



Article Chromium Distribution, Leachability and Speciation in a Chrome Plating Site

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Abstract: Hexavalent chromium (Cr(VI)) waste produced by chrome plating activities pollutes the surrounding environment and harms human health. However, information about the chromium (Cr) pollution characteristics of actual electroplating sites is still lacking. In this study, the concentration, leachability and speciation of Cr in soils from a typical chrome plating site were analyzed. Our results showed that this site was severely contaminated by Cr (7.2 to 7735.2 mg/kg) and Cr(VI) reached the mean concentration of 138.7 mg/kg. The spatial distribution of Cr(VI) was related to the plating processes. Chrome plating and sewage treatment areas could be considered as the hot spots of contaminated sites. The vertical distribution of Cr(VI) was mainly affected by soil properties, where the loam layer retained and reduced a large amount of Cr(VI) due to its high content of iron minerals and finer particle fractions. Additionally, the chemical extraction results showed that Cr was mainly in non-residual fractions and the existence of Cr(VI) led to a high leaching toxicity based on the toxicity characteristic leaching procedure (TCLP) results. Moreover, X-ray photoelectron spectroscopy (XPS) results revealed the speciation of Cr in the long-term contaminated soils. A large amount of Cr(VI) was reduced into Cr(III) and mainly existed as Cr(OH)₃ and Cr₂O₃. Furthermore, Cr(VI) tended to precipitate as CaCrO₄ and persisted in soils. Therefore, it is necessary to find appropriate strategies to remediate these contaminated soils. Overall, these findings strengthen our understanding of Cr(VI) behaviors and lay a foundation for the future pollution investigation, ecological remediation and risk assessment of sites contaminated by electroplating.

Keywords: hexavalent chromium; chrome plating site; pollution distribution; leachability; speciation

1. Introduction

Chromium (Cr) is a common element in nature, which mainly comes from natural geologic and anthropogenic sources [1,2]. Serpentine soils are considered as the most important natural source of Cr [3]. In non-serpentine soils, the high Cr concentration is mainly attributed to anthropogenic activities, such as electroplating, steel and automobile manufacturing, leather tanning and wood preservation [4–6]. The oxidation states of Cr range from divalent Cr(II) to hexavalent Cr(VI), but the common forms in soil are Cr(VI) and trivalent Cr(III) [7,8]. These states exhibit different chemical reactivities and toxicities [9,10]. Cr(III) is dominant in reducing conditions, has a low solubility and prefers to strongly sorb onto reducing substances [2,6]. Cr(VI) is highly mobile in soil and it mainly exists as oxyanions, such as CrO_4^{2-} , HCr O_4^{-} and $Cr_2O_7^{2-}$ [11]. Due to its mutagenicity, carcinogenicity and teratogenic effects, Cr(VI) has been listed as one of the priority control pollutants by many countries and organizations [12]. Chromate, the main form of Cr(VI) compound, is commonly used in the electroplating industry [2,3]. Waste containing Cr(VI) is discharged from electroplating activities, especially chrome plating processes, which results in serious soil contamination [13,14].



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With rapid industrialization, the electroplating industry has developed tremendously and there are more than 20,000 chrome plating process parks and workshops in China [15]. A growing number of studies have focused on the sources, compositions and pollution degrees of contaminated soils near electroplating plants [16–18]. Previous studies reported that the soil contaminated by electroplating had the characteristics of polymetallic pollution, of which Cr pollution was the most significant [2,16]. The Cr pollution level was relevant to the distance from and number of surrounding electroplating plants, as reported by Lin et al. [19] and Xiao et al. [16]. Electroplating activities can pollute the surrounding soil in many ways, including the leaking of plating solution, discharging of wastewater and stacking of electroplating sludge [16,20]. Additionally, contaminated soil generally has significant Cr(VI) concentrations with high carcinogenic risks [21,22]. Due to its high mobility, Cr(VI) can migrate into unsaturated zones and even be transported into groundwater, resulting in severe environmental pollution [5,23]. However, most previous studies have just focused on the Cr concentration in topsoil and have paid little attention to Cr(VI) and its vertical migration characteristics. Limited by time and space scale, it is difficult to accurately simulate the vertical migration of Cr(VI) in soil under laboratory conditions. Additionally, in situ remediation strategies have been largely performed in contaminated soil and the premise of this study is to determine the migration range of pollutants [24]. Therefore, it is necessary to study the vertical distribution of Cr(VI) in an actual electroplating site in order to clarify the migration characteristics of Cr(VI), which is of utmost importance to pollution remediation.

The chemical speciation of Cr is important for evaluating the leachability and environmental risk linked with Cr contaminated soil [1,25,26]. Species transformation often occurs during Cr(VI) migration, which is complicated in natural soil environments [27,28]. Soil properties, such as pH, particle size, organic matter and clay minerals, can influence the geochemical behaviors of Cr by controlling its speciation [29–31]. Generally, Cr(VI) is considered to be available because it usually sorbs to oxide surfaces, predominantly as the outer-sphere complexes or weak inner-sphere complexes in soil [31,32]. Most Cr(VI) is commonly reduced by reducing substances (e.g., clay minerals, organic matter, microorganisms) and converted into less mobile and toxic Cr(III) in soil [33,34]. However, Cr(VI) can also be distributed in stable fraction via precipitation and the recrystallization of soil [35,36]. Identifying the speciation of chromium in contaminated soil is a prerequisite for pollution remediation and risk assessment [35,37]. To the best of our knowledge, the speciation characteristics of Cr in actual soils contaminated by electroplating have not been studied in depth.

Various industries need chrome metal coatings to prevent corrosion and enhance physical properties [21,38]. The manufacturing processes of chrome plating are diverse and thereby make the soil pollution conditions more complicated. High-concentration chromic acid waste liquid is the main industrial waste from electroplating, which is different from other chromium pollution industries, such as chromium salt production and leather making, and which may cause the soil pollution to be different from other industrial sites in terms of availability and speciation. In this study, Cr contaminated soils from a typical abandoned electroplating site were collected in order to: (i) determine the concentration and distribution characteristics of Cr_T and Cr(VI) in the soil; (ii) assess the leachability and environmental risk of Cr in contaminated soil; and (iii) identify the speciation characteristics of Cr in contaminated soil. These results will help us to understand the geochemical behaviors of Cr(VI) in actual contaminated soils and also provide scientific information for risk assessment and pollution remediation.

2. Materials and Methods

2.1. Site Description

The study site is a chrome plating site located in an urban area of Hebei Province, with an area of 820.14 m² (Figure 1A). This area is covered with quaternary sediments and the soil is mainly loess. This electroplating site began operation in 2005 and closed

in 2015 and contained three workshops: an electroplating workshop; an electroplating laboratory; and a post-treatment workshop. The electroplating workshop was mainly used for hard chromium plating, decorative chromium plating and zinc plating. A small electroplating sewage tank of 8 m in length and 4 m in width also existed in this workshop. The preparation and testing of the plating solution were carried out in the electroplating laboratory. The post-plating treatment workshop was used for drying, packaging and storing raw materials. According to our previous site survey, the chromium pollution of soils in this area is obvious and the soil is alkaline, in which Cr(VI) exhibits a strong migration ability and high ecological risk [22,39].



Figure 1. The satellite image of study area (A) and the sketch maps of sampling points (B,C).

2.2. Sample Pretreatment

The soil sampling points in this study were set at six different electroplating process sections: the electroplating laboratory (S1); hard chromium plating (S2); decorative chromium plating (S3); zinc plating (S4); the sewage tank (S5); and the post-treatment process (S6) (Figure 1B). Based on the preliminary investigation, the soil was sampled at different equidistant points. As the soil in the top layer (0–1 m) was usually heavily polluted, the sampling interval was 0.2 m. In deeper soil, the chromium pollution might have abated, so the sampling interval correspondingly increased to 0.4 m (Figure 1C). Similar sampling methods have been used in previous studies [23]. The groundwater was buried below 60 m and was not found within our sampling depth range. All these soil samples were sealed in polyethylene plastic bags, stored in the dark and placed in a 4 °C refrigerator for subsequent analysis. The sample collection, storage and transportation were carried out in accordance with the Technical Guidelines for Site Environmental Investigation in China (HJ 25.1-2014). Stones, plant tissues and other dopants present in the soil samples were discarded before air-drying. After proper drying, all samples were crushed, homogenized and sieved through a 2mm sieve, and then prepared for further analysis.

2.3. Soil Characterization

A series of physical and chemical properties of the soil was measured. Soil pH was measured in a 1:2.5 soil:water (w/v) solution using a pH meter after 30 min of shaking.

Organic matter content was determined by the ignition loss method. Particle size analysis was determined using the pipette method and classified according to the USDA soil classification. Thermogravimetric analysis was conducted to determine the concentration of CaCO₃ in the soils using a thermogravimetric (TG, 209F3, Netsch, Germany). The mineralogical composition was determined by X-ray diffraction (XRD, D8 Advance, Bruker, Germany). According to the soil textural triangle [39], loam and sandy loam were the major textures of the soil, which were covered with a 0.5-m thick backfill soil layer. Detailed soil characteristics can be found in Table 1. The backfill soil contained construction waste and large-grain gravel, etc. The loam was mainly composed of fine-grained silt and had poor permeability. At the bottom, there were some large particles in the sandy loam, so its permeability was better than the loam layer.

After grinding the soil samples through a 100-mesh screen, uniform soil powders were obtained for heavy metal content and chemical speciation analysis. The Cr(VI) in the soil was extracted by alkaline digestion according to the US Environmental Protection Agency Method (EPA 3060A). After digestion, the extracted solution was filtered through a 0.22-µm filter membrane and the Cr(VI) concentration was determined by the by the 1.5 diphenylcarbazide spectrophotometric method using a UV-Vis spectrum (EPA Method 7196A). A given amount (0.2 g) of the soil samples was digested with HNO₃/HF/HCLO₄ (7:5:5, v/v/v) [40]. The total Cr, Zn and Cu in the digestion solution were analyzed by a flame atomic absorption spectrophotometer (FAAS, PinAAcle 900F, PerkinElmer, Singapore) after filtration and dilution. The mobility and leachability of Cr(VI) in the soil samples were determined using TCLP analyses (USEPA Method 1311).

2.4. Chemical Fraction and Speciation Analyses of Cr

We conducted Cr chemical fractions analysis on representative soils which came from different soil layers of three polluted points. Heavy metals in the soil were classified into the following five fractions using sequential extraction method carried out by Tessier et al. [41]: exchangeable fraction (F1); carbonate bound fraction (F2); Fe–Mn oxide bound fraction (F3); organic matter bound fraction (F4); and residual fraction (F5). A two-step sequential extraction method was used for the fractionation analysis of mobile Cr(VI) and immobile Cr(VI) in the soil [35,42]. The total concentration of the recovered Cr and Cr(VI) ranged from 91.8% to 118.2% and 83.5% to 103.6%, respectively, suggesting that these sequential extraction results were reliable. The chemical state of Cr was identified using X-ray photoelectron spectroscopy (XPS, Thermo Scientific K-Alpha, Waltham, MA, USA).

2.5. *Quality Assurance (QA) and Quality Control (QC)*

All reagents used in this study were analytical grade and purchased from Sinopharm Chemical Reagent Co., Ltd. Deionized water was used throughout the experiments. QA and QC were implemented using duplicates and regent blanks. All analyses were performed in triplicate under the same conditions and the standard deviations were less than 5.0%. We chose the optimum detection wavelength for elements when using atomic adsorption spectroscopy. The linearity was kept strong, with correlation coefficients > 99.9%, by preparing calibration curves with a series of concentrations (0.5 mg/L-4 mg/L). Additionally, the accuracy of the analytical procedure was checked by certified material GBW07449.

2.6. Statistical Analysis and Calculation

All statistical analyses were conducted with the IMB SPSS Statistics Ver 20.0 software and Excel 2010. The figures were generated using ArcGIS 10.5 and Origin Ver 9.0. The geo-accumulation index (I_{geo}) is a commonly used method to assess the severity of heavy metal contamination in soils [28,43,44]. This method was introduced by Muller [45] and can be defined as follows:

$$I_{geo} = \log_2 [C_n / (1.5 \times B_n)],$$
 (1)

where I_{geo} is the geo-accumulation index (soil contamination severity index) and Cn is the heavy metal content in soil. Bn is the average concentration of element in the

background rock sample, and we selected the local soil chromium content background value of 61.0 mg/kg. Pollution levels on the basis of the I_{geo} can be classified as (I) practically unpolluted (≤ 0), (II) unpolluted to moderately polluted (0–1), (III) moderately polluted (1–2), (IV) moderately to heavily polluted (2–3), (V) heavily polluted (3–4), (VI) heavily to extremely polluted (4–5) and (VII) extremely polluted (>5).

3. Results and Discussion

3.1. Total Concentration and Oxidation State of Chromium in Soils

The Cr_T and Cr(VI) contents of the soil samples are shown in Table 1. The results showed that the Cr_T concentrations of the soil ranged from 7.2 to 7735.2 mg/kg. The mean concentration of Cr_T in the soil was 948.2 mg/kg, which was more than 15 times higher than the background values for soils in China [46]. The pollution degree of this electroplating site appeared to be serious. The I_{geo} value ranged from 0.06 to 6.23, and six samples even reached the extremely polluted level (I_{geo} > 5) (Tables S1–S3). Chromic acid solution was the raw material used in the chrome plating activities and it could easily enter nearby soil by escaping, emitting, dripping and leaking during the production processes [21,47]. In this area, the average Cr(VI) concentration was 138.74 mg/kg, which significantly exceeded the China Environmental Quality Standards for Soils [48].

Comparisons with previous studies reveal that the Cr(VI) pollution caused by electroplating activities was lighter than that of chromite ore processing residue (4575–6530 mg/kg) [49] and chromate production (3120–7934 mg/kg) [50], but it was significantly more serious than that of leather tanning (51.5–144.2 mg/kg) [51] and wood preservation (ND– 70.7 mg/kg) [52]. These results illustrate that electroplating activities caused severe chromium pollution in the soil and might have affected the health of surrounding humans. In addition, the relatively high standard deviation values reflect that the chromium concentration varied among the different sampling points and soil depths.

Table 1. The basic statistical parameters of the soil chromium contents in the electroplating site.

Sampling Points	S 1	S2	S 3	S 4	S 5	S 6	S 1	S2	S 3	S 4	S 5	S 6	Deferrere
	Total Cr (mg/kg)						Cr(VI) (mg/kg)						Kererences
Mean	18.0	98.4	4081.2	19.2	523.0	20.9	0.3	29.5	763.7	0.3	38.5	0.7	(In this study)
Median	12.9	87.4	3855.9	15.0	114.5	21.1	0.1	25.0	356.6	0.3	20.9	0.2	
Min	7.2	42.1	33.4	8.2	42.2	ND	ND	5.2	32.4	ND	6.5	ND	
Max	33.6	164.1	7735.2	39.5	3178.2	26.9	1.1	80.1	2298.2	1.0	163.5	2.0	
StDev ¹	10.1	42.8	3100.6	13.2	980.4	4.1	0.5	23.9	880.9	0.3	49.0	0.8	
OSR (%) ²	-	80.0	80.0	10.0	70.0	-	-	50.0	100.0	-	30.0	-	
BVSC ³	61.0					-						[46]	
SRSD ⁴	-						30.0					[48]	

¹ StDev: Standard deviation. ² OSR: Over-standard rate. ³ BVSC: Background values for soils in China. ⁴ SRSD: Soil environmental quality risk control standard for the soil contamination of development land (GB36600-2018).

Detailed soil characteristics can be found in Table 2. According to the soil textural triangle [53], loam and sandy loam were the major textures of the soil, which were covered with a 0.5-m thick backfill soil layer. The backfill soil contained construction waste and large-grain gravel, etc. The loam was mainly composed of fine-grained silt and had poor permeability. At the bottom, there were some large particles in the sandy loam, so its permeability was better than the loam layer. Additionally, the backfill soil and the loam layer contained more iron minerals, based on the XRD results shown in Figure S1. The soil in this area was alkaline and the pH > 8.0 at all soil layers, with significant CaCO₃ levels present. CaCO₃ could increase the soil pH and reduce the availability of heavy metals [54]. Such an alkaline condition was conducive to the transport of Cr(VI), as the adsorption and reduction processes were inhibited [55]. However, an obvious decrease in soil pH values can be observed and shows a significant negative relationship with Cr(VI) concentration (r = -0.817, p < 0.01) (Tables S1–S3). This phenomenon was mainly attributed to the acid electroplating effluent, and similar results were also found by Xiao [16] and Bedbabis [56].

The acidification tended to cause more positive charge on the soil particle surface, thereby enhancing the Cr(VI) retention, as reported in other studies [39,57]. Furthermore, the $CaCO_3$ content also decreased with the Cr accumulation, especially at the most polluted sampling point S3 (Tables S1–S3). Therefore, electroplating activities also caused the acidification of the soil and the loss of $CaCO_3$, which might have affected Cr behaviors in the soil.

Soil Layers	Depth		рН	ОМ	CaCO ₃	Permeability Coefficient		
	m	2~0.05 mm	0.05~0.002 mm	<0.002 mm	-	%	%	cm/s
Backfill soil	0~0.5	-	-	-	8.56	0.46	9.83	-
Loam	0.5~2	33.78%	44.04%	22.18%	8.43	0.34	8.62	$8.59 imes 10^{-7}$
Sandy loam	>2	54.01%	30.75%	15.25%	8.65	0.45	7.00	$1.56 imes 10^{-4}$

Table 2. The physicochemical properties of the soil layers at this chrome plating site.

To sum up, electroplating activities caused serious soil chromium pollution and changes in soil properties due to the insufficient anti-seepage measures. Although most of the Cr(VI) had been reduced into Cr(III) (>80%), the proportion of Cr(VI) to Cr_T at this site was larger than that at other chromium contaminated sites [16,21,51]. The toxicity and environmental risks cannot be neglected. Furthermore, the Cr(VI) contents varied in different soil samples. Therefore, investigating the distribution of Cr(VI) in both spatial and vertical aspects is essential for future remediation and risk control.

3.2. Spatial and Vertical Distribution Characteristics of Chromium in Soils

Figure 2 compares the concentrations of Cr_T and Cr(VI) in the soils from the different sampling points. Relatively high Cr(VI) was observed in the electroplating workshop, where the Cr(VI) values in the soils of hard chromium plating (HCP), decorative chromium plating (DCP) and sewage tank (ST) ranged from 5.2 to 80.1 mg/kg (S2), from 32.4 to 2298.2 mg/kg (S3) and from 6.5 to 163.5 mg/kg (S5), respectively (Figure 2a). In contrast, Cr(VI) occurred at much lower concentrations in the soils from S1, S4 and S6. Cr_T presented similar characteristics as Cr(VI) in terms of distribution (Figure 2b). It was heterogeneously distributed in this contaminated area and concentrated in those processes that directly involved the use and collection of Cr(VI), as previous studies reported [58–60]. Contrasting with the two plating points S2 and S3, most of the Cr(VI) had been converted to Cr(III) before it leaked into the soil during the sewage treatment processes [61], therefore the Cr(III) species was dominant at S5. Additionally, obvious Zinc (Zn) and cooper (Cu) concentrations were detected in the soils at S3, S4 and S5 (Figure 2c,d). Cu is usually used as the intermediate coating in DCP processes or/and as the metal matrix in Zinc plating processes [62,63]. The sewage tank collected all wastewater produced during the electroplating activities, so the nearby soil had polymetallic pollution characteristics. Therefore, the chromium distribution in an actual electroplating site was related to the specific manufacturing processes and was accompanied by the characteristics of polymetallic enrichment. The chrome plating and sewage treatment areas could be considered as the hot spots of the contaminated site.

The Cr_T and Cr(VI) contents in the contaminated soils at various depths are shown in Figure 3. Cr(VI) could be still detected in the bottom samples at S2, S3 and S5 (80.1, 32.4 and 21.8 mg/kg, respectively), indicating the deeper pollution range and higher vertical diffusion of Cr(VI) compared to other contaminated sites [21,49]. As for the vertical aspect, the soil chromium pollution was closely related to the soil layers. The pollutants firstly tended to concentrate in the surface layer of the backfill soil and then accumulate to a certain level, in line with previous site studies [23,60,64]. There was a certain degree of Cr(VI) accumulation within the loam layer (0.5–2 m in depth) and it even reached the highest concentration of 2298.2 mg/kg (Figure 3b). On the contrary, the Cr(VI) content

in the sandy loam layer was much lower than the other two soil layers. Cr(III) occurred at various depths and exhibited similar distribution characteristics to Cr(VI) (Figure 3). Cr pollutants produced by electroplating were mainly in the Cr(VI) form, and the Cr(III) contents could reflect the reduction ability of the soil [34,39]. Cr(VI) accounted for 3.8% to 37.8% of the Cr_T in the loam layer, while it was the dominant species and just a small proportion of Cr(VI) (<30%) reduced into Cr(III) in the sandy loam layer. It was indicated that the reduction of Cr(VI) was also in various different soil layers. It was concluded that the vertical distribution of Cr and its specie interconversion was strongly influenced by soil properties.



Figure 2. The concentrations of heavy metals in the soils at the different sampling points. (a) Cr(VI), (b) Total Cr, (c) Cu and (d) Zn.



Figure 3. The vertical distribution of CrT and Cr(VI) in the soils at contaminated sampling point S2 (**a**), S3 (**b**) and S5 (**c**).

The loam layer made a great contribution to the retention and reduction of hexavalent chromium, as Figure 3 shows. It contained a relative proportion of clay fraction (<2 μ m),

with a permeability coefficient of 8.6×10^{-7} cm/s (Table 2). During downward migration, Cr(VI) could be hindered and retained by this layer due to its low permeability, which had been demonstrated both in a laboratory experiment [65] and in site surveys [66]. Moreover, the smaller sized particles had a larger cation exchange capacity, specific surface areas and clay component contents, which resulted in its greater Cr adsorption ability [67,68]. On the contrary, larger and more coarse particles were found in the backfill soil and the sandy loam layer. Cr(VI) can easily migrate downward under the eluviation of groundwater. Thus, the soil texture determined the vertical distribution of the pollutants to a certain extent. In soil, the potential interconversion between Cr(III) and Cr(VI) was dependent on the content of reduction substances [1,42]. The backfill soil and loam layer contained more clay minerals, especially iron minerals (Figure S1), which were main storage sinks for Cr, as well as main reducing agents contributing to the Cr(VI) transformation [34,69]. The content of soil organic matter, another main reduction substance, had relatively narrow gaps among these soil layers, so the effect of the organic matter on the difference between the soil layers was minimal. Furthermore, soil environmental variables, such as pH [6,55], redox potential (ORP) [57,69] and metal stress [21,24], may affect chromium behaviors in soil. In this study, pH played a non-negligible role in Cr(VI) distribution. As discussed in the above section, the soil acidification might have exaggerated the Cr(VI) retention.

At S3 and S5, Zn and Cu were detected at various depths and their vertical distributions were similar to Cr (Figure S2). The Pearson correlation analysis (Figure 4) shows that there were positive correlations among the concentration of Cr, Zn and Cu in the soil. The correlation coefficients found in the pairs of Zn–Cr(VI) (r = 0.758, p < 0.01) and Cu–Cr(VI) (r = 0.535, p < 0.05) were positive, where Zn showed better affinity with Cr(VI) than Cu. The coexisting heavy metals may promote or inhibit their adsorption in soil [70,71], which is closely related to the metal valence state, concentration, adsorption capacity and affinity in soil [70]. Some previous research reported that Cu could affect the adsorption and transformation of Cr(VI) in soil [70,71], while related studies on Zn are limited. It was concluded that the coexistence of multiple metals was an important characteristic affecting the Cr distribution in the soil, and the interaction mechanism is worthy of further investigation.



Figure 4. The correlation matrix analysis of the heavy metals in the soils (* = p < 0.05, ** = p < 0.01).

3.3. Leachability Characteristics and Mobility of Chromium in Soils

Besides the total chromium content, more information about heavy metal availability is necessary in order to estimate the potential risk. The toxicity characteristic leaching procedure (TCLP) has been widely used to evaluate the mobility of heavy metals in soil and to estimate their leachability and availability under acidic conditions (USEPA 1992). The Cr(VI) concentrations leached by TCLP were 0.2 to 58.9 mg/L (S2), 24.8 to 421.1 mg/L (S3) and 1.5 to 48.7 mg/L (S5), respectively (Figure 5b). The leaching concentrations of Cr_T were 0.3 to 63.3 mg/L (S2), 26.6 to 430.2 mg/L (S3) and 1.9 to 58.8 mg/L (S5), respectively (Figure 5a). These results show that Cr(VI) accounted for a high proportion of the total leached Cr, suggesting that Cr(VI) was the significant contributor to the pollution diffusion risk of the contaminated soil. Meanwhile, the availability of chromium at the DCP point (S3) was the highest because of the high Cr(VI) content in the soil. In addition, not only the Cr(VI) proportion of the total Cr but also the extracted rate of Cr(VI) (extracted Cr(VI)/total Cr(VI)) was the highest in the sandy loam layer. This means that Cr(VI) leached from contaminated soils has greater abilities to diffuse deeper in the bottom sandy loam layer. The leaching concentration of Cr(VI) in the 17 contaminated soils in this electroplating site appeared to have a high Cr(VI) diffusion risk and can serve as a potential source of Cr(VI) for the surrounding environment.



Figure 5. The contents of (**a**) total Cr and (**b**) Cr(VI) extracted by TCLP in contaminated soils at S2, S3 and S5.

We conducted sequential extraction to evaluate the mobility of Cr_T . The sequential extraction method divided the total heavy metal into five fractions: exchangeable fraction (F1); carbonate bound fraction (F2); Fe–Mn oxide bound fraction (F3); organic matter bound fraction (F4); and residual fraction (F5) (Figure 6). F5 was the most stable fraction and the relatively low proportion of F5 clearly indicated the higher mobile potential of Cr compared to other Cr contaminated sites [59,72]. F3 and F4 were the main fractions of Cr in the contaminated soils. Heavy metals in the fractions of F3 and F4 were unstable, and potentially mobile and bioavailable under certain environmental conditions [59,73]. F1 and F2 were considered as mobile fractions that can easily be released from the soil [6,27]. The percentage of Cr in the mobile portion (F1 and F2) was relatively high (>25%) in the sandy loam, which suggested a high diffusion risk in accordance with our TCLP results.



Figure 6. The chemical fractions of Cr(VI) (a) and total Cr (b) based on sequential extraction.

From the outset, Cr(VI) was the main pollutant and contributor to leaching toxicity. The results of the two-step sequential extraction show that mobile Cr(VI) accounted for only 24.2% to 38.3% of the total Cr(VI) in the backfill soil, 9.8% to 26.6% in the loam and 17.3% to 37.8% in the sandy loam, demonstrating that the majority of Cr(VI) in these soils was in the immobile fraction (Figure 6). Cr(VI) is toxic and highly mobile in soil [74], and while these results show that Cr(VI) was mainly distributed in a stable fraction, they were inconsistent with the hypothesis that Cr(VI) was easy to extract from soils [26,57]. The stable fraction of Cr(VI) in the long-term naturally contaminated soils has been reported and has attracted more attention [35,37]. Wisconsin et al. [75] found that only a small fraction (<10%) of the total Cr(VI) was extracted with a phosphate buffer in soils polluted by electroplating. Therefore, immobilization is also an important fate of Cr(VI) in soils contaminated by electroplating. Comparing the Cr(VI) concentrations, Cr(VI) leached by TCLP was higher than that extracted by the phosphate buffer solution, indicating that Cr(VI) in this stable fraction could be gradually leaching soluble Cr(VI) into the surrounding soil.

Overall, most of the Cr in the polluted soils of this electroplating site was present in the non-residual fraction and thus, had a greater risk of pollutant release and diffusion. Cr(VI) tended to be distributed in a stable fraction and be retained in soils. However, these stable fractions could also leak Cr(VI) and pollute surrounding areas into acidic environments.

3.4. Speciation Characteristics of Chromium in Soils

The speciation of heavy metals can demonstrate several important trends with respect to the mobility, release potentials and eco-toxicity of heavy metals [59,76]. Figure 7 displays the Cr 2p XPS spectra of the soil samples with a high Cr concentration. There were obvious

Cr peaks in the spectrum and Cr(III) accounted for a large proportion of the total Cr, which was consistent with our previous results. Cr(OH)₃ was the most stable species of Cr(III) and it accounted for the largest proportion, supporting the low mobility of Cr(III) in the soil. Cr₂O₃ was the second Cr(III) species, and a small amount of CrOOH also occurred in soil. Previous studies demonstrated that Cr(III) derived from the Cr(VI) reduction generally form surface complexes near the surface of organic matter and iron oxide [77,78]. In this study, a high proportion of Cr was distributed in the F3 and F4 fractions, which was probably due to the Cr(VI) reduction (Figure 6). Zhao et al. [79] also confirmed that the majority of Cr(VI) was first reduced to Cr(III) in soils, resulting in the content of F3 and F4 with increased time. At S2 and S3, F3 was the dominant Cr fraction in the loam layer (>80%), suggesting that Fe–Mn oxides were the main carriers of Cr in the loam layer. This result was related to the higher iron mineral content in the loam layer (Figure S1), which could have contributed to Cr reduction and accumulation in the loam layer.



Figure 7. The X-ray photoelectron spectroscopy Cr 2p spectra of the soil samples (**a**) S3-1, (**b**) S3-6, (**c**) S3-7 and (**d**) S5-2.

As for Cr(VI), it precipitates as moderately soluble CaCrO₄ (Ksp 7.1×10^{-4}), which was clearly identified in the XPS analysis (Figure 7) and accounted for a major proportion of the total Cr(VI). This explained the stable Cr(VI) fraction detected in the two-step sequential extraction (Figure 6). Similar results were found in naturally contaminated soils by Szecsody et al. [36], who proved the presence of CaCrO₄ in the vadose zone and aquifer sediments in Hanford, Washington. In soil, CaCO₃ could reduce the availability of heavy metals [80]. In this study, significant CaCO₃ content was detected, as Table 1 shows. We can speculate that CaCO₃ and Cr(VI) recrystallized to form CaCrO₄ crystals, resulting in the immobilization of Cr(VI) in the soil [81]. These results reflect that a certain proportion of Cr(VI) existed in a relatively fixed and stable form, especially in the severely contaminated soils.

We can concluded that most of the Cr(VI) discharged from the electroplating activities was reduced to Cr(III) and fixed in the soil. Immobilization as CaCrO₄ was an important fate of Cr(VI) at this actual electroplating site. However, the potential risk of pollution diffusion should not be neglected because the immobile fraction could dissolve and continuously release Cr(VI) slowly during long-term leaching activities [36]. Furthermore, this insoluble CaCrO₄ is recalcitrant and difficult to treat for the same reason that Cr(VI) incorporated in the calcite is hard to contact with reducing agents [81]. Therefore, CaCrO₄ precipitation was the main stable form of Cr(VI) in the soils, and more attention should be paid during the pollution remediation.

4. Conclusions

At this chrome plating site, the chromium distribution was associated with the electroplating processes. Soils from the chrome plating processes and the sewage tank area were contaminated by Cr(VI), with a high leaching toxicity. The coexistence of cationic metals (Cu and Zn) was also observed at some sampling points. The vertical distribution and migration of Cr(VI) were mainly affected by the soil properties, such as particle size and iron mineral content. Cr(VI) was mainly retained and reduced in the loam layer, and further accumulated in this layer reaching its maximum concentration. In the sandy loam layer, Cr(VI) reduction was limited and it was the dominant specie of Cr. Most of the Cr was distributed in the non-residual fraction, and the existence of Cr(VI) resulted in a high diffusion risk for the surrounding environment. Furthermore, long-term electroplating activities can cause Cr(VI) to persist in contaminated soil because most Cr(VI) is fixed in soil via precipitation as insoluble CaCrO₄. This study can provide more practical guidance for the future investigation and remediation of electroplating sites. The in situ remediation efficiency can be improved based on the distribution characteristics of Cr(VI) in contaminated sites. In contaminated calcareous soil, the formation of insoluble compounds is a significant fate of Cr(VI). Before reduction treatment, dissolving these precipitations can improve the reparation effect. Considering the diversity of electroplating activities, more actual site studies are needed to enrich our understanding.

Supplementary Materials: The following are available online at https://www.mdpi.com/article/10 .3390/pr10010142/s1: Table S1, pH, CaCO₃ contents, I_{geo} and Cr concentrations extracted by TCLP of soils at contaminated sampling point S2; Table S2, pH, CaCO₃ contents, I_{geo} and Cr concentrations extracted by TCLP of soils at contaminated sampling point S3; Table S3, pH, CaCO₃ contents, I_{geo} and Cr concentrations extracted by TCLP of soils at contaminated sampling point S5; Figure S1, X-ray diffraction (XRD) powder pattern of the three soil layers; Figure S2, The vertical distribution of copper and zinc in soils at sampling points S3 and S5.

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