



Article Complex Dynamics of a Novel Chaotic System Based on an Active Memristor

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Abstract: On the basis of the bistable bi-local active memristor (BBAM), an active memristor (AM) and its emulator were designed, and the characteristic fingerprints of the memristor were found under the applied periodic voltage. A memristor-based chaotic circuit was constructed, whose corresponding dynamics system was described by the 4-D autonomous differential equations. Complex dynamics behaviors, including chaos, transient chaos, heterogeneous coexisting attractors, and state-switches of the system were analyzed and explored by using Lyapunov exponents, bifurcation diagrams, phase diagrams, and Poincaré mapping, among others. In particular, a novel exotic chaotic attractor of the system was observed, as well as the singular state-switching between point attractors and chaotic attractors. The results of the theoretical analysis were verified by both circuit experiments and digital signal processing (DSP) technology.

Keywords: memristor; chaos; coexisting attractors; heterogeneous multistability; DSP

1. Introduction

The memristor postulated by Chua in 1971 [1] is a nonlinear device with memorability, whose resistance depends on the history of the current (or voltage). Due to the lack of physical verification, it has not attracted much attention in the scientific community for over 30 years. The memristor theory and resistive switching was linked by HP lab in 2008 for the first time [2], which experimentally confirmed Chua's theoretical hypothesis. Due to potential applications of memristors, it caused a booming interest in many research fields today, including the nonvolatile memory [3,4], artificial intelligence [5,6], neural networks [7,8], nonlinear chaotic circuits [9,10], and other fields.

As a nonlinear device, memristors are introduced to design chaotic circuits [11–13]. Some memristor-based nonlinear oscillators were created by replacing Chua's diodes with memristors, and the dynamical behaviors of these systems were analyzed and explored [14]. Other memristor-based chaotic circuits were reported by Muthuswamy, who provided a generation frame of chaotic sequence for secure communications [15]. A simplest memristor-based chaotic circuit was presented with only three elements in series, whose physical circuit was designed by using solid electronic components, successfully realizing the chaotic oscillation of the system [16]. A generic passive memristor was presented, which was used to design a second-order nonlinear oscillator system [17]. An active memristor based on it was devised and explored in this paper.

Multistable systems are a hot topic recently [18–20]. In general, a system is deemed to be multistable if it is neither stable nor completely unstable and switches between several mutually exclusive states over time. A simplest memristor-based circuit with hidden multistable states was previously analyzed, and the generation mechanism of coexisting attractors was confirmed [21]. A memristive Chua's circuit with the multistability was proposed, and the line equilibrium point and

the stability of the system were analyzed and confirmed [22]. The multistability means that the system has coexisting attractors. The coexistence of attractors, as a permanent subject, has been analyzed and explored in some chaotics systems [23–25]. A memristive system has been presented that has four diverse coexisting attractors: an equilibrium point, a stable limit cycle, a 16-peak periodic attractor, and a strange attractor [26]. A simple chaotic system with various types of multiple coexisting attractors has been presented, and its physical circuit has been realized, displaying the chaotic behaviors [27]. Moreover, some memristive systems with multiple coexisting attractors and even infinitely many attractors have been proposed [28–31]. A parallel inductor-capacitor-memristor circuit has been constructed, which showed the coexistence of multiple attractors [32]. In fact, the above-mentioned systems all own heterogeneous multistability. However, if there are several or even infinitely more coexisting attractors with different properties in a system, the system will be regarded as having heterogeneous multistability. Therefore, a memristor-based chaotic system with heterogeneous multistability. Therefore, a memristor-based chaotic system with heterogeneous multistability.

This paper devised an emulator of the active memristor, which can maintain the stability of hysteresis loops over a wide range of frequencies. A memristor-based fourth-order chaotic system with a novel exotic attractor was proposed, which had complex dynamics, including chaos, coexisting attractors, transient chaos, and heterogeneous multistability. A novel phenomenon, switching between a point attractor and a chaotic attractor, was found with the change of the initial values. The remainder of this paper is organized as follows: the AM is presented and its emulator is implemented by Multisim in Section 2. A memristive chaotic oscillator was constructed and the stability of the equilibria of the system is analyzed in Section 3. Dynamics of the proposed system are explored, including symmetry, coexisting bifurcations, coexisting attractors, and multistability, in Section 4. The results of circuit implementation and digital signal processing (DSP) implementation of the memristor-based chaotic system are introduced in Section 5. Finally, some conclusions are given in the last section.

2. Memristor Model and its Emulator

2.1. An Active Memristor

A memristor, as a two-port electronic component, has a magnetic flux ϕ that is a nonlinear continuous function of its charge *q* [1]. The generalized memristive system was postulated by Chua in 1976 [34], defined as follows:

$$\begin{cases} \dot{x} = f(x, u, t) \\ y = g(x, u, t)u \end{cases}$$
(1)

where *x* represents the internal state of the system, and *u* and *y* represent the input and output of the system, respectively. The bistable bi-local active memristor (BBAM) presented in [17] is described by the memconductance W(x), as follows:

$$W(x) = x^2(t) \tag{2}$$

The dynamics of the memristor are

$$\begin{cases} \frac{dx(t)}{dt} = -x(t)|x(t)| + Ax(t) + Bv(t) \\ i_M(t) = W(x)v(t) \end{cases}$$
(3)

where x(t) represents the memristive state and changes nonlinearly over time t, v(t) is the input, and $i_M(t)$ represents the output of the memristor. The instantaneous power of the BBAM is obtained as

$$p(t) = W(x)v^{2}(t) = x^{2}(t)v^{2}(t) \ge 0$$
(4)

When $t \ge t_0$, the integration of the energy from t_0 to t satisfies

$$\int_{t_0}^t p(\tau) d\tau \ge 0 \tag{5}$$

Therefore, it was passive. However, an active device is feasible and effective for designing the chaotic circuit. Thus, a composite component named active memristor was constructed by using the memristor with a negative conductance in parallel, as shown in Figure 1.



Figure 1. Sketch map of the active memristor.

According to the Kirchhoff's law and the properties of the component, the dynamics of the active memristor are described as follows:

$$\begin{cases} \frac{dx(t)}{dt} = -x(t)|x(t)| + Ax(t) + Bv(t) \\ i_M(t) = [x^2(t) - G]v(t) \end{cases}$$
(6)

2.2. Memristive Emulator

A memristive emulator was designed to explore the electrical performance of the memristor by utilizing the basic circuit theory in this subsection. On the basis of the addition, subtraction, multiplication, division, integration, and differentiation of input voltage easily realized in series and parallel circuits of operational amplifiers, multipliers, and other devices, the emulator of the active memristor (AM) was designed by using off-the-shelf electronic components for confirming volt-ampere fingerprints of the memristor.

According to Equation (6), the relationship between the internal state x(t) of the system and the input voltage v(t) is

$$x(t) = x(0) + \int_0^t \left[-x(\tau) |x(\tau)| + Ax(\tau) + Bv(\tau) \right] d\tau$$
(7)

where x(0) is an initial value of memristive internal state and obtained below:

$$x(0) = \int_{-\infty}^{0} \left[-x(\tau) |x(\tau)| + Ax(\tau) + Bv(\tau) \right] d\tau$$
(8)

It can be seen from Equations (7) and (8) that the different values of x(0) can cause the variation of memconductance of the AM, indicating the characteristics of memory of the memristor. To facilitate

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the circuit emulator of the memristor, consider the initial value x(0) = 0. According to Equations (6)–(8), one gets

$$i_M(t) = \left\{ \left(\int_0^t \left[-x(\tau) |x(\tau)| + Ax(\tau) + Bv(\tau) \right] d\tau \right)^2 - G \right\} v(t)$$
(9)

Thus, a memristive emulator based on Equation (9) was devised, which was composed of six operational amplifiers, three multipliers, and some resistors as shown in Figure 2. The voltage $v_0(t)$ between nodes A and B is the input of the emulator. Define the output voltage v_{U_5} of the amplifier U_5 as the internal state x(t) of the memristor. When the output voltage x(t) of the amplifier U_5 passes through an absolute circuit consisting of two amplifiers U_1 and U_2 , two diodes D_1 and D_2 and some resistors, signal x(t) implements the absolute value operation, i.e., $x(t) \rightarrow |x(t)|$. Thereafter, the signal |x(t)| is converted to -|x(t)| through the inverter consisted of U_3 , R_9 , and R_{10} . The signals -|x(t)| and x(t) are converted to -|x(t)|x(t) through the multiplier A_1 , which is to be the input of the adder consisting of U_4 , R_1 , R_2 , R_3 , and R_4 . Next, at the output of the amplifier U_4 , the voltage v_{U_4} is

$$v_{U_4}(t) = \frac{R_4}{R_2} x(t) |x(t)| - \frac{R_4}{R_3} x(t) - \frac{R_4}{R_1} x(t)$$
(10)



Figure 2. Emulator of the active memristor (AM).

The voltage signal v_{U_4} passes through the inverter integrator consisting of U_5 , C_1 , and R_{11} , and the internal state x(t) is obtained below:

$$x(t) = \int_0^t -v_{U_4}(\tau)d\tau = \frac{1}{R_{11}C_1} \int_0^t \left[-\frac{R_4}{R_2} x(\tau) |x(\tau)| + \frac{R_4}{R_3} x(\tau) + \frac{R_4}{R_1} v_0(\tau) \right] d\tau$$
(11)

From the signal x(t), through the multipliers A_2 and A_3 , the voltage $v_{A_3} = x^2(t)v_0(t)$ is obtained at the output of multiplier A_3 . Finally, the volt-ampere characteristics of the AM are derived through the amplifier U_6 , as follows:

$$i_{M} = \frac{R_{12}}{R_{13}} \left\{ \frac{1}{R_{14}} \left\{ \frac{1}{R_{11}C_{1}} \int_{0}^{t} \left[-\frac{R_{4}}{R_{2}} x(\tau) |x(\tau)| + \frac{R_{4}}{R_{3}} x(\tau) + \frac{R_{4}}{R_{1}} v_{0}(\tau) \right] d\tau \right\}^{2} - \frac{1}{R_{14}} \right\} v_{0}(t)$$
(12)

Let the capacitor C_1 and the associated resistors take the corresponding parameter values in Figure 2, and the pinched hysteresis loops of the memristor are observed, as shown in Figure 3, with the driven voltage $v(t) = U_m \sin(2\pi ft)$, $U_m = 6$ V, and different frequencies. It can be seen from the figure that these curves pass through the origin on the volt-ampere plane. The memristor has complex dynamics behaviors under the driven signal with the low frequencies, such as f = 15 Hz, 30 Hz, and 40 Hz, as shown in Figure 3a. It tends to a single value curve as the frequency continually increases, as shown in Figure 3b. When the frequency of the applied signal tends to infinity, the memristor degenerates into a linear resistance. This indicates that the memristor satisfies the frequency-dependence. Moreover, it is noteworthy that the hysteresis loops keep the symmetrical font "8" when the frequency is higher than 300 Hz, with a wide range of stable frequency.



Figure 3. Multisim simulations of pinched hysteresis loops of the AM emulator under an applied sinusoidal input with different frequencies: (**a**) f = 15 Hz, f = 3.0 Hz, and f = 40 Hz; (**b**) f = 80 Hz, f = 300 Hz, and f = 3000 Hz.

The evolution of pinched hysteresis loops of the AM emulator was obtained, as shown in Figure 4, with the frequency f = 650 Hz and different amplitudes $U_m = 10$ V, $U_m = 8$ V, $U_m = 6$ V, and $U_m = 4$ V. It can be seen from the figure that the pinched hysteresis loop of the memristor was compressed and the shape remained unchanged as the amplitude of the applied voltage signal decreased, with the frequency f = 650 Hz. The Multisim circuit experiment indicated that the features of the memristor depend on the amplitude and frequency of the applied voltage.



Figure 4. Pinched hysteresis loops of the AM emulator under the sinusoidal input voltage with the frequency f = 650 Hz and different amplitudes: $U_m = 10$ V, $U_m = 8$ V, $U_m = 6$ V, and $U_m = 4$ V.

3. Chaotic Circuit Topology and Circuit Dynamics

3.1. Chaotic Circuit Ttopology

The memristor-based chaotic circuit was designed, with two resistors, an inductance, two capacitors, and the active memristor, as shown in Figure 5.

According to Kirchhoff's laws, the dynamics of the system are described as

$$\begin{cases}
\frac{dv_1}{dt} = \frac{1}{R_1C_1}(v_2 - v_1 + GR_1v_1 - R_1\varphi^2v_1) \\
\frac{dv_2}{dt} = \frac{1}{R_1C_2}(v_1 - v_2 + R_1i) \\
\frac{di}{dt} = -\frac{1}{L}v_2 - \frac{R_2}{L}i) \\
\frac{d\varphi}{dt} = -\varphi|\varphi| + A\varphi + Bv_1
\end{cases}$$
(13)

where ϕ is a magnetic flux of the memristor, and v_1 and v_2 are voltages of capacitors C_1 and C_2 , respectively. Let $x = v_1$, $y = v_2$, z = i, $\phi = \varphi$, $a = \frac{1}{C_1}$, $b = \frac{1}{L}$, $c = \frac{R_2}{L}$, h = G, $C_2 = 1$, and $R_1 = 1$, and Equation (13) is reset below

$$\begin{cases} \dot{x} = a(y - x + hx - \varphi^2 x) \\ \dot{y} = x - y + z \\ \dot{z} = -by - cz \\ \dot{\varphi} = -\varphi|\varphi| + A\varphi + Bx \end{cases}$$
(14)

Let the parameters of Equation (14) be fixed as in Table 1, and a novel attractor is found in Equation (14), as shown in Figure 6, with the initial conditions (0, 0.001, 0, 0).



Figure 5. Memristor-based chaotic circuit.

Table 1. Parameter values of typical attractors of the memristor-based chaotic system.



Figure 6. Cont.



Figure 6. Phase diagrams of the novel chaotic attractor of the AM-based oscillatory circuit: (**a**) on the (x, y, z) space; (**b**) on the (y, z, φ) space; (**c**) on the (y, z) plane; (**d**) on the (x, y) plane; (**e**) on the (y, φ) plane; (**f**) on the (x, φ) plane.

As can be seen in Figure 6b, the attractor is comprised of two scroll shape attraction disks and bonding brands, with a small scroll on the upper and a large scroll on the lower. The trajectory is folded vertically from the center of the small scroll and goes to the periphery of the scroll. The outer trajectory is spirally rotated from the outer to the inner of the large scroll. Then, the trajectory from the center of the large scroll is vertically folded into the outer periphery of the small scroll. Thereafter, it spirally rotates into the center of a small scroll and keeps repeating, forming the novel attractor. The phase diagram in Figure 6a is the projection of the large scroll and the small scroll in the (x, y, z) space. It can be seen from Figure 6c that the inner circumference of the large scroll overlaps with the outer one in a small scroll. Figure 6f shows the projection of the attractor on the (x, φ) plane, which is a manifestation of a backward and forward folding perpendicular to the (x, φ) plane at the upper and lower vertical lines of x = 0. Combing Figure 6d,e, the running law of the trajectory is clear. In addition, the Lyapunov exponents of the system are $LE_1 = 0.4488$, $LE_2 = 0$, $LE_3 = -2.3519$, and $LE_4 = -58.0488$, and the Lyapunov dimension of this attractor is obtained below:

$$D_L = j + \frac{1}{|LE_{j+1}|} \sum_{i=1}^{j} LE_i = 3 + \frac{LE_1 + LE_2 + LE_3}{LE_4} = 3.0328$$

These indicate that the attractor of the system is chaotic. Further, the Poincaré mapping of the trajectory on the (y, z) plane is confirmed, as shown in Figure 7a, and the time domain waves of x, y, z, and φ are reported, as shown in Figure 7b, which indicates that the system is the aperiodicity and pseudorandomness.



Figure 7. (a) Poincaré mapping on the (y, z) plane; (b) the time domain waves of the states x, y, z, and φ .

In short, the system is a chaotic oscillator system, which is confirmed by using the phase diagrams, Poincaré mapping, time-domain waves, the Lyapunov exponents, and its corresponding dimensions.

3.2. Stability of the System

Let the parameters be fixed as in Table 1, and $\dot{x} = \dot{y} = \dot{z} = \dot{\varphi} = 0$, and the equilibria of Equation (14) are obtained as

$$E_1 = \{(x, y, z, \varphi) | x = y = z = \varphi = 0\}$$
$$E_{2,3} = \{(x, y, z, \varphi) | x = y = z = 0, \varphi = \pm 5\}$$
$$E_{4,5} = \{(x, y, z, \varphi) | x = \pm 0.004917, y = \pm 0.000032, z = \mp 0.004885, \varphi = \mp 4.8996\}$$

At the equilibrium of the system, the Jacobian matrix *J* is

$$J = \begin{bmatrix} a(h-1-\varphi^2) & a & 0 & -2ax\varphi^2 \\ 1 & -1 & 1 & 0 \\ 0 & -b & -c & 0 \\ 100 & 0 & 5-\varphi \operatorname{sign}(\varphi) - |\varphi| \end{bmatrix}$$
(15)

When the system parameters are set as in Table 1, accordingly the characteristic equation is

$$a_{10}\lambda^4 + a_{11}\lambda^3 + a_{12}\lambda^2 + a_{13}\lambda + a_{14} = 0$$

where

$$\begin{split} a_{10} &= 1 \\ a_{11} &= |\varphi| + \varphi^2 \text{sign}(\varphi) + 7.5\varphi^2 - 182.7 \\ a_{12} &= 7.5\varphi^2 |\varphi| - 177.7 |\varphi| + 7.5\varphi^3 \text{sign}(\varphi) + 1500x\varphi - 177.7\varphi \text{sign}(\varphi) - 20.25\varphi^2 + 667.3 \\ a_{13} &= 17.25\varphi^2 |\varphi| - 221.2 |\varphi| + 17.25\varphi^3 \text{sign}(\varphi) + 3450x\varphi - 221.2\varphi \text{sign}(\varphi) + 1416\varphi^2 - 34957.75 \\ a_{14} &= 1502.25\varphi^2 |\varphi| - 36063.75 |\varphi| + 1502.25\varphi^3 \text{sign}(\varphi) + 300450x\varphi - 36063.75\varphi \text{sign}(\varphi) - 7511.25\varphi^2 + 180318.75 \end{split}$$

One has $\Delta_0 = a_{10}$, $\Delta_1 = a_{11}$, $\Delta_2 = -\frac{a_{10}a_{13}-a_{11}a_{12}}{a_{11}}$, $\Delta_3 = -\frac{a_{11}a_{14}-a_{13}\Delta_2}{\Delta_2}$, and $\Delta_4 = a_{14}$, where symbols Δ_0 , Δ_1 , Δ_2 , Δ_3 , and Δ_4 are the first column of the Routh table. On the basis of the Routh Criterion, if Δ_0 , Δ_1 , Δ_2 , Δ_3 , and Δ_4 are all positive, and the eigenvalues of the system are all negative, then the equilibrium of the system is stable. Otherwise, it is unstable.

At the equilibrium E_1 , the four values $\Delta_0 = 1$, $\Delta_1 = -182.7$, $\Delta_2 = 667.3$, $\Delta_3 = -34,957.75$, and $\Delta_4 = 180,318.75$ were not all positive, and the eigenvalues of the system were $\lambda_1 = 0.0500$, $\lambda_2 = 1.8004$, and $\lambda_{3,4} = -0.0017 \pm 0.1410i - \lambda_1$ and λ_2 are the positive real numbers, and λ_3 and λ_4 are a pair of conjugate complex numbers with a negative real part. Therefore, E_1 is an unstable saddle focus with index 2, foreshadowing the emergence of chaos.

At the equilibria E_2 and E_3 , the four positive values $\Delta_0 = 1$, $\Delta_1 = 14.8$, $\Delta_2 = 87.2426$, $\Delta_3 = 1276.8$, and $\Delta_4 = 7462.5$ determine that points E_2 and E_3 are unstable. The eigenvalues were $\lambda_1 = -5.0000$, $\lambda_2 = -7.6984$, and $\lambda_{3,4} = -1.0508 \pm 13.8840i$ — λ_1 and λ_2 are negative real numbers, and λ_3 and λ_4 are a pair of conjugate complex numbers with a negative real part. Thus, E_2 and E_3 are stable foci.

Similarly, at the equilibria E_4 and E_5 , the corresponding $\Delta_0 = 1$, $\Delta_1 = 7.1487$, $\Delta_2 = 2376.3566$, $\Delta_3 = 5208.8159$, and $\Delta_4 = 723,859.588$ were all positive, and the eigenvalues were $\lambda_1 = -8.9473$, $\lambda_2 = 4.1657$, and $\lambda_{3,4} = -1.1766 \pm 13.8809i$. The eigenvalue λ_1 is a negative real number, λ_2 is a positive real number, and λ_3 and λ_4 are a pair of conjugate complex numbers with the negative real part. Hence, E_4 and E_5 are the unstable saddle foci with index 1.

4. Dynamics of the Memristor-Based Oscillator

4.1. Symmetry

Equation (14) is invariant when state variables (x, y, z, φ) are transformed into (-x, -y, -z, $-\varphi$), i.e., Equation (14) is symmetric with respect to the origin O(0, 0, 0, 0). Let the parameters of Equation (14) be set as in Table 1, and the phase diagrams of the typical attractors are obtained, as shown in Figure 8

with two symmetrical initial conditions, (0, 2, 0, 0) and (0, -2, 0, 0). It can be seen from Figure 8 that each of the two attractors is asymmetric, and that they are symmetric to each other with respect to the origin.



Figure 8. Projections of the attractors on the (y, z) plane with different initial conditions: (**a**) (0, 2, 0, 0); (**b**) (0, -2, 0, 0).

4.2. Dynamics of the Memristor-Based Oscillator with the Varying Parameter c

The dynamics of the system are analyzed with the varying parameter *c* in this subsection. The Lyapunov exponents and the corresponding bifurcation diagram were calculated, as shown in Figure 9, where the parameter *c* varies in the interval (0.4, 1.5), and other circuit parameters remained unchanged as in Table 1. It is seen from Figure 9 that the system had multiple periodic oscillations and chaotic oscillations. The period-1 attractors existed in the interval $c \in (0.4, 0.6)$, the period orbits evolved from period-1 to multiple periods through doubling bifurcation in the interval $c \in (0.4, 0.79)$, and the chaotic states with several periodic windows existed in the interval $c \in (0.79, 1.5)$. The phase portraits of the corresponding periodic and point attractors were given, as shown in Figure 10, with different parameters *c*.



Figure 9. Dynamics of the system with the parameter $c \in (0.4, 1.5)$: (a) bifurcation diagram; (b) Lyapunov exponents.



Figure 10. Cont.



Figure 10. Phase portraits of the periodic and point attractors on the (x, y) plane with the different parameters: (**a**) period-1 attractor with c = 0.45; (**b**) period-2 attractor with c = 0.70; (**c**) period-4 attractor with c = 0.78; (**d**) a point attractor with c = 1.5.

4.3. Coexisting Bifurcation and Coexisting Attractors with the Varying Parameter a

The coexisting bifurcation is a bifurcation phenomenon that depends on initial conditions. Considering the change of the parameter *a* and other circuit parameters as in Table 1, the coexisting bifurcation diagram was obtained, as shown in Figure 11a, where the orbit colored with red originated from initial conditions (0, 0.001, 0, 0) and those colored in blue started from initial conditions (0, -0.001, 0, 0, 0). It can be seen from Figure 11a that the dynamical evolution of the memristor-based chaotic system was that from the convergence point to chaotic orbit by period-doubling bifurcations as the parameter *a* increased. In addition, several periodic windows were observed in the chaotic region. The corresponding Lyapunov exponents further confirmed the dynamics of the system, as shown in Figure 11b.



Figure 11. Dynamics of the system with the varying parameter *a*: (**a**) coexisting bifurcation diagram; (**b**) Lyapunov exponents.

Using the phase diagram, the evolution of the coexisting attractors was analyzed with the varying parameter *a*. Several coexisting attractors were obtained, as shown in Figure 12, with different initial conditions (0, 0.001, 0, 0) and (0, -0.001, 0, 0). The attractors from initial conditions (0, 0.001, 0, 0) are painted red and the counterpart from (0, -0.001, 0, 0) are blue. It can be seen from Figure 12 that the coexisting attractors evolved from a pair of symmetrical point attractors to symmetrical chaotic attractors, then to a period-2 attractor pair, and finally to a period-1 attractor pair. This is consistent with the dynamics of the system in Figure 11.



Figure 12. Evolution of coexisting attractors with the varying parameter *a*: (**a**) a = 7.38; (**b**) a = 7.5; (**c**) a = 8.0; (**d**) a = 8.2.

4.4. Heterogeneous Multistability

If several or even infinite kinds of coexisting attractors are found in a dynamics system, then the system has heterogeneous multistability [35]. The typical attractors can be obtained as shown in Figure 13, when the system parameter values were set as in Table 1 and the initial conditions are (0, y(0), 0, 0). It can be seen from this figure that the point attractors and chaotic attractors switched with the change of component y(0) of the initial conditions. The corresponding Lyapunov exponents and bifurcation diagrams were calculated, as shown in Figure 14. It can be seen from Figure 14 that the system had state-switching between point attractors and chaotic attractors. The point attractors and chaotic attractors are two kinds of attractors with different properties. Thus, the system has heterogeneous multistability.



Figure 13. The state-switching between point attractors and chaotic attractors with the varying component y(0).



Figure 14. Dynamics of the system with $y(0) \in (-3, 3)$: (a) bifurcation diagram; (b) Lyapunov exponents.

4.5. Transient Chaos

Let the parameter c = 1.42 and other parameters remain unchanged as in Table 1, and the time domain wave of the state y is displayed, with the initial conditions (0, 0.001, 0, 0), as shown in Figure 15a, which confirms the system has a transient oscillation. To observe the specific evolution of the corresponding orbits, the attractors with different time durations on the (y, z) plane were found, as shown in Figure 15b,c.



Figure 15. The transient phenomenon of the system: (a) the time-domain wave of the state *y*; (b) the attractor with the time duration t = 0-23; (c) the attractor with the time duration t = 23-30.

It can be seen from Figure 15 that the system state was chaotic at the time duration t = 0-23, and the corresponding attractor on the *y*-*z* plane is shown in Figure 15b. In addition, the amplitude of the state *y* gradually decreased to zero over time *t*, and the corresponding trajectory is shown in Figure 15c. This indicated that the system has transient chaos.

In short, the system has the symmetrical coexisting attractors, transient chaos, and heterogeneous multistable states. Additionally, an interesting state-switching between different attractors was found with the varying initial component.

5. The Physical Realization of the Memristor-Based Chaotic System

In this section, an analog circuit of the memristor-based chaotic system is designed to verify the dynamic behaviors of the system, as shown in Figure 16.

The output voltages of the amplifier U_2 , U_5 , U_7 , and U_{12} are marked as v_{U_2} , v_{U_5} , v_{U_7} , and $v_{U_{12}}$, representing the state variables x(t), y(t), z(t), and $\varphi(t)$ of the system. When the output voltages y(t) and x(t) pass through the inverters U_1 and U_3 , the signals y(t) and x(t) are converted to -y(t) and -x(t). The signals $\varphi(t)$ and x(t) are converted to $\varphi^2(t)x(t)$ through the multipliers A_1 and A_2 . They are to be the input of the inverse integrator U_2 , then the first equation of the Equation (16) is obtained. The signals x(t) and z(t) are converted to -x(t) and -z(t) through the inverters U_6 and U_7 . The second equation of Equation (16) is generated with the signals -x(t), y(t), and -z(t) at the input of the inverse integrator U_5 . With the inverse integrator U_7 , we can obtain the third equation of Equation (16). Through an

absolute circuit consisting of two amplifiers U_9 and U_8 , two diodes D_1 and D_2 , and some resistors, signal $\varphi(t)$ implements the absolute value operation, i.e., $\varphi(t) \rightarrow |\varphi(t)|$. Then, the signal $\varphi(t)$ is multiplied by the multiplier A_3 to obtain $\varphi(t)|\varphi(t)|$ as the input of inverse integrator U_{12} . The final equation of the Equation (16) is obtained by the action of the amplifier U_{12} . The dynamics of the circuit are described as

$$\frac{dX}{dT} = \frac{R_2}{C_1 R_1 R_3} Y - \frac{1}{C_1 R_4} \Phi^2 X + \frac{R_7}{C_1 R_5 R_6} X$$

$$\frac{dY}{dT} = \frac{R_{12}}{C_2 R_8 R_{11}} X - \frac{1}{C_2 R_9} Y + \frac{R_{13}}{C_2 R_{10} R_{14}} Z$$

$$\frac{dZ}{dT} = -\frac{1}{C_3 R_{16}} Y - \frac{1}{C_3 R_{15}} Z$$

$$\frac{d\Phi}{dT} = -\frac{1}{C_4 R_{24}} \Phi |\Phi| + \frac{R_{22}}{C_4 R_{21} R_{25}} \Phi + \frac{R_{27}}{C_4 R_{23} R_{26}} X$$
(16)



Figure 16. Circuit diagrams of the system.

In general, the larger the time scale transformation factor, the faster the time-domain orbit of the system runs and the denser the phase trajectory. Conversely, the smaller the time scale transformation factor, the slower the time domain orbit of the system runs and the sparser the phase trajectory. When the chaotic oscillator is designed, the time scale conversion can make up for the problem of the slow evolution of the time-domain of the system caused by excessive integration capacitance and can reduce the resistance value of the integration circuit. Accordingly, it is convenient for circuit debugging. The amplitude scale conversion is to constrain the range of system variables to the reference voltage (-15V, 15V) to prevent circuit saturation distortion. On the basis of Equation (16), the time scale transformation is performed first, and the inter-scale transformation factor K_1 is set as 100, i.e., $t = K_1T = 100T$.

Letting $x = K_2 X$, $y = K_2 Y$, $z = K_2 Z$, and $\Phi = K_2 \varphi$, Equation (16) is transformed to

$$\begin{cases} \frac{dx}{dt} = \frac{R_2}{K_1 C_1 R_1 R_3} y - \frac{K_2^2}{K_1 C_1 R_4} \varphi^2 x + \frac{R_7}{K_1 C_1 R_5 R_6} x \\ \frac{dy}{dt} = \frac{R_{12}}{K_1 C_2 R_8 R_{11}} x - \frac{1}{K_1 C_2 R_9} y + \frac{R_{13}}{K_1 C_2 R_{10} R_{14}} z \\ \frac{dz}{dt} = -\frac{1}{K_1 C_3 R_{16}} y - \frac{1}{K_1 C_3 R_{15}} z \\ \frac{d\phi}{dt} = -\frac{K_2}{K_1 C_4 R_{24}} \varphi |\varphi| + \frac{R_{22}}{K_1 C_4 R_{21} R_{25}} \varphi + \frac{R_{27}}{K_1 C_4 R_{23} R_{26}} x \end{cases}$$
(17)

where $K_2 = 2$. Comparing Equation (14) and Equation (17), one has

$$a = \frac{R_2}{K_1 C_1 R_1 R_3} = \frac{K_2^2}{K_1 C_1 R_4}, \ b = \frac{1}{K_1 C_3 R_{16}}, \ c = \frac{1}{K_1 C_3 R_{15}}, \ ah - a = \frac{R_7}{K_1 C_1 R_5 R_6},$$

$$\frac{R_{12}}{K_1 C_2 R_8 R_{11}} = \frac{1}{K_1 C_2 R_9} = \frac{R_{13}}{K_1 C_2 R_{10} R_{14}} = \frac{K_2}{K_1 C_4 R_{24}} = 1, A = \frac{R_{22}}{K_1 C_4 R_{21} R_{25}}, B = \frac{R_{27}}{K_1 C_4 R_{23} R_{26}}$$

when

$$\begin{split} C_1 &= C_2 = C_3 = C_4 = 10nf, \\ R_1 &= R_2 = R_6 = R_7 = R_{11} = R_{12} = R_{13} = R_{14} = R_{18} = R_{19} = R_{20} = R_{22} = R_{23} = R_{26} = R_{27} = 10k\Omega, \\ R_8 &= R_9 = R_{10} = 1000k\Omega, R_3 = 133k\Omega, R_4 = 33k\Omega, R_5 = 5.4k\Omega, R_{15} = 770k\Omega, R_{16} = 4.2k\Omega, \\ R_{24} &= 500k\Omega, R_{25} = 200k\Omega, R_{21} = 20k\Omega. \end{split}$$

The typical chaotic attractor of the system is obtained by Multisim experiment, as shown in Figure 17, which starts from the initial conditions (0, 0.001, 0, 0), and is consistent with those of the numerical simulation shown in Figure 6c.



Figure 17. The typical chaotic attractor of the memristive chaotic system by Multisim.

Correspondingly the physical circuit of the memristor-based chaotic system is given to further verify the above-mentioned theoretical analysis. The experimental result of the circuit is obtained, as shown in Figure 18, where the multiplier is AD633JN and the operational amplifier is OP07CP. The typical chaotic attractor is displayed in Figure 18a, which is captured by the oscilloscope DSO-X3034A. The experimental result is also consistent with the numerical simulation in Figure 6c.



Figure 18. Cont.



Figure 18. The experimental results of the memristive chaotic system from the physical circuit: (a) the typical chaotic attractor from the oscilloscope; (b) experimental platform; (c) the corresponding circuit board.

6. Implementation of the Chaotic System by DSP Technology

Although the memristive chaotic systems can be implemented by the analog circuits, the system characteristics that depend on the initial conditions are difficult to control. Moreover, chaotic artificial circuits cannot be used directly in digital encryption systems because random signal disturbances make the circuit output unstable.

Hence, the presented system was further discretized and realized on DSP (digital signal processing) platform, which makes the system controllable and stable enough to be used for chaotic encryption. There are usually three algorithms for the discretization and digitization of continuous chaotic systems: simple Euler algorithm, improved Euler algorithm, and Runge–Kutta algorithm. Each of these three algorithms has its advantages and disadvantages. The improved Euler algorithm and the Runge–Kutta algorithm have higher precision, but they occupy more resources. The simple Euler algorithm is accepted for DSP implementation as the simple Euler algorithm requires less resources and satisfies experimental requirements. The simple Euler algorithm comes from the following derivative:

$$\frac{\mathrm{d}x}{\mathrm{d}t} = \lim_{T \to 0} \frac{x(t_n + T) - x(t_n)}{T} \approx \frac{x_{n+1} - x_n}{T} \underline{\det} \frac{\mathrm{def}}{T} \frac{x(n+1) - x(n)}{T}.$$
(18)

Substituting Equation (18) into Equation (14) yields

$$\begin{cases} \frac{x(n+1)-x(n)}{T} = a[y(n) - x(n) + hx(n) - \varphi^2(n)x(n)] \\ \frac{y(n+1)-y(n)}{T} = x(n) - y(n) + z(n) \\ \frac{z(n+1)-z(n)}{T} = -by(n) - cz(n) \\ \frac{\phi(n+1)-\phi(n)}{T} = -\varphi(n)|\varphi(n)| + A\varphi(n) + Bx(n) \end{cases}$$
(19)

Equation (19) is reset as

$$\begin{cases} x(n+1) = a[y(n) - x(n) + hx(n) - \varphi^2(n)x(n)] \ T + x(n) \\ y(n+1) = [x(n) - y(n) + z(n)] \ T + y(n) \\ z(n+1) = [-by(n) - cz(n)] \ T + z(n) \\ \varphi(n+1) = [-\varphi(n)|\varphi(n)| + A\varphi(n) + Bx(n)] \ T + \varphi(n) \end{cases}$$
(20)

where the parameters *a*, *b*, *c*, *h*, *A*, and *B* are set as in Table 1. The digital signal is obtained by solving Equation (20) in a digital signal processor, where the integration step T = 0.001 and the initial conditions are set as x(0) = 0, y(0) = 0.001, z(0) = 0, and $\varphi(0) = 0$. The experimental results of the memristor-based chaotic system by DSP technology are obtained, as shown in Figure 19, which shows the typical chaotic attractor on the (*y*, *z*) plane, the coexisting chaotic attractors, coexisting period-1 attractors on the (*y*, *z*) plane, the point attractors, and chaotic attractors on the (*x*, *z*) plane in Figure 19a–e, respectively. It can

be seen from Figure 12b,c that the upper attractor was bright with the initial conditions (0, 0.001, 0, 0), and the lower attractor was dark with the initial condition (0, -0.001, 0, 0)). Additionally, Figure 19d,e confirms the existence of two states with switching. These are the point attractor and chaotic attractor, where the point attractor is obtained with the initial conditions (0, -0.2, 0, 0) and the chaotic attractor with the initial conditions (0, -0.1, 0, 0).



Figure 19. Digital signal processing (DSP) implemental results of the chaotic system: (**a**) the typical chaotic attractor; (**b**) the coexisting chaotic attractor; (**c**) the coexisting period-1 attractor; (**d**) the point attractor; (**e**) the typical chaotic attractor.

The results obtained by circuit experiment and DSP technology further verify the theoretical analysis of the system.

7. Conclusions

In this paper, a flux-controlled active memristor was presented and its emulator was designed, which showed its characteristic fingerprints. The hysteresis loops keep the symmetrical font "8" when the frequency is more than 300Hz, which indicates that the emulator is a suitable device to explore the circuit properties of the memristor. The memristor-based chaotic system was designed and a novel attractor was found in the system. The system not only has heterogeneous multistability, but also has the novel state-switching between point attractors and chaotic attractors with the change of the initial conditions. Furthermore, coexisting attractors and the transient chaotic attractor were implemented by

the analog circuit and DSP technology, respectively, which verified the results of theoretical analysis. More rigorous theoretical analyses of the proposed memristor-based chaotic system will be further studied in the near future.

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