|e_{yk}\| \leq \mu \|d_k\|$ of the output, the matrix J_n in (50) can be presented as:

$$J_n = \begin{bmatrix} \bar{e}_k \\ d_k \end{bmatrix}^T \begin{bmatrix} \frac{1}{\mu} \bar{C}_k^T \bar{C}_k & 0 \\ 0 & -\mu I_d \end{bmatrix} \begin{bmatrix} \bar{e}_k \\ d_k \end{bmatrix} \leq 0 \quad (50)$$

A matrix T_n is defined as:

$$T_n = \Delta V_k + J_n \quad (51)$$

Equation (52) can be described using (49) and (51) as:

$$\begin{aligned} T_n &\leq \lambda^T \begin{bmatrix} F_n^T P_n F_n - P_n + \varepsilon \bar{\zeta}^T \bar{\zeta} + \frac{1}{\mu} \bar{C}_k^T \bar{C}_k & F_n^T P_n \Sigma & F_n^T P_n \Sigma \bar{D}_d \\ * & \Sigma^T P_n \Sigma - \varepsilon I_{\bar{n}} & \Sigma^T P_n \Sigma \bar{D}_d \\ * & * & (\Sigma \bar{D}_d)^T P_n \Sigma \bar{D}_d - \mu I_d \end{bmatrix} \lambda \\ &= \lambda^T \Pi_n \lambda \end{aligned} \quad (52)$$

where

$$\Pi_n = \begin{bmatrix} F_n^T P_n F_n & F_n^T P_n \Sigma & F_n^T P_n \Sigma \bar{D}_d \\ * & \Sigma^T P_n \Sigma & \Sigma^T P_n \Sigma \bar{D}_d \\ * & * & (\Sigma \bar{D}_d)^T P_n \Sigma \bar{D}_d \end{bmatrix} + \begin{bmatrix} -P_n + \varepsilon \bar{\zeta}^T \bar{\zeta} + \frac{1}{\mu} \bar{C}_k^T \bar{C}_k & 0 & 0 \\ * & -\varepsilon I_{\bar{n}} & 0 \\ * & * & -\mu I_d \end{bmatrix} \quad (53)$$

Applying the Schur lemma [33] to (51) with $\Pi_n < 0$, we obtain:

$$\Pi_{n'} = \begin{bmatrix} -P_n + \varepsilon \bar{\zeta}^T \bar{\zeta} + \frac{1}{\mu} \bar{C}_k^T \bar{C}_k & 0 & 0 & (\Sigma \bar{A}_k)^T P_n - \bar{C}_k^T Q_n^T \\ * & -\varepsilon I_{\bar{n}} & 0 & \Sigma^T P_n \\ * & * & -\mu I_d & (\Sigma \bar{D}_d)^T P_n \\ * & * & * & -P_n \end{bmatrix} \quad (54)$$

Similarly, applying the Schur complement lemma [33] to (54) with $\Pi_{n'} < 0$, then the inequality (45) is satisfied once $J_n < 0$ satisfies the condition $\|e_{yk}\| \leq \mu \|d_k\|$. \square

Proof of (46). Applying (41) to Lemma 2, then (46) is satisfied. \square

In summary, the design procedure for this fault estimator is implemented in the following steps:

- Step 1: Construct the augmented system (39) for the discrete-time system (37).
- Step 2: Determine the matrices Q_n , P_n , and $L_1 = P_n^{-1} Q_n$ to solve the LMI defined by the matrix inequality (45, 46).
- Step 3: Calculate the gain matrices F_n , L_2 and L using (46).
- Step 4: Obtain the state and fault estimation as $\hat{x}_k = \begin{bmatrix} I_n & 0_{n \times r} \end{bmatrix} \hat{\bar{x}}_k$, and $\hat{s}_k = \bar{C}_s \hat{\bar{x}}_k$, respectively,

where $\bar{C}_s = \begin{bmatrix} 0_{r \times n} & I_r \end{bmatrix}$.

4. Sensor Fault-Tolerant Control in an MMP System

4.1. General Residual from the Sensor Fault Signal

Under the state estimation vector of the UIO, the residual vector is calculated as [12]:

$$r_k = y_k - \hat{y}_k \quad (55)$$

This means that $r_k = 0$ if $s_k = 0$ and $r_k \neq 0$ if $s_k \neq 0$.

4.2. Sensor FTC Compensation

The sensor fault output from the measurements influences the closed-loop behavior and corrupts the state estimation.

The SFTC technique is designed based on the position SFs compensation to handle the sensor fault issues of the MMP system, as shown in Figure 2. The PID main controller will operate conventional close-loop trajectory control. The measurement is employed as [18]:

$$y_{ck} = y_k - F_s \hat{s}_k \quad (56)$$

Fault compensation is operated by a logic process that is based on a residual via a threshold value k equal to 0 if $|r_k| \leq k$, and equal to 1 if $|r_k| > k$ [12].

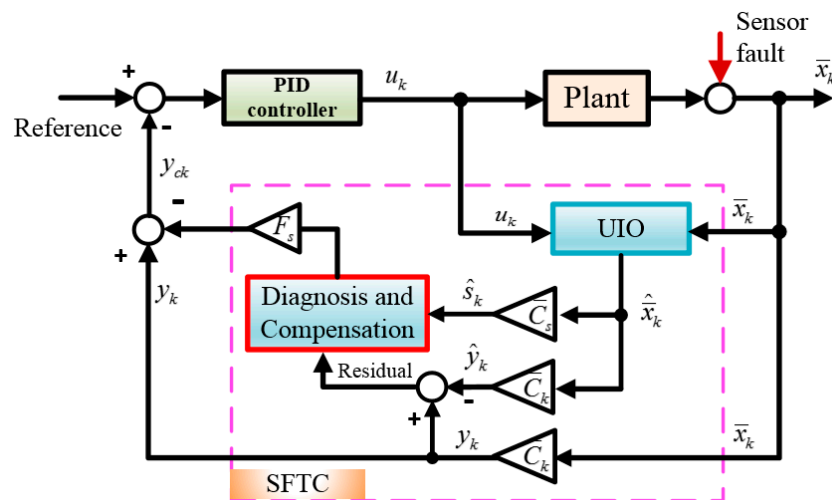


Figure 2. The structure of observer-based fault-tolerant control.

4.3. Simulation and Results

4.3.1. The parameters of the MMP system

The parameters of the MMP system were gathered from a KYB MMP4 by a cylinder of $\varphi 40 - \varphi 20 - 250$ and a motor of DC 24V. Some parameters were determined using the parameter estimation method in MATLAB version 2015a, 64 bits. The resulting parameters of the MMP system are shown in Table 1.

Table 1. Basic parameters of the mini motion package (MMP) system.

Components	Values	Units
A_h	0.0013	m^2
A_r	$9.4\text{e-}4$	m^2
V_{ch}	$2.09\text{e-}4$	m^3
V_{cr}	$4.0065\text{e-}05$	m^3
m_p	10	kg
β_e	$2.9\text{e+}08$	Pa
K_{sp}	2383	Nm
D_p	$3.5\text{e-}6$	m^3

The basic parameters of the MMP system are listed in Table 1 as follows:

The matrices in (16) and (34) of the EHA system were obtained as:

$$B_k = \begin{bmatrix} 0 & 0 & 0 \end{bmatrix}^T; C_k = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix}; F_s = 1;$$

$$A_k = \begin{bmatrix} 1 & 0.001 & 0 \\ 0 & 0.9998 & 0.0005 \\ 0 & -0.2911 & 0.2311 \end{bmatrix}.$$

Based on [35], the sampling time T_s can be selected by $T_s = 1$ ms.

To investigate the MMP tracking control, without loss of generality, a reference trajectory for the positive position of the system cylinder was given as:

$$y_r = \sin(0.85t) + 1.5 \quad (57)$$

and a sensor fault $s(t)$ was simulated by the following function:

$$s(t) = \begin{cases} 0 & \text{if } t < 2.945 \\ 0.75 \sin(8t) + 1 & \text{if } 2.945 \leq t \leq 3.9275 \\ 0.75 & \text{if } 3.9275 \leq t \leq 7 \\ 2.55t - 17.1 & \text{if } 7 \leq t \leq 7.25 \\ -2.55t + 17.7 & \text{if } 7.25 \leq t \leq 7.75 \\ 0.8125t - 6.034375 & \text{if } 8.75 \leq t \leq 10 \\ 0 & \text{if } t > 10 \end{cases} \quad (58)$$

Based on the design experience, the positive scalars ζ , r , α , ε , and μ were selected as $\zeta = 20$; $r = 0.01$, $\alpha = 0.1$, $\varepsilon = 0.1$, and $\mu = 0.2$. The LMI defined by (45, 46) can be solved for P_n , Q_n , and F_n . If the solution is feasible, then the results can be obtained as:

$$\begin{aligned} \Sigma &= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ -1 & 0 & 0 & 0 \end{bmatrix}; H = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix}; Q_n = \begin{bmatrix} -2.3626e+0 \\ 0.1264e-08 \\ -3.1485e-09 \\ -2.3626e+0 \end{bmatrix}; \\ P_n &= \begin{bmatrix} 2.321e+1 & -1.001e-7 & 2.965e-8 & 2.321e+1 \\ -1.001e-7 & 1.914e-9 & 4.062e-10 & -1.001e-7 \\ 2.965e-8 & 4.062e-10 & 3.097e-9 & 2.965e-8 \\ 2.321e+1 & -1.001e-7 & 2.965e-8 & 2.321e+1 \end{bmatrix}; \\ L_1 &= \begin{bmatrix} -6.2519e+02 \\ -9.3052e-02 \\ 9.2219e-02 \\ 6.2509e+02 \end{bmatrix}; L = \begin{bmatrix} -2.2737e-13 \\ -2.7756e-17 \\ 2.7756e-17 \\ 2.2737e-13 \end{bmatrix}; \\ F_n &= \begin{bmatrix} 6.262e+2 & 9.999e-4 & 3.244e-7 & 6.252e+2 \\ 9.305e-2 & 9.998e-1 & 5.250e-4 & 9.305e-2 \\ -9.222e-2 & -2.911e-1 & 2.311e-1 & -9.222e-2 \\ -6.261e+2 & -9.999e-4 & -3.244e-7 & -6.251e+2 \end{bmatrix}. \end{aligned}$$

4.3.2. The Evaluated Equations of the PID Controller for the MMP System

To evaluate the PID controller's efficiency, the control error is normally one of the most important factors to evaluate the PID controller.

Considering that a position control error estimation is calculated as:

$$e_{ck} = y_r - y_{ck} \quad (59)$$

a maximum error result $e_{ck\max}$ of the position control error e_{ck} is computed as:

$$e_{ck\max} = y_{r\max} - y_{ck\max} \quad (60)$$

where $y_{r\max}$ and $y_{ck\max}$ are the maximum reference signal and the maximum response signal, respectively.

The error performance $^pe_{ck\max}$ of the PID controller of the position control error $e_{ck\max}$ is defined as:

$$^pe_{ck\max} = \left(1 - \frac{e_{ck\max}}{e_{s\max}}\right) 100\% \quad (61)$$

where

$$e_{s\max} = s_{\max} - s_{\min}$$

with s_{\max} and s_{\min} being the maximum and minimum sensor fault $s(t)$, respectively.

4.3.3. Simulation Results and Discussion

To assess the effectiveness of the developed control approach, we conducted a comparative simulation study on the system tracking performance, between the proposed SFTC and the traditional PID control without an FTC module. This control had been built in a MATLAB/Simulink environment, and a sampling time of $T_s = 1\text{ms}$ was selected for all the simulations.

Numerical simulations were then carried out with the developed MMP model to follow the given trajectory (57) under the disturbed environment, including the faulty sensor condition (58) without disturbance ($d_k = 0$), or with disturbance [$d_k = 0.0045\text{random}(2, t)$]. By using the PID tuning tool of the Matlab Simulink toolbox, the parameters of the PID controller are obtained ($K_P = 1.536$, $K_I = 1.32$ and $K_D = 0.0015$) and applied to all the simulations.

The simulation results from Figures 3–6 show that the PID response signal and its estimation signal followed the reference signal at locations without fault impacts, whereas when the SFTC was not applied for the system, these signals were affected by the fault at locations where the fault occurred (Figure 3a). In Figure 3a,b, the PID response signal without the SFTC clearly shows the effect of the unknown input disturbance. This influence of the fault estimation signal is similar to the sensor fault signal in Figure 3a, which demonstrates that the fault estimator of the system worked well. Nevertheless, there is the big difference between the fault estimation of Figure 3b compared with Figure 3a due to influences of the unknown input disturbance.

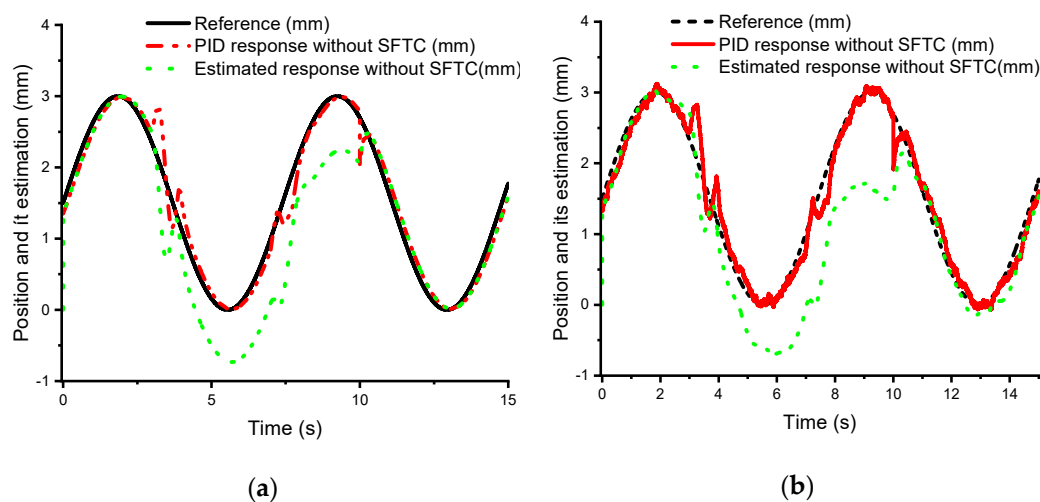


Figure 3. Position response and its estimation without SFTC of (a) disturbance $d_k = 0$, and (b) disturbance $d_k = 0.0045\text{random}(2, t)$.

Figure 4a shows that the fault estimation signal reaches the sensor fault. This means that the fault estimator is performed well. Figure 4b shows the influences of disturbance to the fault estimation signal. The PID response signal and its estimation signal followed the reference signal when we applied the SFTC technology to our system even though the system is affected by the SFs in Figure 5a and unknown input disturbances in Figure 5b. Furthermore, the estimated fault can be reduced to zero when the SFTC technique is implemented by the compensation process, in cases with and without unknown inputs disturbance. Previous issues, to demonstrate that the MMP system works well when the proposed SFTC technology is utilized by the fault compensation process. Disturbances coming from an actuator are canceled after fault compensation; hence, we can use only the SFTC for fault compensation, which does not need an added actuator FTC for fault compensation.

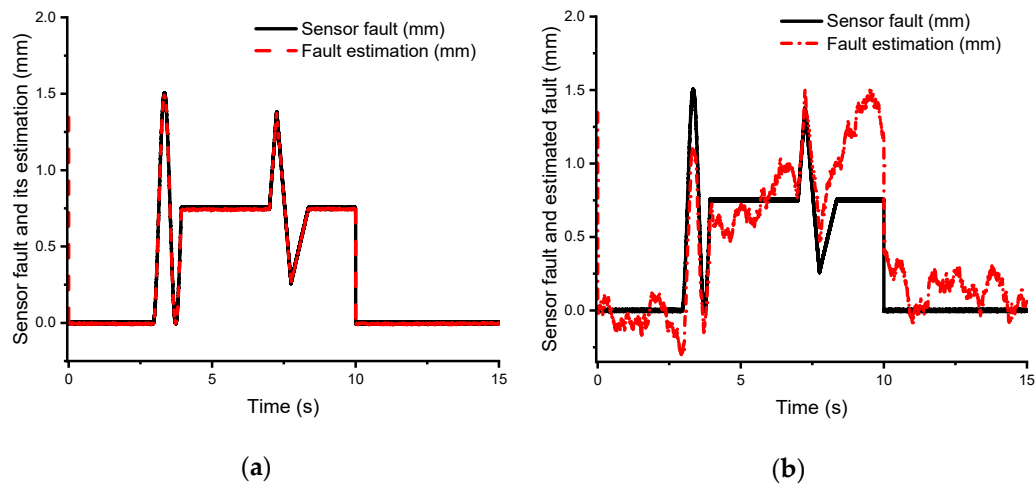


Figure 4. Sensor fault and its estimation without SFTC (a) disturbance $d_k = 0$, and (b) disturbance $d_k = 0.0045\text{random}(2,t)$.

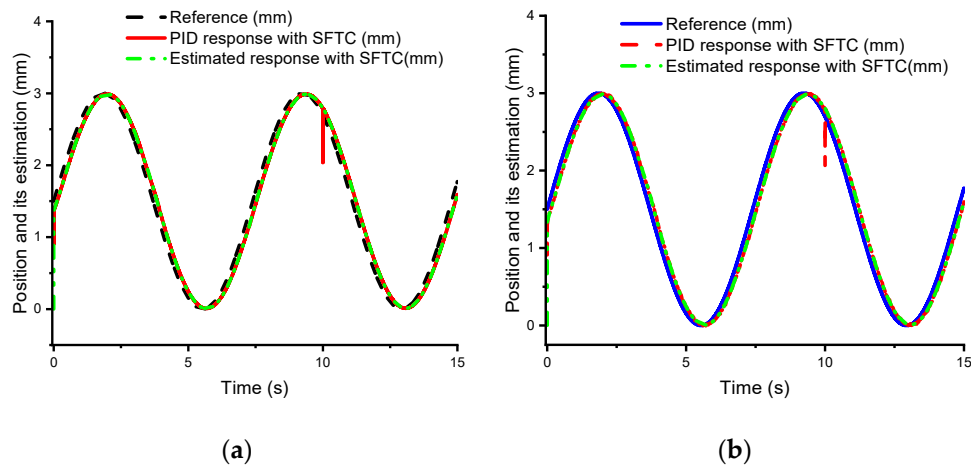


Figure 5. Position response and its estimation with SFTC (a) disturbance $d_k = 0$, and (b) disturbance $d_k = 0.0045\text{random}(2,t)$.

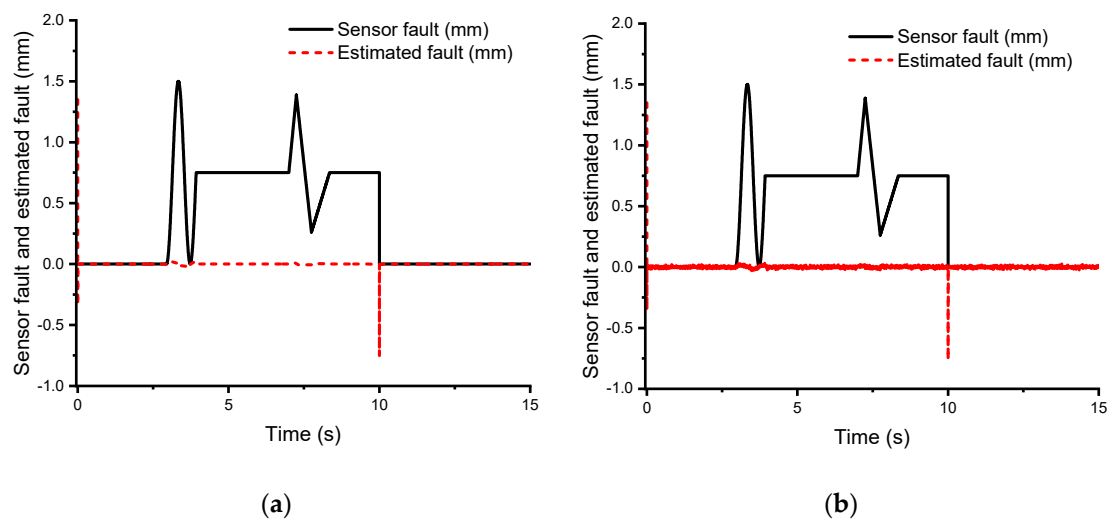


Figure 6. Sensor fault and its estimation with SFTC (a) disturbance $d_k = 0$, and (b) disturbance $d_k = 0.0045\text{random}(2,t)$.

In Figure 6a,b, the estimated error signal reaches zero value when the SFTC technology is used to perform error compensation.

To evaluate the PID controller performance, some data are listed in Table 2. Here, the control error result e_{ck} is compared between cases with and without sensor faults in Figure 7a. Moreover, the superior performance of the proposed SFTC compared with the traditional tracking controller PID is evidenced by the difference between the control error e_{ck} without SFTC and the control error e_{ck} with SFTC, which is described in Table 2 and displayed in Figure 7a,b. The error performance $p_{e_{ckmax}}$ of the PID controller with the SFTC averaged about 98.258% from 0.2 s to 9 s, whereas it averaged about 27.785% without the SFTC (Table 2). In contrast, the control error barely changed from 9 s to 15 s, even though there were fewer errors with the SFTC. This can be explained by the fact that the compensation process is executed in the second step of two adjacent steps. Therefore, signals with a vertical direction change will not be performed for compensation, as can be seen in Figure 5a,b at time 10 s.

Table 2. The error assessment e_{ckmax} with disturbance $d_k = 0$.

The Requirement Content	Without SFTC		With SFTC	
	e_{ckmax} (mm)	$p_{e_{ckmax}}$ (%)	$ftc_{e_{ckmax}}$ (mm)	$p_{e_{ckmax}}$ (%)
From 0.2 s to 5 s	1.194	20.67	0.0194	98.06
From 5 s to 9 s	0.6074	34.9	0.0149	98.51
From 0.2 s to 9 s	1.194	27.79	0.0194	98.26
From 9 s to 15 s	0.7511	24.89	0.7515	24.50

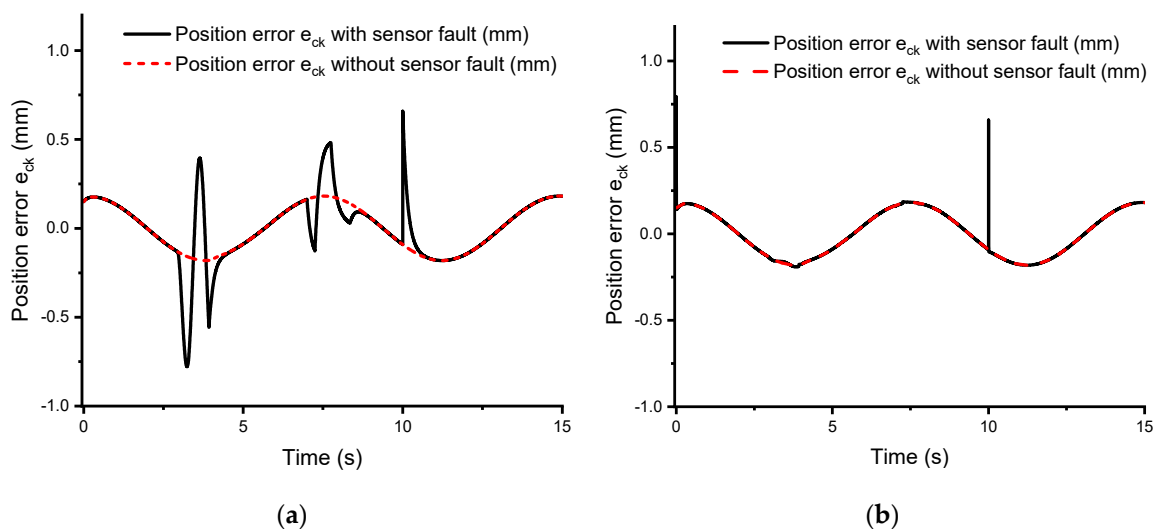
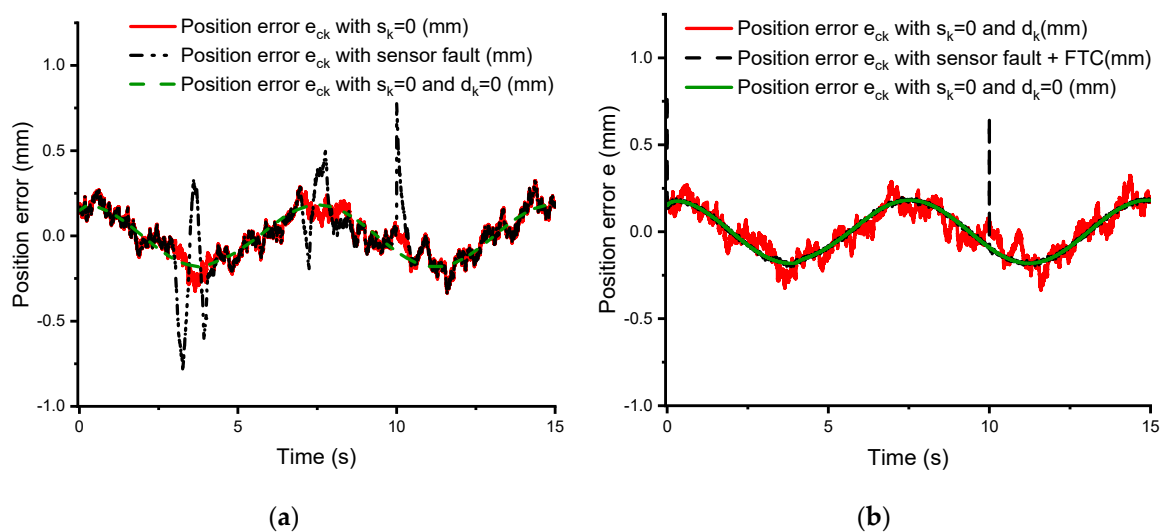


Figure 7. The position control error e_{ck} for the case without disturbance d_k of (a) without SFTC, and (b) with SFTC.

Table 3 summarizes the position control error e_{ckmax} of the PID controller under an unknown input disturbance d_k condition, with and without SFTC. In the case with disturbance d_k , from 0.2 s to 9 s, the average performance of the PID controller decreased by 0.83% (from 27.79% to 26.96%) without an SFTC and by 26.5% (from 98.26% to 71.76%) with an SFTC due to the effect of the disturbance. The PID controller performance was strongly decreased, from 24.89% to -11.88%, from 9 s to 15 s without an SFTC and from 24.50% to 13.46% with an SFTC (Figure 8a,b).

Table 3. The error assessment e_{ckmax} using a PID controller with disturbance d_k .

Content	Without SFTC				With SFTC			
	$d_k=0$		With d_k		$d_k=0$		With d_k	
	e_{ckmax} (mm)	$P e_{ckmax}$ (%)	e_{ckmax} (mm)	$P e_{ckmax}$ (%)	$ftc e_{ckmax}$ (mm)	$P e_{ckmax}$ (%)	$ftc e_{ckmax}$ (mm)	$P e_{ckmax}$ (%)
From 0.2 s to 5 s	1.1940	20.67	1.1181	25.46	0.0194	98.06	0.3961	73.60
From 5 s to 9 s	0.6074	34.9	0.7154	28.46	0.0149	98.51	0.3003	69.97
From 0.2 s to 9 s	1.1940	27.79	1.1181	26.96	0.0194	98.26	0.3961	71.76
From 9 s to 15 s	0.7511	24.89	1.1188	-11.88	0.7515	24.50	0.8654	13.46

**Figure 8.** The position control error e_{ck} with disturbance d_k of (a) without SFTC, and (b) with SFTC.

5. Conclusions

In this paper, an advanced SFTC technique is developed for a class of nonlinear discrete-time systems. This technique is successfully applied to control the position of an MMP system with sensor faults and an unknown input disturbance. The developed control technique, including SFs and system disturbances, is first estimated using the UIO and an LMI optimization algorithm. The estimated signals are utilized to generate compensation control to overcome the control challenges. By using the proposed SFTC, the system output follows the desired trajectory very well, even under the disturbed environment and concurrent sensor faults. Simulations are carried out to demonstrate the superior performance of the proposed SFTC technique over the traditional control method without fault-tolerant control features, as summarized in Table 2. With the SFTC technique, the control performance is determined to be 98.26% for the case without disturbance d_k and 71.76% for the case of disturbance d_k , as shown in Table 3. In future work, practical experiments with the developed rig will be carried out to confirm the applicability of the developed SFTC approach in real-time.

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