



Article

Contamination Particles and Plasma Etching Behavior of Atmospheric Plasma Sprayed Y₂O₃ and YF₃ Coatings under NF₃ Plasma

Je-Boem Song 1,2,+, Jin-Tae Kim 1,+, Seong-Geun Oh 2 and Ju-Young Yun 1,*

- ¹ Materials and Energy Measurement Center, Korea Research Institute of Standards and Science (KRISS), Daejeon 34113, Korea; sjb@kriss.re.kr (J.-B.S.); kimjt@kriss.re.kr (J.-T.K.)
- ² Department of Chemical Engineering, Hanyang University, Seoul 04763, Korea; seongoh@hanyang.ac.kr
- * Correspondence: jyun@kriss.re.kr; Tel.: +82-42-868-5669
- † These authors contributed equally to this study.

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Abstract: Yttrium oxide (Y_2O_3) and yttrium oxyfluoride ($Y_3O_6F_{2.1}$) protective coatings were prepared by an atmospheric plasma spraying technique. The coatings were exposed to a NF₃ plasma. After the NF₃ plasma treatment, the mass loss of the coatings showed that the etching rate of $Y_3O_6F_{2.1}$ was larger than that of the Y_2O_3 . X-ray photoelectron spectroscopy revealed that $Y_3O_6F_{2.1}$ was present in the Y_2O_3 coating, whereas $Y_3O_6F_{2.2}$ was present in the $Y_3O_6F_{2.1}$ coating. Transmission electron microscope analysis conducted on contamination particles generated during the plasma etching showed that both coatings were mainly composed of Y_3F_3 . The contamination particles estimated by in-situ particle monitoring sensor revealed that the $Y_3O_6F_3$ compared with the Y_2O_3 coatings produced 65% fewer contamination particles.

Keywords: yttrium oxide (Y₂O₃); yttrium oxyfluoride (YOF); yttrium fluoride (YF₃); atmospheric plasma spraying (APS); contamination particle; plasma etching; NF₃ plasma

1. Introduction

Plasmas are widely used for etching and cleaning in the semiconductor and display industries. Ceramic parts such as electrodes, shower heads, liners, and focusing rings used in these processes are exposed to the plasma. These parts erode and produce contamination particles, which cause serious problems, such as lowering the yield of mass-production [1–5]. In particular, when the dual frequency coupled plasma is applied, the showerhead in the position facing the wafer is heavily etched in a high flux of plasma [6-10]. Corrosion can be minimized with the use of ceramic coatings, which have outstanding plasma resistance. Yttrium oxide (Y_2O_3) is widely used as a coating material, owing to is low etching rate and low chemical reactivity. Recently, YOF and YF₃ coatings have been reported as a new candidate, which can inhibit chemical reactions with fluorine gases, such as CF4, SF₆, and NF₃. The etching characteristics of fluorocarbon gases, such as CF₄ and C₂F₆, have been widely studied. However, etching with these gases is often accompanied by the formation of an unnecessary fluorocarbon polymer layer; hence, NF₃ gas is used as an alternative to fluorocarbon gases. Another advantage is that NF3 is almost fully dissociated in the discharge, which results in a high etching rate [11–14]. The erosion behaviors of Y₂O₃, YOF, and YF₃ coatings in CF₄/O₂/Ar plasmas have been reported in previous works [15-34]. However, there have been no studies on the corrosion behavior of the yttrium-based materials or contamination particles generated from them in NF3 plasmas. In this study, we examine and compare the etching behavior and the generation of Coatings 2019, 9, 102 2 of 8

contamination particles in an NF₃ plasma from Y₂O₃ and YO_{0.6}F_{2.1} coatings, fabricated by atmospheric plasma spraying (APS).

2. Experimental

The disc-like substrates were made of Al alloy 6061 and had a diameter of 76 mm and thickness of 3 mm. The substrates were then coated with Y_2O_3 and $YO_{0.6}F_{2.1}$ by atmospheric plasma spraying (APS) [23–31], with the use of a plasma spray system (Mettech's Axial III, Northwest Mettech Corp., North Vancouver, BC, Canada), where the Y_2O_3 and YF_3 were in a powder form (99.99%, D50 = 30 μ m, Shin-Etsu, Tokyo, Japan). The sprayed coatings of Y_2O_3 and $YO_{0.6}F_{2.1}$ were respectively 110 and 70 μ m thick. The APS coating was performed as follows; the Ar, N_2 , and H_2 at flow rates were 80, 80, and 20 L/min, respectively, were used to generate a plasma arc and the plasma arc current was 230 A.

Figure 1 shows a schematic diagram of the capacitively coupled plasma system. A specimen was placed in the upper electrode, as shown in Figure 1. The NF3 gas was used for plasma generation and was supplied through a showerhead with a mass flow controller. Magnets were inserted in the upper electrode to enhance the plasma density. A dry pump and turbo pump were used in the vacuum system and the working pressure of the experiment was 26.6 Pa. The power was set to be 13.56 MHz (Sizer Generator, Advanced Energy, Fort Collins, CO, USA), and an impedance matching network (Navigator, Advanced Energy, Fort Collins, CO, USA) was used to deliver the maximum power. The RF power applied to the plasma was 400 W. Before and after the NF3 plasma etching, the surface morphology and composition of the Y_2O_3 and $YO_{0.6}F_{2.1}$ coatings were analyzed by the field-emission scanning electron microscopy (FE-SEM, S-4800, Hitachi, Tokyo, Japan) and X-ray photoelectron spectroscopy (XPS) (Monochromatic Al-K α , AXIS-NOVA, Manchester, UK), respectively. The mass of the specimen was measured before and after the plasma etching test using a XP205 analytical balance (Mettler Toledo, Greifensee, Switzerland). After plasma etching was performed for 10 min, the specimen was taken out and the mass loss was measured. This procedure was repeated until the accumulated plasma exposure time was 60 min.

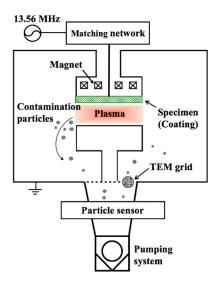


Figure 1. Schematic diagram of capacitively coupled plasma (CCP) etching system.

The contamination particles produced from the Y_2O_3 and $YO_{0.6}F_{2.1}$ coatings were measured in real time according to the NF $_3$ plasma exposure time. A light scattering sensor ISPM (Stiletto, In Situ Particle Monitor, Inficon, Heidiland, Switzerland) was attached to the exhaust line to measure the amount and size of the contamination particles. This system was capable of measuring contamination particles in real time as they passed through the exhaust pipe. The minimum measurable particle size was ~0.2 μ m. The sensor was based on the principles of laser light scattering, and more details of its working principles can be found in previous reports [35,36]. The contamination particles generated

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during the plasma etching were collected on a TEM grid and observed for shape and composition under a transmission electron microscope (TEM, Taitan 300 K, Renton, WA, USA). As shown in Figure 1, the TEM grid was placed at the bottom of the chamber.

3. Results and Discussion

Figure 2 shows FE-SEM images of the surface of Y_2O_3 and $YO_{0.6}F_{2.1}$ coatings before and after exposure to NF₃ plasma; Figure 2a,b for Y_2O_3 and Figure 2c,d for $YO_{0.6}F_{2.1}$. Before NF₃ plasma etching, the surfaces of the Y_2O_3 and $YO_{0.6}F_{2.1}$ coatings had a similar rough surface. After plasma etching, the Y_2O_3 coating showed more cavities than the $YO_{0.6}F_{2.1}$ coating, as denoted in Figure 2b. This result is consistent with a recent report [29]. Figure 3 shows the mass loss of Y_2O_3 and $YO_{0.6}F_{2.1}$ vs. the NF₃ plasma etching time. The $YO_{0.6}F_{2.1}$ coating was etched more than the Y_2O_3 coating. The etch rates of the Y_2O_3 and $YO_{0.6}F_{2.1}$ coatings were ~29 and 117 nm/min/m², respectively. After the plasma exposure of the coatings, the amounts of Y (Yttrium), Y (Oxygen) and Y (Fluorine) were measured by Y analysis. The results are presented in Table 1. Compared to a before etching specimen, the Y_2O_3 coating on the electrode after plasma exposure had less Y0, but more Y1. This result not surprising and is consistent with previous studies [29–31].

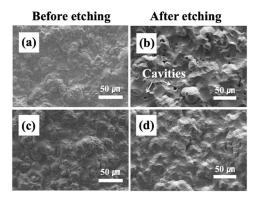


Figure 2. FE-SEM images of the surface of Y₂O₃ and YO_{0.6}F_{2.1} coatings before and after exposure to NF₃ plasma; (a) Y₂O₃ and (c) YO_{0.6}F_{2.1} before etching, (b) Y₂O₃ and (d) YO_{0.6}F_{2.1} after etching.

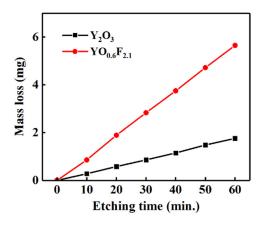


Figure 3. Mass loss owing to NF3 plasma etching: Y2O3 and YO0.6F2.1 coatings.

Table 1. XPS analysis results of Y₂O₃ and YO_{0.6}F_{2.1} coatings before and after exposure to the NF₃ plasma.

Compound	Y2O3 Coating		YO _{0.6} F _{2.1} Coating	
Content (at.%)	Before Etching	After Etching	Before Etching	After Etching
Yttrium (Y3d)	28.3	29.2	26.9	27.3
Oxygen (O1s)	70.3	15.0	16.8	11.8

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Fluorine (F1s)	1.4	55.8	56.3	60.9
		00.0		

Figure 4 shows the XPS spectra for yttrium in Y_2O_3 and $YO_{0.6}F_{2.1}$ before and after the plasma treatment. We assigned dash lines the peaks in the XPS spectra to the cations of $Y_3d_{5/2}$ and $Y_3d_{3/2}$. The two peaks had a difference of 2.05 eV with an intensity ratio of 3:2 in their binding energy, which is consistent with the figure provided by national institute of standards and technology (NIST) [37]. In the case of pristine Y_2O_3 , the $Y_3d_{5/2}$ peak positions were 157.35 and 156 eV, and the $Y_3d_{3/2}$ peak positions were 159.4 and 158.05 eV. When Y_2O_3 was exposed to the NF₃ plasma, XPS analysis revealed binding energies of 158.65 eV for $Y_3d_{5/2}$ and 160.7 eV for $Y_3d_{3/2}$, which indicated binding of yttrium to fluorine and formation of Y–F bonds. Figure 4a consists of three Y–O peaks located at 159.4, 158.05, and 156 eV. As shown in Figure 4c, the peak shifted to higher energy could be attributed to the Y–F bond, which is possibly attributed to the different electronegativity of fluorine and oxygen atoms. When the oxygen atoms around the cations are replaced by fluorine atoms, more electrons transferred to fluorine. Therefore, the electron density around the cation decreases and the binding energy is enhanced [20]. This result indicates that the surface of Y_2O_3 reacted with fluorine radicals and was composed of Y_2O_3 . However, the Y_3O_3 coating showed less change in the composition after the plasma treatment.

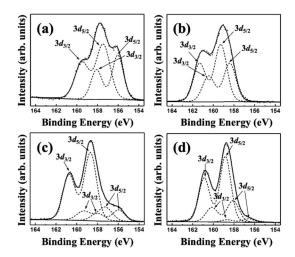


Figure 4. Peak positions of the XPS spectra of the surface; **(a)** Y₂O₃ and **(b)** YO_{0.6}F_{2.1} before etching, **(c)** Y₂O₃ and **(d)** YO_{0.6}F_{2.1} after etching.

Figure 5 shows the real-time concentration of accumulated contamination particles generated from the Y₂O₃ and YO_{0.6}F_{2.1} coatings during the NF₃ plasma treatment of 60 min. The YO_{0.6}F_{2.1} coating produced fewer contamination particles than did the Y₂O₃ coating; the concentration of particles measuring over 0.2 µm from the YO_{0.6}F_{2.1} coating was less than 65% that of the Y₂O₃ coating. Figure 6 shows the distribution of the sum of contamination particles from Figure 5. Most contamination particles had sizes falling in the range of 0.2 to 0.5 µm. The etching rate of YO_{0.6}F_{2.1} was higher than that of Y2O3 in NF3 plasma. However, YO0.6F2.1 produced less contamination particle than Y2O3. This can be explained as follows. The boiling temperature of Y₂O₃ and YF₃ are 4570 and 2500 K, respectively. In addition, the sublimation enthalpies of Y₂O₃ are also higher than that of YF₃. Hence, Y₂O₃ is more stable and more difficult to vaporize than YF₃. Therefore, its sputtering yield by ion bombardment may be lower for the Y₂O₃ than for the YF₃ containing a relatively large amount of oxygen. This is consistent with the result of Reference 17 and 30, where the etching rate differences depend on the bias voltage [17,30]. On the surface of Y₂O₃, YO_xF_y layer and volatile NO_x are formed by the chemical reaction with the fluorine radical. On the other hand, YO_xF_y layer and NO_x can be formed less on the surface of YO_{0.6}F_{2.1} because Y–F bond already exists. Also, the less oxygen on the coating surface, the smaller the chemical reaction. Thus, the Y₂O₃ surface provides a more appropriate environment for the growth of YO₃F_y (or YF₃) contamination particles, and, therefore, more

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contamination particles from Y_2O_3 are generated compared to $YO_{0.6}F_{2.1}$ [28,29]. Furthermore, in the case of $YO_{0.6}F_{2.1}$ surface, physical etching is more likely to occur than chemical etching by fluorine radical. $YO_{0.6}F_{2.1}$ is relatively inadequate to grow YF_3 contamination particle compared to Y_2O_3 .

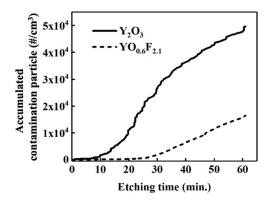


Figure 5. Real-time detection of accumulated contamination particle concentration, over $0.2 \mu m$ size, generated from Y₂O₃ and YO_{0.6}F_{2.1} during the 60 min NF₃ plasma treatment.

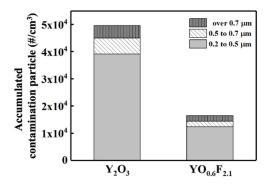
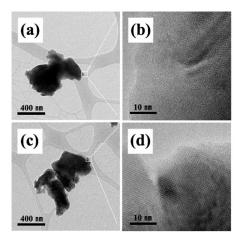


Figure 6. Size distribution of contamination particles, over $0.2 \mu m$ size, generated from Y_2O_3 and $YO_{0.6}F_{2.1}$ during the 60 min NF₃ plasma treatment.

Figure 7 shows TEM images of particles that detached from the coatings during plasma etching. The particles were of various sizes, and the selected particle was approximately 500 nm in size. The particles that fell off the Y_2O_3 and $YO_{0.6}F_{2.1}$ coatings had irregular shapes and crystalline structures. In addition to observing particle shapes by TEM, we used energy dispersive X-ray spectroscopy (EDS) to examine their composition. These results are listed in Table 2. The contamination particles derived from Y_2O_3 and $YO_{0.6}F_{2.1}$ contained almost no oxygen and their chemical composition was most likely YF_x , and rather close to YF_3 , which is consistent with Reference [29–31].



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Figure 7. TEM images of contamination particles; (a), (b) generated from Y_2O_3 and (c), (d) generated in $YO_{0.6}F_{2.1}$.

Table 2. EDS analysis results of contamination particles generated in Y₂O₃ and YO_{0.6}F_{2.1} coatings after exposure to the NF₃ plasma.

Compound Content (wt.%)	Particle Generated in Y2O3 Coating	Particle Generated in YO _{0.6} F _{2.1} Coating
Yttrium	63.5	61.8
Oxygen	0.8	0.6
Fluorine	35.7	37.6

4. Conclusions

We exposed Y_2O_3 and $YO_{0.6}F_{2.1}$ coatings prepared by atmospheric plasma spraying (APS) to NF₃ plasma. Both coatings had rough surfaces in the pristine state, and no differences were observed between the two. When subjected to a NF₃ plasma treatment, the Y_2O_3 coating showed many defects, and cavities formed in the coatings whereas the $YO_{0.6}F_{2.1}$ coating did form any cavities. We estimated the etching rates of Y_2O_3 and $YO_{0.6}F_{2.1}$ coatings from the mass loss to be ~29 and 117 nm/min/m², respectively. During etching, the surface of Y_2O_3 reacted with fluorine radicals to form particles composed of YO_xF_y and YF_x . However, particles from the $YO_{0.6}F_{2.1}$ coating showed almost no change in composition. Fewer contamination particles over 0.2 μ m size were generated for the $YO_{0.6}F_{2.1}$ coating than for the Y_2O_3 coating. The particles produced from both coatings had irregular shapes, mainly consisting of YF_x , with a composition close to YF_3 . These results indicate that the fluorine radicals replaced oxygen at the Y_2O_3 surface such that YF_x particles were formed. The $YO_{0.6}F_{2.1}$ coating did not provide conditions suitable for YF_x particles to grow. This study demonstrates that the $YO_{0.6}F_{2.1}$ coating might be used by the semiconductor industry as a candidate material to reduce contamination particles over 0.2 μ m size.

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Conflicts of Interest: The authors declare no conflict of interest.

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