



Article Bifurcation Diagram of the Model of a Lagrange Top with a Vibrating Suspension Point

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Abstract: The article considers a model system that describes a dynamically symmetric rigid body in the Lagrange case with a suspension point that performs high-frequency oscillations. This system, reduced to axes rigidly connected to the body, after the averaging procedure, has the form of the Hamilton equations with two degrees of freedom and has the Liouville integrability property of a Hamiltonian system with two degrees of freedom, which describes the dynamics of a Lagrange top with an oscillating suspension point. The paper presents a bifurcation diagram of the moment mapping. Using the bifurcation diagram, we presented in geometric form the results of the study of the problem of stability of singular points, in particular, singular points of rank zero and rank one.

Keywords: completely integrable Hamiltonian systems; Lagrange top; bifurcation diagram

MSC: 37J35; 37J20; 70H33

1. Introduction

In the framework of this article, we study a bifurcations of Liouville tori, equilibrium positions and special periodic motions that arise in dynamics of a heavy rigid body with an axial symmetry of mass distribution moving in a uniform gravitational field around one of its points. This point (suspension point) lies on the axis of dynamical symmetry. The position of the suspension point, in a general case, does not coincide with the center of inertia of the body. The suspension point performs high-frequency periodic or conditionally periodic oscillations (vibrations) of small amplitude. The cause of these forced oscillations, the differential equations of the motion of a rigid body, describing its orientation relative to the inertial frame of reference, explicitly depend on time. In the works of Markeev [1-3]and Kholostova [4], the procedure of averaging over the period of the driving force is indicated. This leads the original equations of motion, presented in the form of Euler-Poisson equations, to an approximate system with respect to new variables, which also has the form of Euler-Poisson equations but is already autonomous. It turns out that the reduced system of differential equations is completely integrable in a Liouville sense Hamiltonian system with two degrees of freedom. Such a system can be subjected to bifurcation analysis and clearly demonstrate the problems of stability research based on the analysis of the types of singularities; namely, stable solutions correspond to elliptic nondegenerate singularities, and unstable solutions correspond to hyperbolic non-degenerate ones [5].

One of the fundamental concepts in the analysis of phase topology and the study of bifurcations of Liouville tori, equilibrium positions, and periodic motions is the integral mapping and analytical representation of the critical subsystem, which, for given specific values of the physical parameters of the system, is an almost Hamiltonian system



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Copyright: © 2023 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). with one degree of freedom. The concept of a critical subsystem arose in the works of M. P. Kharlamov, published in the first years of the 2000s, devoted to the study of irreducible integrable systems with more than two degrees of freedom [6]. In the case of integrable Hamiltonian systems with *n* degrees of freedom, which have the Hamilton function and additional first integrals in the form of a polynomial or a rational expression, it was shown that the set of critical values of the integral mapping \mathcal{F} can be written as the relation P = 0, where P is a polynomial with respect to phase variables. Factorization of this polynomial into irreducible factors $P = \prod_i L_i$ allows us to define the critical subsystem \mathcal{M}_i as the set of critical points of the zero level of some function L_i . From this point of view, the critical point of an integral mapping of rank k is locally the intersection point of n - k subsets of critical subsystems. Then, the integrals L_i of these subsystems make it possible to obtain symplectic operators A_{L_i} whose eigenvalues determine the type of the corresponding critical point. The bifurcations that arise when the surfaces $\mathcal{F}(M_i)$ intersect at the point $\mathcal{F}(x)$ make it possible to obtain a semilocal classification of singular points. For a number of integrable cases of rigid body dynamics (the Kowalevski top under the action of two force fields, the Kowalevski-Sokolov top, the Kowalevski-Yehia integrable case), it was possible to efficiently implement bifurcation analysis based on the analytical description of critical subsystems [7–9].

2. Model and Definitions

Consider a rigid body with dynamic symmetry, the center of inertia of which belongs to the axis of dynamic symmetry. Let the body move around one of its points (suspension point), in the general case, not coinciding with the center of mass. It is well known that the equations of motion of such a body have the form of the generalized Kirchhoff equations

$$\dot{M} = M \times \frac{\partial H}{\partial M} + \gamma \times \frac{\partial H}{\partial \gamma}, \qquad \dot{\gamma} = \gamma \times \frac{\partial H}{\partial M}$$
 (1)

with Hamilton function

$$H = \frac{1}{2} \left(M_1^2 + M_2^2 + c M_3^2 \right) + a \gamma_3 - \frac{1}{2} b \gamma_3^2.$$
⁽²⁾

We introduced the notation $M = \{M_1, M_2, M_3\}$ and $\gamma = \{\gamma_1, \gamma_2, \gamma_3\}$ for the components of the angular momentum and the unit vector of the vertical, with respect to a coordinate system rigidly connected to the rigid body, the axes of which are directed along the principal axes of inertia and pass through the suspension point. The physical meaning of the parameters *a*, *b* and *c* can be interpreted according to [1,3]. Namely, *a* means a parameter related to the distance from the point of attachment to the center of mass. Everywhere below the sign of *a* is assumed to be fixed. The value *b* describes the difference between the averaged squared projections of the velocity of the suspension point onto the axis *OX* and *OX* in the coordinate system *OXYZ* with the origin at the suspension point. The value of *b* can be either positive or negative. The parameter *c* is a positive value characterizing the ratio of the principal components of the tensor of inertia of the considered dynamically symmetric body.

We can rewrite Equation (1) in Hamiltonian form

$$\dot{\boldsymbol{M}} = \{\boldsymbol{M}, \boldsymbol{H}\}, \quad \dot{\boldsymbol{\gamma}} = \{\boldsymbol{\gamma}, \boldsymbol{H}\}$$

with respect to Lie–Poisson bracket which corresponds to the Lie algebra e(3),

$$\{M_i, M_j\} = -\varepsilon_{ijk}M_k, \{M_i, \gamma_j\} = -\varepsilon_{ijk}\gamma_k, \quad \{\gamma_i, \gamma_j\} = 0.$$

$$(3)$$

It is well known that Lie–Poisson bracket (3) is degenerate and has two Casimir functions, which commute with respect to the structure (3) with any functions of M, γ :

$$L = (M, \gamma)$$
 (integral of areas),
 $\Gamma = |\gamma|^2$ (geometric integral).

Due to the existence of Casimir functions, the phase space \mathcal{P} of a system under consideration is the tangent bundle $T\mathbb{S}^2$ of the two-dimensional sphere \mathbb{S}^2 :

$$\mathcal{P} = \{ (\boldsymbol{M}; \boldsymbol{\gamma}) : L = \ell, \Gamma = 1 \}.$$

In addition, system (1) has one additional first integral, linear of angular momentum, namely the Lagrange integral

$$F = M_{3}$$
.

The first integral F and Hamilton function H form a complete involutive set of integrals of system (1) on \mathcal{P} and according to the Liouville–Arnold theorem existence, such a set of integrals are sufficient for complete integrability of our Hamiltonian system in a Liouville sense. It means that a regular level surface of the first integrals of our system is a non-connective union of tori filled with conditionally periodic trajectories [10]. The integral mapping (momentum mapping)

$$\mathcal{F}: \mathcal{P} \to \mathbb{R}^2, \tag{4}$$

by definition is $(f,h) = \mathcal{F}(x) = (F(x), H(x))$. Let \mathcal{C} denote the set of all critical points of the integral mapping, i.e., points at which the rank of mapping is not maximal rank $d\mathcal{F}(x) < 2$. The set of critical values, i.e., image of critical set of integral mapping $\Sigma = \mathcal{F}(\mathcal{C} \cap \mathcal{P})$, is called the bifurcation diagram. In the present paper, we continue the study of the singularities of the momentum mapping, which was started in [11], where the points of rank 0 were determined. Be reminded that rank-zero singularities of the integral mapping correspond to equilibrium points of dynamical system. Paper [3] contains stability analysis of the upper equilibrium with the classical approach. Our results, which were obtained by using an analysis of the type of singularities of the integral mapping, showed analogous conclusions about the upper equilibrium like for the classical method, and in addition revealed conditions under which the lower equilibrium position becomes unstable. Another unique phenomenon is observed in the considered mechanical system, namely the appearance of a double pinched torus.

Finally, in the current paper, we derive in analytical manner the bifurcation diagram Σ of the momentum mapping \mathcal{F} for the system (1).

3. Regular Precessions—Critical Points of Rank 1 Integral Mapping

The critical points of the integral mapping (4) can be determined from the condition

$$\operatorname{rank}(H \times F \times L \times \Gamma) < 4.$$
(5)

This method will lead to a description of the critical subsystem for the rank 1 features of the integral mapping (4).

The condition (5) is equivalent to a redundant system of nonlinear equations on \mathcal{P} :

$$F_k = 0, \quad k = 1, \dots, 5,$$
 (6)

where

$$\begin{split} F_1 &= \gamma_1 M_2 - \gamma_2 M_1, \\ F_2 &= \gamma_3 M_1^2 - \gamma_1 M_1 M_3 + (a - b\gamma_3) \gamma_1^2, \\ F_3 &= \gamma_3 M_2^2 - \gamma_2 M_2 M_3 + (a - b\gamma_3) \gamma_2^2, \\ F_4 &= (a - b\gamma_3) \gamma_1 \gamma_2 + (\gamma_3 M_2 - \gamma_2 M_3) M_1, \\ F_5 &= (a - b\gamma_3) \gamma_1 \gamma_2 + (\gamma_3 M_1 - \gamma_1 M_3) M_2. \end{split}$$

Note that there is a functional relationship between F_k in the form of the following relations:

$$(F_{3}\gamma_{1}^{-} - \gamma_{2}F_{2} - 2F_{1}^{-}\gamma_{3})^{2} - 4\gamma_{2}^{2}[M_{3}^{2}\gamma_{1}^{2} + 2\gamma_{3}F_{2} - 4\gamma_{1}^{2}\gamma_{3}(a - b\gamma_{3})]F_{1}^{2} = 0,$$

$$(F_{4,5}\gamma_{1} \mp M_{3}\gamma_{1}F_{1} - \gamma_{2}F_{2})^{2} - [M_{3}^{2}\gamma_{1}^{2} + 2\gamma_{3}F_{2} - 4\gamma_{1}^{2}\gamma_{3}(a - b\gamma_{3})]F_{1}^{2} = 0,$$

$$F_{4} - F_{5} = M_{3}F_{1}.$$

$$(7)$$

It follows from the relations (7) that F_3 , F_4 and F_5 are functionally expressed in terms of F_1 and F_2 , which, as it is easy to check, are independent on $\mathcal{P} \setminus \{M_1 = M_2 = \gamma_1 = \gamma_2 = 0, M_3 = \pm \ell, \gamma_3 = \pm 1\}$. Denoted by \mathcal{M} is the closure of the set of solutions of the following system

$$\mathcal{M}: \begin{cases} F_1 = 0, \\ F_2 = 0. \end{cases}$$
(8)

Thus, the redundant system of nonlinear Equation (6) is equivalent to (8), which defines *critical subsystem* M by P.

Theorem 1. The set of critical points \mathcal{M} integral mapping (4) coincides with the set of solutions of the system (8). The set \mathcal{M} on \mathcal{P} is a two-dimensional invariant submanifold of the system (1) with the Hamiltonian (2).

Proof. To prove the invariance of the set \mathcal{M} , we find the brackets $\{F_1, H\}$ and $\{F_2, H\}$:

$$\begin{split} \dot{F}_1 &= \{F_1, H\} = -F_3 - F_4, \\ \dot{F}_2 &= \{F_2, H\} = 2[-b\gamma_1^2 - 2\gamma_3(a - b\gamma_3) \\ + M_1^2 + (1 - c)M_3^2]F_1 + 2M_3(1 - 2c)F_4. \end{split}$$

Since the expressions F_3 and F_4 are functionally expressed in terms of F_1 and F_2 from the relations (7), the invariance of \mathcal{M} follows from here. \Box

Theorem 2. The image of the critical subsystem M, i.e., the bifurcation diagram Σ , is part of the discriminant set of the polynomial R(x), where

$$R(x) = -bx^{4} + 2ax^{3} + [b + (c - 1)f^{2} - 2h]x^{2} + 2(f\ell - a)x + 2h - cf^{2} - \ell^{2}.$$
(9)

Proof. For the proof, we use easily verifiable equalities that are valid at all points of the phase space \mathcal{P} :

$$\begin{cases} R(\gamma_3) = F_1^2, \\ F_2 + F_3 = -\frac{1}{2}R'(\gamma_3). \end{cases}$$
(10)

From the relations (7) and (10) follows $R(\gamma_3) = R'(\gamma_3) = 0$, i.e., at the points of the critical subsystem \mathcal{M} , the polynomial R(x) for $x = \gamma_3$ has multiple roots. \Box

Thus, the theorem shows that the bifurcation diagram, as an image of the set of critical points of the moment mapping, is part of the discriminate set of the polynomial R(x). We present the parametrization of the critical subsystem (8), which will be used in the future to determine the types of features and study the stability of the critical subsystem \mathcal{M} :

$$M_{1} = \lambda_{1,2} \frac{\gamma_{1}}{\gamma_{3}}, M_{2} = \lambda_{1,2} \frac{\gamma_{2}}{\gamma_{3}}, M_{3} = \gamma_{3} = s,$$

$$\gamma_{1} = C_{1} \sin(A_{1,2}t) + C_{2} \cos(A_{1,2}t),$$

$$\gamma_{2} = C_{1} \cos(A_{1,2}t) - C_{2} \sin(A_{1,2}t),$$
(11)

where

$$A_{1,2} = cf - \lambda_{1,2},$$

$$\lambda_{1,2} = \frac{1}{2} \Big[f \pm \sqrt{f^2 - 4s(a - bs)} \Big].$$
(12)

In the Formula (11), the constant *s* is a parameter of the curve Σ :

$$\begin{cases} f = \frac{(1+s^2)\ell \pm (1-s^2)\sqrt{\ell^2 - 4s(a-bs)}}{2s}, \\ h = \frac{Q \pm \sqrt{\ell^2 - 4s(a-bs)}(1-s^2)[(c-1)s^2 + c]\ell}{4s^2}, \end{cases}$$
(13)

where

$$Q = 2bs^{2}[c(1-s^{2})^{2}-s^{4}] + 2as[s^{2}(1+s^{2})-c(1-s^{2})^{2} + [c+s^{2}+(c-1)s^{4}]\ell^{2}.$$

Note that the curve Σ is a parametrization of the discriminant set of the polynomial R(x) given by the formula (9).

The curve (13) has two cusp points depending on the values of the parameters *a*, *b*, ℓ . The parameter *s* = γ_3 , which defines the cusp points, satisfies the equation

$$P(s) = 0$$

where

$$P(s) = (a + 3as^2 - 4bs^3)^2 -[b - 3bs^2(s^2 + 2) + 2as(s^2 + 3)]\ell^2 + \ell^4$$

The resultant of the polynomial P(s) defines a family of curves Δ_k , k = 1, ..., 5 (*atlas of the bifurcation diagrams*):

$$\begin{aligned} \Delta_1 : \ell &= 0, \quad \Delta_2 : a^2 - b\ell^2 = 0, \\ \Delta_3 : (a^2 + 4b^2)^2 - 16b^3\ell^2 &= 0, \\ \Delta_4 : \ell^2 - 4(a - b) &= 0, \quad \Delta_5 : \ell^2 + 4(a + b) = 0, \end{aligned}$$

when passing through these, the structure of the discriminant set containing the bifurcation diagram changes qualitatively.

Figure 1 shows an atlas of bifurcation diagrams for a fixed value of the parameter a = -1, consisting of curves Δ_k that split the plane of parameters (b, ℓ) into five regions (a), (b), (c), (d), (e). In each of these domains, the bifurcation diagram is the same.

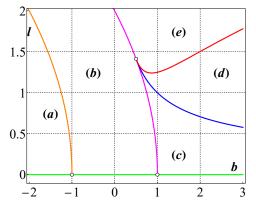


Figure 1. The atlas of the bifurcation diagrams.

Various types of bifurcation diagrams are shown in Figure 2. The values of the constants of the first integrals corresponding to the equilibrium positions determine two points P^{\pm} on the plane $\mathbb{R}^2(f, h)$

$$P^{+}: \begin{cases} f = \ell \\ h = \frac{1}{2}c\ell^{2} + a - \frac{b}{2}, \end{cases} P^{-}: \begin{cases} f = -\ell, \\ h = \frac{1}{2}c\ell^{2} - a - \frac{b}{2} \end{cases}$$

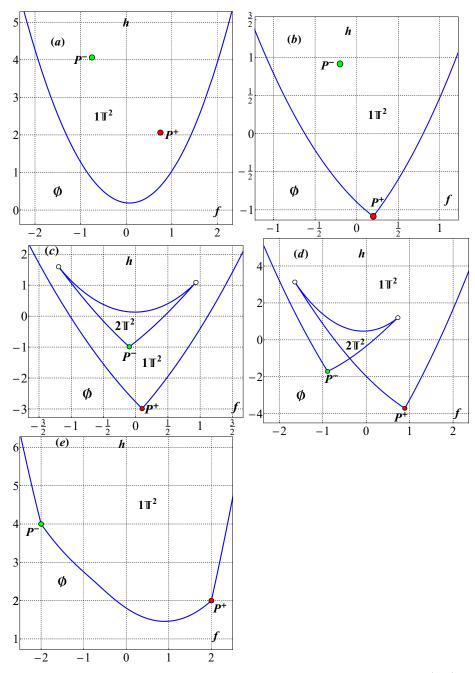


Figure 2. The regions marked with the empty set correspond to the points of the (f,h)-plane in which there are no possible motions. The points of bifurcation curves correspond to the critical values of the momentum map, which are the images of critical points of rank 1 (periodic motions). The regions of the (f,h)-plane marked with $1\mathbb{T}^2$ or $2\mathbb{T}^2$ correspond to the values of the first integrals for which preimage of the momentum map contains 1 or 2 two-dimensional tori, respectively. Points P^+ and P^- correspond to focus singularities of rank 0 (equilibrium points). Qualitatively different types of bifurcation diagrams (**a–e**) are determined by the constants (b, ℓ) and correspond to the regions shown in Figure 1.

We find, explicitly, the bracket $\{F_1, F_2\}$ at the point of the critical subsystem \mathcal{M} :

$$\{F_1, F_2\} = \frac{\gamma_1^2}{2\gamma_3^2}P(s)$$

As expected, the degeneracy of the symplectic structure occurs at the points where the polynomial P(s) vanishes, i.e., at the cusp points of the bifurcation curve Σ .

4. Stability of Critical Trajectories

As an application, we investigate the problem of the stability of critical trajectories (11). It is sufficient to determine the type (elliptic/hyperbolic) at any one of the points (f, h) of the smooth branch of the curve Σ given by the formula in (13).

The type of critical point x_0 of rank 1 in an integrable system with two degrees of freedom is calculated as follows. It is necessary to specify the first integral *G*, such that $dG(x_0) = 0$ and $dG \neq 0$ in the neighborhood of this point. The point x_0 turns out to be fixed for the Hamiltonian field sgrad *G* and it is possible to calculate the linearization of this field at a given point – the symplectic operator A_G at the point x_0 . This operator will have two zero eigenvalues, the remaining multiplier of the characteristic polynomial has the form $\mu^2 + \mu_0$, where $\mu_0 = \frac{1}{2}$ trace (A_G^2) . At $\mu_0 > 0$, we get a point of type "center" (the corresponding periodic solution has an elliptic type, is a stable periodic solution in phase space, the limit of a concentric family of two-dimensional regular tori), and at $\mu_0 < 0$ we get a point of type "saddle" (the corresponding periodic solution has a hyperbolic type, there are movements asymptotic to this solution lying on two-dimensional separatrix surfaces). As an integral of *G*, we can take the function

$$G = H - A_{1,2}F - \frac{\lambda_{1,2}}{s}L + \frac{\lambda_{1,2}f - as + bs^2}{2s^2}\Gamma.$$

Here, the expressions $A_{1,2}$ and $\lambda_{1,2}$ are defined by the Formula (12), and the parameter *s* defines a point on the bifurcation curve (13).

The coefficient μ_0 for the characteristic polynomial A_G has the explicit form

$$\mu_0 = \frac{1}{2} \operatorname{trace} \left(A_G^2 \right) = P(s),$$

where is the polynomial P(s) is responsible for the cusp points of the bifurcation curve (13). Thus, where the polynomial P(s) has a negative sign, regular precessions will be unstable. In Figure 2c,d, this corresponds to the branch of the bifurcation curve Σ between the cusp points. At the remaining points of the Σ bifurcation curve, regular precessions have an elliptical type, which corresponds to the stability of regular precessions.

Note that the work [3] is devoted to the study of the stability of regular precessions of a Lagrange top with a vibrating suspension point. In the present paper, the study of the stability of regular precessions is carried out on the basis of determining the type of singularity and geometric presentation on the bifurcation diagram of the equilibrium point and periodic motion stability.

The most important advantages of the method used in this paper to study the Lagrange top with a vibrating suspension point are the geometric clarity of the form of presentation of the results and general methods for studying the phase topology of integrable Hamiltonian systems. Having constructed the image of the critical set, we obtain a partition of the parameter space of the system under study into areas, inside which the number of connected components of the level set of first integrals does not change, and the nature of the singularities of the Liouville foliation is determined by the eigenvalues of the linearization of the symplectic operator at singular points. The bifurcation diagram, in such a clear geometric way, contains information about the nature of the stability of equilibrium positions and periodic solutions. In contrast to this technique, when studying the stability of equilibrium positions or periodic motions using standard methods used, for example, in [1-4], there is a need to construct the Lyapunov function or study the normal form in the vicinity of the equilibrium position (periodic motion). Here, there is a finding which, in itself, is a non-trivial mathematical problem and the construction of the Lyapunov function or normal form is the central problem of stability theory. On the other hand, classical methods almost always answer the question about the type of stability of singular solutions, even when the system is not Liouville integrable or is not Hamiltonian at all. However, the method presented in the article gives an answer to the question of

the stability of primarily Liouville integrable Hamiltonian systems. At the moment, this approach is generalized to nonholonomic systems and in the case of dissipative systems, the question of the possibility of generalizing it is currently open.

Finally, we should note the results of the publication [12] where the authors presented four generic types of bifurcation diagrams. In this paper, we present five different types of bifurcation diagrams. This fact is not a contradiction because the objects that are being classified are different. Lagrange top was studied in [12] as a system with three degrees of freedom with three-dimensional bifurcation diagrams, and there are four types. In the present paper, the reduction of the top to the body frame is studied, which is a system with two degrees of freedom and hence a two-dimensional bifurcation diagram, and there are five types. The objects are related in that planar slices of the bifurcation diagram in [12] give the bifurcation diagrams in this paper, but the number of topologically different planar slices can be larger than the number of topologically different three-dimensional diagrams.

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