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Design and Performance Analysis of a Stand-alone PV System with Hybrid Energy Storage for Rural India

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Abstract: The operations of domestic stand-alone Photovoltaic (PV) systems are mostly dependent on storage systems due to changing weather conditions. For electrical energy storage, batteries are widely used in stand-alone PV systems. The performance and life span of batteries depend on charging/discharging cycles. Fluctuation in weather conditions causes batteries to charge/discharge quite often, which decreases the operational life and increases the maintenance cost. This paper proposes a domestic stand-alone PV system with Hybrid Energy Storage System (HESS) that is a combination of battery and supercapacitor. A new Fuzzy Logic Control Strategy (FHCS) is implemented to control the power flow of the battery and supercapacitor. Simulation studies are performed with real data collected in Sultanpur, India to investigate the proposed system's performance (Latitude [N] 26.29 and Longitude [E] 82.08). The results show that FHCS successfully controls the power flow of HESS components to increase the system efficiency. The developed system is validated to provide an effective alternative that would enhance the battery life span and reduce the system maintenance cost. While considering the prohibitive upfront costs for rural systems, such an improvement helps to electrify more underserved communities.

Keywords: Hybrid Energy Storage System (HESS); stand-alone PV system; Fuzzy logic; control strategy; supercapacitor

1. Introduction

India is one of the fastest developing countries in the renewable energy sector. The Indian government is now concentrating on energy generation using renewable energy sources. A large number of solar power plants are setup by the government, and many are in progress under government-initiated schemes. Many steps are also taken to make people aware about the attributes of domestic Photovoltaic (PV) systems. Specifically, the domestic stand-alone PV system is a promising solution for green energy in rural areas. On the other side, the requirement of large battery storage and its expensive maintenance makes it a burdensome option for Indian consumers [1].

The operation of stand-alone PV systems is very much dependent on batteries to satisfactorily fulfil power demands. Generally, in these systems, the batteries are charged in peak sun time and the stored energy is used when required [2]. The solar radiation varies all over the day and this irregular radiation pattern affects the PV power generation [3]. In the literature, different forecasting methods are developed to estimate the solar radiation [4,5]. A battery suffers from rapidly changing charging/discharging patterns due to intermittent radiation conditions appearing in a day. This condition affects the battery performance, decreases the life span, and adds to the battery replacement cost [6–8]. Hybrid energy storage system (HESS) is a solution to minimize the

stress of unnecessary charging/discharging on batteries. It is reported that a combination of battery and supercapacitor as a HESS enhances the stand-alone PV system's performance and minimizes the battery maintenance cost [9,10]. A battery-supercapacitor duo has been widely considered in most HESS developments, as they complement the limitations of each other and have relatively low costs [11]. The implementation of HESS would also reduce the dynamic stress on battery during fast transient or sudden climate change condition.

A control strategy is essential to optimize the stand-alone PV system performance and to exploit the advantages of HESS [12,13]. This control strategy manages the power flow of the battery and supercapacitor according to input irradiance and load demand conditions. For HESS control, two control strategies are commonly found in the literature. First is the Rule Based Control (RBC), which is simple and easy to implement. However, it lacks the ability to adopt real time weather conditions, since it has a pre-defined set of rules and threshold values for operations [14,15]. Second is the Filtration Based Control (FBC). It decomposes the dynamic power demand into high and low frequency components while using a filter [16,17]. The performance of FBC based controller is good in smoothing the system output current, but it neglects the HESS state of charge (SOC) parameters. The SOC of HESS is also a trivial parameter in the control strategy, so it is not effective in minimizing the dynamic stress of the battery.

Different strategies that are based on particle swarm optimization (PSO) or Combined Heat & Power (CHP) control have been developed for HESS, but these techniques are very complex and not suitable for small-scale stand-alone PV systems [18–20]. P. Thoungthong [21] developed a renewable energy-based power plant while using supercapacitor, but, in this proposed scheme, PV system has a limited power backup. D. Brunelli et al. [22] attempted to develop a battery less Solar-Harvesting circuit using supercapacitor for embedded systems, but this technique is not suitable for domestic stand-alone PV systems due to its complexity and high-cost. Therefore, there is a need for a simple and efficient control strategy that can optimally control the power flow of battery and supercapacitor in a HESS that is used in domestic stand-alone PV applications.

In this paper, a stand-alone PV system with HESS is proposed for domestic applications in rural areas. The motive is to set up the supercapacitor as secondary energy storage source in order to reduce the dynamic charging/discharging stress on the battery. A Fuzzy Logic based HESS Control Strategy (FHCS) is also proposed to control the power flow of battery/supercapacitor. This proposed control strategy uses supercapacitor during fast transients and it prevents battery charge/discharge. Battery is utilized to feed the load, only if there is a linear radiation change. This technique reduces the unnecessary charging/discharging of the battery, prevents the battery to deepen discharge and, consequently, reduces the maintenance cost of stand-alone PV system and enhances the battery life.

The organization of this paper is as follows. Section 2 presents of HESS system configuration and modeling. The control strategies for HESS control and proposed Fuzzy logic-based Control Strategy is described in Sections 3 and 4, respectively. The HESS system size calculations and system descriptions are given in Section 5, while the simulation results and their analysis are presented in Section 7 describes the effects of charging/discharging cycle on battery performance. It also compares battery lifetime with and without the developed FHCS. Finally, Section 8 draws the conclusions.

2. General HESS System Configuration and Modelling

2.1. HESS Configuration

Figure 1 shows a separate converter type HESS based PV system. In this type of configuration, two bidirectional buck-boost converters are used to control the energy flow of battery and supercapacitor. A separate boost converter is also used with PV modules to implement maximum power point tracking (MPPT) in this configuration. The beauty of this type of configuration is that it can independently control the energy of both energy storage systems (battery and supercapacitor).

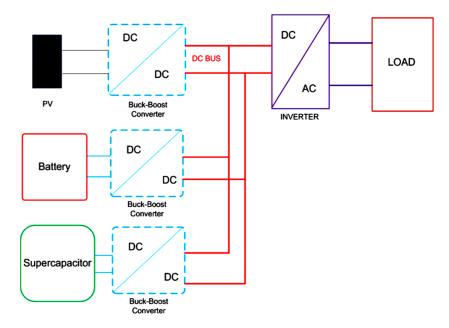


Figure 1. Hybrid energy storage system (HESS) Based Photovoltaic (PV) System.

2.1.1. Modeling of HESS

A HESS comprises of more than one energy storage component. In this paper, the battery and supercapacitor are connected together as a HESS. The mathematical modeling of supercapacitor and HESS based PV system are described below.

2.1.2. Modeling of Supercapacitor

The model of supercapacitor is a simple series RC model, as illustrated in Figure 2 The supercapacitor is nothing but a simple capacitor having large electric charge storing capacity. This adapted supercapacitor model is simple and accurate in validating the HESS in small PV systems [19]. Equation (1) shows the voltage and current relationship of supercapacitor.



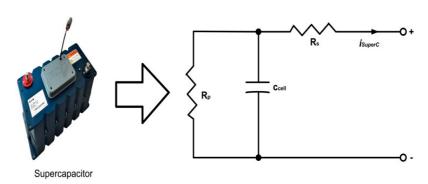


Figure 2. Supercapacitor Model.

2.2. Modeling of Proposed HESS Based PV System

Figure 3 depicts the proposed HESS based PV system. This HESS based PV system is based on mixed converter type topology. In this topology, separate bidirectional buck/boost converters are used to control the power flow of battery and supercapacitor. A control algorithm controls both buck/boost

converters that are associated with the battery and the supercapacitor to meet the power demand on the DC bus. The overall system equation is as given in (2).

$$P_{PV} + P_{BT} + P_{SC} - P_L = 0 (2)$$

where P_{PV}, P_{BT}, P_{SC}, and P_L denoted the power outputs of PV, battery, supercapacitor, and load power, respectively.

The efficiencies of supercapacitors and batteries are represented as in (3) and (4), where P_{ASC} and P_{ABT} are the ratings of supercapacitor and battery, respectively. Their efficiencies of supercapacitor and battery are denoted by η_{SC} and η_{BT} , respectively.

$$P_{SC} = \eta_{Sc} * P_{ASC} \tag{3}$$

$$P_{BT} = \eta_{BT} * P_{ABT} \tag{4}$$

The required power, ΔP , on the DC bus is as expressed in (5)

$$\Delta P = P_{PV} - P_L \tag{5}$$

The storage devices are required to provide ΔP , as in (6).

$$\Delta P = P_{PV} - P_L \tag{6}$$

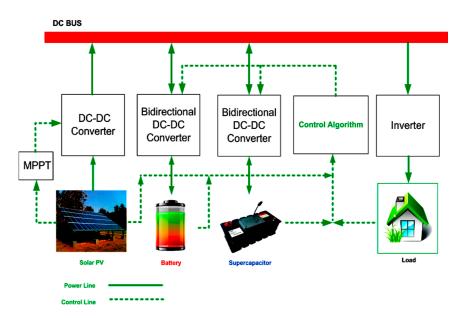


Figure 3. Proposed HESS Based Stand-alone PV System for Domestic Application.

3. Control Strategies for HESS

Different strategies are used to control the power flow between DC bus and HESS. In the literature, the control strategies are classified as classical and intelligent control strategies [23]. Rule based controller (RBC) and filtration-based controller (FBC) are two further categories of classical strategies. RBC and FBC are simple and easy to implement, but the former is very sensitive while the latter is rigid [24–26]. Intelligent control strategies, such as fuzzy logic control (FLC), are reliable and efficient options.

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3.1. Rule Based Controller (RBC)

RBC uses a set of rules to decide the power flow between the battery/DC Bus or Supercapacitor/DC Bus. Due to the simplicity of this technique, it does not require high processing, however it is very sensitive to system parameter variations. An RBC, in [27], is reworked and shown in Figure 4a. The IB1 and IB2 are the battery current thresholds and K1 and K2 are the slope gradients. When the battery current is within the limit of IB1 and IB2 the battery only supplies the power to load. When the battery current exceeds the threshold limit IB1 or IB2, the extra power demand will be provided by both the battery and the SC. The general design and performance analysis of RBC controller are explained in detail in [28].

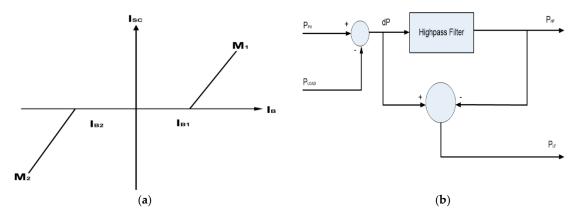


Figure 4. (a) Rule Based Controller (RBC), (b) Filtration Based Controller (FBC).

3.2. Filtration Based Controller (FBC)

The FBC based controller uses a filter to extract the dynamic components of the power as high-frequency and low-frequency components. Due to simplicity, this technique requires less complication. Figure 4b illustrates the high-pass filter (HPF) based FBC, which is adopted from [29]. The high frequency component (PHF) and low frequency component (PLF) describe the power demand. The design and performance analysis are described in detail in [30].

4. Proposed Fuzzy based HESS Control Strategy (FHCS)

The proposed FHCS is described in Figure 5a. This control strategy controls the power flow between HESS and DC bus according to the proposed fuzzy rules. Solar irradiance I_r , DC bus voltage V_{DC} and current I_{DC} used as the input parameters to fuzzy controller. ΔP is deficient or required power and ΔI_r is change in solar irradiance. The fuzzy controller controls the power between the supercapacitor to DC bus and battery to DC bus while using a switch connected between them. The FHCA generates SCG and SBG control signal to operate the switches, respectively, and also controls the buck/boost converter duty cycle associated with them. This control scheme also decides when power should be delivered to the DC bus or when the battery/supercapacitor should be charged. Thus, duty cycle, SCG, and SBG control signals are considered as the output parameters of fuzzy controller, as shown in Figure 5b. For developing a fuzzy control strategy, the first step is to define different membership functions and the values of input and output parameters in each function. For the proposed FHCS the values of different membership functions considered, in this paper, are listed Table 1 Based on the possible maximum and minimum ranges of different parameters, eight membership functions with combinations of different parameter value ranges are defined. The fuzzy rules that formed based on the membership functions are shown in Figure 6a–e.

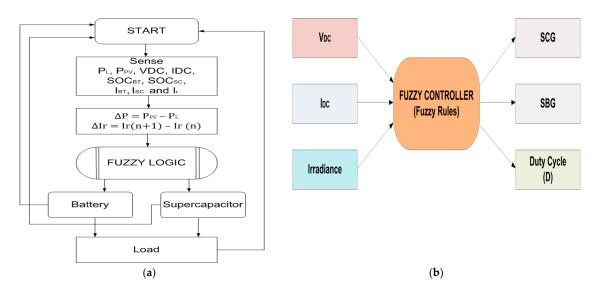
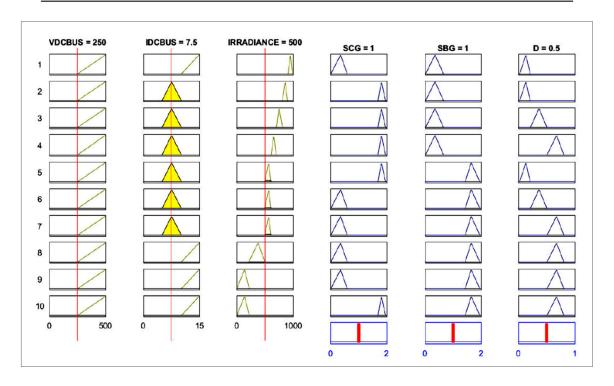
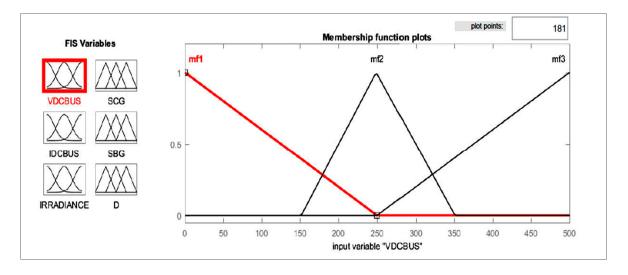


Figure 5. (a) Proposed Fuzzy based HESS Control (b) Input and Output of Fuzzy Logic System.

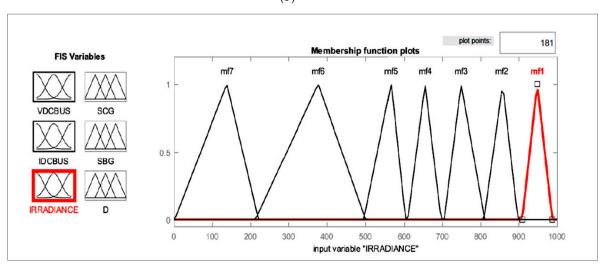
mf	V _{DC} BUS (volt)	I _{DC} BUS (amp)	Irradiance (W/m²)	SCG	SBG	DUTY CYCLE (%)
mf1	0-250	0–5	900-1000	0	0	5–10
mf2	150-350	5–10	800-900	1	1	10-20
mf3	250-500	10-15	700-800			20-30
mf4			600-700			30-40
mf5			500-600			40-50
mf6			200-500			50-60
mf7			0-200			60–70
mf8						70–80



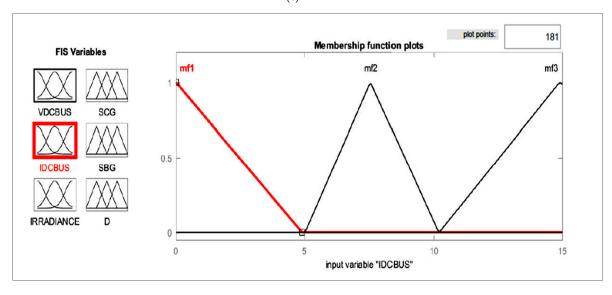
(a)



(b)



(c)



(d)

Figure 6. Cont.

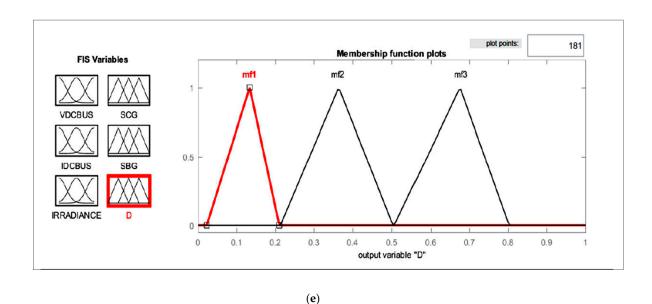


Figure 6. (a) Fuzzy Rules Diagram; (b) DC Bus Voltage Membership Functions; (c) DC Bus Current Membership Functions; (d) Irradiance Membership Functions; and, (e) Duty Cycle Membership Functions.

4.1. Battery Control

FHCS generates a control signal (SBG) to open/close the switch connected between them to control the power flow between battery and DC bus. This control signal allows for the power flow from battery to DC bus and vice versa according to input conditions. The benefit of this control strategy is that it also controls the duty cycle of battery buck/boost converter according to the demand of DC bus. The power of battery is only used during linear transient conditions; during fast transient and constant radiation conditions, only the supercapacitor is used to compensate the deficient power on DC bus. This control mechanism stabilizes the power at DC bus based on load side demand and available input power. The membership function of SBG and its values are summarized in Figure 6a–c and Table 1.

4.2. Supercapacitor Control

The supercapacitor has the property of charging and discharging very fast. It can provide high power for a short interval of time. Therefore, it is beneficial to balance the power flow on DC bus under the fast transient or partial shading condition. The FHCS detects the fast-transient conditions and controls the supercapacitor power flow using SCG signal as well as buck/boost converter's duty cycle D. The supercapacitor power is only used during fast transient conditions to stabilize the power on the DC bus. This control mechanism saves the battery from unnecessary charge/discharge operation and enhances the battery life, which is the key motive of this work. The membership function of SCG and its values are described in Figure 6a–c and Table 1.

4.3. HESS Duty Cycle Control

The duty cycle of book/boost converter is used to control power flow of battery/supercapacitor to the DC bus. The duty cycle varies between 5% and 80% according to power deficiency and load demand. The variation in buck/boost converter duty cycle makes DC bus voltage and current stable. The membership functions, *mf1* to *mf8*, and Table 1 shows their values.

5. HESS Size Calculations and Stand-alone PV System Description

In this work, a standalone PV system is designed to evaluate the performance of HESS based stand-alone PV system. A 5-kW standalone PV system is considered with HESS for energy backup. HESS is formulated with battery and supercapacitor connected in separate converter type topology.

The battery and supercapacitor sizes depend on PV system capacity, amount of backup needed, and radiation transients.

5.1. HESS Size Calculations

The size of HESS affects the performance of standalone PV system and its overall cost. The basic size of battery and supercapacitor is formulated, as follows.

5.1.1. Battery Size Calculation

The battery capacity is considered in amperes hours (Ah).

$$P = I \times V_b \tag{7}$$

where, P is power, I is current in amperes, and V_b is battery voltage in volts.

$$I = i_b \times h \tag{8}$$

where i_b is battery current and h is time in hours.

$$i_b \times h \text{ is in Ah (Amp hours)}$$
 (9)

Replacing these values in Equation (7), we get

$$P = Ah \times V_h \tag{10}$$

Now, rearranging the equation gives

$$Ah = P/V_b \tag{11}$$

where Ah is the required battery capacity and it is represented in terms of P, rated power of PV system.

5.1.2. Supercapacitor Size Calculation

Supercapacitor size is considered in Farad (F).

$$q = V_{SC} \times C_{SC} \tag{12}$$

$$q/t = I_{SC} \tag{13}$$

where q is charge, V_{SC} is voltage, C_{SC} is capacitance, I_{SC} is current, and t is time.

From Equations (12) and (13), it can be derived

$$I_{SC} = (V_{SC} \times C_{SC})/t \tag{14}$$

$$P = I_{SC} \times V_{SC} \tag{15}$$

$$P = \frac{V_{SC}^2}{t} \times C_{SC} \tag{16}$$

$$C_{SC} = \frac{V_{SC}^2}{t} \times P \tag{17}$$

where C_{sc} is supercapacitor size in Farad, V_{sc} is supercapacitor voltage, and P is PV system power.

5.2. Stand-alone PV System Description

In the studied model, a standalone PV system consists of a PV array, a charge controller, battery bank, and an inverter. In this work, a Canadian Solar CS6P-250PT 250 W PV module is used to simulate

the PV system. Four PV modules in total are connected for a 5 kW standalone PV system having two strings and each string consists of two modules. Figure 7 shows the characteristics of Canadian solar PV module. A classical DC-DC boost converter is used to boost up the voltage of PV array and a DC-DC buck-boost converter is used to charge and discharge the battery/supercapacitor. Table 2 lists the components, their quantities, and ratings. Battery and supercapacitor ratings are calculated while using Equations (11) & (17).

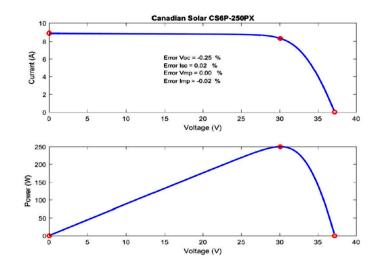


Figure 7. Canadian Solar Module Characteristics.

S.No.	Component	Rating	Quantity
1	PV Module	250 W	20
2	Battery	65 Ah	1
3	Supercapacitor	100 F	1
4	Load	5 kW	1

Table 2. List of Components.

6. Simulation Results and Analysis

The designed HESS based PV system with FHCS. as described above, is simulated while using MATLAB/Simulink simulation environment. This PV system is simulated for 60 s using input irradiance defined for real time data is shown in Figure 8a–c. The input radiation is split into three time slots. The fast transient phase is from 0 to 10 s, linear changing phase is of 10 to 50 s, and a radiation constant phase of 50 to 60 s. The generated PV system power, DC bus power, and output power are shown in Figure 8a–c, respectively. Figure 8b shows DC bus power, voltage, and current variation. Here, the DC bus power is the sum of generated PV power and HESS power.

6.1. Fast Transient Phase Analysis (0 to 10 s)

During the fast-transient phase, the irradiance is frequently changing. The input current changes according to irradiance and the input voltage oscillates between 200 to 300 volts as shown in Figure 8a. The DC bus current has a few oscillations and DC bus voltage has minimal spikes. The DC bus power is constant at 5kW with some oscillations between 0 to 10 s. The output or AC power, AC voltage, and AC current are almost constant, irrespective of radiation change, as shown in Figure 8c. Figure 8d,e show the battery and supercapacitor current and SOC graph. The battery current is zero and the SOC is 70.3% and supercapacitor current and SOC are changing according to irradiance change. The supercapacitor current and SOC are changing from -11 to 13 amp and 24% to 80%, respectively. This clearly indicates that, during the fast transient phase, this algorithm only uses the supercapacitor power to compensate the deficient power on DC bus and saves battery from an unnecessary charging/discharging process.

6.2. Linear Changing Phase Analysis (15 to 50 s)

From 15 to 50 s, the irradiance linearly changes, as shown in Figure 8a. During this phase the input power is changing according to irradiance, but DC bus power and output power are constant. The battery current and SOC changes from 0 to 4.5 amp and 70.35% to 70.15% respectively. The supercapacitor current and SOC do not change in this phase. This algorithm compensates the deficient power on DC bus using battery bank.

6.3. Constant Phase Analysis (10 to 15 and 50 to 60 s)

The phase in which there is no change in irradiance is called constant phase. From 10 to 15 s, the supercapacitor current and SOC changes -10 to 0 amp and approximately 30% to 80%, which indicates that supercapacitor is charging. In this phase, the battery current and SOC is constant. During 50 to 60 s the battery current is changing from 0 to -4 amp approx. and SOC changes 70.25% to 70.35%. In this phase, supercapacitor and battery current are not used, because there is sufficient PV power is available. There is no deficiency of power on the DC bus.

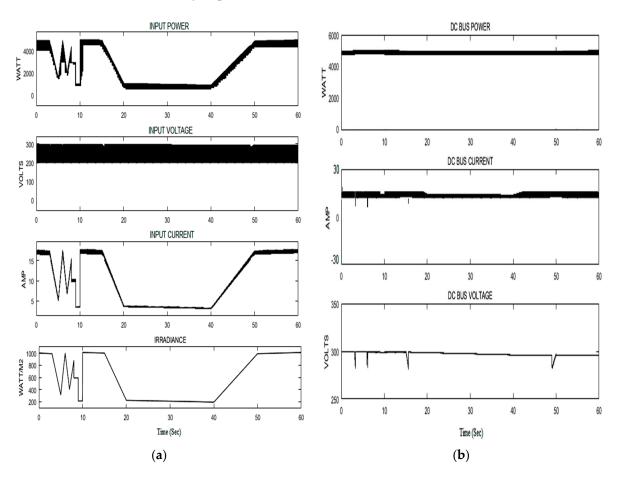


Figure 8. Cont.

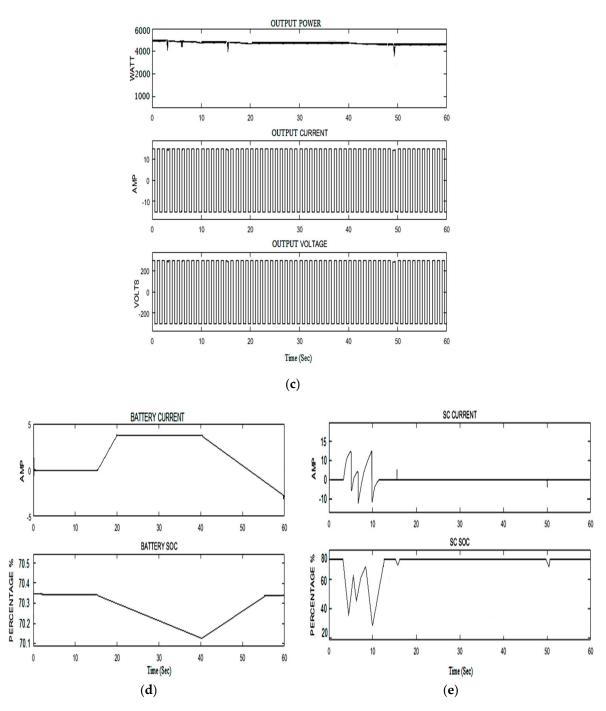


Figure 8. (a) Generated PV Power, Voltage, Current and Input Irradiance; (b) DC bus Power, Current and Voltage; (c) Output AC Power, Current and Voltage; (d) Battery Current and state of charge (SOC); and, (e) Supercapacitor Current and SOC.

7. Battery Charging/Discharging Cycle and its Effects on Battery Life Span

7.1. Battery Charging/Discharging Cycle

Frequent or irregular battery charging/discharging process affects the battery performance, degrades the storage capacity and also leads to the loss of energy [31,32]. For a prolonged life span, the battery needs to be charged with a constant current for specific time duration. The generated solar power is radiation dependent and variable. It varies according to weather conditions and it damages the battery by inducing dynamic charging/discharging stress, and thus reduces the life span.

The amount of true cycle capacity loss is directly proportional to the square root of charge-discharge cycle numbers and can be expressed, as given below in Equation 18 [33].

Amount of Capacity Loss =
$$kc * N^{1/2}$$
 (18)

where, kc is reaction constant.

The battery life span can be enhanced by reducing charge-discharge cycle numbers. The proposed system reduces the dynamic stress on battery using supercapacitor as secondary energy storage.

The supercapacitor prevents the battery from unnecessary charge-discharge operations and compensates the deficient power during fast transient or sudden radiation change condition. In this work, the performance of the proposed HESS based PV system is investigated while using 10 s input transient. The output power during this time span is constant and voltage is found to be stable. The SOC and current of supercapacitor change, but battery SOC and current are constant during this transient. This HESS based PV system and control algorithm prevents the battery due to worst effect of several numbers of these fast transients during the whole day.

7.2. Battery Life Span Analysis

Solar transients affect the battery operation and decrease its life span. One-year data of Sultanpur, India (latitude [N] 26.29 longitude [E] 82.08) is analyzed to investigate the number of fast and linear transient's pattern of solar radiation. Figure 9 shows an example of identified fast or linear transients. The discrimination of fast and linear transient is decided while using Equation (19) below.

$$Transient = \begin{cases} if, \ \Delta Ir \le 50/minthen \ Fast \ Transient \\ Otherwise \ Linear \ Transient \end{cases}$$
 (19)

Table 3 provides the average numbers of fast and linear transients that were obtained for each month. The maximum number of fast and linear transients are encountered in the months of August (389) and February (168), respectively. The total number of charge-discharge cycles used without and with HESS based PV system are 3701 and 1079, respectively. From Table 4, it is evident that the total number of cycles saved is 2622 during whole year with maximum being in the month of July i.e. Hence, HESS based PV system saved 70.84% cycles as compared to no HESS based PV system case.

Table 3. Transient Analysis of Sultanpur, India for 2016 (Latitude [N] 26.29 and Longitude [E] 82.08
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			No of Averag	e Transients/ M	onth			
N F 4	No of Average Transients		Battery Charging/Discharging Cycles without HESS			Battery Charging/Discharging Cycles with HESS		
Month	Fast Transients	Linear Transients	During Fast Transients	During Linear Transients	Total Cycle	During Fast Transients	During Linear Transients	Total Cycle
January	247	101	247	101	348	0	101	101
February	252	168	252	168	420	0	168	168
March	124	87	124	87	211	0	87	87
April	107	61	107	61	168	0	61	61
May	92	51	92	51	143	0	51	51
June	88	43	88	43	131	0	43	43
July	521	57	521	57	578	0	57	57
August	389	116	389	116	505	0	116	116
September	357	102	357	102	459	0	102	102
October	133	117	133	117	250	0	117	117
November	66	59	66	59	125	0	59	59
December	246	117	246	117	363	0	117	117
	Total	Number of Cy	cles		3701			1079

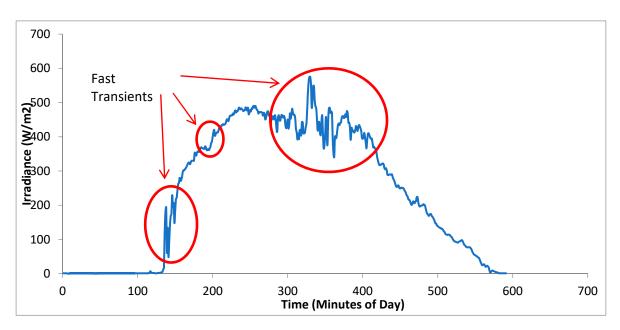


Figure 9. Typical Example of One Day Solar Radiation for Identification of Fast Transients Occurs on Latitude [N] 26.29 and Longitude [E] 82.08 (Sultanpur, India) Location.

Month	Number of Cycles Saved	Cycles Saved (%)		
January	247	70.9%		
February	252	60.0%		
March	124	58.7%		
April	107	63.6%		
May	92	64.3%		
June	88	67.1%		
July	521	90.1%		
August	389	77.0%		
September	357	77.7%		
October	133	53.2%		
November	66	52.8%		
December	246	67.7%		
Total	2622	70.84%		

Table 4. Average Cycles Saved Analysis.

8. Conclusions

In this work, a HESS based stand-alone PV system and a FHCS is developed for domestic rural applications. The HESS is composed of battery and supercapacitor. The performance of the system is investigated under fast transient and linearly changing radiation conditions. Simulation studies of the proposed FHCS based stand-alone PV system are carried out while using real data collected in Sultanpur, India (Latitude [N] 26.29 and Longitude [E] 82.08). The output power and voltage are found stable under both conditions. The charging-discharging stress on battery is also reduced, which enhances the battery life span and reduces the maintenance cost of the system. In contrast with other control strategies for HESS based stand-alone PV system, FHCS is more reliable, yet a simple and effective solution. As future work, the efficacy of the proposed FHCS strategy can be further investigated by implementing it on a real stand-alone PV system or a test bed with relevant hardware.

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References

- 1. Almeshqab, F.; Ustun, T.S. Lessons learned from rural electrification initiatives in developing countries: Insights for technical, social, financial and public policy aspects. *Renew. Sustain. Energy Rev.* **2019**, 102, 35–53. [CrossRef]
- 2. Hubble, A.H.; Ustun, T.S. Composition, placement, and economics of rural microgrids for ensuring sustainable development. *Sustain. Energy Grids Networks* **2018**, *13*, 1–18. [CrossRef]
- 3. Ustun, T.S.; Nakamura, Y.; Hashimoto, J.; Otani, K. Performance analysis of PV panels based on different technologies after two years of outdoor exposure in Fukushima, Japan. *Renew. Energy* **2019**, *136*, 159–178. [CrossRef]
- 4. Bruno, S.; Dellino, G.; La Scala, M.; Meloni, C. A Microforecasting Module for Energy Management in Residential and Tertiary Buildings. *Energies* **2019**, *12*, 1006. [CrossRef]
- 5. Dellino, G.; Laudadio, T.; Mari, R.; Mastronardi, N.; Meloni, C.; Vergura, S. Energy production forecasting in a PV plant using transfer function models. In Proceedings of the 2015 IEEE 15th International Conference on Environment and Electrical Engineering (EEEIC), Rome, Italy, 10–13 June 2015; pp. 1379–1383.
- 6. Ju, C.; Wang, P.; Goel, L.; Xu, Y. A Two-Layer Energy Management System for Microgrids With Hybrid Energy Storage Considering Degradation Costs. *IEEE Trans. Smart Grid* **2018**, *9*, 6047–6057. [CrossRef]
- 7. Kan, S.Y.; Verwaal, M.; Broekhuizen, H. The use of battery–capacitor combinations in photovoltaic powered products. *J. Power Sources* **2006**, *162*, 971–974. [CrossRef]
- 8. Nadeem, F.; Hussain, S.M.S.; Tiwari, P.K.; Goswami, A.K.; Ustun, T.S. Comparative Review of Energy Storage Systems, Their Roles, and Impacts on Future Power Systems. *IEEE Access* **2019**, *7*, 4555–4585. [CrossRef]
- 9. Baisden, A.; Emadi, A. ADVISOR-Based Model of a Battery and an Ultra-Capacitor Energy Source for Hybrid Electric Vehicles. *IEEE Trans. Veh. Technol.* **2004**, *53*, 199–205. [CrossRef]
- 10. Dougal, R.A.; Liu, S.; White, R.E. Power and life extension of battery ultracapacitor hybrids. *IEEE Trans. Compon. Package Technol.* **2002**, *25*, 120–131. [CrossRef]
- 11. Jing, W.; Lai, C.H.; Wong, S.H.W.; Wong, M.L.D.; Wong, W.; Wong, M.L.D. Battery-supercapacitor hybrid energy storage system in standalone DC microgrids: A review. *IET Renew. Power Gener.* **2017**, 11, 461–469. [CrossRef]
- 12. Thounthong, P.; Rael, S.; Davat, B. Analysis of Supercapacitor as Second Source Based on Fuel Cell Power Generation. *IEEE Trans. Energy Convers.* **2009**, 24, 247–255. [CrossRef]
- 13. Wang, G.; Ciobotaru, M.; Agelidis, V.G. Power Smoothing of Large Solar PV Plant Using Hybrid Energy Storage. *IEEE Trans. Sustain. Energy* **2014**, *5*, 834–842. [CrossRef]
- 14. Chia, Y.Y.; Lee, L.H.; Shafiabady, N.; Isa, D. A load predictive energy management system for supercapacitor-battery hybrid energy storage system in solar application using the Support Vector Machine. *Appl. Energy* **2015**, *137*, 588–602. [CrossRef]
- 15. Pan, T.L.; Wan, H.-S.; Ji, Z.-C. Stand-alone wind power system with battery/ supercapacitor hybrid energy storage. *Int. J. Sustain. Eng.* **2014**, *7*, 103–110. [CrossRef]
- 16. Song, Y.D.; Cao, Q.; Du, X.; Karimi, H.R. Control Strategy Based on Wavelet Transform and Neural Network for Hybrid Power System. *J. Appl. Math.* **2013**, 2013, 1–8. [CrossRef]
- 17. Gee, A.M.; Robinson, F.V.P.; Dunn, R.W. Analysis of Battery Lifetime Extension in a Small-Scale Wind-Energy System Using Supercapacitors. *IEEE Trans. Energy Convers.* **2013**, *28*, 24–33. [CrossRef]
- 18. Chong, L.W.; Wong, Y.W.; Rajkumar, R.K.; Isa, D. An optimal control strategy for standalone PV system with Battery-Supercapacitor Hybrid Energy Storage System. *J. Power Sources* **2016**, *331*, 553–565. [CrossRef]
- 19. Wieczorek, M.; Lewandowski, M. A mathematical representation of an energy management strategy for hybrid energy storage system in electric vehicle and real time optimization using a genetic algorithm. *Appl. Energy* **2017**, *192*, 222–233. [CrossRef]
- 20. Wang, X.; Yu, D.; Le Blond, S.; Zhao, Z.; Wilson, P. A novel controller of a battery-supercapacitor hybrid energy storage system for domestic applications. *Energy Build.* **2017**, *141*, 167–174. [CrossRef]

21. Thounthong, P. Model Based-Energy Control of a Solar Power Plant with a Supercapacitor for Grid-Independent Applications. *IEEE Trans. Energy Convers.* **2011**, *26*, 1210–1218. [CrossRef]

- 22. Brunelli, D.; Moser, C.; Thiele, L.; Benini, L. Design of a Solar-Harvesting Circuit for Batteryless Embedded Systems. *IEEE Trans. Circuits Syst. I Regul. Pap.* **2009**, *56*, 2519–2528. [CrossRef]
- 23. Chong, L.W.; Wong, Y.W.; Rajkumar, R.K.; Rajkumar, R.K.; Isa, D. Hybrid energy storage systems and control strategies for stand-alone renewable energy power systems. *Renew. Sustain. Energy Rev.* **2016**, *66*, 174–189. [CrossRef]
- 24. Brka, A.; Kothapalli, G.; Al-Abdeli, Y.M. Predictive power management strategies for stand-alone hydrogen systems: Lab-scale validation. *Int. J. Hydrog. Energy* **2015**, *40*, 9907–9916. [CrossRef]
- 25. Garcia-Torres, F.; Bordons, C. Optimal Economical Schedule of Hydrogen-Based Microgrids With Hybrid Storage Using Model Predictive Control. *IEEE Trans. Ind. Electron.* **2015**, *62*, 5195–5207. [CrossRef]
- 26. Kuperman, A.; Aharon, I. Battery-ultracapacitor hybrids for pulsed current loads: A review. *Renew. Sustain. Energy Rev.* **2011**, *15*, 981–992. [CrossRef]
- 27. Ali Akcayol, M. Application of adaptive neuro-fuzzy controller for SRM. *Adv. Eng. Softw.* **2004**, *35*, 129–137. [CrossRef]
- 28. Zhang, Y.; Jiang, Z.; Yu, X. Control strategies for Battery/Supercapacitor Hybrid Energy Storage Systems. In Proceedings of the 2008 IEEE Energy 2030 Conference, Atlanta, GA, USA, 17–18 November 2008; pp. 5–10.
- 29. Kollimalla, S.K.; Mishra, M.K.; Narasamma, N.L. Design and Analysis of Novel Control Strategy for Battery and Supercapacitor Storage System. *IEEE Trans. Sustain. Energy* **2014**, *5*, 1137–1144. [CrossRef]
- 30. Mendis, N.; Muttaqi, K.M.; Perera, S. Active power management of a super capacitor-battery hybrid energy storage system for standalone operation of DFIG based wind turbines. In Proceedings of the 2012 IEEE Industry Applications Society Annual Meeting, Las Vegas, NV, USA, 7–11 October 2012; pp. 1–8.
- 31. Lei, Y.; Zang, C.; Gao, Y.; Li, T. Charging optimization of Lithium-ion Batteries Based on Capacity Degradation Speed and Energy Loss. *Energy Procedia* **2018**, *152*, 544–549. [CrossRef]
- 32. Serhan, H.A.; Ahmed, E.M. Effect of the different charging techniques on battery life-time: Review. In Proceedings of the 2018 International Conference on Innovative Trends in Computer Engineering (ITCE), Aswan, Egypt, 19–21 February 2018.
- 33. Yoshida, H.; Imamura, N.; Inoue, T.; Takeda, K.; Naito, H. Verification of Life Estimation Model for Space Lithium-Ion Cells. *Electrochemistry* **2010**, *78*, 482–488. [CrossRef]



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