



Article Developed Gorilla Troops Technique for Optimal Power Flow Problem in Electrical Power Systems

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Abstract: This paper presents a developed solution based on gorilla troops optimization technique for OPFP in EPSs. The GTOT is motivated by gorillas' group behaviors in which several methods are replicated, such as migration to an unfamiliar location, traveling to other gorillas, migration toward a specific spot, accompanying the silverback, and competing for adult females. The multi-dimension OPFP in EPSs is examined in this article with numerous optimizing objectives of fuel cost, power losses, and harmful pollutants. The system's power demand and transmission losses must be met as well. The developed GTOT's evaluation is conducted using an IEEE standard 30-bus EPS and practical EPS from Egypt. The created GTOT is employed in numerous evaluations and statistical analyses using many modern methods such as CST, GWT, ISHT, NBT, and SST. When compared to other similar approaches in the literature, the simulated results demonstrate the GTOT's solution efficiency and robustness.

Keywords: gorilla troops optimization technique; electrical power systems; optimal power flow; harmful pollutants; fuel costs; power losses

MSC: 90-08

1. Introduction

The optimum operational analysis is critical in determining the projected financial return for electrical networks. The energy supply is shifting around the globe towards sustainability, low carbon content, and high efficiency [1]. The increased load demand acts as an urgent challenge for power system operators. The economic and environmental prospects of power generations in modern power systems are considered the weighty research targets and the key concern of electric utility operators. The OPFP is a non-linear, multi-model issue in EPSs for power system control and operation. Using OPFP, pecuniary and safe operating circumstances of EPSs can be elaborated [2]. The solution of OPFP is currently the principal strategy for controlling and operating the modern power grids [3]. The OPFP can optimize one or even more targets such as cost of fuel, EPS sources pollution, and system losses. These goals may be met while maintaining load flow balancing and keeping operating variables inside the corresponding limitations, including voltages restrictions, transmission network limits, valve constraints, and generator output limits [4].



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Copyright: © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). Various standard mathematic methodologies were proposed to address the OPFP, such as semidefinite programming [5], non-linear programming [6], linear programming [7,8], quadratic programming [9,10], fuzzy linear programming [11], sequential unconstrained minimization technique [12], Newton-based method [13,14] and interior point approach [15–17]. A myriad of these approaches can effectively impose inequality restrictions and possess high convergence properties. Nevertheless, these conventional methods cannot generate the real optimal results because they rely on the initial settings, and consequently, they may get stuck in a local minimum. Additionally, every approach should be modeled with particular variants for OPFP, and they cannot deal with variables of discrete and integer natures smoothly. Hence, it is pivotal to develop metaheuristic techniques to overcome the mentioned disadvantages. The rapid growth of computers in the last two decades has led to a trend to solve diverse OPFP challenges using several heuristic (population-based) techniques [18,19]. Examples of these population-based heuristics are CBOA [20], BBO [21], PSO [22,23], HGWODE [24], GA [25], EMM [26], TLBO [27], and SAO [28].

In addition to that, recent techniques have been manifested to attain the solution of the large-scale OPFP: QMFT [29], COA [30], CSSO [31], and WCEMFT [32]. Moreover, a multi-group strategy was combined with the marine predators method to subdivide the original population into numerous separate groups in order to reduce the operation costs of power systems to maximize the economic advantages [33]. To tackle the economic dispatch difficulties of thermal generators, the DE method based on nondominated sorting was used to reduce pollution emissions and economic costs taking into account the dynamical schedule of thermal power units with consideration of ramp-rate, valve-point impact, and balance of power [34]. This method has been applied to two different systems with 13 and 40 thermal generating units.

Various augmentations of the algorithm strategies can be used to identify the best OPFP solution. An emended moth swarm algorithm (EMSA), in [35], has been presented to the OPFP with adjustment of quasi-opposition-based learning. Moreover, AGST, developed in [36], has been illustrated and applied with three objectives which are the fuel cost, emission, and losses taking into consideration different equality and inequality constraints. Additionally, ISSO was presented to minimize fuel costs, emissions, and power losses [37] by adjusting the movement technique of male and female spiders to acceptable ratios. In [38], a modified JAYA has been manifested by proposing modifying the equation for solutions that rely on the worst and best solutions, and technique has been applied to fuel cost, emission, voltage profile, and losses functions. Furthermore, IADE has been handled, in [39], with the self-adaptive penalty constraint technique and applied to the OPFP. To enhance exploration capability and the solution optimality convergence, quasioppositional-based learning has emerged with the Jaya technique in [40] to attain the OPFP solution. Moreover, an improved NSGA-III has been utilized with constraint management and decreasing selecting attempts to solve fuel costs, losses, and emission functions, as depicted in [41]. In [42], MRFO was implemented for EPSs to decrease the costs of fuel, losses, and pollution with/without the inclusion of voltage-source-converter stations.

Recently, a technique named gorilla troops optimization technique (GTOT) [43] proposed by (Benyamin Abdollahzadeh et al.) is developed in this article for multi-dimension OPFP in EPSs by adding valve constraint to the OPFP. GTOT is developed with five strategies to enlighten the exploitation and exploration of the optimization progression. To deal with the exploration phase, three strategies are verified: migration to a not recognized place, movement to other gorillas, and migration to a recognized location. Nevertheless, in the exploitation phase, two strategies are verified: follow the silverback and struggle for adult females. The superiority of this technique is that it has few parameters to be adjusted as well as it is simple to be implemented for engineering applications. The evaluation of GTOT quality is illustrated by applying it to various systems: IEEE standard 30 bus and practical WD Area. The results of the GTOT are compared with recent techniques and other existing techniques to demonstrate its efficacy and superiority between these techniques. The following are important contributions discussed in this work.

- The designed GTOT is exploited to reduce different target functions for minimizing the fuel costs, power losses, and pollutant emissions related to EPSs and applied on the IEEE standard 30 bus and practical WD.
- Multi-dimension operations with two or three objectives are developed in this work.
- The developed GTOT outperforms a number of current approaches, including CST, GWT, ISHT, NBT, and SST.
- Statistical analyses and stability assessments are developed in this work to demonstrate the capability of the proposed GTOT in handling the OPFP with different sizes and objective functions.
- The simulation results of related techniques in the literature are compared with the developed GTOT to demonstrate the robustness and solution quality of GTOT.
- Substantial consistency is accompanied by the proposed GTOT for handling the OPFP in EPSs.

The other portions of the whole work are as follows: Section 2 illustrates the GTOT approach. Section 3 establishes the OPFP construction, whereas Section 4 manifests the designed GTOT for OPFP. Furthermore, the simulated findings and discussions are denoted in Section 5, whilst the concluding notes are provided in Section 6.

2. Gorilla Troops Optimization Technique

The gorilla troops optimization technique (GTOT) simulates five strategic options to clarify the optimizing process's exploitation and exploration, as manifested in the following paragraphs.

2.1. Exploration Phase

In GTOT, every gorilla is denoted by a candidate solution, but at every optimizing operational phase, the global optimal solution is designated as a silverback. For the exploratory stage of development, three distinct methods are used. The first one is the movement to an unknown destination to raise GTOT exploration, while the second method is the movement of other gorillas to enhance the consistency between exploratory and exploitation. Moreover, the third method is the gorilla's movement in the path of a recognized destination to raise GTOT capabilities to discover varied computation spaces. In this technique, the factor (Pr) should be supplied in the band [0:1] prior to the optimizing process. When a factor (Pr) is greater than a random number, the movement to an undetermined location strategy is selected [44]. Additionally, if a random number is more than or equal to 50%, a movement in the path of an identifiable place is decided, whereas if a random number is less than 50%, a movement in the path of a recognized site is selected. Those three exploratory tactics can be mathematically stated as follows:

$$GX(g+1) = \begin{cases} LL + rd_1 \times (UL - LL), & \Pr > rand, \\ H \times L + X_r(g) \times (rd_2 - C), & 0.5 \le rand, \\ X(g) + (X(g) - GX_r(t)) \times rd_3 - (X(g) - GX_r(g) \times L^2), & 0.5 > rand \end{cases}$$
(1)

F

$$C = F \times (1 - Iter / MaxIter), \tag{2}$$

$$=\cos(2\times rd_4)+1,\tag{3}$$

$$L = C \times l \tag{4}$$

$$H = Z \times X(g) \tag{5}$$

$$Z = [-C, C]. \tag{6}$$

2.2. Exploitation Phase

In the exploitation stage of GTOT, two methods are used: following the silverback and competing for female adults. Based on factor *C* and contrasting it to the variable (*W*) (which can be changed), one of the two methods is selected.

The leader of the gorillas' group is the silverback that can make choices and directs the others to sources of food. If the *C* is greater than or equal to the value of *W*, this approach is chosen. Equation (7) can be used to illustrate this phenomenon.

$$GX(g+1) = L \times M(g) \times (X(g) - X_{siverback}) + X(g)$$
(7)

$$M(g) = \left(\left| (1/N) \sum_{i=1}^{N} GX_i(g) \right|^{2^L} \right)^{\left(\frac{1}{2^L}\right)}$$
(8)

If *C* is less than *W*, the next approach is competing for female adults, which is specialized for the evaluation stage. When adolescent gorillas reach adolescence, they engage in a violent rivalry with other males for the selection of female adults. This behavior is formulated as follows:

$$GX(g) = X_{silverback} - (X_{silverback} \times Q - X(g) \times Q) \times A,$$
(9)

$$Q = 2 \times rd_5 - 1 \tag{10}$$

$$A = \beta \times E \tag{11}$$

$$E = \begin{cases} N_1 & rand \ge 0.5\\ N_2 & rand < 0.5 \end{cases}$$
(12)

At the end of the exploitation stage, the cost of GX(g) is compared to its counterpart X(g), and if the cost of GX(g) is less than X(g), the GX(g) solution replaces it and becomes the optimal option (silverback). Figure 1 depicts the major processes of the developed GTOT for extracting characteristics from solar cell models [44].



Figure 1. Main steps of the GTOT.

3. Problem Formulation

In OPFP, the dependent and independent variables are represented. To illustrate, the generators' real power output and the reactive power injections of switching capacitors and reactors, voltages of the generators, tap changer settings, the number of on-load tap changers, generators, and reactive power sources, generator reactive power outputs, load bus voltage magnitudes, and transmission flow limits, number of transmission lines and load buses are the main pillars of OPFP. This problem can be expressed as follows:

$$Min OJ = \{OJ_1(x, y), OJ_2(x, y), \dots, OJ_m(x, y)\}$$
(13)

Subject to :
$$F(x,y) = 0$$
 (14)

$$M(x,y) \le 0 \tag{15}$$

3.1. Objectives

The primary goal is to calculate the OJ_1 in dollars per hour as follows:

$$OJ_1 = \sum_{k=1}^{Ng} C_k \times Pg_k^2 + B_k \times Pg_k + A_k$$
(16)

Because of the constant change in steam values in power plants, the value-point load influence generates fluctuations in the FCs. As a consequence, the FCs formula is produced by integrating sinusoidal rectifications to the quadratic formula, and OJ_2 can be represented as follows:

$$OJ_{2} = \sum_{k=1}^{Ng} C_{k} \times Pg_{k}^{2} + B_{k} \times Pg_{k} + A_{k} + \left| E_{k} \times (\sin(F_{k}(Pg_{k} - Pg_{k}^{\min}))) \right|$$
(17)

The second goal is to minimize OJ_3 from the power plants, which can be formulated as:

$$OJ_3 = \sum_{k=1}^{Ng} (\gamma_k \times Pg_k^2 + \beta_k \times Pg_k + \alpha_k) / 100 + \zeta_k \times e^{\lambda_k \times Pg_k}$$
(18)

The third goal is to minimize the overall power loss throughout the transmission system, which is mathematically stated as:

$$OJ_4 = \sum_{m=1}^{Nb} \sum_{n=1}^{Nb} G_{mn} \times (V_m^2 + V_n^2 - 2(V_m \times V_n \times \cos \theta_{mn}))$$
(19)

3.2. System Constraints

The load flow balance equations, Equations (20) and (21), manifest the equality constraints:

$$Pg_j - PL_j - V_j \times \sum_{k=1}^{Nb} V_k \times (G_{jk} \times \cos \theta_{jk} + B_{jk} \times \sin \theta_{jk}) = 0, \ j = 1, \dots, Nb$$
(20)

$$QL_j - V_j \times \sum_{k=1}^{Nb} V_k \times (G_{jk} \times \sin\theta_{jk} - B_{jk} \times \cos\theta_{jk}) = 0, \ j = 1, 2, \dots, Nb$$
(21)

Furthermore, the operating variables and the accompanying restrictions are written as follows:

$$Pg_k^{\min} \le Pg_k \le Pg_k^{max}, \ k = 1, \ 2, \ \dots, \ Ng$$
 (22)

$$Vg_k^{\min} \le Vg_k \le Vg_k^{\max}, \ k = 1, \ 2, \ \dots, \ Ng$$

$$(23)$$

$$Qg_k^{\min} \le Qg_k \le Qg_k^{\max}, \ k = 1, \ 2, \ \dots, \ Ng$$
(24)

$$Tap_{Tr}^{\min} \le Tap_{Tr} \le Tap_{Tr}^{\max}, \ Tr = 1, \ 2, \ \dots, \ Nt$$
(25)

$$Qc_{VAR}^{\min} \le Qc_{VAR} \le Qc_{VAR}^{max}, VAR = 1, 2, \dots, Nq$$
(26)

$$VL_j^{\min} \le VL_j \le VL_j^{\max}, \ j = 1, \ 2, \ \dots, \ NPQ$$

$$(27)$$

$$\left|S_{fl}\right| \leq S_{fl}^{max}, \, fl = 1, \, 2, \, \dots, \, Nf$$
 (28)

4. Developed Solution-Based GTOT for OPFP in EPSs

The equality and inequality constraints are indeed considered while handling the stated OPFP problem. To satisfy the equality conditions that describe power flow balance models, the NRA is applied. It depicts the steady-state operation of electric grids and meets the balance constraints. Consequently, the NRA is used by MATPOWER and represents a key framework for demonstrating three-phase systems [45].

4.1. Improvement of GTOT for Incorporating Operational Limitations of Independent Variables

The operational limitations of independent variables of Equations (22)–(26) may be rewritten as follows:

$$Pg_{k} = \begin{cases} Pg_{k}^{\min} & \text{if } Pg_{k} \leq Pg_{k}^{\min} \\ Pg_{k}^{\max} & \text{if } Pg_{k} \geq Pg_{k}^{\max} \end{cases}, \ k = 1, 2, \dots, Ng$$

$$(29)$$

$$Vg_{k} = \begin{cases} Vg_{k}^{\min} & \text{if } Vg_{k} \leq Vg_{k}^{\min} \\ Vg_{k}^{\max} & \text{if } Vg_{k} \geq Vg_{k}^{\max} \end{cases}, \ k = 1, 2, \dots, Ng$$
(30)

$$Qg_{k} = \begin{cases} Qg_{k}^{\min} & \text{if } Qg_{k} \leq Qg_{k}^{\min} \\ Qg_{k}^{\max} & \text{if } Qg_{k} \geq Qg_{k}^{\max} \end{cases}, \ k = 1, 2, \dots, Ng$$
(31)

$$Tap_{Tr} = \begin{cases} Tap_{Tr}^{\min} & \text{if } Tap_{Tr} \leq Tap_{Tr}^{\min} \\ Tap_{Tr}^{\max} & \text{if } Tap_{Tr} \geq Tap_{Tr}^{\max} \end{cases}, \ Tr = 1, 2, \dots, Nt$$
(32)

$$Qc_{VAR} = \begin{cases} Qc_{VAR}^{\min} & \text{if } Qc_{VAR} \leq Qc_{VAR}^{\min} \\ Qc_{VAR}^{\max} & \text{if } Qc_{VAR} \geq Qc_{VAR}^{\max} \end{cases}, VAR = 1, 2, \dots, Nq$$
(33)

As shown, the variables continue to reach their limitations, and if one of these surpasses ratings, they are regenerated randomly inside the appropriate constraints.

4.2. Improvement of GTOT for Incorporating Operational Limitations of Dependent Variables

Moreover, the target cost objective expands and penalizes the second category's limitations. Therefore, if the gorilla's location exceeds any of the appropriate constraints, it would be discarded in the next round. Such concepts may be used to construct the contemplated objective (*OJ*), as shown in Equation (34).

$$OJ = OJ_j + Pen_1 \sum_{NPQ} \Delta V_{LL}^2 + Pen_2 \sum_{Nq} \Delta Q_{GG}^2 + Pen_3 \sum_{N_f} \Delta S_{FF}^2, \ j = 1, \dots, m$$
(34)

where ΔV_{LL} , ΔQ_{GG} , and ΔS_{FF} are presented as:

$$\Delta V_{LL} = \begin{cases} V_L^{\min} - V_L & \text{if } V_L < V_L^{\min} \\ V_L^{max} - V_L & \text{if } V_L > V_L^{max} \end{cases}$$
(35)

$$\Delta Q_{GG} = \begin{cases} Q_G^{\min} - Q_G & \text{if } Q_G < Q_G^{\min} \\ Q_G^{\max} - Q_G & \text{if } Q_G > Q_G^{\max} \end{cases}$$
(36)

$$\Delta S_{FF} = S_F^{max} - S_F \quad if \ S_F > S_F^{max} \tag{37}$$

Figure 2 displays the stages of the designed GTOT for OPFP in EPSs.



Figure 2. Developed solution-based GTOT for OPFP in EPSs.

On the other side, in order to handle the model of multi-objectives, the different objective functions can be augmented using the weighted sum approach as follows:

$$OJ = w_1 \frac{OJ_1}{OJ_{1max}} + w_2 \frac{OJ_2}{OJ_{2max}} + w_3 \frac{OJ_3}{OJ_{3max}} + w_4 \frac{OJ_4}{OJ_{4max}}$$
(38)

where

$$\sum_{i=1}^{4} w_i = 1 \tag{39}$$

5. Simulation Results

The developed GTOT is implemented on the standard IEEE 30-bus EPS, a practical Egyptian EPS called West Delta-EPS (WD-EPS). Thirty simulation runs are conducted based on the developed GTOT with peak iterations of 300 and gorillas' group of 25 members. The first EPS is depicted in Figure 3, which consists of 41 transmission lines, 30 buses, 4 tap changers, 6 generators, and 9 reactive power devices. The complete data of this EPS are extracted from [46]. The highest and minimum generator voltages are 1.1 and 0.95 p.u., respectively. The second EPS is described in Figure 4, which consists of 52 buses. The highest and lowest generator voltages are 1.06 and 0.94 p.u., respectively. The developed GTOT and various other innovative techniques were presented to minimize the fuel generation costs such as CST [47], SST, NBT [48], and ISHT. MatlabR2017b is utilized to carry out the simulations using CPU (2.5 GHz) Intel(R)-Core (TM) i7-7200U and 8 GB of RAM.



Figure 3. IEEE 30-bus EPS [42,49].



Figure 4. Real WD-EPS [50,51].

5.1. Results of the First EPS

For this EPS, six scenarios are examined:

- Scenario 1: *OJ*₁ minimization of FGCs described in Equation (16);
- Scenario 2: *OJ*₂ minimization of FGCSs described in Equation (17);
- Scenario 3: *OJ*₃ minimization of PE described in Equation (18);
- Scenario 4: *OJ*₄ minimization of OPL described in Equation (19);
- Scenario 5: Merging *OJ*₁ and *OJ*₃ as a multi-objective function;
- Scenario 6: Merging *OJ*₁, *OJ*₃, and *OJ*₄ as a multi-objective function.

5.1.1. Scenario 1

For this scenario, the proposed GTOT is implemented, and the results are shown in Table 1. In this table, the values of the voltages of the six generators (Vg 1, Vg 2, Vg 5, Vg 8, Vg_{11} , and Vg_{13}) started at 1.05, 1.04, 1.01, 1.01, 1.05, and 1.05, respectively, and ended at 1.1, 1.088, 1.0619, 1.0696, 1.1, and 1.0, respectively. In addition to this, the values of four tap changer settings (Tap 6-9, Tap 6-10, Tap 4-12, and Tap 28-27) started at 1.0780, 1.0690, 1.0320, and 1.0680, respectively, and ended at 1.0551, 0.90, 0.99, and 0.9669, respectively. Additionally, the values of all nine reactive power devices (Qc 10, Qc 12, Qc 15, Qc 17, Qc 20, Qc 21, Qc 23, Qc 24, and Qc 29) started at 0 and ended at 5.0, 5.0, 5.0, 5, 4.4549, 4.978, 2.7861, and 5.0, respectively. Furthermore, the values of all six generators' real power output (Pg 1, Pg 2, Pg 5, Pg 8, Pg 11, and Pg 13) started at 99.24, 80.0, 50.0, 20.0, 20.0, and 20.0, respectively, and ended at 177.0191, 48.7234, 21.2921, 21.0921, 11.8996, and 12.0, respectively. As demonstrated in this table, the proposed GTOT reduces FGCs from 901.96 USD/h to 799.0831 USD/h compared to the initial case. This decrease is a proportion of 11.406%. In addition, Figure 5 depicts the convergent characteristic of the proposed GTOT, where it obtains the optimal solution in a short time with the effectiveness and robustness of the solution.

Variables		Initial	First Scenario
	Gen 1	1.0500	1.1000
_	Gen 2	1.0400	1.0880
Voltage setting of the generators (n.u)	Gen 5	Initial First Gen $_1$ 1.0500 1 Gen $_2$ 1.0400 1 Gen $_5$ 1.0100 1 Gen $_5$ 1.0100 1 Gen $_1$ 1.0500 1 Gen $_{11}$ 1.0500 1 Gen $_{13}$ 1.0500 1 Gen $_1$ 99.2400 17 Gen $_2$ 80.0000 2 Gen $_5$ 50.0000 2 Gen $_5$ 50.0000 2 Gen $_1$ 20.0000 1 Tr $_{6-9}$ 1.0780 1 Tr $_{6-9}$ 1.0780 1 Tr $_{6-9}$ 1.0690 0 Tr $_{6-10}$ 1.0690 0 Tr $_{6-27}$ 1.0680 0 Bus $_{10}$ 0.0000 5 Bus $_{10}$ 0.0000 5 Bus $_{12}$ 0.0000 5 Bus $_{21}$ 0.0000 2 Bus $_{21}$ 0.0000 5 </th <th>1.0619</th>	1.0619
voltage setting of the generators (p.u) =	Gen 1 1.0500 1.1000 Gen 2 1.0400 1.0880 Gen 5 1.0100 1.0619 Gen 8 1.0100 1.0619 Gen 11 1.0500 1.1000 Gen 13 1.0100 1.0696 Gen 11 1.0500 1.1000 Gen 13 1.0500 1.1000 Gen 13 1.0500 1.1000 Gen 13 1.0500 1.1000 Gen 2 80.0000 48.7234 Gen 5 50.0000 21.2921 Gen 11 20.0000 11.8995 Gen 13 20.0000 11.8995 Gen 13 20.0000 10.0511 Tr 6-9 1.0780 1.0551 Tr 6-9 1.0780 0.0900 Tr 28-27 1.0680 0.9668 Bus 10 0.0000 5.0000 Bus 12 0.0000 5.0000 Bus 20 0.0000 5.0000 Bus 21 0.0000 5.0000 Bus 23	1.0696	
_		1.0500	1.1000
_		1.0500	1.1000
	Gen 1	99.2400	177.0191
_	Initial Gen 1 1.0500 Gen 2 1.0400 Gen 5 1.0100 Gen 1 1.0500 Gen 11 1.0500 Gen 13 1.0500 Gen 13 1.0500 Gen 13 1.0500 Gen 2 80.0000 Gen 5 50.0000 Gen 1 20.0000 Gen 13 20.0000 Tr 6-9 1.0780 Tr 4-12 1.0320 Tr 28-27 1.0680 Bus 10 0.0000 Bus 12 0.0000 Bus 15 0.0000 Bus 20 0.0000 Bus 21 0.0000 Bus 23 0.0000 Bus 24 0.0000 Bus 29 0.0000	80.0000	48.7234
Output powers of the generators (MW)	Gen 5	Initial 1.0500 1.0400 1.0100 1.0100 1.0500 1.0100 1.0500 1.0500 1.0500 1.0500 1.0500 1.0500 1.0500 1.0500 20.0000 20.0000 1.0780 1.0780 1.0690 2.1.0320 7 1.0680 0.0000 2.0.0000 0.0000	21.2921
Sulput powers of the generators (1997) =	Initial First Gen 1 1.0500 1.0400 Gen 2 1.0400 1.0100 Gen 5 1.0100 1.0100 Gen 11 1.0500 1.0100 Gen 11 1.0500 1.0100 Gen 11 1.0500 1.0100 Gen 13 1.0500 1.0100 Gen 13 1.0500 1.0100 Gen 2 80.0000 4 Gen 5 50.0000 2 Gen 6 20.0000 1 Gen 11 20.0000 1 Gen 13 20.0000 1 Gen 13 20.0000 1 Tr 6-9 1.0780 1 Tr 4-12 1.0320 0 Bus 10 0.0000 1 Bus 12 0.0000 1 Bus 15 0.0000 1 Bus 20 0.0000 1 Bus 21 0.0000 1 Bus 23 0.0000 1 Bus 24 <td< th=""><th>21.0921</th></td<>	21.0921	
_	Gen 11	20.0000	11.8995
	Gen 13	20.0000	12.0000
	Tr 6-9	1.0780	1.0551
	Tr ₆₋₁₀	1.0690	0.9000
Tap setting of the transformers (p.u)	Tr ₄₋₁₂	1.0320	0.9900
		1.0680	0.9668
	Bus 10	0.0000	5.0000
	Bus 12	0.0000	5.0000
	Bus 15	Initial Firm 1 1.0500 2 1.0400 5 1.0100 8 1.0100 11 1.0500 13 1.0500 1 99.2400 2 80.0000 5 50.0000 8 20.0000 11 20.0000 13 20.0000 14 20.0000 15 50.0000 10 1.0690 12 1.0320 27 1.0680 10 0.0000 12 0.0000 12 0.0000 13 0.0000 14 0.0000 15 0.0000 16 0.0000 17 0.0000 13 0.0000 14 0.0000 15 0.0000 16 0.0000 17 0.0000 19 0.0000 29 </th <th>5.0000</th>	5.0000
	Bus 17		5.0000
Sources ar buses (MVAr)	Gen 1 1.0500 1.1000 Gen 2 1.0400 1.0880 Gen 5 1.0100 1.0619 Gen 8 1.0100 1.0696 Gen 11 1.0500 1.1000 Gen 13 1.0500 1.1000 Gen 13 1.0500 1.1000 Gen 1 99.2400 177.0191 Gen 2 80.0000 48.7234 Gen 5 50.0000 21.2921 Gen 5 50.0000 21.0921 Gen 11 20.0000 11.8995 Gen 13 20.0000 12.0000 Tr 6-9 1.0780 1.0551 Tr 6-9 1.0780 0.9900 Tr 4-12 1.0320 0.9900 Tr 28-27 1.0680 0.9668 Bus 10 0.0000 5.0000 Bus 12 0.0000 5.0000 Bus 15 0.0000 5.0000 Bus 20 0.0000 4.4549 Bus 21 0.0000 2.7861 Bus 24	4.4549	
	Bus 21	0.0000	4.9780
_	Bus 23	0.0000	2.7861
_	Bus 24	0.0000	5.0000
	Bus 29	0.0000	2.6571
Cost_Pg		901.9600	799.0831
Losses		5.8324	8.6263

 Table 1. Simulation outcomes based on the designed GTOT for the first scenario.

For this Scenario, Table 2 includes the comparison of reducing FGCs with a variety of other approaches. As shown, the developed GTOT obtains the minimum FGCs of 799.0831 USD/h, among other techniques.

 Table 2. Comparison for Scenario 1.

Technique	FGCs (USD/h)	Technique	FGCs (USD/h)
Developed GTOT	799.0831	IMFT [52]	800.3848
GWT [53]	800.4330	SOST [54]	801.5733
TLT [27]	800.4212	ICT) [55]	801.843
GT [56]	800.9728	DHST [57]	802.2966
MCST [58]	799.3332	GA [41]	802.1962
BHBT [57]	799.9217	AGT [56]	800.0212
MST [59]	800.5099	CST [47]	799.8266
IEOT [60]	799.688	EMRFT [42]	798.9888
NBT [61]	799.7516	JFST [62]	799.1065



Figure 5. Convergence feature of developed GTOT for Scenario 1.

5.1.2. Scenario 2

Taking into account the valve point impact, the developed GTOT is used to reduce FGCSs. For this scenario, the regarding results are shown in Table 3. In this table, the values of the voltages of the six generators (Vg 1, Vg 2, Vg 5, Vg 8, Vg 11, and Vg 13) started at 1.050, 1.040, 1.010, 1.010, 1.050, and 1.050, respectively, and ended at 1.1000, 1.0809, 1.0550, 1.0653, 1.0999, and 1.1000, respectively. In addition to this, the values of four tap changer settings (Tap 6-9, Tap 6-10, Tap 4-12, and Tap 28-27) started at 1.0780, 1.0690, 1.0320, and 1.0680, respectively, and ended at 1.1000, 0.9203, 1.0595, and 0.9936, respectively. Additionally, the values of all nine reactive power devices (Qc 10, Qc 12, Qc 15, Qc 17, Qc 20, Qc 21, Qc 23, Qc 24, and Qc 29) started at 0 and ended at 5.0000, 4.994, 4.8523, 5.0000, 5.0000, 5.0000, 3.7342, 4.5993, and 2.8053, respectively. Furthermore, the values of all six generators' real power output (Pg $_1$, Pg $_2$, Pg $_5$, Pg $_8$, Pg $_{11}$, and Pg $_{13}$) started at 99.2400, 80.0000, 50.0000, 20.0000, 20.0000, and 20.0000, respectively, and ended at 194.7610, 47.7489, 19.0111, 10, 10.0000, and 12.0014, respectively. As shown, the developed GTOT reduces the FGCSs from 901.9600 USD/h in the initial scenario to 832.7696 USD/h in the final scenario. This reduction in cost represents a percentage of 7.6700%. Additionally, Figure 6 displays the convergent characteristic of the proposed GTOT, where it obtains the optimal solution in a short time with the effectiveness and robustness of the solution.

Table 3. Simulation outcomes based on the designed GTOT for the second scenario.

Variables		Initial	Second Scenario
	Gen 1	1.0500	1.1000
	Gen ₂	1.0400	1.0809
 Voltage setting of the generators (p.u) - 	Gen 5	1.0100	1.0550
	Gen ₈	1.0100	1.0653
	Gen 11	1.0500	1.0999
	Gen 13	1.0500	1.1000

Variables		Initial	Second Scenario
	Gen 1	99.2400	194.7610
-	Gen 2	80.0000	47.7489
Output powers of the generators (MW)	Gen 5	50.0000	19.0111
	Initial Secon Gen 1 99.2400 19 Gen 2 80.0000 44 Gen 5 50.0000 14 Gen 8 20.0000 14 Gen 11 20.0000 14 Gen 13 20.0000 14 Gen 14 20.0000 14 Gen 15 0.00 14 Tr 6-10 1.0690 00 Tr 4-12 1.0320 11 Tr 28-27 1.0680 00 Bus 10 0.0 5 Bus 12 0.0 4 Bus 20 0.0 5 Bus 23 0.0 3 Bus 24 0.0 4 Bus 29 0.0 2 901.9600 83 3	10.0000	
	Gen 11	20.0000	10.0000
-	Gen 13	Initial S 1 99.2400 2 80.0000 5 50.0000 8 20.0000 11 20.0000 13 20.0000 9 1.0780 10 1.0690 12 1.0320 -27 1.0680 10 0.0 12 0.0 13 0.0 14 0.0 15 0.0 16 0.0 17 0.0 20 0.0 21 0.0 22 0.0 23 0.0 24 0.0 901.9600 5.8324	12.0014
	Tr 6-9	1.0780	1.1000
	Tr 6-10	1.0690	0.9203
Tap setting of the transformers (p.u)	p.u) Tr _{4–12} 1.0320	1.0595	
-	Tr 28-27	1.0680	0.9936
	Bus 10	0.0	5.0000
	Gen 1 99.2400 1 Gen 2 80.0000 4 Gen 5 50.0000 1 Gen 11 20.0000 1 Gen 11 20.0000 1 Gen 13 20.0000 1 Gen 14 20.0000 1 Gen 15 0.00 1 Tr 6-9 1.0780 1 Tr 4-12 1.0320 1 Bus 10 0.0 1 Bus 12 0.0 1 Bus 12 0.0 1 Bus 20 0.0 1 Bus 21 0.0 1 Bus 23 0.0 1 Bus 24 0.0 1 901.9600 8 1 901.9600 8 1	4.9949	
		4.8523	
	Bus 17	0.0	5.0000
Sources ar buses (MVAr)	Bus 20	0.0	5.0000
	Bus 21	n_2 80.0000 4 n_5 50.0000 1 n_8 20.0000 1 n_{11} 20.0000 1 n_{13} 20.0000 1 n_{13} 20.0000 1 n_{-9} 1.0780 1 $6-9$ 1.0780 1 $6-9$ 1.0780 1 $6-9$ 1.0780 1 $6-9$ 1.0780 1 $6-9$ 1.0780 1 $6-9$ 1.0780 1 $6-9$ 1.0780 1 $6-9$ 1.0780 1 $8-27$ 1.0680 1 $8 \cdot 10$ 0.0 $8 \cdot 12$ 0.0 $8 \cdot 17$ 0.0 $8 \cdot 21$ 0.0 $8 \cdot 23$ 0.0 $8 \cdot 24$ 0.0 $8 \cdot 29$ 0.0 $8 \cdot 29$ 0.0 901.9600 $8 \cdot 5.8324$ $5 \cdot 8324$ $1 \cdot 3 \cdot 10^{-1}$	5.0000
-	Bus 23	0.0	3.7342
-	Bus 24	0.0	4.5993
-	Bus 29	0.0	2.8053
Cost_Pg		901.9600	832.7696
Losses		5.8324	10.1201





5.1.3. Scenario 3

As demonstrated in Table 4, the designed GTOT minimizes the PEs in the third scenario. In this table, the values of the voltages of the six generators (Vg $_1$, Vg $_2$, Vg $_5$, Vg $_8$, Vg $_{11}$, and Vg $_{13}$) started at 1.0500, 1.0400, 1.0100, 1.0100, 1.0500, and 1.0500, respectively, and ended at 1.1000, 1.0961, 1.0784, 1.0859, 1.1000 and 1.1000, respectively.

Table 4. Simulation outcomes based on the designed GTOT for the third scenario.

Variables		Initial	Third Scenario
	Gen 1	1.0500	1.1000
	Gen ₂	1.0400	1.0961
Voltage setting of the generators (n.u.)	Gen 5	1.0100	1.0784
voltage setting of the generators (p.u)	Gen ₈	1.0100	1.0859
	Gen 11	1.0500	1.1000
	Gen 13	1.0500	1.1000
	Gen 1	99.2400	63.9480
	Gen 2	80.0000	67.4323
Output nowers of the generators (MW)	Gen 5	Initial 1.0500 1.0400 1.0100 1.0100 1.0500 1.0500 1.0500 99.2400 80.0000 20.0000 20.0000 20.0000 1.0780 1.0690 1.0680 0.0000	50.0000
Output powers of the generators (WW)	Gen ₈	20.0000	35.0000
-	Gen 11	Gen 1 1.0500 Gen 2 1.0400 Gen 5 1.0100 Gen 1 1.0500 Gen 11 1.0500 Gen 13 1.0500 Gen 1 99.2400 Gen 2 80.0000 Gen 3 20.0000 Gen 4 20.0000 Gen 5 50.0000 Gen 6 20.0000 Gen 7 20.0000 Gen 8 20.0000 Gen 13 20.0000 Gen 13 20.0000 Gen 13 20.0000 Gen 14 20.0000 Gen 13 20.0000 Gen 13 20.0000 Gen 13 20.0000 Gen 13 20.0000 Gen 14 20.0000 Gen 15 0.0000 Bus 12 0.0000 Bus 15 0.0000 Bus 21 0.0000 Bus 23 0.0000 Bus 24 0.0000 Bus 29 0.0000 901.9600 5.8324 0.2390 0.2390 </th <th>30.0000</th>	30.0000
-	Gen 13	20.0000	40.0000
	Tr 6–9	1.0780	1.0696
	Gen $_{13}$ 20.0000 Tr $_{6-9}$ 1.0780 Tr $_{6-10}$ 1.0690 Tr $_{4-12}$ 1.0320	0.9001	
Tap setting of the transformers (p.u)	Tr ₄₋₁₂	1.0320	0.9864
		0.9731	
	Bus 10	0.0000	4.9999
-	Bus 12	0.0000	4.9999
-	Bus 15	0.0000	5.0000
	Bus 17	Initial 1.0500 1.0400 1.0100 1.0100 1.0500 1.0500 1.0500 1.0500 99.2400 80.0000 20.0000 20.0000 20.0000 1.0780 1.0690 1.0680 0.0000 0.2390	5.0000
Output reactive powers of the VAR sources ar buses (MVAr)	Bus 20	0.0000	4.3098
	Bus 21	0.0000	4.9999
-	Bus 23	0.0000	2.3956
-	Bus 24	0.0000	5.0000
-	Bus 29	0.0000	2.3154
Cost_Pg		901.9600	943.5287
Losses		5.8324	2.9803
Emissions		0.2390	0.2046

In addition to this, the values of four tap changer settings (Tap $_{6-9}$, Tap $_{6-10}$, Tap $_{4-12}$, and Tap $_{28-27}$) started at 1.0780, 1.0690, 1.0320, and 1.0680, respectively, and ended at 1.0696, 0.9001, 0.9864, and 0.9731, respectively. Additionally, the values of all nine reactive power devices (Qc $_{10}$, Qc $_{12}$, Qc $_{15}$, Qc $_{17}$, Qc $_{20}$, Qc $_{21}$, Qc $_{23}$, Qc $_{24}$, and Qc $_{29}$) started at zero and ended at 4.9999, 4.9999, 5.0000, 5, 4.3098, 4.9999, 2.3956, and 5.0000, respectively. Furthermore, the values of all six generators' real power output (Pg $_1$, Pg $_2$, Pg $_5$, Pg $_8$, Pg $_{11}$, and Pg $_{13}$) started at 99.2400, 80.0000, 50.0000, 20.0000, and 40.0000, respectively. It is illustrated from this table that the obtained PE value is 0.2046 ton/h.

In addition to this, Figure 7 depicts the convergence properties of the generated GTOT for Scenario 3, where it obtains the optimal solution in a short time with the effectiveness and robustness of the solution. Table 5 compares it to other metaheuristics optimization techniques. It is illustrated from the table the developed GTOT attains the minimum PE objective of 0.2046 ton/h. It outperforms the other metaheuristics that are shown in the mentioned table.



Figure 7. Convergence feature of the developed GTOT for Scenario 3.

Technique	PEs (tonne/h)	Technique	PEs (ton/h)
Developed GTOT	0.2046	AGT [56]	0.2048
Stud KHT [63]	0.2048	GT [56]	0.2049
ARBT [21]	0.2048	Modified TLT [64]	0.2049
KHT [63]	0.2049	EMRFT [42]	0.2048
CST [58]	0.2051	NBT [58]	0.2052
JFST [62]	0.2047	MCST [58]	0.2049

Table 5. Comparison for Scenario 3.

5.1.4. Scenario 4

The proposed GTOT achieves the minimizing of the OPLs in the fourth scenario, as shown in Table 6. In this table, the values of the voltages of the six generators (Vg $_1$, Vg $_2$, Vg $_5$, Vg $_8$, Vg $_{11}$, and Vg $_{13}$) started at 1.0500, 1.0400, 1.0100, 1.0100, 1.0500, and 1.0500, respectively, and ended at 1.1000, 1.0975, 1.0797, 1.0868, 1.1000, and 1.1000, respectively. In addition to this, the values of four tap changer settings (Tap $_{6-9}$, Tap $_{6-10}$, Tap $_{4-12}$, and Tap $_{28-27}$) started at 1.0780, 1.0690, 1.0320, and 1.0680, respectively, and ended at 1.0675, 0.9000, 0.9872, and 0.9728, respectively. Additionally, the values of all nine reactive power devices (Qc $_{10}$, Qc $_{12}$, Qc $_{15}$, Qc $_{17}$, Qc $_{20}$, Qc $_{21}$, Qc $_{23}$, Qc $_{24}$, and Qc $_{29}$) started at 0 and ended at 5.0000, 5.0000, 5.0000, 4.999, 5, 1.4887, 5.0000, and 2.2640, respectively. Furthermore, the values of all six generators' real power output (Pg $_1$, Pg $_2$, Pg $_5$, Pg $_8$, Pg $_{11}$, and Pg $_{13}$) started at 99.2400, 80.0000, 50.0000, 20.0000, and 20.0000, respectively. It

is illustrated from the table the acquired value of OPLs is 2.8525 MW, whereas the value of OPLs is 5.8324 MW in the initial scenario. This reduction in cost represents a percentage of 51.09%. Additionally, Figure 8 depicts the convergent characteristic of the designed GTOT for Scenario 4, where it obtains the optimal solution in a short time with the effectiveness and robustness of the solution.



Figure 8. Convergence feature of the developed GTOT for Scenar	io 4.
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Table 6. Sim	ulation outcomes	based on the	designed	GTOT f	or the f	ourth scenario

Variables		Initial	Fourth Scenario
	Gen 1	1.0500	1.1000
-	Gen 2	1.0400	1.0975
Voltage setting of the generators (n 1)	Gen 5	1.0100	1.0797
voltage setting of the generators (p.u) -	Gen ₈	1.0100	1.0868
-	Gen 11	1.0500	1.1000
-	Gen 13	1.0500	1.1000
	Gen 1	99.2400	51.2525
	Gen ₂	80.0000	80.0000
Output powers of the generators (MW)	Gen 5	50.0000	50.000
Sulput powers of the generators (WW)	Gen ₈	20.0000	35.0000
	Gen 11	20.0000	30.0000
	Gen 13	20.0000	40.0000
	Tr ₆₋₉	1.0780	1.0675
	Tr 6-10	1.0690	0.9000
Tap setting of the transformers (p.u)	Tr 4-12	1.0320	0.9872
-	Tr 28-27	1.0680	0.9728

Variables		Initial	Fourth Scenario
	Bus 10	0.0000	5.0000
	Variables Initial Bus 10 0.0000 Bus 12 0.0000 Bus 15 0.0000 Bus 15 0.0000 Bus 17 0.0000 Bus 20 0.0000 Bus 21 0.0000 Bus 23 0.0000 Bus 24 0.0000 Bus 29 0.0000 Bus 29 0.0000 Bus 29 0.0000	5.0000	
_	Bus 15	0.0000	5.0000
	Bus 17	0.0000	5.0000
Sources ar buses (MVAr)	Bus 20	0.0000	4.9999
	Bus 21	0.0000	5.0000
-	Bus 23	0.0000	1.4887
	Bus 24	0.0000	5.0000
	Bus 29	0.0000	2.2640
Cost_Pg		901.9600	967.0722
Losses		5.8324	2.8525

Table 6. Cont.

5.1.5. Stability Assessment of the Developed GTOT for the First EPS

To make a detailed evaluation of the stability of the developed GTOT for the first EPS, the obtained objectives of the thirty runs are recorded. For each scenario, the related average objective is calculated, and a graph is plotted to describe the percentage of every objective value to Ind_{OJk}, so the closeness of every run compared to the mean can be described. Figure 9 describes the obtained indicators of the related objective percentages via the developed GTOT.

$$\operatorname{Ind}_{OJ_{k}} = \frac{OJ_{k}}{\frac{1}{30}\sum\limits_{k=1}^{30}OJ_{k}}, \ k = 1, 2, \dots m$$
(40)

As it can be observed from the figure, the developed GTOT always has the ability to find a close percentage to 100% where its mean is near to its minimum value. The highest percentage of the index is 100.085% in the first scenario, while it reached 101.1680% in the second scenario. For the third scenario, the maximum index percentage is 101.0400, while it reached 100.05% in the fourth scenario. This demonstrates the high stability of the developed GTOT for all scenarios. Additionally, Table 7 indicates the statistical data for the four scenarios. As manifested in this table, the best, mean, and worst values obtained by the developed GTOT are very close, which illustrates the robustness of the developed GTOT.

Table 7. Statistical data based on the designed GTOT for the 4 scenarios.

Statistical Indices	Scenario 1	Scenario 2	Scenario 3	Scenario 4
Best	799.0831	832.8144	0.2046	2.8525
Mean	799.2081	833.4394	0.2050	2.9128
Worst	799.8904	843.1896	0.2072	3.1655
Standard deviation	0.2140	1.8636	0.0008	0.0824
Standard error	0.0390	0.3402	0.0001	0.0150
Best-Worst	0.1010%	1.2458%	1.2350%	10.9711%
Mean-Worst	0.0853%	1.1698%	1.0667%	8.6738%
Best-Mean	0.0156%	0.0750%	0.1665%	2.1139%



Figure 9. Obtained objectives percentages by means of the designed GTOT.

Moreover, other statistical indices are conducted on the four scenarios, which are standard deviation, standard error, |Best-Worst|, |Mean-Worst|, and |Best-Mean|. The standard deviations for the four scenarios are 0.214, 1.8636, 0.0001, and 0.0150, while the standard errors are 0.0390, 0.3402, 0.0001, and 0.0150. Additionally, another important index, which is |Best-Mean|, represents the difference between the best and mean values obtained by the proposed GTOT. The values of |Best-Mean| are 0.0156%, 0.0750%, 0.1665%, and 2.1139%. These statistical indices illustrate the effectiveness and robustness of the developed GTOT.

5.1.6. Scenario 5 and Scenario 6

In the fifth scenario, two different objective functions are considered for the minimization of both the FGCs and PE. In the sixth scenario, three different objective functions are considered for the minimization of FGCs, PE, and OPL. For both cases, the proposed GTOT is applied, and the optimal settings of the control variables and the regarding objectives are shown in Table 8. In this table, the values of FGCs and PE in the fifth scenario started at 901.9600 and 0.2390, respectively, and ended at 890.1029 and 0.2127, respectively, when applying the GTOT on this system. In addition to this, the values of FGCs, PE, and OPL in the sixth scenario started at 901.9600, 0.2390, and 5.8324, respectively, and ended at 895.4292, 0.2123, and 4.6529, respectively.

Table 8. Simulation outcomes based on the designed GTOT for the fifth and sixth scenario.

Variables		Initial	Fifth Scenario	Sixth Scenario
	Gen 1	1.0500	1.1000	1.0057
	Gen 2	1.0400	1.0960	1.0045
Voltage setting of the	Gen 5	1.0100	1.0771	1.0003
generators (p.u)	Gen ₈	1.0100	1.0881	1.0111
	Gen 11	1.0500	1.1000	1.0007
	Gen 13	1.0500	1.0546	1.0018
	Gen 1	99.2400	1.0553	1.0137
	Gen 2	80.0000	1.1000	0.9097
Output powers of the	Gen 5	50.0000	1.1000	0.9814
generators (MW)	Gen ₈	20.0000	1.1000	0.9741
	Gen 11	20.0000	$6.243 imes 10^{-9}$	5.0000
	Gen 13	20.0000	0.0000	5.0000
Tap setting of the transformers (p.u)	Tr ₆₋₉	1.0780	5.0000	5.0000
	Tr ₆₋₁₀	1.0690	4.6221	5.0000
	Tr 4-12	1.0320	0.0000	5.0000
	Tr _{28–27}	1.0680	5.0000	5.0000
	Bus 10	0.0000	5.0000	5.0000
	Bus 12	0.0000	5.0000	5.0000
	Bus 15	0.0000	5.0000	4.9517
Output reactive powers of	Bus 17	0.0000	82.1327	81.8371
the VAR sources ar buses (MVAr)	Bus 20	0.0000	62.7968	62.4782
	Bus 21	0.0000	37.4611	38.7375
	Bus 23	0.0000	35.0000	35.0000
	Bus 24	0.0000	30.0000	30.0000
	Bus 29	0.0000	40.0000	40.0000

Variables	Initial	Fifth Scenario	Sixth Scenario
Cost_Pg	901.9600	890.1029	895.4292
Losses	5.8324	3.9906	4.6529
Emissions	0.2390	0.2127	0.2123
Fitness	1.0000	0.7705	0.6691

Table 8. Cont.

Additionally, Table 9 indicates the statistical data for the fifth and sixth scenarios. As manifested in this table, the best, mean, and worst values obtained by the developed GTOT are very close, which illustrates the robustness of the developed GTOT. Moreover, other statistical indices are conducted on the four scenarios, which are standard deviation, standard error, |Best-Worst|, |Mean-Worst|, and |Best-Mean|, that illustrate the effectiveness and robustness of the developed GTOT.

Statistical Indices	Scenario 5	Scenario 6
Best	0.7705	0.6691
Mean	0.7819	0.6896
Worst	0.7914	0.7473
Standard deviation	0.0909	0.0043
Standard error	0.0166	0.0008
Best-Worst	2.7057%	11.6914%
Mean-Worst	1.2176%	8.3600%
Best-Mean	1.4701%	3.0743%

Table 9. Simulation outcomes of the designed GTOT for the fifth and sixth scenario.

Additionally, Table 9 indicates the statistical data for the fifth and sixth scenarios. As manifested in this table, the standard deviations for the four scenarios are 0.0909 and 0.0043, while the standard errors are 0.0166 and 0.0008. Additionally, the values of |Best-Mean| obtained by the proposed GTOT are 1.4701% and 3.0743%. These statistical indices illustrate the effectiveness and robustness of the developed GTOT.

5.2. Results of the Second EPS

For this EPS, the three scenarios listed below are studied:

- Scenario 7: *OJ*₁ minimization described in Equation (16);
- Scenario 8: *OJ*₄ minimization described in Equation (19);
- Scenario 9: Merging OJ_1 and OJ_4 as a multi-objective function.

5.2.1. Scenario 7

For this case, the designed GTOT is implemented, and the results are shown in Table 10. In this table, the values of the voltages of the eight generators (Vg ₁, Vg ₂, Vg ₃, Vg ₄, Vg ₅, Vg ₆, Vg ₇, and Vg ₈) started at 1 and ended at 1.0600, 1.0590, 1.0599, 1.0599, 1.0599, 1.0599, 1.0599, 1.0599, 1.0599, 1.0599, 1.0599, 1.0455, and 1.0517, respectively. In addition to this, the values of all eight generators' real power output (Pg ₁, Pg ₂, Pg ₃, Pg ₄, Pg ₅, Vg ₆, Pg ₇, and Pg ₈) started at 85.6900, 157.4000, 139.3100, 113.6900, 166.4800, 31.7100, 92.000, and 122.4900, respectively, and ended at 189.5676, 10.0000, 214.6980, 180.4253, 10.0000, 234.0139, 56.3042, and 32.1957, respectively. As illustrated, the proposed GTOT reduces FGCs from 25,098.7000 USD/h to 22,953.42472 USD/h in comparison with the initial scenario. This decrease is a percentage of 8.54%. Furthermore, Figure 10 depicts the convergent characteristic of the proposed GTOT, where it obtains the optimal solution in a short time with the effectiveness and robustness of the solution.

Variables		Initial	Fifth Scenario
	Gen 1	1.0000	1.0600
-	Gen 2	1.0000	1.0599
_	Gen 3	1.0000	1.0599
Voltage setting of the generators (n.u)	Gen ₄	1.0000	1.0599
voltage setting of the generators (p.u) -	Gen 5	1.0000	1.0599
_	Gen ₆	1.0000	1.0599
_	Gen 7	1.0000	1.0455
	Gen ₈	1.0000	1.05173
	Gen 1	85.6900	189.5676
	Gen ₂	157.400	10.0000
	Gen 3	139.3100	214.6980
	Gen ₄	113.6900	180.4253
Sulput powers of the generators (1111) -	Gen 5	166.4800	10.0000
-	Gen ₆	31.7100	234.0139
	Gen 7	92.0000	56.3042
	Gen ₈	122.4900	32.1957
FGCs (USD/h)		25,098.7000	22,953.4247
OPLs (MW)		19.0150	37.4550

Table 10. Simulation outcomes based on the designed GTOT for the seventh scenario.



Figure 10. Convergence feature of developed GTOT for Scenario 7.

For such a scenario, the created GTOT is contrasted to a number of other novel approaches used in this instance, as shown in Table 11. As can be observed, the produced GTOT beats all other strategies in terms of minimizing FGCs, with the developed GTOT obtaining the smallest FGCs of 22,953.4247 USD/h.

Technique	FGCs (USD/h)	Technique	FGCs (USD/h)
Developed GTOT	22,953.4247	ISHT [65]	22,958.7800
NBT [48]	22,960.8100	CST [47]	22,959.3600
SST [65]	22,965.5900	MCST [47]	22,955.5500
GWT [65]	22,957.7200		

Table 11. Comparison for Scenario 7.

5.2.2. Scenario 8

The proposed GTOT achieves the minimizing of the OPLs in the eighth scenario, as shown in Table 12. In this table, the values of the voltages of the eight generators (Vg $_1$, Vg $_2$, Vg $_3$, Vg $_4$, Vg $_5$, Vg $_6$, Vg $_7$, and Vg $_8$) started at 1 and ended at 1.0595, 1.0600, 1.0600, 1.0600, 1.0600, 1.0600, and 1.0600, respectively. In addition to this, the values of all eight generators' real power output (Pg $_1$, Pg $_2$, Pg $_3$, Pg $_4$, Pg $_5$, Vg $_6$, Pg $_7$, and Pg $_8$) started at 85.6900, 157.4000, 139.3100, 113.6900, 166.4800, 31.7100, 92.0000, and 122.4900, respectively, and ended at 60.4617, 58.8194, 180.6455, 130.7554, 117.9838, 105.4722, 156.5709, and 86.2761, respectively. The proposed GTOT, as demonstrated, reduces the OPLs from 19.0150 MW to 7.2353 MW compared with the initial scenario. This decrease reflects a 61.95 percent reduction. In addition, Figure 11 depicts the related convergent characteristic of the proposed GTOT for Scenario 8, where it obtains the optimal solution in a short time with the effectiveness and robustness of the solution.

Table 12. Simulation outcomes based on the designed GTOT for the eighth scenario.

Variables		Initial	Sixth Scenario
	Gen 1	1.0000	1.0595
-	Gen 2	1.0000	1.0600
_	Gen 3	1.0000	1.0600
Voltage setting of the generators (n 1)	Gen ₄	1.0000	1.0600
voltage setting of the generators (p.u) -	Gen 5	1.0000	1.0600
_	Gen ₆	1.0000	1.0600
_	Gen 7	1.0000	1.0600
-	Gen ₈	1.0000	1.0600
	Gen 1	85.6900	60.4617
	Gen 2	157.4000	58.8194
	Gen 3	139.3100	180.6455
	Gen ₄	113.6900	130.7554
	Gen 5	166.4800	117.9838
	Gen ₆	31.7100	105.4722
	Gen 7	92.0000	156.5709
	Gen ₈	122.4900	86.2761
FGCs (USD/h)		25,098.7000	24,773.0865
OPLs (MW)		19.0150	7.2353



Figure 11. Convergence feature of the developed GTOT for Scenario 8.

5.2.3. Stability Assessment of the GTOT for the Second EPS

For this EPS, similarly, the obtained objectives of the thirty runs are recorded. For every scenario, the estimated indicators of the percentages of the objectives via the proposed GTOT are displayed in Figure 12.



Figure 12. Estimated objective percentages via the designed GTOT.

As seen, the developed GTOT always has the ability to find close percentage to 100% where its mean is near to its minimum. For the first scenario, the highest indicator percent is 100.0000167%, while the minimum index percent is 99.9999%. The maximum index percent is 100.123%, while the minimum index percent is 99.9862%. This demonstrates the high stability of the developed GTOT for all scenarios.

Additionally, Table 13 indicates the statistical data for the seventh and eighth scenario. As manifested in this table, the standard deviations for the two scenarios are 7.3505 and 1.28×10^{-5} while the standard errors are 1.3420 and 2.33×10^{-6} . Additionally, the values of |Best-Mean| obtained by the proposed GTOT are 0.0137% and 0.0002%. These statistical indices illustrate the effectiveness and robustness of the developed GTOT.

Statistical Indices	Scenario 7	Scenario 8
Best	22,953.4200	7.2353
Mean	22,956.5800	7.2353
Worst	22,984.9400	7.2353
Standard deviation	7.3505	$1.28 imes10^{-5}$
Standard error	1.3420	$2.33 imes10^{-6}$
Best-Worst	0.1373%	0.0003%
Mean-Worst	0.1235%	0.0001%
Best-Mean	0.0137%	0.0002%

Table 13. Simulation outcomes based on the GTOT for the seventh and eighth scenarios.

5.2.4. Scenario 9

The designed GTOT achieves the minimization of both the FGCs and OPL in the ninth scenario, as shown in Table 14. In this table, the values of FGCs and OPL in the ninth scenario have started with 25,098.7000 and 19.0150, respectively, and ended with 24,586.3700 and 7.3036, respectively.

Table 14. Simulation outcomes based on the designed GTOT for Scenario 9.

Variables		Initial	Ninth Scenario
	Gen 1	1.0000	1.0600
	Gen 2	1.0000	1.0600
	Gen 3	1.0000	1.0600
Voltage setting of the generators (p.u)	Gen ₄	1.0000	1.0600
forme occurs of the generators (pra)	Gen 5	1.0000	1.0599
	Gen ₆	1.0000	1.0600
	Gen 7	1.0000	1.0599
	Gen ₈	1.0000	1.0600
	Gen 1	85.6900	67.2453
	Gen 2	157.4000	51.3626
	Gen 3	139.3100	183.2907
Output powers of the generators (MW)	Gen ₄	113.6900	133.4820
Sulput powers of the generators (MIT)	Gen 5	166.4800	108.3223
	Gen ₆	31.7100	123.8325
	Gen 7	92.0000	148.2581
	Gen 8	122.4900	81.2601
FGCs (USD/h)		25,098.7000	24,586.3700
OPLs (MW)		19.0150	7.3036
Fitness		1.0000	0.6818

In addition, Figure 13 depicts the convergent characteristic of the designed GTOT for Scenario 9, where it obtains the optimal solution in a short time with the effective-ness and robustness of the solution. Moreover, Table 15 indicates the statistical data for the ninth scenario. As manifested in this table, the standard deviation for this scenario is 1.9551×10^{-8} , while the standard error is 3.5696×10^{-9} . Additionally, the value of |Best-Mean| obtained by the proposed GTOT is 3.4413×10^{-6} %. These statistical indices illustrate the effectiveness and robustness of the developed GTOT.



Figure 13. Convergence feature of the developed GTOT for Scenario 9.

Table 15. Simulation outcomes based on the designed GTOT for the seventh and eighth scenario.

Statistical Indices	Scenario 9
Best	0.6818
Mean	0.6818
Worst	0.6818
Standard deviation	$1.9551 imes 10^{-8}$
Standard error	$3.5696 imes 10^{-9}$
Best-Worst	$6.1814 imes 10^{-6}\%$
Mean-Worst	$2.7401 imes 10^{-6}\%$
Best-Mean	$3.4413 imes 10^{-6}\%$
Worst Standard deviation Standard error Best-Worst Mean-Worst Best-Mean	$\begin{array}{r} 0.6818\\ \hline 1.9551 \times 10^{-8}\\ \hline 3.5696 \times 10^{-9}\\ \hline 6.1814 \times 10^{-6}\%\\ \hline 2.7401 \times 10^{-6}\%\\ \hline 3.4413 \times 10^{-6}\%\end{array}$

6. Conclusions

In this paper, a methodology centered on the gorilla troops optimization technique (GTOT) is developed for optimal power flow problem (OPFP) in electrical power systems (EPSs). The assessment of the designed GTOT is carried out utilizing an IEEE specified 30 bus EPS and actual WD-EPS from Egypt. Nine different scenarios are evaluated, each with a different goal function of fuel expense, transmission losses, and harmful pollutants. Significant decreases in the objective goals are achieved for all tested circumstances. The main outcomes of this paper are developed as follows:

 Multi-dimension objectives combining two and three objectives for both systems are developed in this work.

- Their percentages of reduction for the single objectives are reached (11.406%, 7.67%, 14.39%, 51.09%, 8.54%, and 61.95%) for the six single objective scenarios in comparison to the initial circumstance.
- The GTOT is employed in different evaluations and statistical analyses with many modern methods such as GWT, CST, SST, NBT, and ISHT.
- The developed GTOT always has the ability to find a close percentage to 100% where its average is near to its minimum for both EPSs.
- When developed GTOT compared to other similar approaches in the literature, the simulated results demonstrate the designed GTOT's solution validity and stability.
- The developed GTOT derives considerable stability for all scenarios.

Considering the high efficacy of the suggested algorithm in the OPFP application in this paper, it is preferred that the proposed algorithm be tested in the future for resolving the OPFP with high penetration of renewable energies in power grids. It may also be designed for AC-DC electrical systems with the incorporation of modern voltage source converters.

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List of Acronyms

AGT	Adaptive GT
ARBT	Adaptive real biogeography-based technique
AGST	Adaptive group search technique
BBO	Biogeography-based optimization
BHBT	Black-hole-based technique
CBOA	Colliding bodies optimization algorithm
COA	Coyote optimization algorithm
CSSO	Chaotic salp swarm optimizer
CST	Crow search technique
DE	Differential evolution
DHST	Differential harmony search technique
EMM	Electromagnetism-like mechanism
EPSs	Electrical power systems
EMRFT	Enhanced manta ray foraging technique
EMSA	Emended moth swarm algorithm
FGCs	Fuel generation costs
FGCSs	FGC with sinusoids
GA	Genetic algorithm
GTOT	Gorilla troops optimization technique
GT	Grasshopper technique
GWT	Grey wolf technique
HGWODE	Hybridization of GWT and DE
ICT	Imperialist competitive technique
IEOT	Improved electromagnetism-like technique
IMFT	Improved moth-flame technique
INSGA-III	Improved non-dominated sorting genetic algorithm
ISHT	Improved spotted-hyena technique

ISST	Improved social spider technique
	Adaptive differential evolution
IFST	Induptive underential evolution
	Keill hard tashnigua
	Krill nero technique
MCSI	Modified crow search technique
NBT	Novel bat technique
MRFT	Manta-ray foraging technique
MST	Moth swarm technique
OPFP	Optimal power flow problem
OPL	Overall power loss
PE	Produced emissions
PSO	Particle swarm optimization
OCMFT	Quantum computing and moth flame technique
SAO	Simulated annealing optimization
SOST	Symbiotic organisms search technique
CCT	Symbolic organisms search technique
551 TIT	Tagahing laguning taghning
	reaching-learning technique
WCEMFI	Combination of water cycle with moth flame technique
WD	West delta
WD-EPS	West Delta-EPS
List of Variables	
A	Level of violence in a fight
Xr Xr	The current group position of gorilla
	Variables' minimum bound
LL $V(z)$	Variables minimum bound
A(g)	Vector of gorilla location in the giteration
GX(g+1)	Vector of gorilla location in the $g + 1$ iteration
rand, rd1, rd2, rd3	Random values ranging from 0 to 1
Pr	Migrating coefficient
GXr	Candidate group position of gorilla
UL	Variables' maximum bound
Iter	Present iteration number
MaxIter	Maximum iteration number
rd4	Random value inside the bound [0:1]
1	Random values between -1 and 1
X(g)	Vector of gorilla location
0	Force of impact
rd5	Random value within bound [0:1]
β	Pre-optimization value
Ē	Violence efficacy
$V\sigma_1 V\sigma_2 V\sigma_3 $	Voltages of the generators
Tan_{a} Tan_{a} Tan_{a}	Tap changer settings
$np_1, np_2, \dots np_{Nt}$	Number of on load tan changers
$Qg_1, Qg_2, \dots, Qg_{Ng}$	Generator reactive power outputs
$Pg_1, Pg_2, \ldots, Pg_{Ng}$	Generators real power output
0J	Investigated vector of several <i>m</i> targets
OJ_1	Costs of fuel generation in dollars per hour
Pg_k	Real power output in megawatts of generator
OJ ₂	Costs of fuel generation with sinusoids
θ	Phase angle
G _{mn}	Conductance of a line between buses m and n
QL	Power consumption in its reactive components
G _{ik}	Mutual conductance of line between bus <i>j</i> and <i>k</i>
VL_i	Load voltage at bus <i>j</i>
OI_i	Each objective function
NRA	Newton–Raphson approach

Penalty coefficient for any violation in line flow
Number of on-load generators
Number of on-load reactive power sources,
Transmission flow limits
Random values between [-c:c]
The best solution which is the silverback
Population of gorillas
Level of violence in a fight
Load bus voltage magnitudes
The number of load buses,
Independent variables
Dependent variables
Vector of several targets
Cost factors of generator k
Number of transmission lines
Reactive power injections of switching capacitors
Lowest limitation of generator k
Generator k's sinusoid cost factors
Produced ton/hr emissions from the power plants
Emission factors of generator <i>k</i>
Number of buses
Voltage
Power consumption in its active components
Mutual susceptance of a line between bus j and k
Power flow via line
Penalty coefficient for violation in load voltage
Penalty coefficient for violation in reactive power output
from generators
Mean value

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