

## Article

# Characterization of Poly(Ethylene Oxide) Nanofibers—Mutual Relations between Mean Diameter of Electrospun Nanofibers and Solution Characteristics <sup>†</sup>

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**Abstract:** The quality of electrospun poly(ethylene oxide) (PEO) nanofibrous mats are subject to a variety of input parameters. In this study, three parameters were chosen: molecular weight of PEO (100, 300, 600, and 1000 kg/mol), PEO concentration (in distilled water), and shear viscosity of PEO solution. Two relations free of any adjustable parameters were derived. The first, describing the initial stage of an electrospinning process expressing shear viscosity using PEO molecular weight and concentration. The second, expressing mean nanofiber diameter using concentration and PEO molecular weight. Based on these simple mathematical relations, it is possible to control the mean nanofiber diameter during an electrospinning process.

**Keywords:** electrospinning; poly(ethylene oxide); nanofiber diameter; molecular weight; concentration

## 1. Introduction

At present, nanofibrous mats are efficiently used in many applications: filters, tissue engineering, drug delivery systems, antibacterial wound dressing, protective clothing, nanocomposite materials, to name a few. One of the ways one can produce nanofibrous mats is through the process of electrospinning. In this process, polymer solution or melt is exposed to a high-voltage electric field (in orders of tens kV) under which viscoelastic polymer jets emanate from so-called Taylor cones [1] formed at the polymer surface. After passing approximately 10–20 cm in length, the material of the jets (after evaporation of a solvent) is cumulated on an earthed collector [2–4] at the shape of individual nanofibers forming a non-woven textile.

The problem is that some promising materials, such as chitosan, keratin, and other protein-based materials, cannot be electrospun in their pure forms. This contrasts with the easy spinnability [5,6] of, e.g., poly(ethylene oxide) (PEO). Fortunately, even the negligible presence of PEO (up to 2%) in solutions of the above-listed materials completely changes their disposition to being electrospun (see below). Intensive study of PEO behavior during the electrospinning process has been undertaken due to this fact and because of the excellent biodegradability, biocompatibility, and non-toxicity. These attributes also reflect PEO nanofiber applications in biomedicine and the food industry [7–10] apart from the above already mentioned improvements in spinnability in combination with chitin or chitosan [11–14], keratin [15,16], silk [17,18] and other materials.

As in any electrospun material the resulting properties of PEO nanofibrous mats are subject to four groups of entry parameters: the polymer (molecular weight, molecular weight distribution, topology of macromolecules), solvent (surface tension, solubility parameters, relative permittivity), solution (viscosity, concentration, specific conductivity), and process parameters (electric field strength, tip-to-collector distance, temperature, humidity). In no way can these parameters be analyzed separately as many of them are mutually interlaced as can be documented, for example, in the case of molecular weight, concentration, and viscosity.

The whole process of electrospinning is so complex that there is no possibility to express the behavior of one parameter—e.g., a mean nanofiber diameter—through the remaining ones. This can be documented by a relatively complicated process of nanofiber formation starting from an initial straightforward stable motion of liquid material towards a collector, consecutively changed to a ‘whipping’ (unstable, chaotic) motion, and finally, after solvent evaporation, converting to solid nanofibers. Therefore, there is a necessity to choose a limited number of crucial parameters that participate in the setting of a nanofiber diameter and fixing of the others.

Experimentally this approach was applied to determine the dependence of a mean nanofiber diameter on polymer concentration [19–28], on applied voltage [22–26,28,29], on viscosity [20,21], on solution flow rate [22,23,25,26,29], on tip-to-collector distance [22–24,30], on addition of salts [24,29], on the composition of the mixed solvent [31], on elasticity of the solution [32], on addition of nanoparticles [33,34], on addition of polyelectrolyte [35].

Electrospinning is a complex phenomenon to analyze because of the coupling between the electric field and the deformation of the fluid, the latter, in turn, determined by the rheology of the material [36]. The first theoretical approach in describing the process where electrospinning starts with a Taylor cone, passes through both regions (straightforward and spiraling) of viscoelastic jet, and then up to the deposition of nanofibers onto a collector, appeared approximately two decades ago. The beads–spring model (not to be confused with the appearance of unwanted beads violating the straight geometry of final nanofibers) was presented in [37]. A list of this and other models [38–46] describing the flow behavior of electrified and electrospun viscoelastic jets is introduced in [2].

The authors in [44] concluded that a final nanofiber diameter can be determined from knowledge of the flow rate, electric current, and the surface tension of the fluid. In [27], the authors present the independence of an initial straight jet diameter on solution concentration and indicate that a mean nanofiber diameter depends dominantly on the jet-whipping process. In [47], the authors applied the theoretical modeling in [42,43] and stated that the final diameter also depends on the initial diameter of a jet. They classify the importance of 13 entry parameters with respect to their influence on a mean nanofiber diameter and sort them into three groups: strong, moderate, and minor. The model involving solution viscosity, evaporation rate, and containing specific charge (electric current divided by the spinning throughput) was introduced in [48,49]. A prediction of a final nanofiber diameter published in [50] is based on the model published in [36]. However, the assumptions limit the model to relatively low polymer–solvent concentrations (<12 wt.%). A determination of the final nanofiber diameter considers solution flow rate, applied voltage, and polymer concentration.

Applicability of the electrospun nanofibrous mats (filters, membranes, etc.) is closely related to their permeability. Hence, the passage of the particles through the mats can also be controlled by molecular weight and concentration of a polymeric material used in the process of electrospinning. The standard experiments providing mean nanofiber diameters and shear viscosity dependent on molecular weights and used concentrations of polymeric material are time-consuming, with higher financial costs and cover only discrete values of entry parameters.

This contribution aims to propose the relations mutually relating three entry parameters (PEO molecular weight, PEO concentration, shear viscosity of PEO solution) and a resulting mean nanofiber diameter. In contrast to the experiments, these relations cover continuously and sufficiently broad regions of entry parameters creating the possibility of achieving a required mean nanofiber diameter.

The proposed relations are compared with the experiments (four various PEO molecular weights), and the mean deviations are practically within the experimental errors.

## 2. Materials and Methods

### 2.1. Materials

Four various poly (ethylene oxide) (Sigma Aldrich, Saint Louis, MO, USA) batches differing in molecular weight (100, 300, 600, and 1000 kg/mol) were consecutively dissolved in distilled water at different concentration ranges (introduced in Table 1) meeting successful spinnability (subjected to a molecular weight) of the PEO solutions. The PEO solutions were prepared using a magnetic stirrer (Heidolph MR Hei-Tec, Schwabach, Germany) with the help of a Teflon-coated magnetic cross applied for 48 h under constant conditions (mixing rate 250 rpm and temperature 25 °C).

**Table 1.** A list of prepared poly(ethylene oxide) (PEO) solutions.

Molecular Weight (kg/mol)	Concentration (wt.%)
100	12, 15, 20, 22, 24, 28, 30, 34
300	5, 7, 8, 9, 10, 11, 12, 13, 15, 17
600	3, 5, 5.4, 6, 7, 8, 9
1000	3, 3.3, 3.75, 4, 5, 6

### 2.2. Rheological Characterization

Shear viscosity of the individual PEO solutions was determined at a constant temperature of 25 °C using a Physica MCR 501 device (Anton Paar, Graz, Austria) equipped with concentric cylinders (26.6/28.9 mm-inner/outer diameters). Each measurement was repeated at least three times with very good reproducibility.

### 2.3. The Electrospinning Process

Laboratory equipment consisting of a high voltage power supply (Spellman SL70PN150, Hauppauge, NY, USA), a carbon steel stick (10 mm in diameter) with a hollowed semi-spherical pit at the end for polymer filling, and equipped with a motionless flat metal collector (for details see [51]) was used for an electrospinning process. The drop of polymer solution filling the pit contains approximately 0.2 mL in volume, a tip-to-collector distance was fixed (20 cm) as well as nearly constant ambient conditions (temperature  $23 \pm 1$  °C, relative humidity  $41 \pm 1\%$ ). Good quality of electrospun mats (elimination of appearance of web blobs) was ensured by a gradual voltage decrease from 25 kV fixed for  $M_w = 100$  kg/mol to 12 kV fixed for  $M_w = 1000$  kg/mol.

### 2.4. Nanofibrous Mat Characterization

A high-resolution scanning electron microscope (SEM) Vega 3 (Tescan, Brno, Czech Republic) was used for imaging of nanofibrous mats after their sputtering with a conductive layer to improve conductivity.

## 3. Results and Discussion

Due to a non-negligible number of entry parameters, the process of electrospinning cannot be simultaneously analyzed from all material, geometrical, and process aspects. It is always necessary to fix a substantial majority of entry parameters and concentrate on a moderate number of selected parameters. The impacts of the individual parameters are usually interlaced, and in the following analysis, we will pay attention to a mutual interplay between PEO molecular weight, PEO concentration, viscosity of a PEO solution in distilled water, and a mean diameter of the resulting nanofibers.

Specifically, the emphasis will focus on the derivation of two dependencies:

(1) A determination of functional relation between shear viscosity ( $\eta$ ), PEO concentration ( $c$ ), and PEO molecular weight ( $M_w$ );

(2) A determination of functional relation between the diameter of nanofibers ( $dia$ ), PEO concentration ( $c$ ), and PEO molecular weight ( $M_w$ ).

From the viewpoint of easy and clear applicability of the proposed relations, they should exhibit the following attributes:

(a) Usage of elementary algebraic functions only;

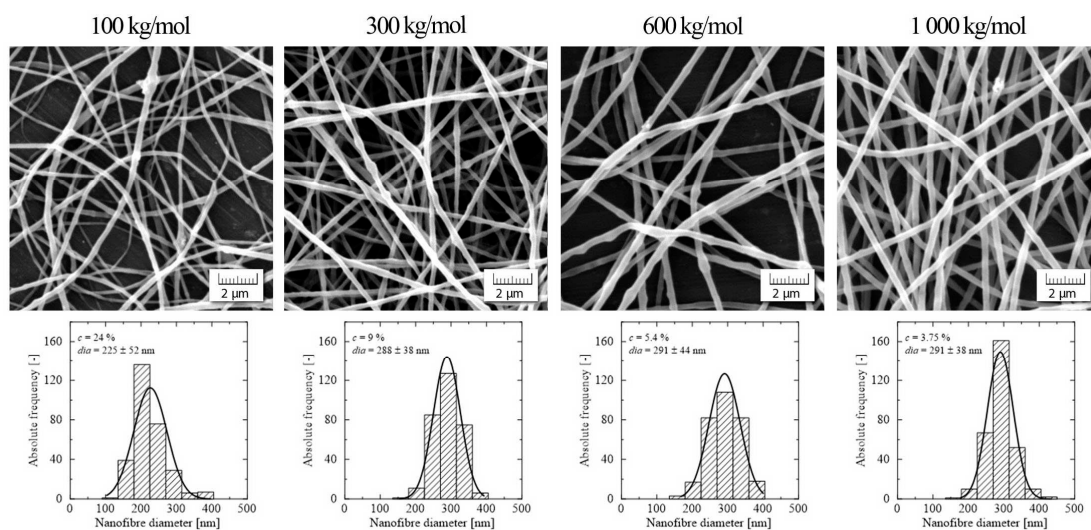
(b) Absence of adjustable parameters;

(c) Their validity should cover sufficiently broad regions of two entry material characteristics—PEO molecular weight and PEO concentrations in distilled water (a range of concentrations shifts with respect to successful electrospinnability of PEO solutions dependent on  $M_w$ );

(d) The correctness of the approximate relations-deviations of their predictions from the experimental data should potentially exceed the experimental errors only moderately.

The least accurate determination of a precise value out of the four studied parameters ( $M_w$ ,  $c$ ,  $\eta$ ,  $dia$ ) is represented by the mean nanofiber diameter  $dia$ .

A mean nanofiber diameter derived from 300 measurements taken from three different images was determined by applying the Adobe Creative Suite software (San Jose, CA, USA). Figure 1 displays SEM images of PEO nanofibers created from various molecular weights at different concentrations. The histograms attached to the individual molecular weights depict a variance of nanofiber diameters. This is also documented in Table 2.

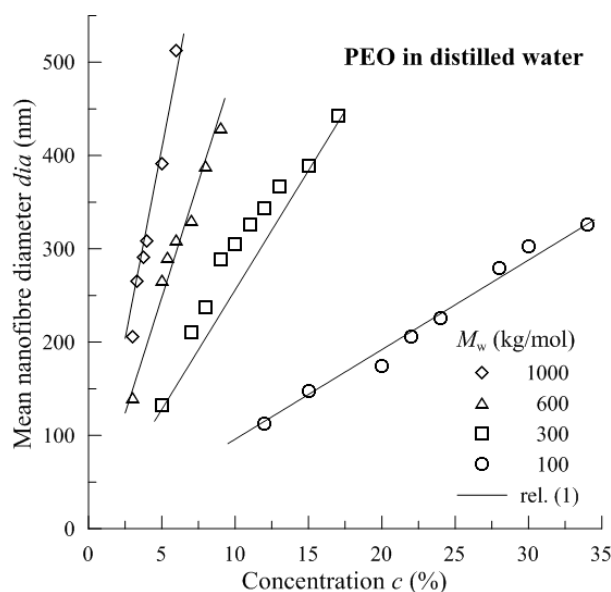


**Figure 1.** SEM pictures of nanofibrous mats for different poly(ethylene oxide) (PEO) solutions:  $M_w = 100$  kg/mol,  $c = 24\%$ ;  $M_w = 300$  kg/mol,  $c = 9\%$ ;  $M_w = 600$  kg/mol,  $c = 5.4\%$ ;  $M_w = 1,000$  kg/mol,  $c = 3.75\%$ . The corresponding histograms describe the variance of nanofiber diameters.

**Table 2.** Variance of the measured nanofiber diameters.

$M_w$ (kg/mol)		Dispersion of Nanofiber Diameters									
100	$c$ (wt.%)	12	15	20	22	24	28	30	34		
	$dia$ (nm)	113 ± 34	147 ± 33	174 ± 52	206 ± 49	225 ± 52	279 ± 56	303 ± 40	326 ± 43		
300	$c$ (wt.%)	5	7	8	9	10	11	12	13	15	17
	$dia$ (nm)	132 ± 26	210 ± 46	237 ± 44	288 ± 38	305 ± 48	326 ± 41	344 ± 47	367 ± 42	389 ± 53	442 ± 46
600	$c$ (wt.%)	3	5	5.4	6	7	8	9			
	$dia$ (nm)	141 ± 30	267 ± 42	291 ± 44	310 ± 44	331 ± 43	389 ± 28	430 ± 46			
1000	$c$ (wt.%)	3	3.3	3.75	4	5	6				
	$dia$ (nm)	206 ± 35	265 ± 29	291 ± 38	308 ± 49	391 ± 52	513 ± 75				

After analyzing and processing the experimental data obtained by consecutive electrospinning of PEO solutions differing in PEO molecular weight (100, 300, 600, and 1000 kg/mol) and concentration (see Table 2), we can calculate the correlation coefficients for the experimental data sets ( $c$ ,  $dia$ ). Their proximity to one (pure linearity behavior, see Table 3) indicates the possibility to approximate a mutual dependence of the mean nanofiber diameter on the concentration by a simple linear relation. To unify this approach, it is also necessary to express a general coefficient of linearity through the values of PEO molecular weights, which results in a slight deviation from the optimized values for the individual molecular weights.



**Figure 2.** Dependence of mean nanofiber diameter ( $dia$ ) on concentration ( $c$ ) and molecular weight ( $M_w$ ).

**Table 3.** Correlation coefficients between ( $c$ ,  $dia$ ) and ( $\log(c)$ ,  $\log(\eta)$ ).

$M_w$ (kg/mol)	Correlation Coefficient [-]	
	( $c$ , $dia$ ) Figure 2	( $\log(c)$ , $\log(\eta)$ ) Figure 4
100	0.992	0.996
300	0.980	0.998
600	0.987	0.997
1000	0.992	0.942

Finally, we propose the following relation

$$dia = (a_1 M_w + a_2) \times c \quad (1)$$

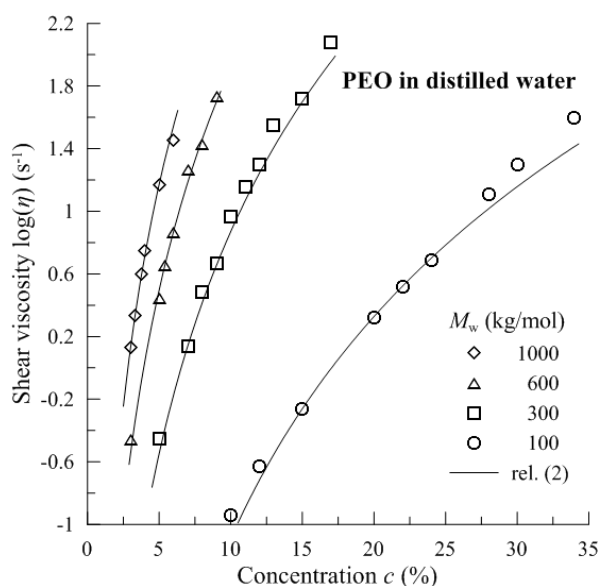
with a linear proportionality between the mean nanofiber diameter and concentration, and with a linear dependence between the mean nanofiber diameter and molecular weight. The numerical values of the constants are  $a_1 = 0.00008$  and  $a_2 = 1.6$ . The correspondence between the experimental and predicted data is depicted in Figure 2, with the mean deviation attaining 6.7%. Relation (1) complies with the tendencies introduced in literature [52,53], i.e., an increase in the nanofiber diameter both with increasing molecular weight and increasing concentration.

Dependence between shear viscosity, molecular weight, and concentration is a little more complicated. If we apply an analogous approach to that above, we obtain the correlation coefficients for the data sets ( $\log(c)$ ,  $\log(\eta)$ ), again in close proximity to one (see Table 3). It justifies the proposal of

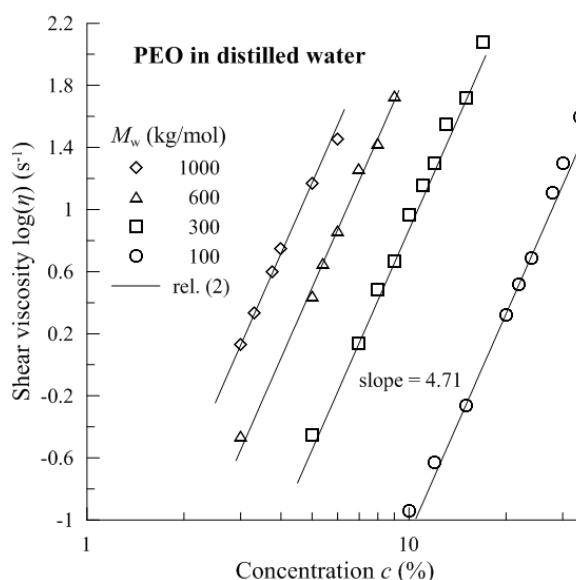
a linear relation between  $\log(c)$  and  $\log(\eta)$ . Unifying both a slope and an intercept with respect to the range of PEO molecular weights, a proposed relation is still algebraically simple.

$$\log(\eta) = b_1 \times \log(c) + [b_2 \times (\log(M_w))^2 + b_3 \times \log(M_w) + b_4], \quad (2)$$

where  $b_1 = 4.71$ ,  $b_2 = -0.82$ ,  $b_3 = 12.7$ ,  $b_4 = -48.8$ . As can be seen, Relation (2) is composed of two separate members, the first one expressing a contribution of concentration only and the second one (in brackets) representing the participation of molecular weight exclusively. Figure 3 documents the courses of the proposed predicted curves attaining a mean deviation of 6.3% in the semi-log coordinates (concentration-linear, shear viscosity-logarithmic), in fully linear coordinates, a mean deviation attained 11.8%. In the log–log coordinates (Figure 4), there is a linear dependence of shear viscosity on PEO concentration with the fixed slope attaining a value of 4.71.



**Figure 3.** Dependence of shear viscosity ( $\log(\eta)$ ) on concentration ( $c$ ) and molecular weight ( $M_w$ ) in semi-log coordinates.



**Figure 4.** Dependence of shear viscosity ( $\log(\eta)$ ) on concentration ( $c$ ) and molecular weight ( $M_w$ ) in log-log coordinates.



#### 4. Conclusions

The introduced relationships propose a hint as to which way the geometrical arrangement of the resulting electrospun nanofibrous mats can be modified. Based on the relatively simple functional Relation (1), it is possible to alter a mean nanofiber diameter by a suitable choice of PEO material (choice of an adequate molecular weight) and setting a corresponding concentration. Relation (2) characterizes the mutual interplay between three input parameters: molecular weight, concentration, and shear viscosity. Both Relations (1) and (2) are valid for the processed material-PEO-solved in distilled water. However, it can be expected that the analogous relations could also be derived for other combinations of polymers and solvents.

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