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Numerical Simulation of Heat Mass Transfer Effects on MHD Flow of Williamson Nanofluid by a Stretching Surface with Thermal Conductivity and Variable Thickness

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Abstract: The current analysis deals with radiative aspects of magnetohydrodynamic boundary layer flow with heat mass transfer features on electrically conductive Williamson nanofluid by a stretching surface. The impact of variable thickness and thermal conductivity characteristics in view of melting heat flow are examined. The mathematical formulation of Williamson nanofluid flow is based on boundary layer theory pioneered by Prandtl. The boundary layer nanofluid flow idea yields a constitutive flow laws of partial differential equations (PDEs) are made dimensionless and then reduce to ordinary nonlinear differential equations (ODEs) versus transformation technique. A built-in numerical algorithm bvp4c in Mathematica software is employed for nonlinear systems computation. Considerable features of dimensionless parameters are reviewed via graphical description. A comparison with another homotopic approach (HAM) as a limiting case and an excellent agreement perceived.

Keywords: numerical solution; analytical solution; MHD; Williamson nanofluid; variable thermal conductivity; variable thickness

1. Introduction

Nanofluid is a kind of liquid that contains small-sized metallic particles having dimensions up to 1–100 nm. Usually, these small metallic particles are made up of graphite, carbon nanotubes, copper, aluminum, oxides, carbide nitrides, and many more. Choi [1] conducted an experimental examination that incorporating these nanoparticles in base liquids results in a significant upsurge in thermal conductivity and heat transfer behavior of base liquid. In recent times, many researchers, engineers, and scientists have utilized the concept of nanofluid to increase the thermal nature and heat transference rate of various base fluids for useful industrial and engineering processes. Buongiorno [2] proposes that this abnormal upsurge in thermal and heat transfer features, namely due to two main reasons, which are the Brownian movement and thermophoretic diffusion in base liquids. An extraordinary research has been undertaken to explore the heat transfer and the effects of thermal radiation by Daungthongsuk and Wongwises [3], Wang and Mujumdar [4,5], Kakac and Pramuanjaroenkij [6]. The results of magnetic field and nonlinear convective Williamson nanofluid in view of the radially stretchable surface with electrical application has been evaluated by Ibrahim and Gamachu [7]. The results of the activation

energy of a mixed convective heat mass transfer effects of Williamson nanofluid, with heat generation and absorption over a stretching cylinder, were deliberated by Ibrahim and Negera [8,9]. Yusuf et al. [10] analyzed the influence of thermal radiation and entropy generation on a stretching sheet with chemical reaction in the presence of MHD flow of Williamson nanofluid. Aldabesh et al. [11] investigate the axisymmetric analysis for the Casson nanofluid due to parallel stretchable disks. Alhamaly et al. [12] have discussed thermal radiation effects on stagnation point nanofluid flow on a linearly stretching surface with heat transfer analysis. MHD and stagnation point nanofluid flow in view of the stretchable surface along with the variable thickness and radiation effects are evaluated by Ramesh et al. [13]. Several further investigators have indicated useful engineering applications of boundary fluid layer flow with thermal generation in view of stretching surfaces for different fields, such as polymer extraction, filing drawing, paper manufacturing, wire coatings analysis for glass fiber production and many more practical uses. Srinivasulu and Goud [14] have investigated heat mass flow and the impact of an aligned magnetic field on Williamson's nanofluid over a stretching surface with convective boundary conditions. Effects of heat generation/absorption on magnetohydrodynamic, dissipative, and mixed convection boundary layer Cu-water nanofluid in a nonlinear stretching/shrinking sheet in the existence of heat generation/absorption and viscous dissipation is analyzed by Reddy et al. [15]. Nayak et al. [16] have diverted their attention toward the hydromagnetic three-dimensional convective flow of a nanofluid in view of the stretchable surface along with thermal radiation and variable magnetic field effect. Williamson fluid is a typical non-Newtonian fluid model having the shear thinning behavior. The model was proposed by Williamson [17]. Rasheed et al. [18] studied the hydromagnetic boundary layer flow of Jeffrey nanofluid past by vertically stretching a cylindrical sheet with Newtonian heating and dissipation effects. Later on, other researchers explored various features with different geometries and discussed flow, thermal and solutal fields by Ibrahim and Negera, [19], Vasudev et al. [20], Nadeem, and Hussain [21]. Gorla and Gireesha [22] have paid attention to stagnation point liquid flow and heat transfer characteristics of non-Newtonian Williamson nanofluid in view of stretching/shrinking sheet surface along with convective boundary conditions. The above-stated citations are all directly related to explored and boundary-layer flow of nanofluid along with the development of heat and thermal conductivity of base liquid over a stretching sheet with different geometrical aspects. The fluid flow and heat transfer of viscoelastic fluids in view of stretching sheet along with variable thickness non flatness can be more applicable to the situation in practical utilizations. Abbas et al. [23] examine entropy generation and heat transfer development on magneto-hydrodynamic slip flow of viscous fluid in a diverging tube. Fang et al. [24] investigated and found for the first time an analytical and numerical approach for the solution of two-dimensional boundary layer flow due to a non-flatness stretching sheet. Furthermore, the same problem was addressed by Subhashini et al. [25] by incorporating the energy term and observing the thermal boundary layer thicknesses for the first solution which were thinner than those of the second solution. A numerical and analytical investigation was carried out for the solution of viscoelastic non-Newtonian fluid over a stretching surface in the presence of porous medium as well as in the thermal radiation effects by Khader and Meghad [26]. Here some relevant applications based on citations of nanofluids directly related to the present investigation have been cited in [27–31].

2. Mathematical formulation

Here, we have assumed hydromagnetic two-dimensional Williamson nanofluid flow in view of a stretchable surface. The center is pointed out at a slit point from which the surface is drawn over the fluid medium. The sheet's velocity, defined by the formula as $U_w = U_0 (x + b)^m$, here, x -axis lies in the direction of the stretchable sheet surface, the y -axis normal to stretching sheet. Further, we considered that the surface is not flat, and thickness is changing with the relation given by $y = A(x + b)^{\frac{1-m}{2}}$, $A \geq 0$ positive constant such that the surface is thin enough, and (m) is velocity power index. When

($m = 1$), represent a flat sheet flow problem. An external magnetic field has been employed having strength (B) in normal direction of fluid flow. As fluid has conducting behavior, the Reynolds number is less than one. The induced magnetic field effect is small in comparison to the applied field. Coordinates axes and flow model configuration is shown in Figure 1.

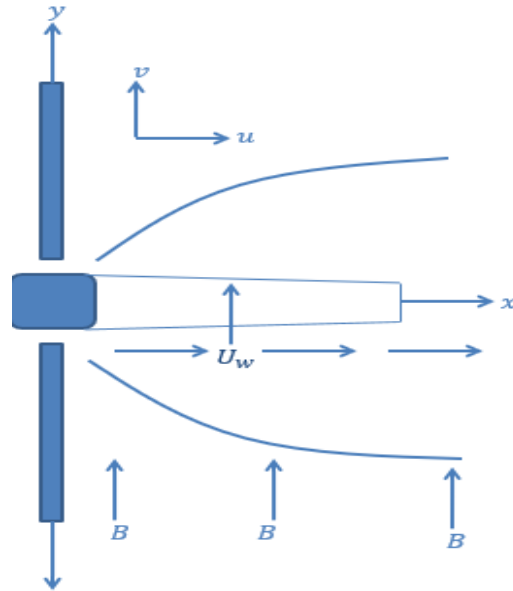


Figure 1. Schematic flow and Coordinate system.

Cauchy stress tensor ($\mathbf{S}$) for Williamson fluid model defined by [19]:

$$\mathbf{S} = -p\mathbf{I} + \tau\tau = \left(\mu_{\infty} + \frac{\mu_0 - \mu_{\infty}}{1 - \Gamma\dot{\gamma}} \right) A_1$$

Whereas $\mathbf{S}$ denotes the extra stress tensor, μ_0 represents the viscosity of the fluid as shear rate is zero and μ_{∞} shows the viscosity for shear rate at infinite, where $\Gamma > 0$ denotes time constant. A_1 denotes first Rivlin Erickson tensor, $\dot{\gamma}$ can be written by the relation given as below:

$$\dot{\gamma} = \sqrt{\frac{1}{2}\pi}, \quad \pi = tr(A_1^2)$$

Herein, we have selected the case when $\mu_{\infty} = 0$ and that of $\Gamma\dot{\gamma} < 1$. Therefore τ may be written as mention below:

$$\tau = \left(\frac{\mu_0}{1 - \Gamma\dot{\gamma}} \right) A_1$$

After utilizing the binomial series, we obtained as follow:

$$\tau = \mu_0(1 - \Gamma\dot{\gamma})A_1.$$

The mathematical expressions for two-dimensional flow laws are [21]:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \quad (1)$$

$$u\left(\frac{\partial u}{\partial x}\right) + v\left(\frac{\partial u}{\partial y}\right) = v\left(\frac{\partial^2 u}{\partial y^2}\right) + \sqrt{2}v\Gamma\left(\frac{\partial u}{\partial y}\right)\left(\frac{\partial^2 u}{\partial y^2}\right) - \frac{\sigma B^2}{\rho}u \quad (2)$$

$$u\left(\frac{\partial T}{\partial x}\right) + v\left(\frac{\partial T}{\partial y}\right) = \frac{1}{\rho c_p}\frac{\partial}{\partial y}\left(\kappa\frac{\partial T}{\partial y}\right) - \frac{1}{\rho c_p}\left(\frac{\partial q_r}{\partial y}\right) + \frac{\rho c_p}{\rho c_f}\left(D_B\frac{\partial C}{\partial y}\frac{\partial T}{\partial y} + \frac{D_T}{T_{\infty}}\left(\frac{\partial T}{\partial y}\right)^2\right) \quad (3)$$

$$u \left(\frac{\partial C}{\partial x} \right) + v \left(\frac{\partial C}{\partial y} \right) = \frac{D_T}{T_\infty} \left(\frac{\partial^2 T}{\partial y^2} \right) + D_B \left(\frac{\partial^2 C}{\partial y^2} \right) \quad (4)$$

Conditions are [21]:

$$\begin{aligned} \text{For } y = (x+b)^{\frac{1-m}{2}} : u = u_w(x) = U_0(x+b)^m, v = 0, T = T_w, C = C_w \text{ and} \\ \text{For } y = \infty : u = 0, T = T_\infty, C = C_\infty \end{aligned} \quad (5)$$

where (u, v) velocity components in x and y directions, ρ is fluid density, g is the gravity force, μ viscosity, ν kinematic viscosity, C_p specific heat, B is field strength, T, C temperature, concentration, T_w, T_∞ fluid temperature at wall, ambient temperature when $y \rightarrow \infty$. Herein D_B Brownian diffusion-coefficient, D_T thermophoretic diffusion-coefficient, $\tau = \frac{(\rho c)_p}{(\rho c)_f}$, ratio between effective heat capacity of nanoparticles material and heat capacity of the fluid, κ temperature dependent thermal conductivity by [32]:

$$\kappa = \kappa_\infty \left(1 + \varepsilon \frac{T - T_\infty}{T_w - T_\infty} \right) \quad (6)$$

Rosseland approximation for radiation defined by:

$$q_r = -\frac{4\sigma^*}{3k^*} \left(\frac{\partial T^4}{\partial y} \right) \quad (7)$$

Here, σ^* denotes Stefan–Boltzmann-constant, k^* is absorption coefficient. Further, we considered that temperature variations inside fluid, in such a way that factor T^4 can be written in the form of linear function of fluid temperature. We obtained series expression for T^4 by utilizing the Taylor theorem at stream temperature T_∞ and ignoring higher powers of T_∞ as:

$$T^4 = 4T_\infty^4 T - 3T_\infty^4 \quad (8)$$

By utilizing (7) and (8), we set:

$$\frac{\partial q_r}{\partial y} = -\left(\frac{16\sigma^* T_\infty^3}{3k^*} \right) \left(\frac{\partial^2 T}{\partial y^2} \right) \quad (9)$$

By introducing similarity functions are:

$$\begin{aligned} \eta = \sqrt{\frac{U_0(m-1)}{2\nu}} (y(x+b)^{\frac{m-1}{2}} - A), \quad \psi = \sqrt{\frac{2\nu U_0}{m+1}} (x+b)^{\frac{m+1}{2}} f(\eta), \\ \theta(\eta) = \frac{T-T_\infty}{T_w-T_\infty}, \quad \phi(\eta) = \frac{C-C_\infty}{C_w-C_\infty} \end{aligned} \quad (10)$$

Here, Equation (1) is true identically while (2)–(5) have the forms:

$$f''' + \lambda f'' f''' + f f'' - \left(\frac{2m}{m+1} \right) (f')^2 - M f' = 0 \quad (11)$$

$$\left(1 + \frac{4}{3} R \right) \left[(1 + \varepsilon \theta) \theta'' + \varepsilon (\theta')^2 \right] + \text{Pr} f \theta' + \frac{Nc}{Le} \phi' \theta' + \frac{Nc}{Le Nbt} (\theta')^2 = 0 \quad (12)$$

$$\phi'' + Le \text{Pr} f \phi' + \frac{1}{Nbt} \theta'' = 0 \quad (13)$$

$$f'(0) = 1, f(0) = \alpha \left(\frac{1-m}{1+m} \right), \theta(0) = 1, \phi(0) = 1, f'(\infty) = 0, \theta(\infty) = 0, \phi(\infty) = 0 \quad (14)$$

Following are the governing pertinent parameters appearing in (11)–(14) are defined as:

$$M = \frac{2\sigma B_0^2}{U_0 \rho (1+m)}, \text{Pr} = \frac{\nu}{\alpha}, \alpha = A \sqrt{\frac{U_0 (1+m)}{2\nu}}, R = \frac{4\sigma^* T_\infty^3}{k_\infty k^*}, Le = \frac{\alpha}{D_B},$$

$$Nc = \frac{\rho_p c_p}{\rho_c} (C_w - C_\infty), Nbt = \left(\frac{B_T T_\infty}{D_T} \right) \left(\frac{C_w - C_\infty}{(T_w - T_\infty)} \right), \lambda = \Gamma \sqrt{\frac{U_0^3 (x+b)^{3m-1} (m+1)}{\nu}},$$

and ε elucidated magnetic field, Prandtl number, wall thickness parameter, radiation parameter, Lewis number, nanofluid heat capacity, Brownian diffusivity/thermophoretic diffusivity, Williamson fluid parameter and thermal conductivity parameter respectively.

Expressions of physical quantities (Cf_x , Nu_x , Sh_x) are

$$Cf_x = \frac{\tau_w}{\rho U_w^2}, Nu_x = \frac{Xq_w}{k_\infty (T_w - T_\infty)} \text{ and } Sh_x = \frac{Xq_w}{k (T_w - T_\infty)} \quad (15)$$

Where q_w and q_m are heat flux and mass flux:

$$q_w = -k_\infty \left(\frac{\partial T}{\partial y} \right)_{at y=0} \text{ and } q_m = -D_B \left(\frac{\partial C}{\partial y} \right)_{at y=0} \quad (16)$$

By simplifying the above equations, we have

$$\sqrt{Re_x} Cf_x = \sqrt{\frac{1+m}{2}} \left(f''(0) + \frac{\lambda}{2} (f''(0))^2 \right) \quad (17)$$

$$\sqrt{Re_x} Cf_x = \sqrt{\frac{1+m}{2}} \left(f''(0) + \frac{\lambda}{2} (f''(0))^2 \right) \quad (18)$$

$$\frac{Sh_x}{\sqrt{Re_x}} = -\sqrt{\frac{1+m}{2}} \left(1 + \frac{4}{3}R \right) \phi'(0) \quad (19)$$

Here, $Re_x = \frac{U_w(x)X}{\nu}$, is the local Reynolds number and $X = x + b$.

3. Numerical Scheme

In this section, the ordinary nonlinear coupled differential flow expressions (11)–(13), subject to conditions in (14) are addressed and solved numerically by utilizing computational algorithm `bvp4c`, a built-in function in Mathematica software. The nonlinear system of couple flow equations is changed to first order differential equations.

Let the appropriate transformation variables be defined by:

$$w_1 = f, w_2 = f', w_3 = f'', w_4 = \theta, w_5 = \theta', w_6 = \phi \text{ and } w_7 = \phi'$$

$$w'_1 = w_2 \quad (20)$$

$$w'_2 = w_3 \quad (21)$$

$$w'_3 = \left(\frac{2m}{m+1} \right) (w_2)^2 + Mw_2 - \lambda_1 w_3 w'_3 - w_1 w_3 \quad (22)$$

$$w'_4 = w_5 \quad (23)$$

$$w'_5 = \frac{-1}{\left(1 + \frac{4}{3}R \right) (1 + \varepsilon w_4)} \left[\left(1 + \frac{4}{3}R \right) \varepsilon (w_5)^2 + \text{Pr} w_1 w_5 + \frac{Nc}{Le} w_7 w_5 + \frac{Nc}{Le Nbt} (w_5)^2 \right] \quad (24)$$

$$w'_6 = w_7 \quad (25)$$

$$w'_7 = - \left[Le \text{Pr} w_1 w_7 + \frac{1}{Nbt} w'_5 \right] \quad (26)$$

Transformed conditions are:

$$w_2(0) = 1, w_1(0) = \alpha \left(\frac{1-m}{1+m} \right), w_4(0) = 1, w_6(0) = 1, w_2(\infty) = 0, w_4(\infty) = 0, w_6(\infty) = 0 \quad (27)$$

Asymptotic convergence is perceived to be achieved for $\eta_{\max} = 5$. All computational outcomes achieved in this problem are subjected to error tolerance 10^{-6} . Further, numerical results are tested and validated by comparing with analytical method to confirm and find excellent agreement. Comparisons are tabularized in Tables 1–3 and disclosed graphically in Figures 2–4. Finally, total squared residual error has been shown graphically in Figure 5. A diminishing trend in average squared residual error is detected for higher-order deformations.

Table 1. Numerical solution via analytical solution for velocity profile.

η	Numerical Solution	HAM Solution	Absolute Error
0.0	1.000000	1.000000	1.110220×10^{-16}
0.5	0.519700	0.521135	0.001435
1.0	0.294745	0.297334	0.002589
1.5	0.173273	0.176578	0.003305
2.0	0.103677	0.107275	0.003598
2.5	0.062508	0.066109	0.003600
3.0	0.037624	0.041122	0.003498
3.5	0.022241	0.025740	0.003499
4.0	0.012367	0.016198	0.003831
4.5	0.005516	0.010293	0.004778
5.0	-8.463110×10^{-9}	0.006738	0.006738

Table 2. Numerical solution via analytical solution for temperature profile.

η	Numerical Solution	HAM Solution	Absolute Error
0.0	1.000000	1.000000	$2.775560'' \times 10^{-15}$
0.5	0.806366	0.807472	0.001106
1.0	0.616598	0.618908	0.002310
1.5	0.616598	0.452817	0.003460
2.0	0.313287	0.317730	0.004443
2.5	0.209106	0.214317	0.005211
3.0	0.132926	0.138699	0.005773
3.5	0.079093	0.085260	0.006167
4.0	0.041981	0.048419	0.006438
4.5	0.016838	0.023460	0.006622
5.0	$2.047920'' \times 10^{-9}$	0.006738	0.006738

Table 3. Numerical solution via analytical solution for concentration of nanoparticle profile.

η	Numerical Solution	HAM Solution	Absolute Error
0.0	1.000000	1.000000	$6.661340'' \times 10^{-16}$
0.5	0.689690	0.691967	0.002278
1.0	0.465531	0.469337	0.003806
1.5	0.318343	0.323069	0.004726
2.0	0.220090	0.225399	0.005309
2.5	0.150765	0.156494	0.005729
3.0	0.099842	0.105898	0.006056
3.5	0.062038	0.068355	0.006317
4.0	0.034250	0.040770	0.006520
4.5	0.014195	0.020862	0.006667
5.0	$-2.062160'' \times 10^{-9}$	0.006738	0.006738

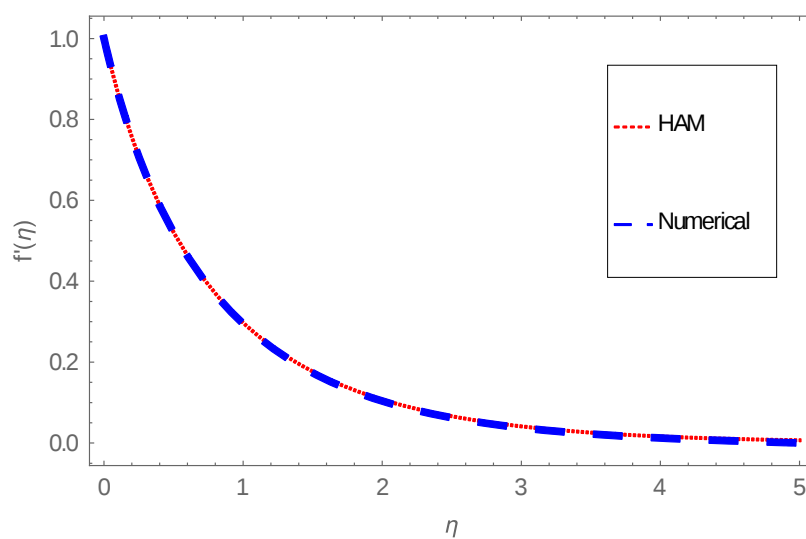


Figure 2. Dual solution for velocity field.

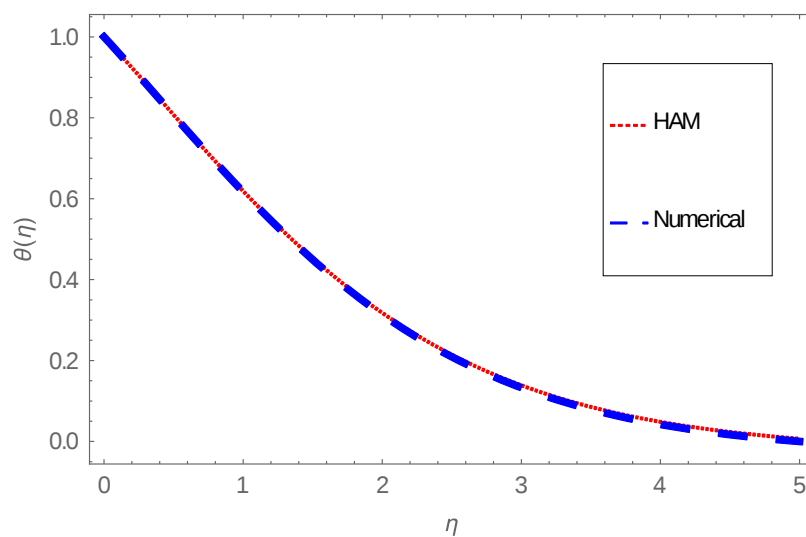


Figure 3. Dual solution for temperature field.

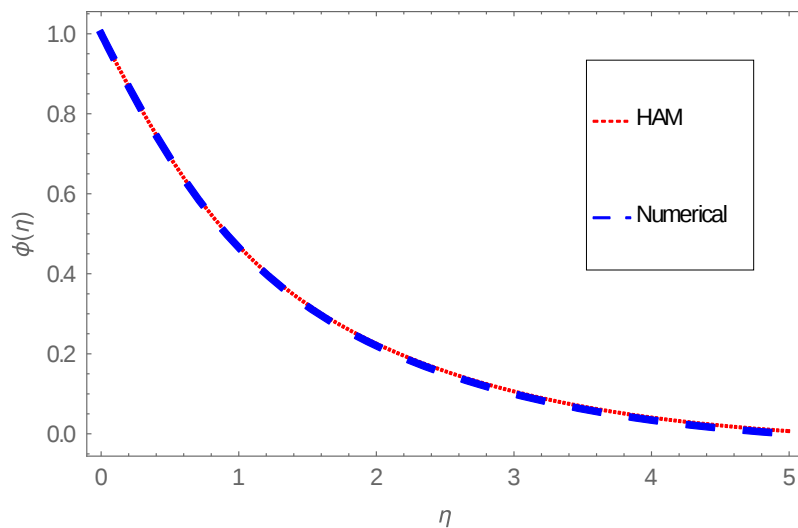


Figure 4. Dual solution for concentration field.

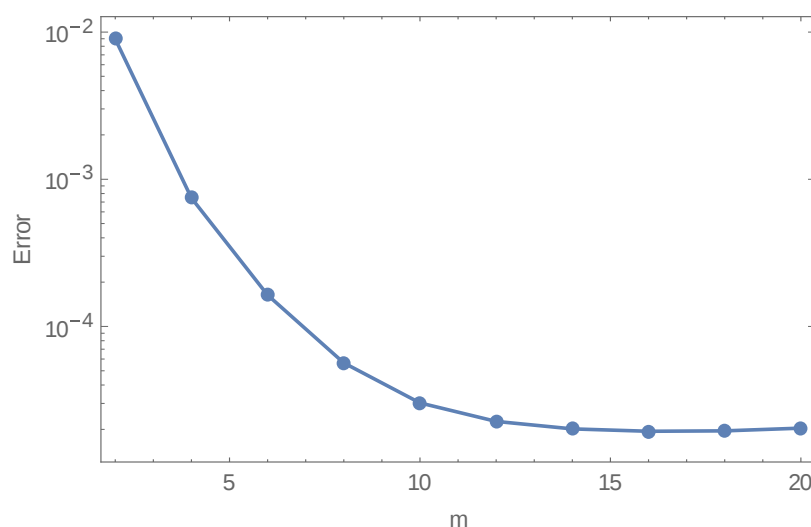


Figure 5. Residual error via order of approximation.

4. Discussion

Noticeable characteristics of α , M , Pr , ε , R , Nc , Nbt , Le and λ against drag force, $Re_x^{0.5}Cf_x$, Nusselt number $Re_x^{-0.5}Nu_x$, Sherwood number $Re_x^{-0.5}Sh_x$, fluid velocity $f'(\eta)$, thermal distribution $\theta(\eta)$ and solutal distribution $\phi(\eta)$ are explained and plotted in Figures 6–34.

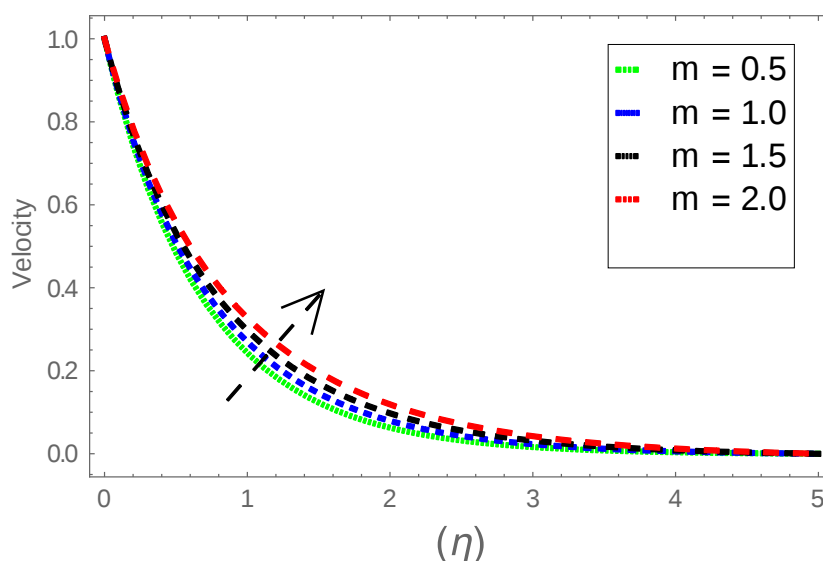


Figure 6. Consequence of (m) via $f'(\eta)$.

Figures 6–8 explain the attributes of velocity power index factor (m) on $f'(\eta)$, $\theta(\eta)$ and $\phi(\eta)$. As anticipated, velocity, temperature and concentration fields are augmented subject to increment in (m) . In consequence, momentum boundary layer thickness and thermal boundary layer thickness dwindle to higher values of (m) . The contribution of Williamson parameter (λ) on $f'(\eta)$, $\theta(\eta)$ and $\phi(\eta)$ are evaluated through Figures 9–11. Here, in Figure 6, we found lower $f'(\eta)$ subject to increment in (λ) . Clearly, $\theta(\eta)$ and $\phi(\eta)$ are the augmenting function of Williamson parameter. In reality, heat transference boosts through larger (λ) . Consequently, the solutal field $\phi(\eta)$ escalates. Attributes of magnetic field influence (M) on velocity, thermal and solutal fields are interpreted in Figures 12–14. Clearly, Figure 12 unveils that velocity diminishes subject to boosts through larger (M) . Physically, as (M) escalates, fluid viscosity increases due to Lorentz force upsurges when (M) is augmented. Moreover, this force has a resistive nature which controls fluid motion.

It is significant interest that yield stress of the fluid can be measured and controlled correctly by changing effect of magnetic parameter. In consequence, the capacity of fluid to transmit force can be measured through an electromagnet which gives numerous possible control-based utilizations, which include MHD power generation, MHD ion propulsion, electromagnetic casting of metals, and many more. Figure 13 depicts variation in thermal $\theta(\eta)$ field subject to higher (M) . One can perceive that $\theta(\eta)$ is an augmenting function of (M) . In reality, heat transference boosts through larger magnetic parameter. Consequently, it escalates $\theta(\eta)$. This reality lies in thermal energy dissipation due to applied magnetic field. Solutal field $\phi(\eta)$ curves for (M) are revealed in Figure 14. Clearly, $\phi(\eta)$ is augmenting function of (M) . In reality, when the magnetic field upsurges due to which fluid nanoparticles diffuse rapidly into the neighboring layers. Accordingly, $\phi(\eta)$ rises. The contribution of wall thickness factor (α) on $f'(\eta)$, $\theta(\eta)$ and $\phi(\eta)$ are evaluated through Figures 15–20. As anticipated, fluid velocity near to the plate dwindles subject to (α) increment for $m < 1$ and escalates for $m > 1$ noticed in Figures 15 and 16. Thermal field $\theta(\eta)$ curves diminish near the plate for $m < 1$ and augments for $m > 1$ boosts through larger (α) shown in Figures 17 and 18. Solutal field $\phi(\eta)$ boundary layer diminishes when $m < 1$ however, reverse appearances are found for $m > 1$ subject to larger wall thickness parameter perceived in Figures 19 and 20. Figures 21 and 22 emphasize variable thermal conductivity parameter (ε) impact on thermal $\theta(\eta)$ field and solutal profile $\phi(\eta)$. Here, the thermal field curves upsurge when thermal conductivity (ε) augmented. In consequence, $\theta(\eta)$ rises. However, reverse appearances are perceived for larger conductivity parameter (ε) in solutal field. Figure 23 explains variations in $\theta(\eta)$ subjected to radiation parameter (R) . This figure discloses $\theta(\eta)$ augmentation for larger (R) . In fact, working fluid achieves extra heat subject to radiation factor. In consequence, $\theta(\eta)$ rises. Attributes of radiation factor on $\phi(\eta)$ are interpreted in Figure 24. Clearly, $\phi(\eta)$ diminishes when (R) is augmented. The contribution of Prandtl number (Pr) on $\theta(\eta)$ is evaluated through Figure 25. Thermal diffusivity reduces when (Pr) upsurges. Hence, thermal field decays. The contribution of $\phi(\eta)$ curves for (Pr) estimations are designed in Figure 26. Higher/larger Prandtl number estimations yield declines in $\phi(\eta)$. In reality, mass diffusivity reduces when (Pr) is increased. Thus, $\theta(\eta)$ diminishes. The contribution of (Nbt) on thermal field $\theta(\eta)$ and solutal field $\phi(\eta)$ curves are evaluated through Figures 27 and 28. Thermal diffusivity reduces when (Nbt) upsurges. Hence, thermal field decays. In consequences, thermal boundary layer thickness diminishes. The solutal field $\phi(\eta)$ reduces significantly subject to increment in (Nbt) . As (Nbt) is defined as the ratio of Brownian diffusivity to thermophoretic diffusivities. An upsurge in (Nbt) factor reasons for larger activity of nanoparticles in side base fluid. Attributes of Lewis number (Le) on thermal field and solutal field are interpreted in Figures 29 and 30. Clearly, $\theta(\eta)$ reduces when (Le) is augmented. Thus, thermal boundary layer thickness diminishes with upsurge in (Le) . Effect of Lewis number on solutal field is disclosed in Figure 30. Here, $\phi(\eta)$ reduces versus higher estimations of (Le) factor. Figure 31 depicts variations in thermal field $\theta(\eta)$ subjected to nanofluid heat capacity parameter (Nc) . This figure discloses $\theta(\eta)$ augmentation for higher (Nc) . In fact, working nanofluid gets extra heat subject to larger (Nc) parameter. In consequence, boundary layer thickness enhances.

Figure 32 emphasize M and α impacts on $Re_x^{0.5} Cf_x$. Here, $Re_x^{0.5} Cf_x$ upsurges when α and M are augmented. However, reverse features are found for larger values of λ and m . The attributes of M and α influences on $Re_x^{-0.5} Nu_x$ are elaborated in Figure 33. This figure confirms that $Re_x^{-0.5} Nu_x$ upsurges subject to α and M are enlarged. Influence of R and α on $Re_x^{-0.5} Sh_x$ are shown in Figure 34. The local Sherwood number, diminishes subject to increment in these parameters.

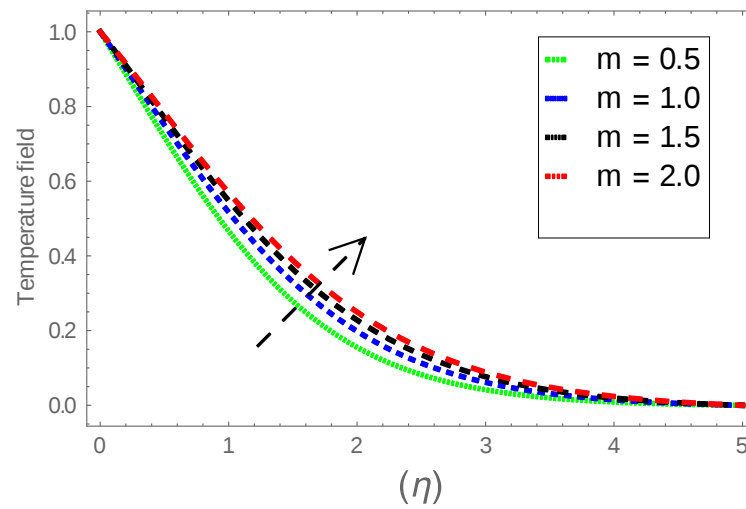


Figure 7. Consequence of (m) via $\theta(\eta)$.

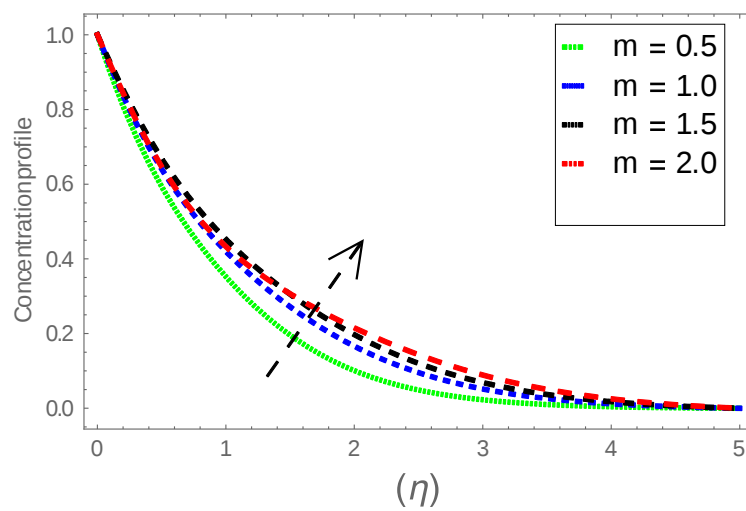


Figure 8. Consequence of (m) via $\phi(\eta)$.

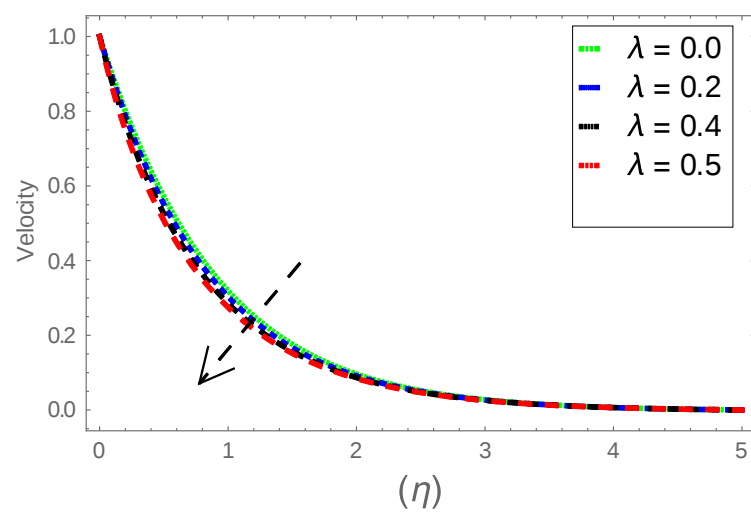


Figure 9. Consequence of (λ) via $f'(\eta)$.

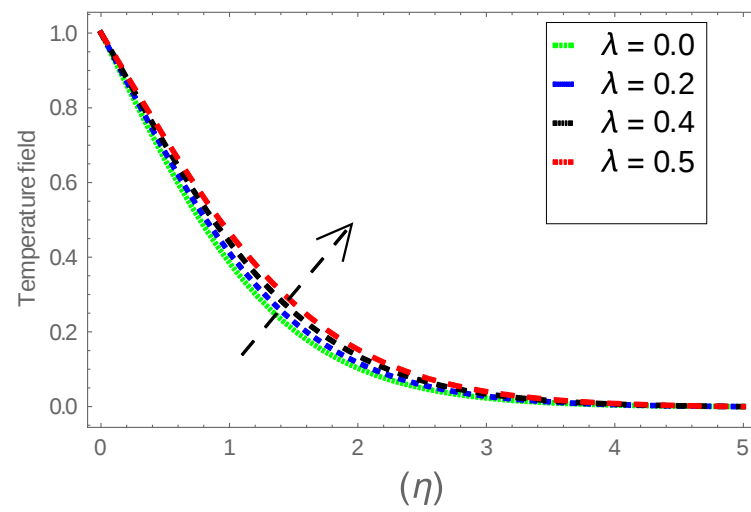


Figure 10. Consequence of (λ) via $\theta(\eta)$.

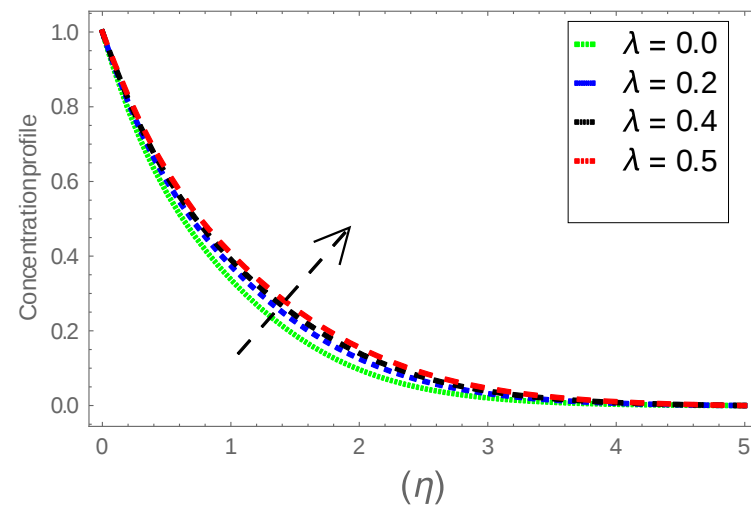


Figure 11. Consequence of (λ) via $\phi(\eta)$.

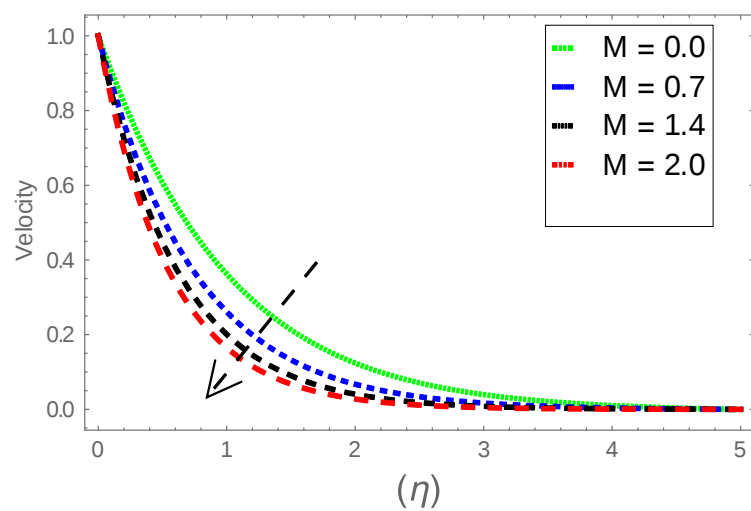


Figure 12. Consequence of (M) via $f'(\eta)$.

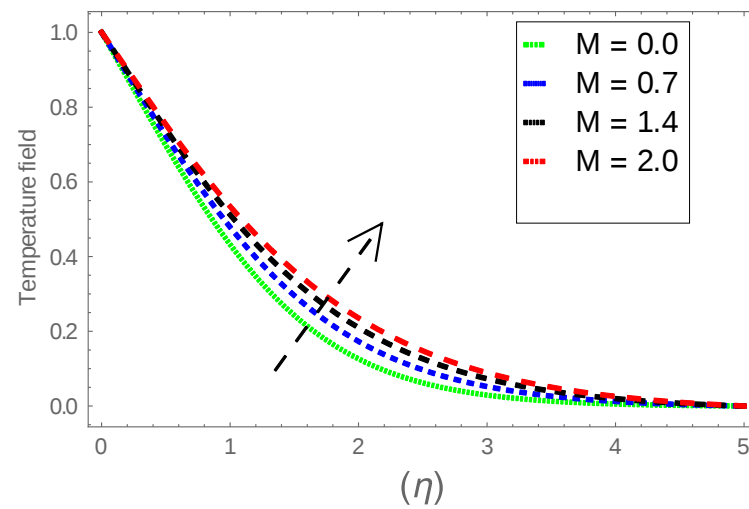


Figure 13. Consequence of (M) via $\theta(\eta)$.

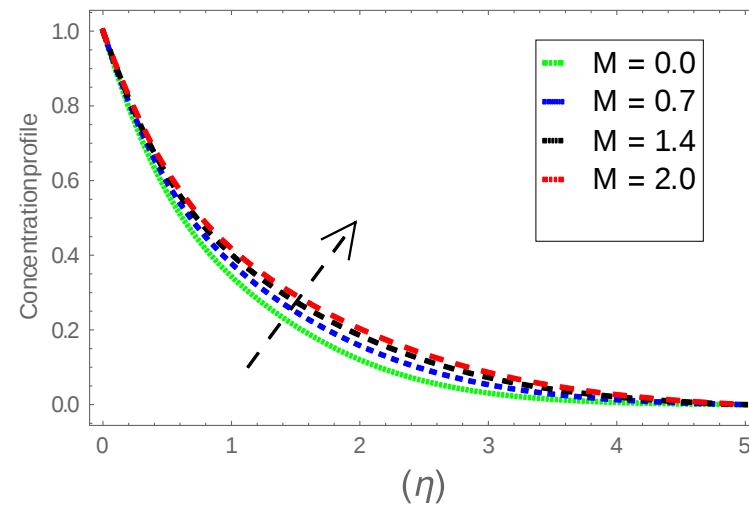


Figure 14. Consequence of (M) via $\phi(\eta)$.

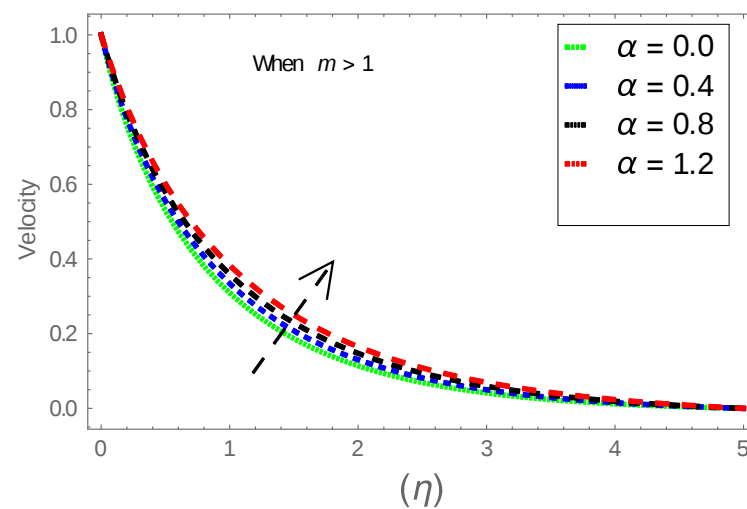


Figure 15. Consequence of (α) via $f'(\eta)$.

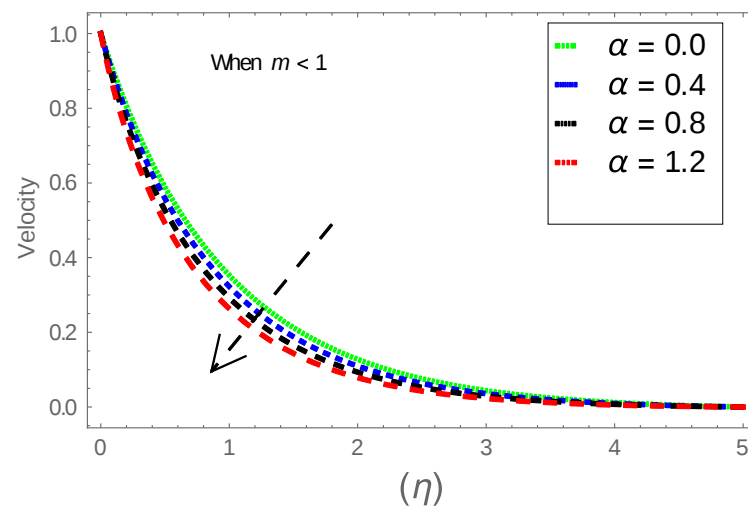


Figure 16. Consequence of (α) via $f'(\eta)$.

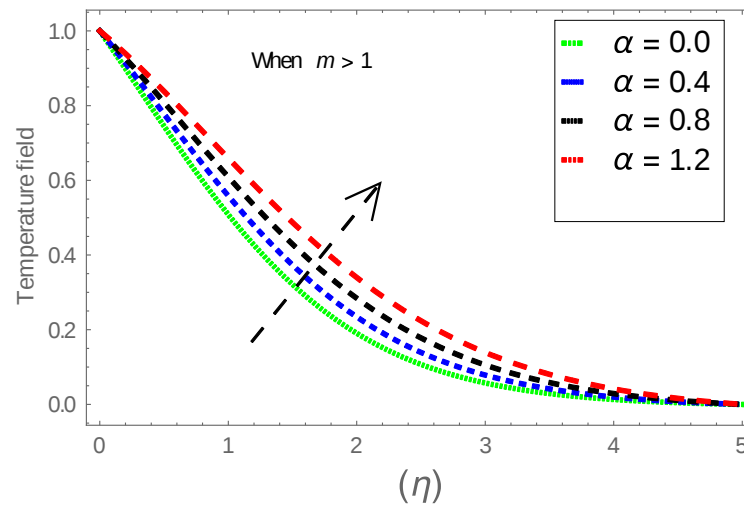


Figure 17. Consequence of (α) via $\theta(\eta)$.

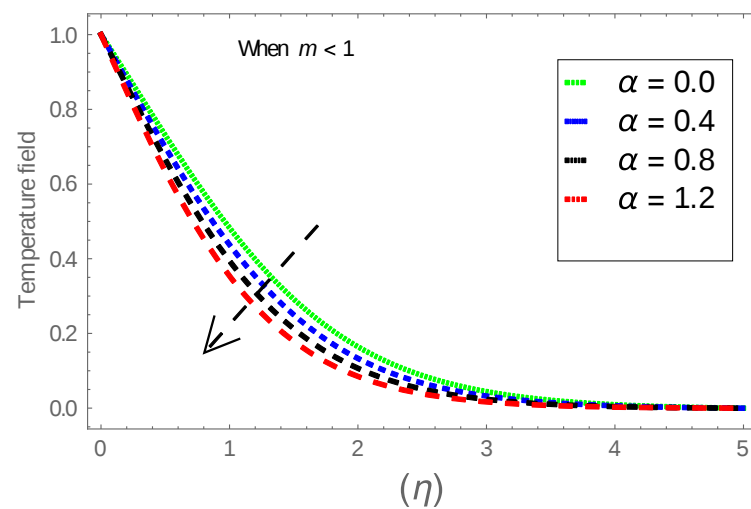


Figure 18. Consequence of (α) via $\theta(\eta)$.

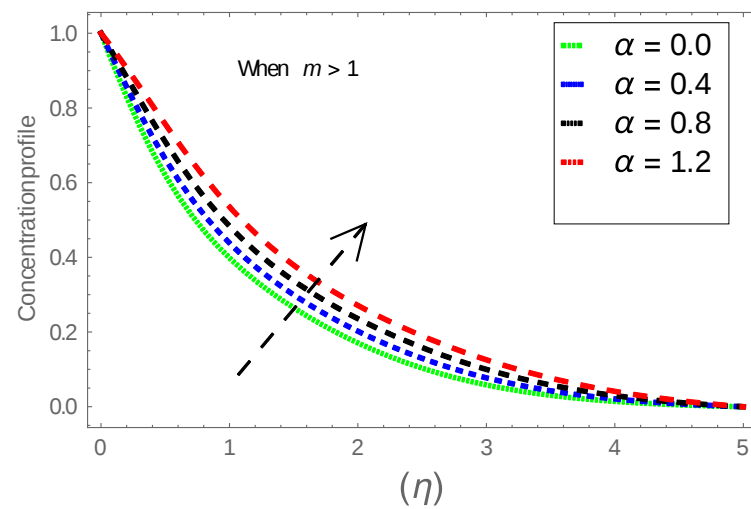


Figure 19. Consequence of (α) via $\phi(\eta)$.

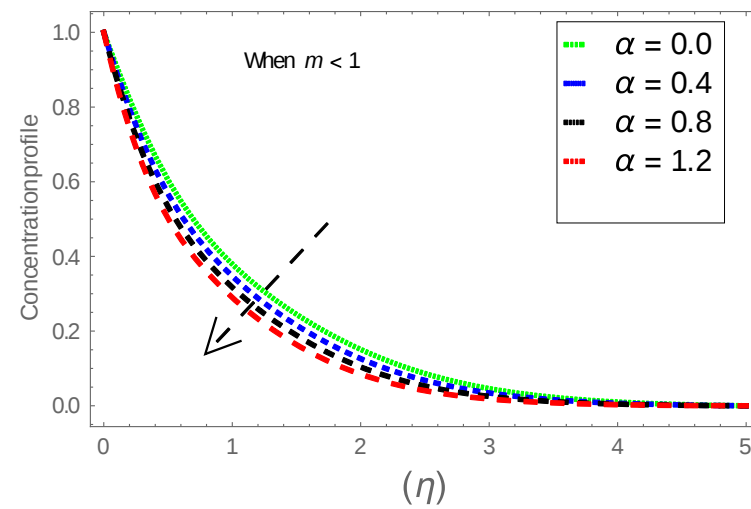


Figure 20. Consequence of (α) via $\phi(\eta)$.

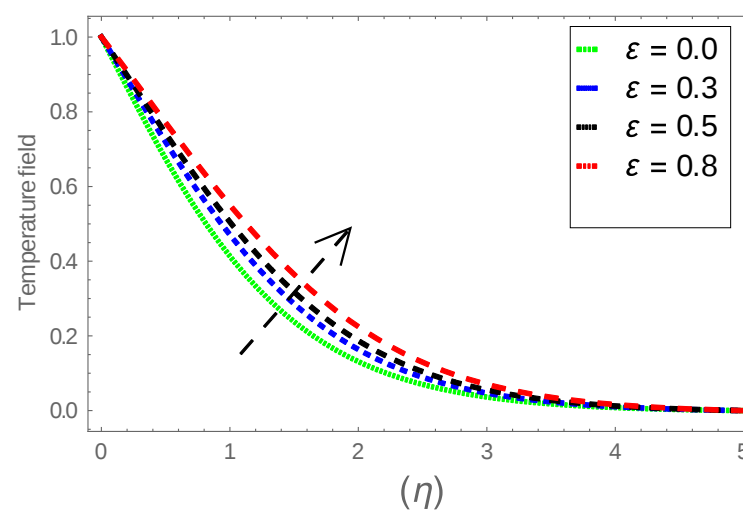


Figure 21. Consequence of (ε) via $\theta(\eta)$.

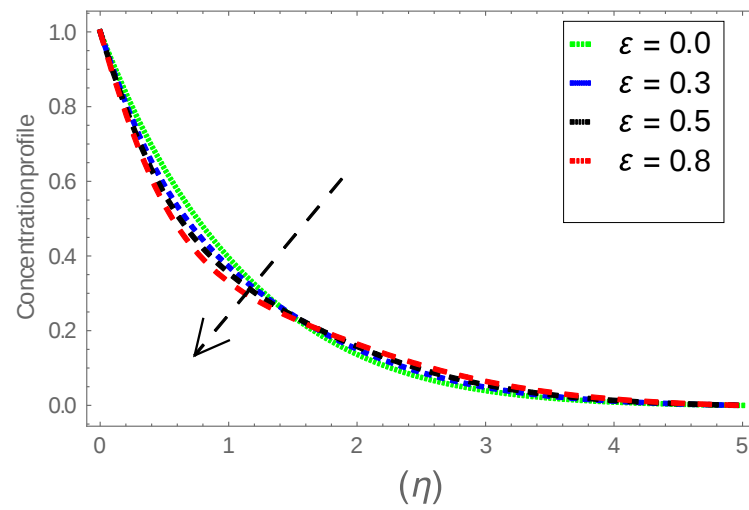


Figure 22. Consequence of (ε) via $\phi(\eta)$.

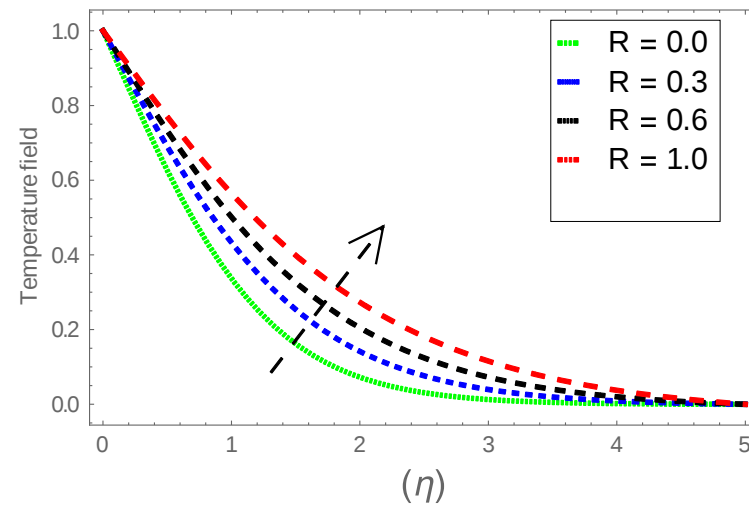


Figure 23. Consequence of (R) via $\theta(\eta)$.

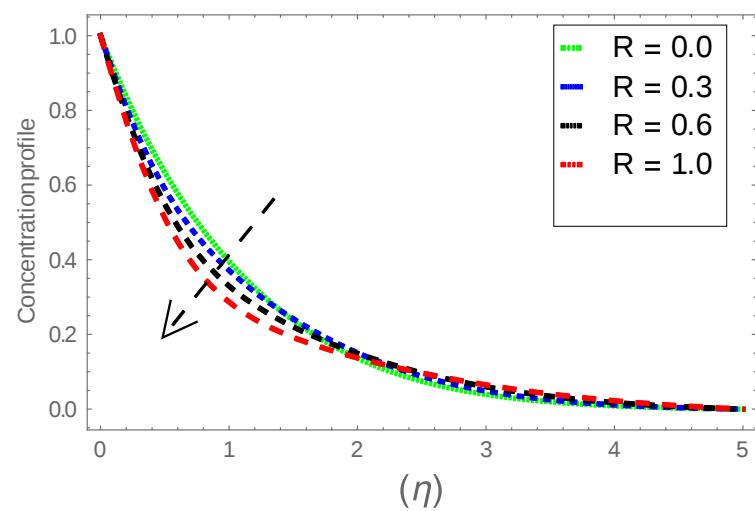


Figure 24. Consequence of (R) via $\phi(\eta)$.

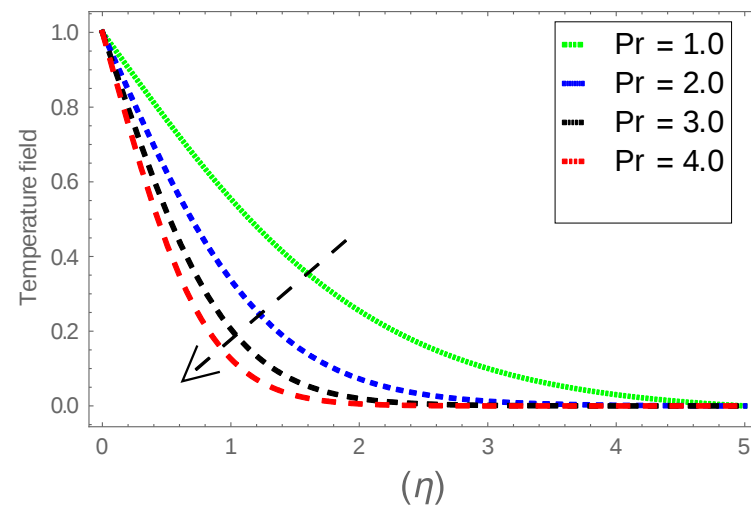


Figure 25. Consequence of (Pr) via $\theta(\eta)$.

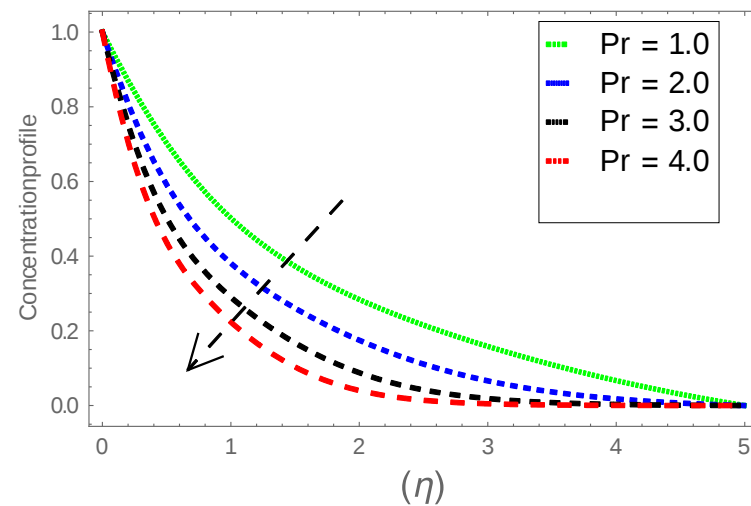


Figure 26. Consequence of (Pr) via $\phi(\eta)$.

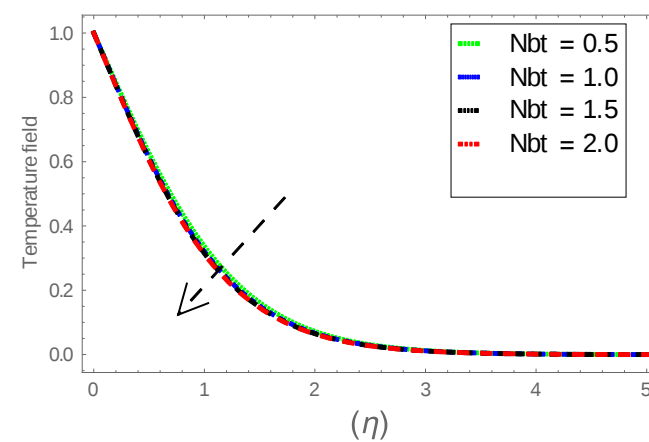


Figure 27. Consequence of (Nbt) via $\theta(\eta)$.

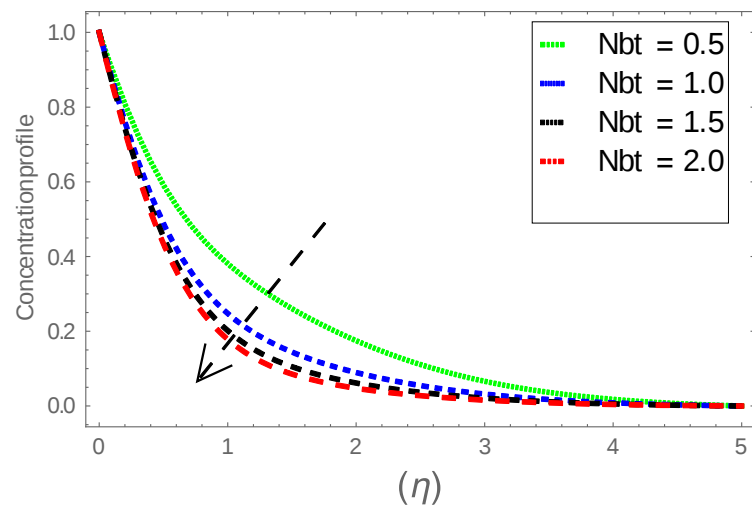


Figure 28. Consequence of (Nbt) via $\phi(\eta)$.

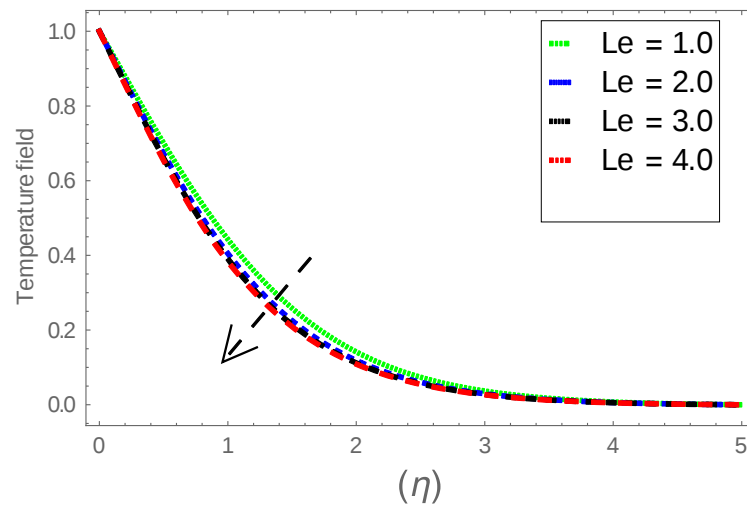


Figure 29. Consequence of (Le) via $\theta(\eta)$.

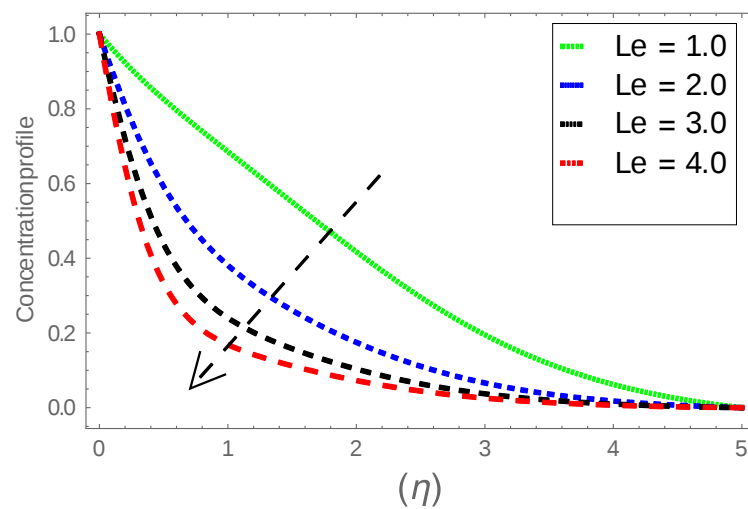


Figure 30. Consequence of (Le) via $\phi(\eta)$.

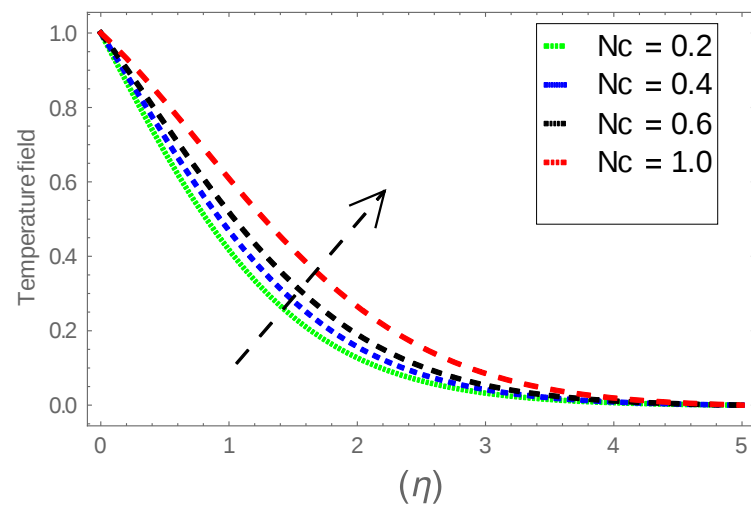


Figure 31. Consequence of (Nc) via $\theta(\eta)$.

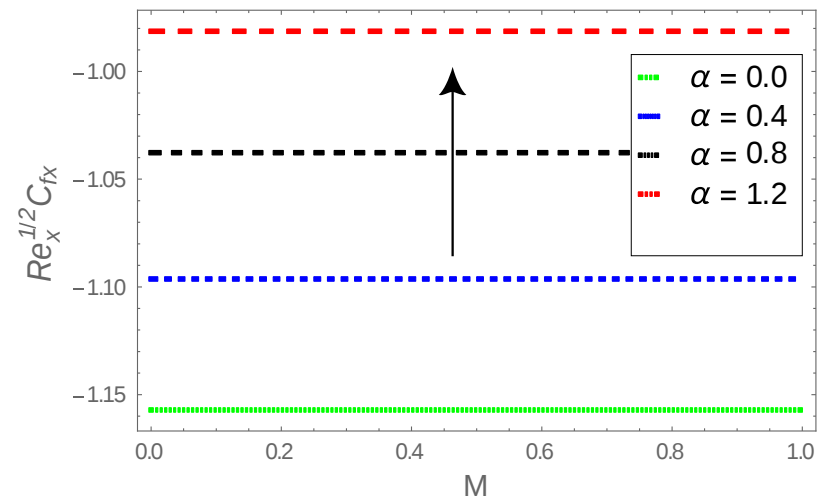


Figure 32. Consequence of $Re_x^{0.5} C_{fx}$ via α and M .

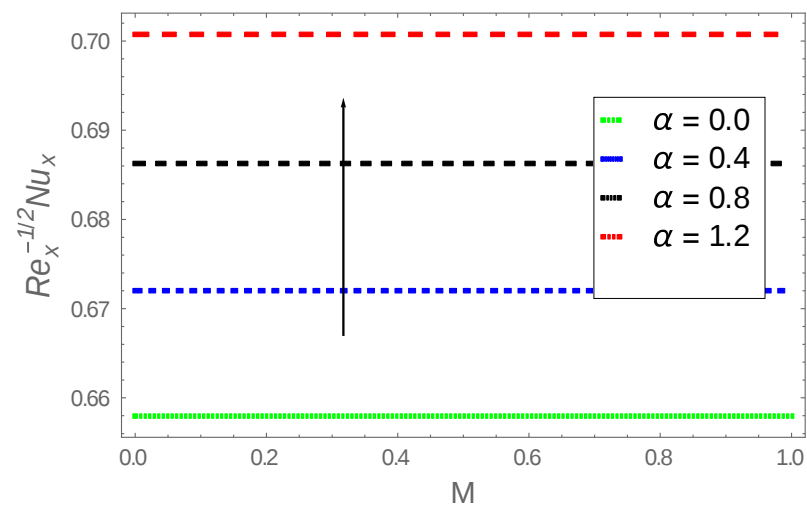


Figure 33. Consequence of $Re_x^{-0.5} Nu_x$ via α and M .

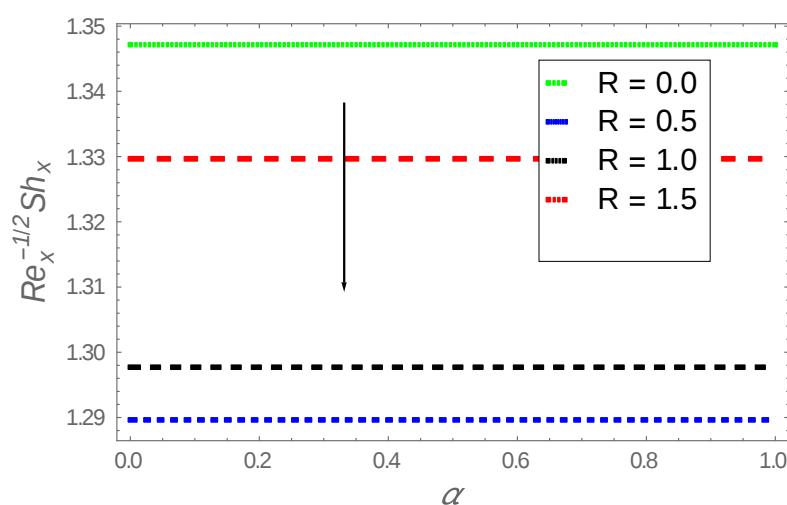


Figure 34. Consequence of $Re_x^{0.5} Sh_x$ via α and R .

5. Closing Remarks

In this study, various aspects of heat transference and radiation effects on hydromagnetic boundary layer Williamson nanofluid flow in view of stretchable surface along with variable thickness and variable thermal conductivity characteristics have been analyzed. A computational numerical algorithm is employed to accomplish convergent solutions. We witnessed notable features through abovementioned investigation:

- It is perceived that velocity field $f'(\eta)$ diminishes when wall thickness factor (α) augments for ($m < 1$) and reverse trends noticed in $f'(\eta)$ when ($m > 1$).
- Thermal $\theta(\eta)$ and solutal $\phi(\eta)$ fields upsurge subject to increment in (M) and $f'(\eta)$ diminishes with higher (M).
- An increment in (λ) parameter yields decays in $f'(\eta)$ and escalates thermal $\theta(\eta)$ and concentration fields.
- Variable thermal conductivity (ϵ) parameter diminishes heat transfer coefficient $-\theta'(0)$.
- Sherwood number $-\phi'(0)$ diminishes subject to increment in R and α .

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