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Effectiveness of Two Different Hydrophobic Topcoats for Increasing of Durability of Exterior Coating Systems on Oak Wood

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Abstract: A top hydrophobic layer can increase the durability of exterior coatings applied on wood. Two hydrophobic topcoats - synthetics and waterborne acrylate resin with wax additives, were tested as top layers on twenty-four different coating systems applied on oak wood in this experiment. Artificial accelerated weathering lasted for six weeks. Changes of color, gloss, surface wetting were evaluated, and microscopic analyses of coated surfaces were done during weathering. The results have shown that a top hydrophobic layer increases the durability of tested coating systems in most cases. However, the effectiveness of the two tested hydrophobic topcoats turned out to be different depending on the specific coating systems used.

Keywords: artificial weathering; durability; exterior coatings; hydrophobic topcoat; oak wood

1. Introduction

Wood in outdoor applications is subjected to degradation caused by abiotic and biotic factors [1]. Even without ground contact (class 3 by EN 350 [2]), the rapid degradation of surface layers caused by the interaction of water and solar radiation takes place [3]. Wood with lower natural durability is more susceptible to biological attack—mainly by wood-destroying fungi and insects [1]. A frequently used option of wood protection against the above-mentioned damage is the application of coating systems [4,5].

Another possibility is the use of hydrophobic coatings or wood hydrophobization itself [6–8]. The hydrophobic compounds generally decrease the amount of absorbed water, which leads to reduction of wood swelling and shrinkage [6,9]. This limitation of dimensional changes leads to a slower degradation process outdoors [10]. Additionally, hydrophobic coatings prevent wet conditions, which create a very favorable environment for the growth of various wood degrading biological organisms (e.g., diverse fungi, bacteria, and insects) [9]. Common surface hydrophobization methods include, but are not limited to, treatments based on silicone [11–13] and surface impregnation with various waxes, oils, or acrylate coatings [9,14–17]. In other studies, wood surfaces were also treated by heat [18] or plasma [19] to improve water resistance. Through the introduction of nanotechnology, the different hydrophobic treatments are developing at a rapid pace [6,20]. Nanoparticles based on titanium dioxide [21], silica nanoparticles [22] or zinc oxide were applied as hydrophobic treatments to wood. Nevertheless, many of these approaches have a negative environmental impact and cause damage to the ecosystem because of the possibility for hazardous chemicals to leak from the surface [6]. When using nanoparticles in industrial applications, the possible negative consequences must be considered [23].

Hydrophobic coatings themselves are not usually able to ensure sufficient protection of wood surfaces against weathering - they do not protect the underlying wood against solar radiation causing decomposition of lignin and extractives, while their leaching is connected with visual color changes [7,8,24]. Another use of hydrophobic coatings is their application as a topcoat to prevent the synergistic action of solar radiation and water [25,26]. In previous studies [27–29], the efficiency of a top hydrophobic coating to prolong the overall service life of a coating system applied on Norway spruce and Black locust wood was proved.

It would be preferable to use oak wood (*Quercus petraea* L.) in the outdoor applications as an available wood with higher durability against biotic damage (EN 350 [2]). Without surface protection, however, it rapidly changes its exterior color [30] and the leaching of extractives occurs, which can aesthetically damage other parts of the construction (balcony, façade, terrace, etc.). The efficiency of several coating systems is reduced on oak wood [31] due to its complex morphological structure of with opened vessels and specific tannins content [32]. A hydrophobic layer applied as a separate coating was characterized by lower efficiency than a multilayered oil-based coating system [8]. From these reasons, it is necessary to find a long-lasting coating system on this wood species in outdoor applications.

The objective of this study is to evaluate the efficiency of transparent and semi-transparent coating systems applied on oak wood and possible enhancement of their durability by application of top hydrophobic layers. The performance of different coating systems is evaluated via measurements of color, gloss and surface wettability changes during artificial weathering and via confocal laser scanning microscopy.

2. Materials and Methods

2.1. Wood Material

The experiment was conducted using oak wood (*Quercus petraea* L.) with mean density of $\rho_0 = 705 \text{ kg/m}^3$ harvested in the Czech Republic. The samples in dimensions of 40 mm × 20 mm × 150 mm (T × R × L) were sanded with a grain size of 120 in a longitudinal direction and visually sorted. Prepared samples were conditioned in laboratory conditions ($20 \pm 2 \text{ }^\circ\text{C}$ and 65% RH) to achieve an equilibrium moisture content of 12% before application of coatings and subsequently before each measurement.

2.2. Coating Application

The oak wood samples were treated with oil-based (OL), acrylate-based waterborne (AC), alkyd-based resins (AL) and other synthetic coatings dissolved in organic compounds (SL) according to producer recommendations. Their specification obtained from commercial providers is listed in Table 1. The coated samples were subsequently treated with two different transparent top hydrophobic coatings (b,c), which were applied by brush according to a recommendation from a producer, the remaining samples were left without hydrophobic treatment for a comparison (a)—see Table 2. The cross ends of samples were sealed using silicon to prevent additional water uptake. The initial properties of prepared coating systems are given in Table 3.

Table 1. Specification of applied transparent and semi-transparent coatings.

Sign	Specification	Polymer Base	Type of Coating	Number of Layers	Spreading Rate (g/m ²)
OL-1	Linseed oil	OIL	T	2	100
OL-2	Oil water emulsion based on modified linseed oil	OIL	T	2	100
OL-3	Based on vegetable oils and fatty acids, with carnauba and candelilla waxes, natural resins, essential oils	OIL	T	2	80
OL-4	Waterborne wood oil with fungicides (BIT * and IPBC **)	OIL	T	2	80
OL-5	Natural oils (linseed, sunflower, rapeseed) with metal oxides pigments and titanium dioxide	OIL	T	2	100
OL-6	Oil with nano UV-absorbers and plant essential oils	OIL	T	2	80
OL-7	Oil with fungicides (BIT and IPBC)	OIL	T	2	80
OL-8	Thin oil-based layer with micronized pigments (TiO ₂) and fungicides (propiconazole < 1%)	OIL	S	2	100
OL-9	Thin oil-based layer slightly pigmented with Fe ₂ O ₃ and fungicides (propiconazole < 1%)	OIL	S	2	100
OL-10	Penetrating oil-based with pigments and terpineol (<2.5%)	OIL	S	2	100
AC-1	Acrylate copolymer in water dispersion, propiconazole and IPBC + Modified linseed oil	ACRYLATE + OIL	T	1 + 2	100 + 100
AC-2	Waterborne medium-solid-glaze with UV blocker, biocides-free fungicides	ACRYLATE	T	2	100
AC-3	Waterborne copolymer dispersion with hydrophobic waxes, UV filters and metal oxides	ACRYLATE	T	2	100
AL-1	Alkyd waterborne stain with fungicides (IPBC 0.4%) and UV-stabilizers (benzotriazoles < 0.8%)	ALKYD	T	2	100
AL-2	Waterborne emulsion of modified linseed oil with biocides and metal oxides + Alkyd waterborne stain with fungicides (IPBC 0.4%) and UV-stabilizers (benzotriazoles < 0.8%)	OIL + ALKYD	T	1 + 1	100 + 100
AL-3	Alkyd stain with UV protective pigments	ALKYD	S	2	100
AL-4	Alkyd medium layer stain in organic solvents with UV absorbers and fungicides	ALKYD	S	2	100
AL-5	Thin film stain based on natural oils and alkyd resins	ALKYD	S	2	100
SL-1	Hybrid polyurethane-alkyd synthetic yacht varnish in organic solvents with butanone oxime as an additive	SYNTHETIC STAIN	T	3	100
SL-2	Synthetic stain in organic solvents with fungicides (IPBC 0.3%) and UV-stabilizers	SYNTHETIC STAIN	T	2	100
SL-3	Thin film synthetic stain in organic solvents with UV protection	SYNTHETIC STAIN	S	2	100
SL-4	Impregnation biocide coating protective against basidiomycetes + Thin film synthetic stain in organic solvents with UV protection	SYNTHETIC STAIN	S	1 + 2	100 + 100
SL-5	Synthetic stain in organic solvents without aromatics and with fungicides (0.3% IPBC)	SYNTHETIC STAIN	S	2	100
SL-6	Synthetic stain in organic solvents without aromatics and with fungicides (0.3% IPBC) + Synthetic stain with fungicides (IPBC 0.3%) and UV-stabilizers	SYNTHETIC STAIN	S	1 + 1	100 + 100

Note: SL-2 was both tested as a top hydrophobic layer (b—see Table 2) and also as coating system; Type of coating: transparent (T) and semi-transparent (S) * BIT stands for Benzisothiazol-3(2h)-one; ** IPBC stands for 3-iodo-2-propynyl-butyl carbamate.

Table 2. Specification of applied hydrophobic topcoats.

Sign	Topcoat Specification	Polymer Base	Transparency (T = Transparent)	Number of Layers	Spreading Rate (g/m ²)
a	Without hydrophobic treatment	—	—	—	—
b	Synthetic stain with fungicides (IPBC 0.3%) and UV-stabilizers	SYNTHETIC STAIN	T	1	100
c	Colorless waterborne protection containing nano-sized polyvalent metal AsS-chelate complex and waxes as hydrophobic polymers, 0.1%–0.2% IPBC	ACRYLATE	T	1	100

Table 3. Mean values of initial color (L^* , a^* , b^* - see Section 2.4.), gloss (see Section 2.5.) and surface wettability (see Section 2.6.) of applied coating systems on oak wood.

Sign	Coating without Hydrophobic Topcoat (a)					Hydrophobic Synthetic Topcoat (b)					Hydrophobic Water-solvent Topcoat (c)				
	L_0^*	a_0^*	b_0^*	G_0^*	CA_0^*	L_0^*	a_0^*	b_0^*	G_0^*	CA_0^*	L_0^*	a_0^*	b_0^*	G_0^*	CA_0^*
OL-1	51.7	14.6	29.6	31.1	102.3	57.6	12.2	31.1	24.3	109.9	59.0	11.0	30.8	44.8	99.3
OL-2	49.6	11.4	26.6	2.5	99.5	58.6	9.8	28.7	5.2	111.5	60.5	8.6	25.5	4.3	97.1
OL-3	58.1	11.8	29.3	7.0	107.9	58.2	11.4	29.3	4.1	111.5	57.0	10.4	28.4	23.7	107.0
OL-4	54.7	12.6	29.1	1.8	116.2	55.6	10.7	29.0	3.6	112.8	61.5	10.2	28.5	3.5	99.4
OL-5	50.4	13.2	30.4	4.3	101.3	47.6	14.4	30.2	7.1	111.8	52.0	13.8	33.1	17.5	96.7
OL-6	63.2	9.0	20.6	19.6	99.9	60.5	8.9	18.4	24.4	110.0	57.1	8.7	18.8	18.9	97.6
OL-7	54.7	12.8	30.0	1.5	120.0	54.7	13.2	30.9	4.1	112.9	53.4	12.7	29.1	6.9	104.1
OL-8	58.7	8.6	16.9	9.6	103.9	60.8	8.3	19.7	13.6	106.7	55.7	8.4	16.7	17.7	88.4
OL-9	43.6	14.5	24.7	12.7	102.9	44.6	14.2	26.9	13.3	106.7	52.3	14.6	35.3	29.2	92.9
OL-10	48.7	13.3	27.1	4.3	100.8	55.8	11.5	29.9	8.5	106.6	56.3	11.9	31.0	5.1	96.7
AC-1	55.6	8.6	22.9	4.1	114.3	52.2	9.0	22.7	5.7	96.1	50.2	8.3	20.5	4.1	94.0
AC-2	65.3	6.1	22.5	12.1	90.9	67.8	6.7	26.0	9.9	116.8	61.0	6.5	22.0	18.0	84.7
AC-3	49.8	10.0	27.5	9.7	90.9	53.5	10.7	30.6	5.8	108.7	51.8	10.1	28.9	13.4	84.7
AL-1	58.4	9.7	25.9	4.8	100.0	50.5	10.0	24.8	11.8	109.5	50.8	10.5	25.4	11.5	103.1
AL-2	49.4	11.5	26.7	4.6	103.1	52.4	11.8	29.6	7.8	111.3	53.7	11.2	29.5	8.3	103.1
AL-3	51.8	20.6	39.8	9.2	90.4	49.5	21.0	38.9	21.5	105.9	50.2	18.6	38.4	28.4	89.4
AL-4	52.6	18.1	36.2	7.0	98.6	55.6	17.8	40.9	18.3	112.8	50.5	17.1	34.5	26.4	92.4
AL-5	55.1	13.8	35.0	4.5	110.2	57.7	16.5	40.7	5.1	116.0	54.3	17.7	40.3	4.2	103.0
SL-1	55.4	11.3	28.0	25.9	103.1	56.2	12.0	30.5	20.7	116.7	53.9	12.4	29.3	19.2	90.5
SL-2	58.0	9.7	28.3	9.6	106.8	60.7	9.6	29.7	13.0	110.8	59.6	10.9	30.4	13.1	95.5
SL-3	50.6	17.2	36.0	9.2	98.6	47.6	15.4	32.2	12.1	111.8	50.7	17.0	36.1	12.5	92.1
SL-4	48.3	14.7	30.1	3.4	105.2	51.7	15.6	34.1	8.4	88.7	46.4	14.7	30.0	9.4	109.6
SL-5	52.2	14.3	34.8	16.4	104.4	46.4	13.9	28.5	11.1	110.8	50.4	14.2	32.4	22.8	94.7
SL-6	44.8	13.6	27.0	13.5	111.4	46.2	15.4	28.7	15.0	109.0	46.7	14.2	29.0	14.6	95.4

2.3. Artificial Weathering (AW)

Artificial weathering was performed in UV-chamber QUV (Q-Lab, Cleveland, OH, USA) on the basis of modified EN 927-6 [33] with the test parameters given in Table 4. During the week cycle of irradiation and spraying, the samples were transferred to a conditioning chamber Discovery My DM340 (ACS, Massa Martana, Italy) and exposed to three cycles lasting 2 h of temperature changes from -25 to $+80$ °C (with 25% RH). The total weathering time consisted of 6 cycles - 1008 h of weathering in UV chamber and 36 h of temperature cycling. The alternation of UV radiation, spray, and low temperature cycles, which leads to more accurate simulation of exterior conditions in Europe, was also used in a study by Van den Bulcke [34] and Pánek [8].

Table 4. One cycle of artificial weathering.

Rank	Phase	Device	Duration	Parameters	Repetition
1.	Condensation	UV-chamber	24 h	$T = 45 \pm 3$ °C, Water-spray (off), UV (off)	1×
2.	UV Irradiance	UV-chamber	2.5 h	$T = 65 \pm 3$ °C, Water-spray (off), UV Irradiance 1.10 W/m^2 at 340 nm	48×
	Water-spray	UV-chamber	0.5 h	$T = 20 \pm 1$ °C, Water-spray (on), UV (off)	
3.	Temperature Cycling	Conditioning chamber	1 h	$T = -25$ °C	3×
	Temperature Cycling	Conditioning chamber	1 h	$T = +80$ °C (RH = 25 %).	

2.4. Color Analysis

The color parameters [35] (CIE 1986) of the test specimens were measured after 1, 3 and 6 weeks of AW using Spectrophotometer CM-600d (Konica Minolta, Osaka, Japan). The device was set to an observation angle of 10° , d/8 geometry and D65 light source, and the SCI method (specular component included) was used. Six measurements per sample were carried out for each weathering

time. Color changes evaluations were done in CIE $L^*a^*b^*$ color space on the basis of L^* , a^* , and b^* color coordinates, where:

L^* is lightness from 0 (black) to 100 (white);

a^* is chromaticity coordinate + (red) or – (green);

b^* is chromaticity coordinate + (yellow) or – (blue).

The relative changes in color (ΔL^* , Δa^* , and Δb^*) between the weathered and the initial state were determined. According to the Euclidean distance, the total color difference ΔE^* (CIE 1986 [8]) was subsequently calculated using Equation (1):

$$\Delta E^* = \sqrt{(\Delta L^*)^2 + (\Delta a^*)^2 + (\Delta b^*)^2}, \quad (1)$$

2.5. Gloss Analysis

Gloss measurements were performed on the basis of EN ISO 2813 [36] using glossmeter MG268-F2 (KSJ, Quanzhou, China). Six measurements at a 60° angle per sample after 1, 3, and 6 weeks of AW were done to evaluate gloss changes.

2.6. Surface Wettability Analysis

The performance of different hydrophobic layers on oak wood surface wettability was investigated. The water contact angle on oak wood tangential surfaces was measured using a goniometer Krüss DSA 30E (Krüss, Hamburg, Germany). The sessile drop method was used to compare the wettability of different surface treatments during artificial weathering. Ten measurements per sample were performed after 1, 3, and 6 weeks of weathering with distilled water drops with a dosing volume of 5 μ L. The value of contact angle was recorded in 5 sec after drop deposition on the surface as in other studies [37–39]. The phenomena of spreading and absorption of water drops on the oak wood surface was investigated via variations of the weathering time, coating system and applied hydrophobic layer.

2.7. Macroscopic and Microscopic Analysis

Surfaces were regularly scanned using Canon 2520 MFP scanner with 300 DPI resolution (Canon, Tokyo, Japan) to evaluate degradation of tested coating systems. Microscopic structural changes of coatings and wood surfaces were studied using confocal laser scanning microscope Lext Ols 4100 (Olympus, Tokyo, Japan) with 108-fold magnification.

2.8. Statistical Evaluation

Statistical analyses were performed in MS Excel (Microsoft, Redmond, WA, USA) and Statistica (StatSoft, Palo Alto, CA, USA) using mean values, scatter plots with mean values and ANOVA (analysis of variance) with significance level $\alpha = 0.05$.

3. Results and Discussion

The changes of surface properties of tested coating systems during AW exposure were evaluated with respect to the type of polymer base (oil, acrylate, alkyd, other synthetic—Table 1) and hydrophobic topcoat (acrylate waterborne and synthetic—Table 2)—see Figure 1.

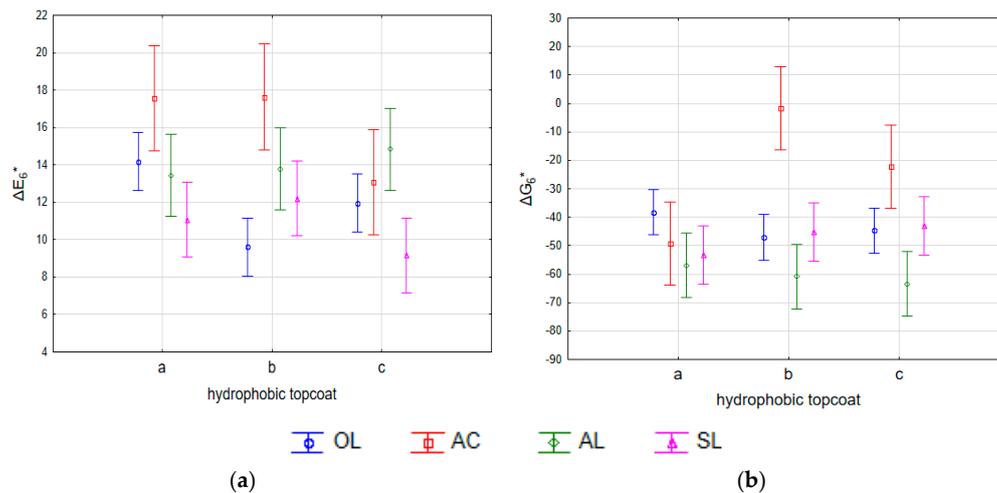


Figure 1. Efficiency of hydrophobic layer on the color (a) and gloss change (b) after 6 weeks of AW.

3.1. Color and Gloss Evaluation

In statistical analysis the effect of the polymer base type on color and gloss parameters was evaluated as statistically significant ($p = 0.00$). In contrast, the effect of hydrophobic topcoat type on color changes was evaluated as statistically insignificant ($p = 0.07$) and significant for gloss changes ($p = 0.03$). The following graphs show the values of gloss and color changes of individual coating systems with an oil and acrylate polymer base (Figure 2) and an alkyd and synthetic base (Figure 3). Based on the results, the lowest color and gloss changes were generally recorded for oil-based coatings (OL) and other synthetic stains (SL) (Figure 1). The color change $\Delta E^* < 3$, which cannot be recognized by the human eye [40], was only observed after an AW test in the case of oil-based coating systems—OL-8c, OL-6c, OL-8a and OL-10b. The decrease of gloss during AW exposure occurred almost in all tested variants of coating systems, except for OL-3b, OL-4a, OL-7a, AC-2b and AC-2c.

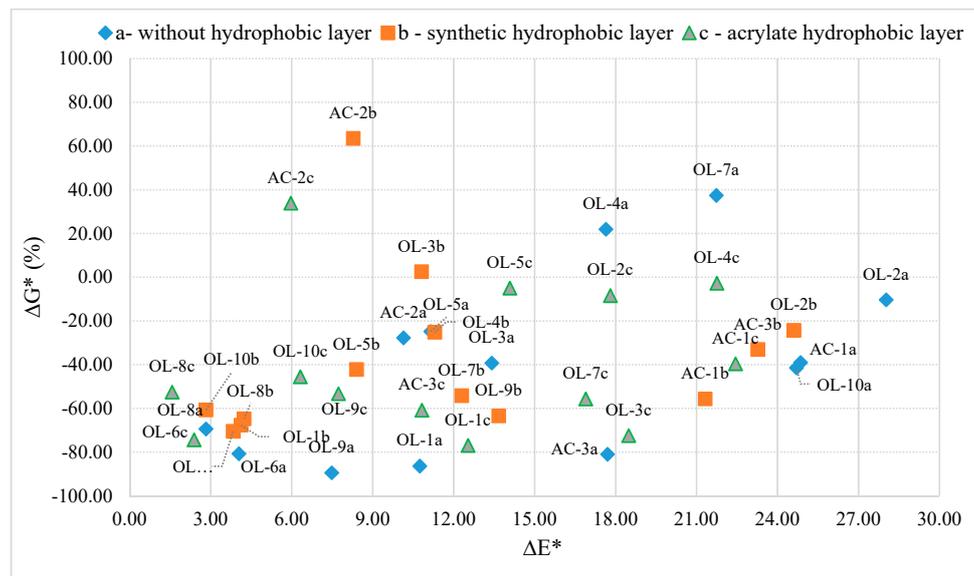


Figure 2. Gloss and color changes of oil-based (OL) and acrylate-based (AC) systems after 6 weeks of AW.

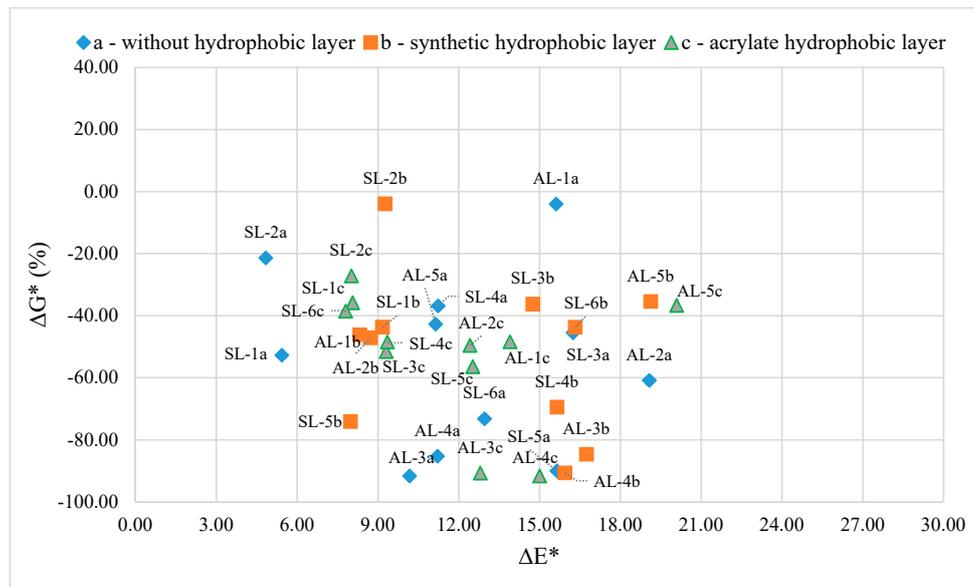


Figure 3. Gloss and color changes of alkyd-based (AL) and other synthetic (SL) coating systems after 6 weeks of AW.

3.2. Surface Wettability Evaluation

The contact angle measurements provide an overview of the functionality of hydrophobic layers during weathering (Figures 4–6). The change of contact angle of tested coating systems during AW exposure was statistically evaluated with respect to the type of polymer base (oil, acrylate, alkyd, other synthetic) and the use of the hydrophobic layer (without hydrophobic treatment, acrylate waterborne and synthetic stain treatment)—see Figure 4. Based on the results, there is a significant loss of contact angle due to AW, mainly when hydrophobic layer was not applied (Figure 4). In the case of coating systems without a hydrophobic layer (a), the AC and SL coatings systems have the lowest contact angle values. The efficiency of hydrophobic topcoats on the surface wettability was observed for both types, but a more pronounced positive effect was observed for the hydrophobic acrylate waterborne topcoat (c) in comparison with a synthetic one (b).

In statistical analysis the effects of polymer base type and hydrophobic topcoat on contact angle values were evaluated as being statistically significant ($p = 0.00$). The following graphs show the values of contact angle changes of oil-based (OL) and acrylate coating systems (AC) (Figure 5) and alkyd-based (AL) and other synthetic (SL) coating systems (Figure 6). At the same time, the factor of total color change is also observed.

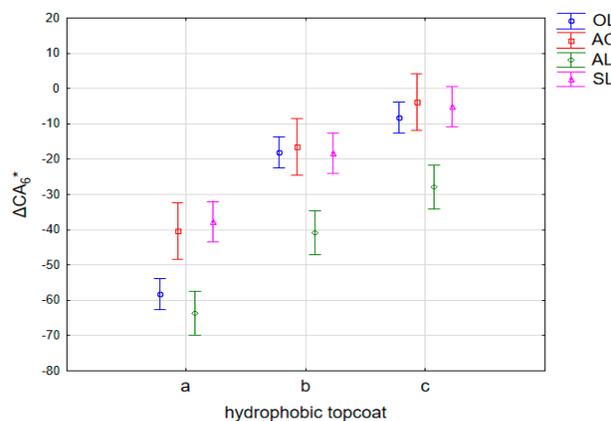


Figure 4. Efficiency of hydrophobic layer on the contact angle change after 6 weeks of AW.

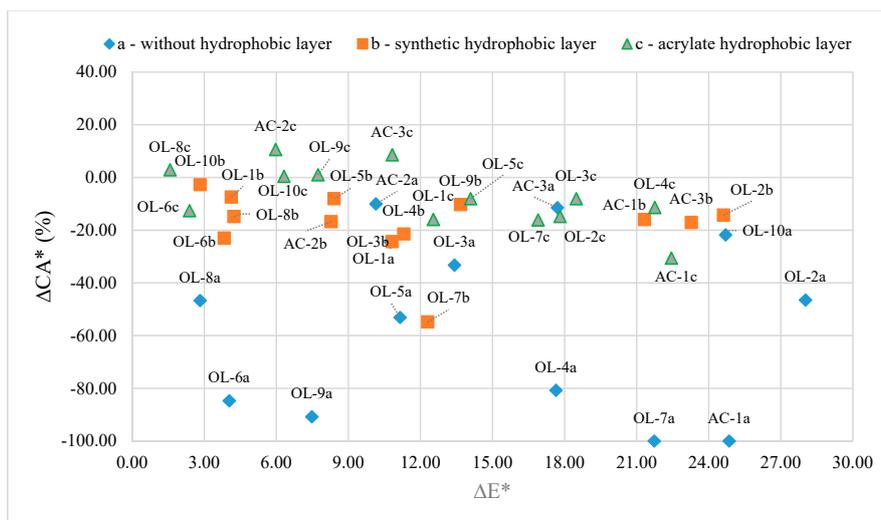


Figure 5. Contact angle change of oil-based (OL) and acrylate-based (AC) coating systems after 6 weeks of AW.

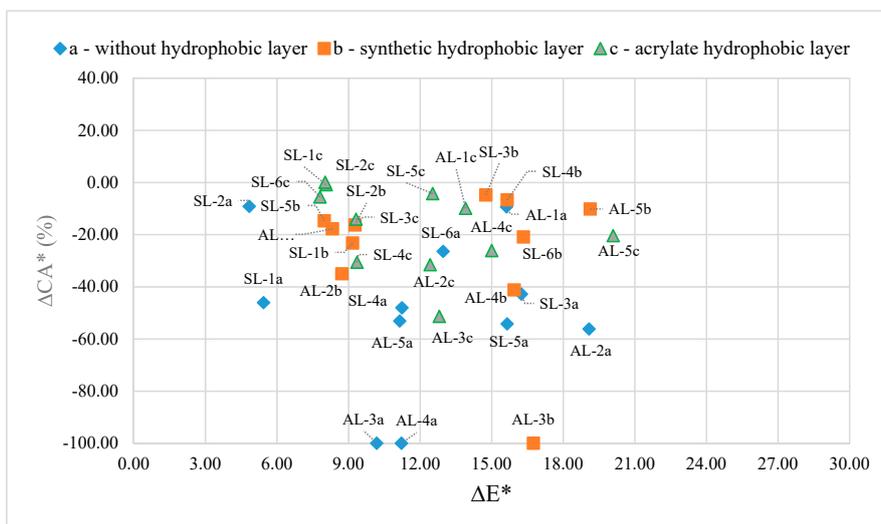


Figure 6. Contact angle change of alkyd-based (AL) and other synthetic (SL) coating systems after 6 weeks of AW.

The only coating systems that were not noted for a decrease of the contact angle but instead for a slight increase after 6 weeks of AW were coating systems AC-2c, AD-3c, OL-8c, OL-9c, OL-10c, SL-1c a SL-2c. That outcome confirmed the results stated in Figure 4—that an acrylate waterborne hydrophobic topcoat had the most positive effect on the wettability of tested surfaces. The rest of the tested coating systems were noted for having a slight or more pronounced decrease of contact angle values after 6 weeks of AW. Full surface wettability (100% decrease of initial value) was determined for some coating systems without a hydrophobic topcoat and alkyd-based (AL) coating system with synthetic hydrophobic layer AL-3b.

3.3. Visual and Microscopic Evaluation

Based on the results presented in Table 5 and Figure 7, it can be seen that the results of color and gloss changes (Figures 2 and 3) or changes in the contact angle (Figures 5 and 6) did not always correspond to visually observed degradation of coating systems. For example, coating systems OL-10b and OL-10c were characterized by a relatively low color change (Figure 2) and minimal decrease of contact angle (Figure 5), but their overall visual degradation was quite pronounced (Table 5 and

Figure 7). If the top layer of coating is degraded, but the penetrated layer remains, the significant visual changes occur, but the contact angle can be unaffected [8,41]. At the same time, it can be stated that coatings with better results of visual evaluation according to Table 5 (e.g. OL-8, OL-9, SL-3, SL-6b) were characterized by a lower decrease of contact angle values ΔCA^* and total color change ΔE^* (except AL-3). For comparison purposes, some selected coating systems were analyzed by confocal laser scanning microscopy before and after an AW test (Figure 8).

Table 5. Degradation of coating systems (based on methodology done by De Windt [42]).

Sign	Without Hydrophobic Topcoat (a)	With Synthetic Hydrophobic Topcoat (b)	With Acrylate Hydrophobic Topcoat (c)
OL-1	10	8	6
OL-2	10	10	10
OL-3	10	10	10
OL-4	10	10	10
OL-5	8	6	4
OL-6	8	4	8
OL-7	10	10	10
OL-8	4	6	4
OL-9	4	4	2
OL-10	10	8	8
AC-1	10	10	10
AC-2	10	8	6
AC-3	8	8	6
AL-1	10	8	10
AL-2	10	8	8
AL-3	2	4	4
AL-4	6	6	6
AL-5	8	8	4
SL-1	8	6	6
SL-2	10	10	8
SL-3	4	4	4
SL-4	8	6	6
SL-5	6	6	2
SL-6	6	2	8

The evaluation was based on the level of degradation: i.e., 0 = none; 2 = small aesthetical changes; 4 = mild (easy to maintain); 6 = moderate (maintainable); 8 = striking (maintenance is difficult); 10 = advanced (maintenance coat cannot remove the defects). De Windt [42].



Figure 7. Visual changes of selected tested coating systems on oak wood. (OL-2a) the same degradation was observed using hydrophobic treatments b and c; (OL-9) positive effect of hydrophobic treatment (c) on color stability of AW samples; (OL-10) partly positive effect of hydrophobic topcoat application b and c; (AL-1) very similar degradation was observed using hydrophobic treatments b and c; (AL-4) positive effect of pigment content increasing durability of alkyd coating (in comparison with transparent (AL-1a); (SL-1) positive effect of application of topcoat b; (SL-6b) positive effect of application of topcoat b.

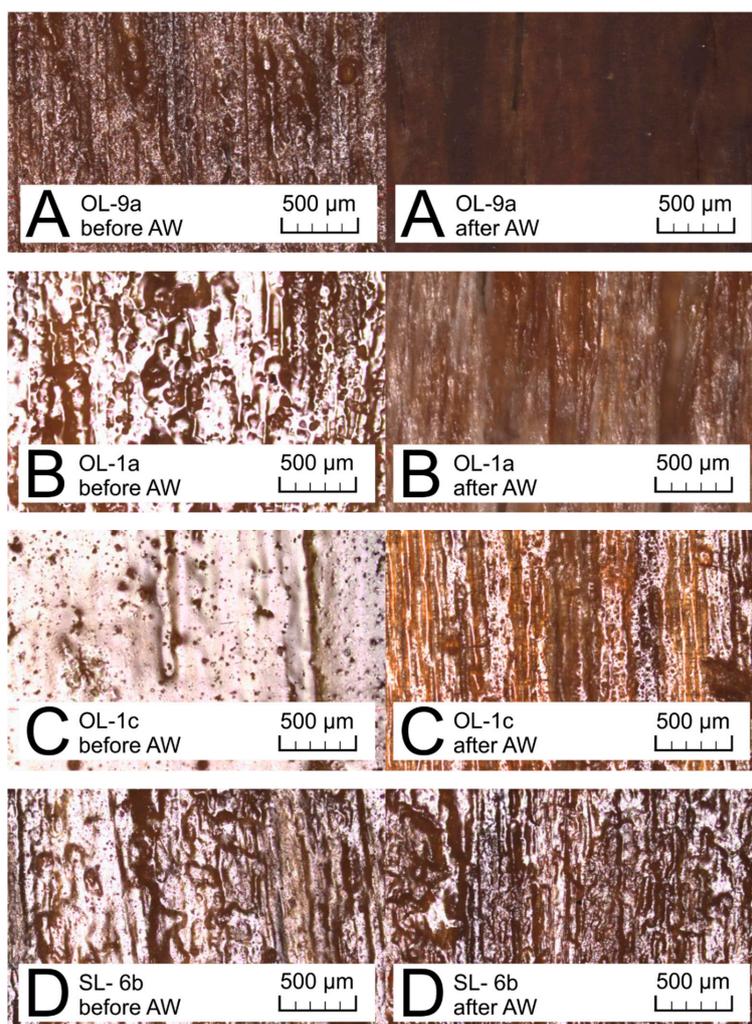


Figure 8. Microscopic changes (using Confocal Laser Scanning Microscopy) of coating surfaces. OL-9a (A), OL-1a (B), OL-1c (C) and SL-6b (D) before (left) and after 6 weeks of AW (right). It is possible to see a loss of gloss and color changes of OL-9a, but the coating layer is not degraded (A); Positive effect of hydrophobic top coat (c) application on OL-1 is visible (B and C); Good durability of SL-6b after AW—only darkening is visible, the surface is relatively unchanged.

3.4. Final Discussion of Results

The results of the experiment in this work confirmed that application of the top hydrophobic layer can extend the overall durability of coating systems on oak wood as well as on other wood species [25,27,29]. However, it is necessary to apply a suitable hydrophobic layer to a specific coating system because the resulting effect differs (Figures 5 and 6). The effect of a specific coating system (polymer base and additive content) on its overall service life was confirmed [42–44]. The choice of a suitable oak wood exterior coating system is crucial (Table 4). The application of the top hydrophobic layer did not significantly improve the properties of less suitable coating systems during exposure (Figures 2–8, Table 5). In the case of oil thin layer systems, the positive effect of pigments on the overall service life and color stability (OL-8 and OL-9 - see Figures 2 and 5) was confirmed, which is consistent with other studies [28,41,42]. However, in the case of penetrating pigmented oil without the top hydrophobic layer OL-10, rapid leaching of coating and loss of functionality occurred. A top hydrophobic layer on alkyd-based coating systems basically had no significant positive effect on the color stability and only a low effect on the increase of the hydrophobicity of tested variants (AL-1 and AL-5). The performance of other tested synthetic coatings (SL) depended on a specific combination

of layers. Only coating system SL-5 with acrylate top hydrophobic layer (c) was characterized by improved functionality, in particular by preserving hydrophobicity after AW (Figure 6). Overall, the topcoat with hydrophobic additives in the acrylate water base (c) appeared to be more appropriate for application on oak wood in comparison with synthetic topcoat (b). From all the tested coating systems, OL-8 and OL-9 oil-based coatings with the use of top hydrophobic layer were shown to be suitable for protection of oak wood in terms of color stability and hydrophobic effect as well as overall durability. However, it is necessary to expect a more pronounced reduction of the gloss parameter [8] and, in the case of OL-9, also a color change (Figure 2). The performance of SL-3, SL-5 with hydrophobic topcoat (c) and SL-6 with hydrophobic topcoat (b) can be positively evaluated from the other tested coatings. In contrast, transparent coating systems have generally not been effective, as their higher vulnerability to degradation in comparison with pigmented ones has been fully manifested [5]. In some cases, their overall service life can be increased by application of a top hydrophobic layer (coatings OL-1, OL-5 and 6, SL-1), which is in line with previous studies on spruce and black locust [27,29]. For the objective determination of coating systems quality after weathering, it is helpful to use the evaluation based on the combination of properties: the overall color and gloss change (Figures 2 and 3) and surface wettability (Figures 5 and 6) followed by a visual evaluation (Table 5, Figure 7).

4. Conclusions

Coated oak wood is relatively quickly subjected to degradation in exterior applications, causing changes in color and gloss and reduced resistance to rainwater. The results of the experiments in this work confirmed that a particular selection of the coating system can both positively and negatively affect the overall service life of oak wood in its exterior. The semi-transparent oil-based coatings were generally more stable in color and retained hydrophobicity in comparison with other variants. However, they were more prone to a decrease of gloss. Subsequent application of the top hydrophobic layer can in the most cases increase the overall durability of the coating system. The topcoat with hydrophobic additives in the acrylate waterborne base appeared to be more appropriate for application on oak wood in comparison with synthetic hydrophobic topcoat. Based on the variants tested, it can be generally recommended to apply the top hydrophobic layer on oil-based and partially acrylate coatings. For alkyd-based systems, the positive effect of an additional hydrophobic layer was minimal. In the case of other tested synthetic stains, the hydrophobic layer only rarely improved the evaluated properties. Although the experiment provided some positive results, oak wood exterior coating systems require further research with the aim of increasing their overall durability, especially for transparent and less pigmented semi-transparent variants, while preserving the natural color and texture of oak wood.

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