

## Article

# Generalization of the Optical Theorem to an Arbitrary Multipole Excitation of a Particle near a Transparent Substrate

Yuri A. Eremin <sup>1</sup>  and Thomas Wriedt <sup>2,\*</sup><sup>1</sup> Faculty of Computational Mathematics and Cybernetics, Lomonosov Moscow State University, Leninskie Gory 1, 119991 Moscow, Russia; eremin@cs.msu.ru<sup>2</sup> Leibniz-Institute für Werkstofforientierte Technologien, University of Bremen, Badgasteiner Str. 3, 28359 Bremen, Germany

\* Correspondence: thw@iwt.uni-bremen.de

**Abstract:** In the present paper, the generalization of the optical theorem to the case of a penetrable particle deposited near a transparent substrate that is excited by a multipole of an arbitrary order and polarization has been derived. In the derivation we employ classic Maxwell's theory, Gauss's theorem, and use a special representation for the multipole excitation. It has been shown that the extinction cross-section can be evaluated by the calculation of some specific derivatives from the scattered field at the position of the multipole location, in addition to some finite integrals which account for the multipole polarization and the presence of the substrate. Finally, the present paper considers some specific examples for the excitation of a particle by an electric quadrupole.

**Keywords:** optical theorem; arbitrary order of multipole; Maxwell's theory; Gauss's theorem; transparent substrate; extinction cross-section



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## 1. Introduction

The objective of the introduction is to trace the path of generalization of the optical theorem, starting from the classical result obtained initially for a scatterer located in free space that is excited by a plane wave; subsequently moving to the case of a scatterer in the presence of a transparent substrate; then focusing on the excitation by dipoles and multipoles in free space; and, finally, considering the generalized result we obtained for a penetrable obstacle located near a transparent substrate, that is excited by an electric multipole of an arbitrary order. The optical theorem introduces the fundamental concept of the extinction cross-section, which shows how much energy the scatterer takes from external excitation, regardless of whether it is a plane wave or a local source.

The optical theorem (OT) is one of the famous theoretical results in the plane wave scattering theory of electromagnetic waves [1]. It states that the sum of the scattering and absorption cross-sections (that is the extinction cross-section) is proportional to the scattered field amplitude in the propagation direction of the exciting plane wave. Similar results can be found in acoustics [2], seismics [3], and quantum mechanics [4]. Over the years, many generalizations and implementations of the OT were suggested [5–7]. In computational electromagnetics, this theorem is employed for the checking or verification of light scattering computer models, since, for a lossless particle, the total scattering cross-section must be equal to the imaginary part of the forward scattering amplitude [8]. The authors themselves have repeatedly used this method to test newly developed codes.

The results based on the optical theorem were analyzed and generalized by numerous researchers, in particular, for problems of plane wave scattering by an obstacle located near a plane transparent prism [9], and electromagnetic wave propagation in anisotropic and bianisotropic media [10,11]. A generalization of the optical theorem to the excitation of an obstacle in free space by a point source and an electric dipole was given by

Athanasiadis et al. [12]. Eremin and Sveshnikov [13] extended the OT to the case of excitation of a scatterer by a point source in the presence of a transparent prism. The excitation of an obstacle by a multipole source occurs in numerous modern applications. These are problems that occur with the excitation by quantum dots [14], the analysis of luminescence processes and Raman spectroscopy [15], and the design of various optical antenna based on plasmon effects [16].

Eremin and Wriedt [17] extended the OT to the case of a local obstacle excitation by an arbitrary order electric multipole. However, in this paper, a special polarization of the multipole was considered. The present paper considers a generalization of the OT to the case of excitation of a local obstacle located near a lossless prism by an electric multipole of arbitrary order and polarization. We used integral transforms for the wave fields to show that the extinction cross-section can be found in clear analytical forms, by applying some differential operators to the scattering field in a single point. This permits the testing of computer models for the case of lossless scatterers by comparing the extinction cross-section with the scattering cross-section. Furthermore, the result enables the absorption cross-section to be computed for local obstacles deposited near a transparent substrate, which is especially important when analyzing plasmonic particles, because they generate a large number of evanescent field components [18].

The paper is organized as follows: in the subsequent section, we consider the mathematical statement of the boundary value scattering problem for an electric multipole of arbitrary order and, then, repeat the basic notations and results obtained for the case of a particle located in free space [17]. Following this section, we will proceed to the generalization of the OT to the case of a penetrable particle deposited near a transparent substrate. In the subsequent section, we formulate the main result in the form of Theorem 1. In the final section, we consider the main formula for some specific multipole excitations.

## 2. Problem Statement and Methods

### 2.1. Boundary Value Problem Statement

Consider the excitation of a bounded isotropic penetrable particle  $D_i$  with a smooth surface  $\partial D_i$  by an electric multipole source of arbitrary order having a momentum  $\mathbf{p}$ . A scheme of the considered scattering problem can be found in Figure 1.

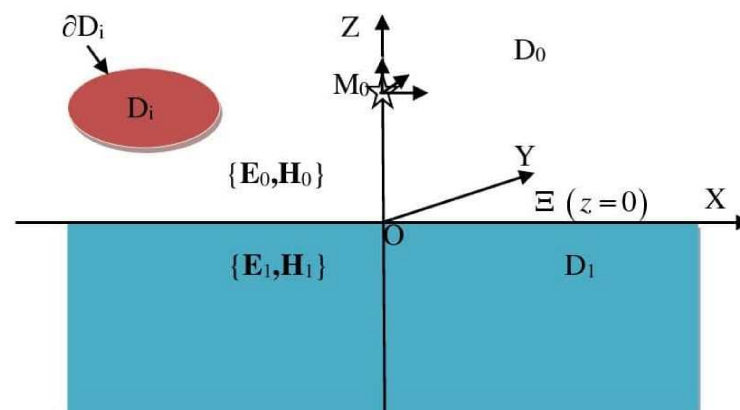


Figure 1. Scheme of the scattering problem.

Let the multipole be deposited at a point  $M_0$ , which is located outside of the particle  $D_i$ . The entire space  $\mathbb{R}^3$  consists of two half-spaces,  $D_0$  ( $z > 0$ ) and  $D_1$  ( $z < 0$ ), separated by the plane interface  $\Xi$  ( $z = 0$ ). Assume that all media are nonmagnetic. Let the particle  $D_i$  be located inside the upper half-space,  $D_i \subset D_0$  and  $M_0 \in D_0$ , too. Subsequently, the mathematical statement of the scattering problem can be written in the following form, including the time-harmonic Maxwell equations;

$$\nabla \times \mathbf{H}_0 = jk\varepsilon_0 \mathbf{E}_0 + \mathbf{J}(M, M_0); \quad \nabla \times \mathbf{E}_0 = -jk\mathbf{H}_0 \text{ in } D_0;$$

$$\nabla \times \mathbf{H}_l = jk\varepsilon_l \mathbf{E}_l; \quad \nabla \times \mathbf{E}_l = -jk\mathbf{H}_l \text{ in } D_l, l = 1, i;$$

the transmission conditions at the particle surface and plane interface;

$$\begin{aligned} \mathbf{n}_q \times (\mathbf{E}_i(q) - \mathbf{E}_0(q)) &= 0, & q \in \partial D_i, & \mathbf{e}_z \times (\mathbf{E}_1(Q) - \mathbf{E}_0(Q)) = 0, \\ \mathbf{n}_q \times (\mathbf{H}_i(q) - \mathbf{H}_0(q)) &= 0, & & \mathbf{e}_z \times (\mathbf{H}_1(Q) - \mathbf{H}_0(Q)) = 0, \end{aligned} \quad Q \in \Xi \quad (1)$$

the Silver–Muller radiation conditions for all directions  $\mathbf{r}/r$ ,  $z \neq 0$ ;

$$\lim_{r \rightarrow \infty} r \cdot \left( \mathbf{H}_l \times \frac{\mathbf{r}}{r} - \sqrt{\varepsilon_l} \mathbf{E}_l \right) = 0, \quad r = |M| \rightarrow \infty, \quad l = 0, 1, \quad z \neq 0;$$

and the additional infinity conditions along the interface  $\Xi$  ( $z = 0$ ) [19]

$$\max(|\mathbf{H}_l|, |\mathbf{E}_l|) = O(\rho^{-\frac{1}{2}}), \quad \rho = \sqrt{x^2 + y^2}, \quad \rho \rightarrow \infty, \quad z = \pm 0.$$

where the  $\{\mathbf{E}_l, \mathbf{H}_l\}$ —electric and magnetic fields in the corresponding domains  $D_l$ ,  $l = 0, 1, i$ ,  $k = \omega/c$ ,  $\mathbf{J} = J(M, M_0)\mathbf{p}$ ,  $\mathbf{n}_q$ —unit external normal at  $\partial D_i$ ,  $\mathbf{e}_z$ —basic vector of the Cartesian coordinate system ( $x, y, z$ ), axis  $OZ$  is orthogonal to  $\Xi$ . Assume that  $\partial D_i \subset C^{(2,\alpha)}$  (Hölder space), the relative permittivity and permeability  $\varepsilon_i$  are continuous complex valued functions inside  $D_i$  and  $\text{Im}\varepsilon_i \leq 0$ ,  $\text{Im}\varepsilon_{0,1} = 0$ . The time dependence was chosen as  $\exp\{j\omega t\}$ . The corresponding radiation conditions were selected in such a form to provide uniqueness of the solution of the scattering problem (1).

Let us specify the  $J(M, M_0)$  function. Choose the origin  $O$  of a Cartesian coordinate system and direct its  $Oz$  axis so that it passes through the point  $M_0 = (0, 0, z_0)$  corresponding to the multipole position. Consider the multipole which, in a spherical coordinate system  $(r, \theta, \varphi)$ , accepts the following form:

$$w_n^m(M, M_0) := h_n^{(2)}(k_0 r) P_n^m(\cos \theta) e^{-jm\varphi}; \quad n = 0, 1, \dots; \quad m = 0, \pm 1, \dots; \quad |m| \leq n. \quad (2)$$

For the multipole (2), the following fundamental representation is valid [20]:

$$h_n^{(2)}(k_0 R_{MM_0}) P_n^m(\cos \theta) e^{-jm\varphi} = (-1)^m j^n \left[ \frac{j}{k_0} \left( \frac{\partial}{\partial x} - j \frac{\partial}{\partial y} \right) \right]^m P_n^{(m)} \left( \frac{j}{k_0} \frac{\partial}{\partial z} \right) h_0^{(2)}(k_0 R_{MM_0}),$$

here,  $k_0 = k\sqrt{\varepsilon_0}$ ,  $h_n^{(2)}(x)$  is a spherical Hankel function,  $R_{MM_0} = |M - M_0|$ ,  $P_n^{(m)}(\cos \theta)$  is an associated Legendre polynomial [21]. Introduce the following differential operator:

$$D_n^m = (-1)^m j^{n-1} \left[ \frac{j}{k_0} e^{-j\varphi} \frac{\partial}{\partial \rho} \right]^m P_n^{(m)} \left( \frac{j}{k_0} \frac{\partial}{\partial z} \right). \quad (3)$$

taking into account the fundamental solution to the Helmholtz equation  $\Psi(M, M_0) : \Delta \Psi + k_0^2 \Psi = -\delta(M - M_0)$ , which has the following form:

$$\Psi(M, M_0) = \frac{e^{-jk_0 R_{MM_0}}}{4\pi R_{MM_0}} = -j \frac{k_0}{4\pi} h_0^{(2)}(k_0 R_{MM_0}), \text{ then}$$

$$\Delta w_n^m + k_0^2 w_n^m = (\Delta + k_0^2) D_n^m \left\{ j h_0^{(2)}(k_0 R_{MM_0}) \right\} = \frac{4\pi}{k_0} D_n^m \delta(M - M_0),$$

where  $\delta$ —Dirac delta function. Subsequently, set up the  $J(M, M_0)$  function in (1) as

$$J(M, M_0) = \frac{4\pi}{k_0} D_n^m \delta(M - M_0). \quad (4)$$

In this case, the scattering problem (1) has a unique solution [22]. In this case the electric field corresponding to the exciting multipole located at  $M_0$  accepts the following form:

$$\mathbf{E}_0^0(M) = -\frac{j}{k_0} \nabla \times \nabla \times \{w_n^m(M, M_0)\mathbf{p}\}. \quad (5)$$

Now we are ready to proceed to the generalization of the optical theorem.

## 2.2. Generalization of the Optical Theorem

Choose a sphere  $D_R$  of  $R$ —radius, centered at the plane  $\Xi$  and enclosing both  $D_i$  and point  $M_0$ , and its boundary will be referred to as  $\Sigma_R$ . The plane  $\Xi$  divides  $D_R$  into two half-spheres  $D_R^\pm$ , deposited in  $D_{0,1}$ , and let  $\Sigma_R^\pm$  be parts of  $\Sigma_R$  belonging to  $D_R^\pm$ , respectively. The application of the Gauss divergence theorem [22] to the solution of the problem (1) of the total electric  $\mathbf{E}_0$  and the complex conjugate magnetic  $\mathbf{H}_0^*$  fields in the domain  $D_R^+/\overline{D}_i$  allows us to obtain the following formula:

$$\begin{aligned} \int_{D_R^+/\overline{D}_i} \nabla \cdot [\mathbf{E}_0 \times \mathbf{H}_0^*] d\tau &= \int_{D_R^+/\overline{D}_i} \{\mathbf{H}_0^* \cdot \nabla \times \mathbf{E}_0 - \mathbf{E}_0 \cdot \nabla \times \mathbf{H}_0^*\} d\tau = \\ &= \int_{D_R^+/\overline{D}_i} \left\{ jk \left( -|\mathbf{H}_0^*|^2 + |\mathbf{E}_0|^2 \right) - (\mathbf{E}_0 \cdot \mathbf{J}^*) \right\} d\tau = \int_{\Sigma_R^+ \cup \Xi_R \cup \partial D_i} [\mathbf{E}_0 \times \mathbf{H}_0^*] \cdot d\mathbf{s}, \end{aligned} \quad (6)$$

where  $\Xi_R := \{M \in \Xi : |M| \leq R\}$  is a part of the plane  $\Xi$ . Taking the real parts from both sides of (6) and rewriting the integrals in the right part we obtain the following formula:

$$\begin{aligned} \operatorname{Re} \int_{\partial D_i} [\mathbf{E}_0 \times \mathbf{H}_0^*] \cdot d\boldsymbol{\sigma} + \operatorname{Re} \int_{\Sigma_R^+} [\mathbf{E}_0 \times \mathbf{H}_0^*] \cdot \frac{\mathbf{r}}{r} d\sigma - \operatorname{Re} \int_{\Xi_R} [\mathbf{E}_0 \times \mathbf{H}_0^*] \cdot \mathbf{e}_z d\sigma = \\ - \operatorname{Re} \int_{D_R^+/\overline{D}_i} (\mathbf{E}_0 \cdot \mathbf{J}^*) d\tau, \end{aligned} \quad (7)$$

A similar application of Gauss's theorem inside  $D_i$  leads to the following:

$$\operatorname{Re} \int_{\partial D_i} [\mathbf{E}_i \times \mathbf{H}_i^*] \cdot d\boldsymbol{\sigma} = k \int_{D_i} \left\{ |\operatorname{Im} \varepsilon_i| |\mathbf{E}_i|^2 \right\} d\tau. \quad (8)$$

The right part of (8) will be referred to as the absorption cross-section  $C_{abs}$  and, subsequently, (7) accepts the following form:

$$C_{abs} + \operatorname{Re} \int_{\Sigma_R^+} [\mathbf{E}_0 \times \mathbf{H}_0^*] \cdot \frac{\mathbf{r}}{r} d\sigma - \operatorname{Re} \int_{\Xi_R} [\mathbf{E}_0 \times \mathbf{H}_0^*] \cdot \mathbf{e}_z d\sigma = - \operatorname{Re} \int_{D_R^+/\overline{D}_i} (\mathbf{E}_0 \cdot \mathbf{J}^*) d\tau. \quad (9)$$

Using Gauss's theorem in the  $D_R^-$  domain and taking the real part, we obtain the following formula:

$$\operatorname{Re} \int_{\Sigma_R^-} [\mathbf{E}_1 \times \mathbf{H}_1^*] \cdot \frac{\mathbf{r}}{r} d\sigma + \operatorname{Re} \int_{\Xi_R} [\mathbf{E}_1 \times \mathbf{H}_1^*] \cdot \mathbf{e}_z d\sigma = 0. \quad (10)$$

Combining equations (9) and (10) yields the following:

$$C_{abs} + \operatorname{Re} \int_{\Sigma_R^+} [\mathbf{E}_0 \times \mathbf{H}_0^*] \cdot \frac{\mathbf{r}}{r} d\sigma + \operatorname{Re} \int_{\Sigma_R^-} [\mathbf{E}_1 \times \mathbf{H}_1^*] \cdot \frac{\mathbf{r}}{r} d\sigma = - \operatorname{Re} \int_{D_R^+/\overline{D}_i} (\mathbf{E}_0 \cdot \mathbf{J}^*) d\tau. \quad (11)$$

Subsequently, consider the far-field patterns  $\mathbf{F}_{0,1}(\theta, \varphi)$  of the fields [22] in the upper and lower half-spaces  $D_R^\pm$

$$\mathbf{E}_{0,1}(M) = \frac{e^{-jkn_{0,1}r}}{r} \mathbf{F}_{0,1}(\theta, \varphi) + o\left(\frac{1}{r}\right), r \rightarrow \infty, z \neq 0.$$

The far-field patterns are defined at the upper and lower unit hemi-spheres  $\Omega^+ = \{0 \leq \varphi \leq 360^\circ; 0 \leq \theta < 90^\circ\}$ ,  $\Omega^- = \{0 \leq \varphi \leq 360^\circ; 90^\circ < \theta \leq 180^\circ\}$ , where  $n_{0,1} = \sqrt{\varepsilon_{0,1}}$ . Then, having a radius  $R$  tending toward infinity leads to the following:

$$\lim_{R \rightarrow \infty} \operatorname{Re} \int_{\Sigma_R^+} [\mathbf{E}_0 \times \mathbf{H}_0^*] \cdot \frac{\mathbf{r}}{r} d\sigma = \operatorname{Re} \lim_{R \rightarrow \infty} \int_{\Sigma_R^+} \mathbf{E}_0 \cdot [\mathbf{H}_0^* \times \frac{\mathbf{r}}{r}] d\sigma = \sqrt{\varepsilon_0} \lim_{R \rightarrow \infty} \int_{\Sigma_R^+} |\mathbf{E}_0|^2 d\sigma = \sqrt{\varepsilon_0} \int_{\Omega^+} |\mathbf{F}_0|^2 d\omega.$$

Similarly, for the lower half-space  $D_1$ :

$$\lim_{R \rightarrow \infty} \operatorname{Re} \int_{\Sigma_R^-} [\mathbf{E}_1 \times \mathbf{H}_1^*] \cdot \frac{\mathbf{r}}{r} d\sigma = \operatorname{Re} \lim_{R \rightarrow \infty} \int_{\Sigma_R^-} \mathbf{E}_1 \cdot [\mathbf{H}_1^* \times \frac{\mathbf{r}}{r}] d\sigma = \sqrt{\varepsilon_1} \lim_{R \rightarrow \infty} \int_{\Sigma_R^-} |\mathbf{E}_1|^2 d\sigma = \sqrt{\varepsilon_1} \int_{\Omega^-} |\mathbf{F}_1|^2 d\omega.$$

The last integrals can be referred to as the scattering cross-sections in the upper and the lower half-spaces  $D_{0,1}$ — $C_{sc}^\pm$ . Therefore, (11) can be rewritten in a simple form:

$$C_{abs} + C_{sc}^+ + C_{sc}^- = -\operatorname{Re} \int_{D_0/\overline{D}_i} (\mathbf{E}_0 \cdot \mathbf{J}^*) d\tau. \quad (12)$$

It is worth noting that the scattering cross-sections  $C_{sc}^\pm$  include a part associated to the multipole radiation patterns. Represent the total fields in  $D_R^\pm$  as  $\mathbf{E}_{0,1} = \mathbf{E}_{0,1}^s + \mathbf{E}_{0,1}^d$ , where  $\mathbf{E}_{0,1}^d$  is the field corresponding to the radiating multipole located at  $M_0$ , and  $\mathbf{E}_{0,1}^s$  is the scattered field corresponding only to the particle  $D_i$ . Because the total field  $\mathbf{E}_{0,1}$  satisfies the transmission conditions at the plane interface  $\Xi$ , both  $\mathbf{E}_{0,1}^s$  and  $\mathbf{E}_{0,1}^d$  should obey the same transmission conditions. We continue the transformation of the integral in the right part of (12) and, by employing the  $\delta$ -function properties [23], we then account for [17]

$$\begin{aligned} \int_{D_0/\overline{D}_i} (\mathbf{E}_0 \cdot \mathbf{J}^*) d\tau &= \int_{D_0/\overline{D}_i} (\mathbf{E}_0^s(Q) + \mathbf{E}_0^d(Q)) \cdot \mathbf{p} \mathbf{J}^*(Q, M_0) d\tau_Q = \frac{4\pi}{k_0} \int_{D_0/\overline{D}_i} D_n^{m*} \delta(Q - M_0) \mathbf{E}_0^s(Q) \cdot \mathbf{p} d\tau_Q \\ &+ \int_{D_0/\overline{D}_i} \mathbf{E}_0^d(Q) \cdot \mathbf{p} \mathbf{J}^*(Q, M_0) d\tau_Q = \int_{D_0/\overline{D}_i} \mathbf{J}^*(Q, M_0) \mathbf{E}_0^d(Q) \cdot \mathbf{p} d\tau_Q + \frac{4\pi}{k_0} [D_n^{m+} (\mathbf{E}_0^s(M) \cdot \mathbf{p})]_{M=M_0}. \end{aligned} \quad (13)$$

The last term has already been obtained in [17]. Here,  $D_n^{m+}$  is Hermitian conjugate operator, with respect to (3) having the following form:

$$D_n^{m+} = (-1)^{m-1} j^{n-1} \left[ \frac{j}{k_0} e^{j\varphi} \frac{\partial}{\partial \rho} \right]^m P_n^{(m)} \left( \frac{j}{k_0} \frac{\partial}{\partial z} \right), \quad (14)$$

Here,  $P_n^{(m)}(-x) = (-1)^{n+m} P_n^{(m)}(x)$  [21]. It should be remembered that  $\mathbf{E}_0^s$  is an analytic function in the region  $D_0$  [22]. To evaluate the first integral in the right part of (13), we need a representation for the electric multipole field satisfying the transmission conditions at the interface  $\Xi$ . This can be obtained based on the electric green tensor (GT) of half-space  $\overset{\leftrightarrow}{\mathbf{G}}(M, M_0)$ , which can be written in the form [24]

$$\overset{\leftrightarrow}{\mathbf{G}}(M, M_0) = \begin{bmatrix} G_{11} & 0 & 0 \\ 0 & G_{11} & 0 \\ \partial g / \partial x_M & \partial g / \partial y_M & G_{33} \end{bmatrix}. \quad (15)$$

The GT components in  $D_{0,1}$  have the following representations:

$$G_{ll}(M, M_0) = \int_0^\infty J_0(\lambda r) v_{ll}(\lambda, z, z_0) \lambda d\lambda, \quad l = 1, 3; \quad g(M, M_0) = \int_0^\infty J_0(\lambda r) v_{31}(\lambda, z, z_0) \lambda d\lambda,$$

where  $r^2 = (x - x_0)^2 + (y - y_0)^2$ ,  $J_0$ —cylindrical Bessel function [21],  $(x_0, y_0, z_0)$ —Cartesian coordinates of point  $M_0$ . The corresponding spectral functions  $v_{11}, v_{33}, v_{31}$  fulfilling the transmission conditions at  $z = 0$  can be found in Appendix A (see formulas (A1) and (A2)).

Following the multipole definition, consider the multipole representation for the GT by extracting the singular part as:

$$\overset{\leftrightarrow}{\mathbf{W}}_n^m(M, M_0) = \frac{4\pi}{k_0} D_n^m \overset{\leftrightarrow}{\mathbf{G}}^e(M, M_0) = w_n^m(M, M_0) \cdot \mathbf{I} + \frac{4\pi}{k_0} D_n^m \overset{\leftrightarrow}{\mathbf{G}}_r^e(M, M_0), \quad (16)$$

where  $\overset{\leftrightarrow}{\mathbf{G}}_r^e(M, M_0)$  is the regular part of the GT multipole representation,  $\mathbf{I}$ —idem factor. Subsequently, the corresponding electric field of the multipole in  $D_0$  appears as:

$$\mathbf{E}_0^d(M) = \mathbf{E}_0^0(M) - \frac{4\pi j}{k_0^2} \nabla \times \nabla \times \left\{ D_n^m \overset{\leftrightarrow}{\mathbf{G}}_r^e(M, M_0) \mathbf{p} \right\} = \mathbf{E}_0^0(M) + \mathbf{E}_0^r(M). \quad (17)$$

Then,

$$\begin{aligned} & -\operatorname{Re} \int_{D_0/\overline{D}_i} J^*(Q, M_0) \mathbf{E}_0^d(Q) \cdot \mathbf{p} d\tau_Q = \\ & -\operatorname{Re} \int_{D_0/\overline{D}_i} J^*(Q, M_0) \mathbf{E}_0^0(Q) \cdot \mathbf{p} d\tau_Q - \operatorname{Re} \int_{D_0/\overline{D}_i} J^*(Q, M_0) \mathbf{E}_0^r(Q) \cdot \mathbf{p} d\tau_Q. \end{aligned}$$

The first integral represents the total energy irradiated by a multipole deposited in free space. This integral is examined in detail in [25]. Let the polarization vector have the Cartesian coordinates  $\mathbf{p} = (p_x, p_y, p_z)$ , then the first integral can be written as

$$-\operatorname{Re} \int_{D_0/\overline{D}_i} J^*(Q, M_0) \mathbf{E}_0^0(Q) \cdot \mathbf{p} d\tau_Q = \frac{\pi}{k_0^2} \left\{ \left[ \frac{2}{3} \beta_n^m + \frac{1}{3} \right] (p_x^2 + p_y^2) + \left[ \frac{2}{3} - \frac{2}{3} \beta_n^m \right] p_z^2 \right\} \|P_n^m\|^2. \quad (18)$$

Substituting a specific expression for  $J(Q, M_0)$ : (4) and  $\mathbf{E}_0^0(Q)$ : (5); taking into account that  $\int_{-1}^1 P_2^0(x) [P_n^m(x)]^2 dx = \beta_n^m \|P_n^m\|^2$  and following [25] we obtain (18), where  $\beta_n^m = C(nn2, 000)C(nn2, mm0)$ ,  $C(\dots)$  are Clebsch–Gordan coefficients, and  $\|P_n^m\|^2$  is the norm of associated Legendre polynomials [21]  $\|P_n^m\|^2 = \frac{2}{2n+1} \frac{(n+m)!}{(n-m)!}$ . Unfortunately, Clebsch–Gordan coefficients do not have an explicit analytical representation for an arbitrary integer  $n, m$  but they can be estimated numerically.

Consider the integral containing the regular field in the right part of the last relation. We start from its  $z$ -component, then

$$\mathbf{p}_z \cdot \nabla \times \nabla \times \left\{ D_n^m \overset{\leftrightarrow}{\mathbf{G}}_r^e(M, M_0) \mathbf{p}_z \right\} = |\mathbf{p}_z|^2 D_n^m \left\{ k_0^2 \overline{G}_{33}(M, M_0) + \frac{\partial^2}{\partial z^2} \overline{G}_{33}(M, M_0) \right\}.$$

By substituting the representation for the current into the integral, we obtain the following formula:

$$\begin{aligned} & \int_{D_0/\overline{D}_i} J^* \mathbf{E}_0^r \mathbf{p}_z d\tau \\ &= \frac{4\pi j}{k_0^2} |\mathbf{p}_z|^2 D_n^{m+} D_n^m \int_{D_0/\overline{D}_i} \int_0^\infty A_{33} J_0(\lambda \rho) \left( k_0^2 + \frac{\partial^2}{\partial z^2} \right) \frac{\exp\{-\eta_0 z\}}{\eta_0} \lambda d\lambda \delta(Q - M_0) d\tau_Q \quad (19) \\ &= \frac{4\pi j}{k_0^2} |\mathbf{p}_z|^2 \int_{D_0/\overline{D}_i} \int_0^\infty A_{33}(\lambda, z_0) D_n^{m+} D_n^m J_0(\lambda \rho) \frac{\exp\{-\eta_0 z\}}{\eta_0} \lambda^3 d\lambda \delta(Q - M_0) d\tau_Q. \end{aligned}$$

It is worth noting that the multipole is located at the 0z axis,  $M_0 = (0, 0, z_0)$ . It can then be realized that

$$D_n^{m+} D_n^m = \frac{1}{k_0^{2m}} \frac{\partial^{2m}}{\partial \rho^{2m}} \left[ P_n^{(m)} \left( \frac{j}{k_0} \frac{\partial}{\partial z} \right) \right]^2.$$

By applying this operator to the integrand of the integral in the right part of (19), the following can be expressed:

$$\left\{ \frac{\partial^{2m}}{\partial \rho^{2m}} J_0(\lambda \rho) \right\}_{\rho=0} \left\{ \left[ P_n^{(m)} \left( \frac{j}{k_0} \frac{\partial}{\partial z} \right) \right]^2 \frac{\exp\{-\eta_0 z\}}{\eta_0} \right\}_{z=z_0},$$

and accounting for  $J_0(\lambda \rho) = \sum_{l=0}^{\infty} \frac{(-1)^l}{(l!)^2} \left( \frac{\lambda \rho}{2} \right)^{2l}$  [21], that the following can be presented:

$$\left\{ \frac{\partial^{2m}}{\partial \rho^{2m}} J_0(\lambda \rho) \right\}_{\rho=0} \left\{ \left[ P_n^{(m)} \left( \frac{j}{k_0} \frac{\partial}{\partial z} \right) \right]^2 \frac{\exp\{-\eta_0 z\}}{\eta_0} \right\}_{z=z_0} = \frac{(-1)^m \lambda^{2m} (2m-1)!!}{(2m)!!} \left[ P_n^{(m)} \left( \frac{j}{k_0} \eta_0 \right) \right]^2 \frac{\exp\{-\eta_0 z_0\}}{\eta_0}.$$

By substituting the formula for  $A_{33}$ : (A4) we obtain the following:

$$\int_{D_0/\overline{D}_i} J^*(Q, M_0) \mathbf{E}_0^r(Q) \mathbf{p}_z d\tau_Q = \frac{4\pi j |\mathbf{p}_z|^2 (2m-1)!!}{k_0^{2m+2} (2m)!!} \int_0^{\infty} \frac{\varepsilon_1 \eta_0 - \varepsilon_0 \eta_1}{\varepsilon_1 \eta_0 + \varepsilon_0 \eta_1} \left[ P_n^{(m)} \left( \frac{j}{k_0} \eta_0 \right) \right]^2 \frac{\exp\{-2\eta_0 z_0\}}{\eta_0} \lambda^{2m+3} d\lambda \quad (20)$$

By taking the real part of the integral, we obtain the following:

$$-\text{Re} \int_{D_0/\overline{D}_i} J^* \mathbf{E}_0^r \cdot \mathbf{p}_z d\tau_Q = \frac{4\pi |\mathbf{p}_z|^2 (2m-1)!!}{k_0^{2m+2} (2m)!!} \text{Im} \int_0^{\infty} \frac{\varepsilon_1 \eta_0 - \varepsilon_0 \eta_1}{\varepsilon_1 \eta_0 + \varepsilon_0 \eta_1} \left[ P_n^{(m)} \left( \frac{j}{k_0} \eta_0 \right) \right]^2 \frac{\exp\{-2\eta_0 z_0\}}{\eta_0} \lambda^{2m+3} d\lambda. \quad (21)$$

Consider the integrand in (21) following to [26]. It is clear that under  $\lambda > \max(k_0, k_1)$  we have  $\text{Im} \eta_{0,1} = 0$ . Based on the properties of  $P_n^{(m)}(jx)$  under  $\text{Im} x = 0$ , depending on the specific integer values of  $n, m$ , the following correlations are relevant: either  $\text{Re} P_n^{(m)}(jx) = 0$ , or  $\text{Im} P_n^{(m)}(jx) = 0$ . Hence,  $\text{Im} \left[ P_n^{(m)} \left( j \frac{\eta_0}{k_0} \right) \right]^2 \equiv 0$  for  $\forall n, m, n \in \mathbb{N}, n \geq m$ , and  $\lambda > \max(k_0, k_1)$ . Therefore, for all real valued  $k_1 > k_0$ , we obtain the following:

$$-\text{Re} \int_{D_0/\overline{D}_i} J^* \mathbf{E}_0^r \cdot \mathbf{p}_z d\tau_Q = \frac{4\pi |\mathbf{p}_z|^2 (2m-1)!!}{k_0^{2m+2} (2m)!!} \text{Im} \int_0^{k_1} \frac{\varepsilon_1 \eta_0 - \varepsilon_0 \eta_1}{\varepsilon_1 \eta_0 + \varepsilon_0 \eta_1} \left[ P_n^{(m)} \left( \frac{j}{k_0} \eta_0 \right) \right]^2 \frac{\exp\{-2\eta_0 z_0\}}{\eta_0} \lambda^{2m+3} d\lambda. \quad (22)$$

We continue to analyze the regular field x-component in the same manner:

$$\mathbf{p}_x \cdot \nabla \times \nabla \times \left\{ D_n^m \overset{\leftrightarrow e}{\mathbf{G}}_r(M, M_0) \mathbf{p}_x \right\} = \mathbf{p}_x \cdot \nabla \times \nabla \times D_n^m \left\{ \overline{G}_{11}(M, M_0) + \frac{\partial}{\partial x} g(M, M_0) \right\} \cdot \mathbf{p}_x = \frac{4\pi j}{k_0^2} |\mathbf{p}_x|^2 D_n^m \left\{ k_0^2 \left[ \overline{G}_{11}(M_0, M_0) + \frac{\partial}{\partial x} g(M, M_0) \right] + \left[ \frac{\partial^2}{\partial x^2} \overline{G}_{11}(M_0, M_0) + \frac{\partial^3}{\partial x^3} g(M, M_0) \right] \right\}. \quad (23)$$

It should be remembered that the presence of any odd order derivatives with respect to x or y of the integral containing  $J_0(\lambda r)$  leads to the nullification of the result at  $M = M_0$  ( $r = 0$ ). This can be easily observed from the series for the Bessel function of zero

order, which contains only even powers of argument. Subsequently, the relation (23) can be written as the following formula:

$$\mathbf{p}_x \cdot \nabla \times \nabla \times \left\{ D_n^m \overset{\leftrightarrow}{\mathbf{G}}_r^e(M, M_0) \mathbf{p}_x \right\} = \frac{4\pi j}{k_0^2} |\mathbf{p}_x|^2 D_n^m \left\{ k_0^2 \overline{G}_{11}(M_0, M_0) + \frac{\partial^2}{\partial x^2} \overline{G}_{11}(M_0, M_0) \right\}.$$

Let us proceed to the consideration of the x-component, that is:

$$\int_{D_0/\overline{D}_i} J^* \mathbf{E}_0^r \mathbf{p}_x d\tau = \frac{4\pi j}{k_0^2} |\mathbf{p}_x|^2 D_n^m \int_{D_0/\overline{D}_i} \int_0^\infty A_{11}(\lambda, z_0) \left( k_0^2 + \frac{\partial^2}{\partial x^2} \right) J_0(\lambda \rho) \frac{\exp\{-\eta_0 z\}}{\eta_0} \lambda d\lambda \delta(Q - M_0) d\tau_Q. \quad (24)$$

Following our previous consideration for the z-component (22) and the explicit formula for  $A_{11}$ : (A3), we can present the following:

$$\begin{aligned} & \int_{D_0/\overline{D}_i} J^* \mathbf{E}_0^r \mathbf{p}_x d\tau \\ &= \frac{4\pi j}{k_0^2} |\mathbf{p}_x|^2 D_n^m \int_{D_0/\overline{D}_i} \int_0^\infty A_{11} \left( k_0^2 + \frac{\partial^2}{\partial x^2} \right) J_0(\lambda \rho) \frac{\exp\{-\eta_0 z\}}{\eta_0} \lambda d\lambda \delta(Q - M_0) d\tau_Q \\ &= \frac{4\pi j |\mathbf{p}_x|^2 (2m)!}{k_0^{2m} [(2m)!!]^2} \int_0^\infty \frac{\eta_0 - \eta_1}{\eta_0 + \eta_1} \left[ P_n^{(m)} \left( \frac{j}{k_0} \eta_0 \right) \right]^2 \frac{\exp\{-2\eta_0 z_0\}}{\eta_0} \lambda^{2m+1} d\lambda + \\ &+ \frac{4\pi j}{k_0^2} |\mathbf{p}_x|^2 \int_0^\infty A_{11}(\lambda, z_0) \left\{ \frac{\partial^{2m}}{\partial \rho^{2m}} \frac{\partial^2}{\partial x^2} J_0(\lambda \rho) \right\}_{\rho=0} \left\{ \left[ P_n^{(m)} \left( \frac{j}{k_0} \frac{\partial}{\partial z} \right) \right]^2 \frac{\exp\{-\eta_0 z\}}{\eta_0} \right\}_{z=z_0} \lambda d\lambda. \end{aligned} \quad (25)$$

Then, the last integral in the previous relation (25) can be transformed as:

$$\begin{aligned} & \int_0^\infty \frac{\eta_0 - \eta_1}{\eta_0 + \eta_1} \zeta_0 \left\{ \frac{\partial^{2m}}{\partial \rho^{2m}} \frac{\partial^2}{\partial x^2} J_0(\lambda \rho) \right\}_{\rho=0} \left\{ \left[ P_n^{(m)} \left( \frac{j}{k_0} \frac{\partial}{\partial z} \right) \right]^2 \frac{\exp\{-\eta_0 z\}}{\eta_0} \right\}_{z=z_0} \lambda d\lambda = \\ & - \frac{(2m+1)!!}{k_0^{2m} (2m+2)!!} \int_0^\infty \frac{\eta_0 - \eta_1}{\eta_0 + \eta_1} \left[ P_n^{(m)} \left( \frac{j}{k_0} \eta_0 \right) \right]^2 \frac{\exp\{-2\eta_0 z_0\}}{\eta_0} \lambda^{2m+3} d\lambda. \end{aligned}$$

The collection of the two previously obtained relations allows us to conclude that

$$\begin{aligned} & \int_{D_0/\overline{D}_i} J^* \mathbf{E}_0^r \mathbf{p}_x d\tau = \frac{4\pi j |\mathbf{p}_x|^2 (2m-1)!!}{k_0^{2m} (2m)!!} \int_0^\infty \frac{\eta_0 - \eta_1}{\eta_0 + \eta_1} \left[ P_n^{(m)} \left( \frac{j}{k_0} \eta_0 \right) \right]^2 \frac{\exp\{-2\eta_0 z_0\}}{\eta_0} \lambda^{2m+1} d\lambda - \\ & - \frac{4\pi j |\mathbf{p}_x|^2 (2m+1)!!}{k_0^{2m+2} (2m+2)!!} \int_0^\infty \frac{\eta_0 - \eta_1}{\eta_0 + \eta_1} \left[ P_n^{(m)} \left( \frac{j}{k_0} \eta_0 \right) \right]^2 \frac{\exp\{-2\eta_0 z_0\}}{\eta_0} \lambda^{2m+3} d\lambda = \\ & \frac{4\pi j |\mathbf{p}_x|^2 (2m-1)!!}{k_0^{2m+2} (2m)!!} \int_0^\infty \frac{\eta_0 - \eta_1}{\eta_0 + \eta_1} \left( k_0^2 - \lambda^2 \frac{(2m+1)}{(2m+2)} \right) \left[ P_n^{(m)} \left( \frac{j}{k_0} \eta_0 \right) \right]^2 \frac{\exp\{-2\eta_0 z_0\}}{\eta_0} \lambda^{2m+1} d\lambda. \end{aligned} \quad (26)$$

Obtaining the real part from both sides of (26) and accounting for (22), we finally apprehend the following

$$\begin{aligned} & -\operatorname{Re} \int_{D_0/\overline{D}_i} J^*(Q, M_0) \mathbf{E}_0^r(Q) \cdot \mathbf{p}_x d\tau_Q = \\ & \frac{4\pi |\mathbf{p}_x|^2 (2m-1)!!}{k_0^{2m+2} (2m)!!} \operatorname{Im} \int_0^{k_1} \frac{\eta_0 - \eta_1}{\eta_0 + \eta_1} \left( k_0^2 - \lambda^2 \frac{(2m+1)}{(2m+2)} \right) \left[ P_n^{(m)} \left( \frac{j}{k_0} \eta_0 \right) \right]^2 \frac{\exp\{-2\eta_0 z_0\}}{\eta_0} \lambda^{2m+1} d\lambda. \end{aligned} \quad (27)$$

It is clear that, for the y-component, we can obtain a similar representation.



### 2.3. Results

In the previous section, we completed all preliminary considerations and are ready to formulate the main result.

**Theorem 1.** Let us consider the boundary value problem of excitation (1) of a penetrable scatterer deposited above a transparent substrate by a multipole of arbitrary order (4) and polarization  $\mathbf{p} = (p_x, p_y, p_z)$ , localized at the point  $M_0 = (0, 0, z_0)$  of the Cartesian coordinate system. Then, the extinction cross-section  $C_{ext} := C_{scs} + C_{abs}$  [27] accepts the following form:

$$C_{ext} = -\frac{4\pi}{k_0} \operatorname{Re} [D_n^{m+}(\mathbf{E}_0^s(M) \cdot \mathbf{p})]_{M=M_0} + \frac{\pi}{k_0^2} \left\{ \left[ \frac{2}{3} \beta_n^m + \frac{1}{3} \right] (p_x^2 + p_y^2) + \left[ \frac{2}{3} - \frac{2}{3} \beta_n^m \right] p_z^2 \right\} \|P_n^m\|^2 +$$

$$\frac{4\pi p_z^2 (2m-1)!!}{k_0^{2m+2} (2m)!!} \operatorname{Im} \int_0^{k_1} \frac{\varepsilon_1 \eta_0 - \varepsilon_0 \eta_1}{\varepsilon_1 \eta_0 + \varepsilon_0 \eta_1} \left[ P_n^{(m)} \left( \frac{j}{k_0} \eta_0 \right) \right]^2 \frac{\exp\{-2\eta_0 z_0\}}{\eta_0} \lambda^{2m+3} d\lambda +$$

$$\frac{4\pi (p_x^2 + p_y^2) (2m-1)!!}{k_0^{2m+2} (2m)!!} \operatorname{Im} \int_0^{k_1} \frac{\eta_0 - \eta_1}{\eta_0 + \eta_1} \left( k_0^2 - \lambda^2 \frac{(2m+1)}{(2m+2)} \right) \left[ P_n^{(m)} \left( \frac{j}{k_0} \eta_0 \right) \right]^2 \frac{\exp\{-2\eta_0 z_0\}}{\eta_0} \lambda^{2m+1} d\lambda. \quad (28)$$

It is clearly observed that, in case of an absence of the substrate  $\varepsilon_1 = \varepsilon_0 \Rightarrow k_1 = k_0 \Rightarrow \eta_1 = \eta_0$ , the Formula (28) is reduced to the following:

$$C_{ext}^0 = -\frac{4\pi}{k_0} \operatorname{Re} [D_n^{m+}(\mathbf{E}_0^s(M) \cdot \mathbf{p})]_{M=M_0} + \frac{\pi}{k_0^2} \left\{ \left[ \frac{2}{3} \beta_n^m + \frac{1}{3} \right] (p_x^2 + p_y^2) + \left[ \frac{2}{3} - \frac{2}{3} \beta_n^m \right] p_z^2 \right\} \|P_n^m\|^2, \quad (29)$$

which represents the OT for multipole excitations of a particle in free space [25].

Let us consider a specific case: excitation by a vertical electric quadrupole  $p_x = p_y = 0$  deposited in  $M_0 = (0, 0, z_0)$ . This case corresponds to  $m = 0$ ,  $n = 1$ . Subsequently,

$$D_1^0 = P_1 \left( \frac{j}{k_0} \frac{\partial}{\partial z} \right) = \frac{j}{k_0} \frac{\partial}{\partial z}.$$

Using an estimate of the second term in (29), and then following [25], we obtain the following:

$$\int_0^\pi [P_1(\cos \theta)] \sin^2 \theta \sin \theta d\theta = \int_{-1}^1 x^2 (1-x^2) dx = \frac{4}{15}.$$

Considering that  $D_1^{0+} = -\frac{j}{k_0} \frac{\partial}{\partial z}$ , Formula (29) can be rewritten as

$$C_{ext}^0 = \frac{4\pi}{k_0^2} \operatorname{Im} \left[ \mathbf{p}_z \cdot \frac{\partial}{\partial z} \mathbf{E}_0^s(M) \right]_{M=M_0} + \frac{4\pi}{15k_0^2}. \quad (30)$$

We subsequently transform the corresponding integral in (28) as

$$\frac{4\pi p_z^2}{k_0^2} \operatorname{Im} \int_0^{k_1} \frac{\varepsilon_1 \eta_0 - \varepsilon_0 \eta_1}{\varepsilon_1 \eta_0 + \varepsilon_0 \eta_1} \left[ \frac{j}{k_0} \eta_0 \right]^2 \frac{\exp\{-2\eta_0 z_0\}}{\eta_0} \lambda^3 d\lambda =$$

$$- \frac{4\pi p_z^2}{k_0^4} \operatorname{Im} \int_0^{k_1} \frac{\varepsilon_1 \eta_0 - \varepsilon_0 \eta_1}{\varepsilon_1 \eta_0 + \varepsilon_0 \eta_1} \exp\{-2\eta_0 z_0\} \eta_0 \lambda^3 d\lambda.$$

Then, we finally obtain the extinction cross-section for the vertical electric quadrupole in the following form:

$$C_{ext} = \frac{4\pi p_z^2}{15k_0^2} + \frac{4\pi}{k_0^2} \operatorname{Im} \left[ \mathbf{p}_z \cdot \frac{\partial}{\partial z} \mathbf{E}_0^s(M) \right]_{M=M_0} - \frac{4\pi p_z^2}{k_0^4} \operatorname{Im} \int_0^{k_1} \frac{\varepsilon_1 \eta_0 - \varepsilon_0 \eta_1}{\varepsilon_1 \eta_0 + \varepsilon_0 \eta_1} \exp\{-2\eta_0 z_0\} \eta_0 \lambda^3 d\lambda. \quad (31)$$

The first term in (31) is responsible for the energy emitted by the excited source at infinity in free space, and the last term is responsible for the presence of the transparent prism.

## 2.4. Discussion

The result obtained is the most important generalization of the optical theorem to the case of a local scatterer of an arbitrary internal structure, located near a transparent substrate, and excited by an electric multipole of arbitrary polarization and arbitrary order. Previous generalizations of the OT were made for the case of a scatterer in free space [17] or for the case of excitation by some special case of multipole excitation [13]. In all these cases, the expression for the extinction cross-section is expressed in a closed analytical form, which includes only definite integrals, and there are no Sommerfeld integrals which are responsible for the near field.

An essential difference between excitation by a multipole and a plane wave is the presence of a constant term in Equations (28) and (29), which is responsible for the radiation energy of the multipole itself, in the absence of a scatterer. This term is absent for the case of the classical formula for excitation by a plane wave, since the energy flux of a plane wave through any closed surface is equal to zero. Therefore, the obtained Formulas (28) and (29) convert into the classical case, even when the local source of excitation is moving to infinity.

The generalized optical theorem (28) obtained can be used to test computer models by comparing the scattering cross-section for non-absorbing particles with the extinction cross-section. The fact is that the extinction cross-section is presented in a closed analytical form, and the scattering cross-section for particles located near a transparent substrate is expressed in terms of elementary functions [24], which makes the implementation of such a test a simple task. In addition, it seems to be useful for analyzing the fine structure of the fluorescence process [28] and for considering the excitation of optical antennas located on a transparent substrate [29]. Some preliminary results obtained from the application of the generalized optical theorem have been published in [30].

## 3. Conclusions

In the present paper, we generalized the optical theorem to the case of a penetrable particle deposited near a transparent substrate excited by an electric multipole of arbitrary order and polarization. The generalization of the OT, performed in the present study, is part of the scientific progress in the accumulation of knowledge and the expansion of its area of application. As noted in the introduction, the generalization of the OT can be used in the same situations as the classical OT. It can be used, for example, for the verification of a new computer model when a local non absorbing particle, in the presence of a transparent substrate, is excited by a multipole, or to perform investigations of the fine structure of the fluorescent process for Raman spectroscopy or for the analysis of the excitation of the optical antennas deposited on a transparent substrate. It should be emphasized that multipoles are increasingly more involved in practical optics. They are most actively used to determine the contribution of various harmonics (dipoles, quadrupoles, among others) to scattering by a local obstacle [6,31].

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## Appendix A

The corresponding spectral functions  $v_{11}, v_{33}, v_{31}$  provide satisfaction of the transmission conditions at  $z = 0$  and accept the following form:

$$v_{ll}(\lambda, z, z_0) = \begin{cases} \frac{\exp\{-\eta_0|z-z_0|\}}{\eta_0} + A_{ll}(\lambda, z_0) \frac{\exp\{-\eta_0 z\}}{\eta_0}, & z_0 > 0, z \geq 0, \\ B_{ll}(\lambda, z_0) \frac{\exp\{\eta_1 z\}}{\eta_0}, & z_0 > 0, z \leq 0, l = 1, 3; \end{cases} \quad (\text{A1})$$

$$v_{31}(\lambda, z, z_0) = \begin{cases} A_{31}(\lambda, z_0) \exp\{-\eta_0 z\}, & z_0 > 0, z \geq 0, \\ B_{31}(\lambda, z_0) \exp\{\eta_1 z\}, & z_0 > 0, z \leq 0 \end{cases} \quad (\text{A2})$$

here  $\eta_{0,1}^2 = \lambda^2 - k_{0,1}^2; k_{0,1} = k \cdot n_{0,1}$  and

$$A_{11}(\lambda, z_0) = \frac{\eta_0 - \eta_1}{\eta_0 + \eta_1} \zeta_0; B_{11}(\lambda, z_0) = \frac{2\eta_0 \zeta_0}{\eta_0 + \eta_1}; \quad (\text{A3})$$

$$A_{33}(\lambda, z_0) = \frac{\varepsilon_1 \eta_0 - \varepsilon_0 \eta_1}{\varepsilon_1 \eta_0 + \varepsilon_0 \eta_1} \zeta_0; B_{33}(\lambda, z_0) = \frac{2\varepsilon_1 \eta_0 \zeta_0}{\varepsilon_1 \eta_0 + \varepsilon_0 \eta_1}; \quad (\text{A4})$$

$$A_{31}(\lambda, z_0) = \frac{2(\varepsilon_1 - \varepsilon_0) \zeta_0}{(\eta_0 + \eta_1)(\varepsilon_1 \eta_0 + \varepsilon_0 \eta_1)}; B_{31}(\lambda, z_0) = \frac{2(\varepsilon_1 - \varepsilon_0) \zeta_0}{(\eta_0 + \eta_1)(\varepsilon_1 \eta_0 + \varepsilon_0 \eta_1)}, \quad (\text{A5})$$

where  $\zeta_0 = \exp\{-\eta_0 z_0\}$ .

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