



Article

UV-Cured Biodegradable Methacrylated Starch-Based Coatings

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Abstract: Promising UV-curable starch-based coatings were fabricated by utilizing methacrylated starch. The aqueous methacrylated starch solution was cast on a glass substrate, and UV-cured after drying. The efficiency of UV-curing process was monitored with gel percentage measurements. The thermal and mechanical properties of the fabricated UV-cured coatings were investigated through differential scanning calorimetry and tensile test and compared with the starch-based uncured casted coatings. A complete characterization of the surface properties was performed by means of pencil hardness, adhesion, solvent resistance, and surface tension measurements. The cross-linking by UV-curing significantly enhanced the mechanical and surface properties of the coating. The effect of UV-curing on the biodegradability of the coating was evaluated by following the enzymatic degradation by α -amylase by determining the amount of glucose and maltose released from the coatings. UV-cured methacrylated starch based coating with promising material and surface properties and retained biodegradation potential was demonstrated.

Keywords: starch; biodegradable coatings; UV-curing



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1. Introduction

Nowadays, we witness a steady rise in introduction of new bio-renewable resources as alternatives for petroleum-derived polymeric materials due to increased environmental concerns and depletion of petroleum feedstocks.

Among bio-renewable monomers, a large variety of molecules containing rigid aromatic backbone have been explored as polymer precursor such as polysaccharides [1], lignin [2], vanillin [3], eugenol [4], and cinnamic acid [5,6]. Thermosetting polymers obtained from those monomers usually possess high mechanical properties, due to the presence of the rigid aromatic backbone structure. It is important to stress that the term "biobased" denotes a product derived from renewable resources but does not imply biodegradability [7]. In fact, the research interest on biobased materials largely focus on increasing the durability and performances, rather than in the biodegradability.

Another attractive class of biobased materials is vegetable oils (VO). In fact, VO are constituted by triglycerides and possess several highly reactive sites. Moreover, they are potentially biodegradable in soil since their glycerol ester bond can be hydrolytically cleaved [8].

While vegetable oils have been widely utilized in non-edible coating applications [9–13], carbohydrate polymers were less explored because of their short shelf time and mechanical weakness. Polycarbohydrates can be obtained from a variety of sources like cellulose (carboxymethylcellulose, methylcellulose, etc.), starch (carboxymethylstarch, hydroxypropyl starch), seaweed extracts (alginate, agar, etc.), exoskeleton of crustaceans and insects (chitin, chitosan, etc.), and different types of microbial gums (xanthan, pullulan, etc.) [14]. Coatings made of polysaccharides are usually colourless and efficient oxygen blockers. Thanks to

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those qualities, they are extensively used as barrier for food protection in the packaging industry [15]. Among carbohydrates, starch is abundant in plants, biodegradable, and very cheap [16]. It is composed of two different polymers consisting of $\alpha(1-4)$ linked D-glucose units: amylose and amylopectin. Amylose is linear, while amylopectin is highly branched with 5%–6% of $\alpha(1-6)$ linkages. The ratio of those polymers varies based on the starch sources. For example, the amylose percentage in tapioca is 17%, in corn 25%–28% and in high amylose maize starch 70%. Starch is also non-toxic, polyfunctional, and has high chemical reactivity. However, the hydrophilicity and tendency of the starch granules to swell and rupture, has limited the industrial use of unmodified starch, especially in material applications [17]. Two strategies can be applied to overcome these drawbacks: (1) starch can be blended with other biobased materials [18–21]; (2) starch can be chemically modified, either by grafting or cross-linking. With well-designed modification both moisture resistance and mechanical properties of the material can be improved [22,23].

Chemically modified starch, therefore, could be an important starting precursor for the production of bio-based coatings. To induce network formation, different cross-linking agents have been proposed [24–27] exploiting thermal curing process.

Compared to conventional thermal-curing, UV-curing technology shows important advantages in-line with principals of green chemistry including very fast curing reaction, low energy consumption and solventless process [28–30].

In previous papers, light processable starch precursors were investigated for hydrogel preparation [31,32]. A few radiative processes involving gamma or electron beam irradiation were also proposed to induce crosslinking of starch [33–38].

The purpose of this study was to exploit and investigate methacrylated starch as a potential precursor for the production of UV-curable film coatings. The UV-curing process of the water-casted films is described, and the mechanical and surface properties of the obtained networks are fully characterized. Finally, the effect of UV-curing on the biodegradability was investigated by subjecting the uncured and cured coatings to α -amylase enzyme. The degradation process was monitored by analysing the amount of glucose and amylose released to the natant medium.

2. Materials and Methods

2.1. Materials

High-amylose Hylon VII maize starch (70% amylose) was obtained from Ingredion, Goole, UK. Methacrylic anhydride (MA), triethylamine (TEA) (>99%), dimethyl sulfoxide (DMSO) (ACS reagent P99.9%), ethanol absolute and bis(acyl)phosphane oxi lithium phenyl-2,4,6-trimethylbenzoylphosphinate (LAP) were purchased from Sigma Aldrich (Milan, Italy).

2.2. Synthesis of Methacrylated Starch

Methacrylated starch (MS) was synthetized as previously reported [32]. Briefly, 6 g of high amylose maize starch was solubilized in 200 mL of DMSO at 70 °C. After 30 min, the solution was let cool down at room temperature. Subsequently, methacrylic anhydride and triethylamine were added dropwise (molar ratio AGU (Anydrous Glucose Unit):MA:TEA of 1:2:0.04). The solution was then left to react for 18 h. The final product was precipitated in ethanol, dissolved in de-ionized water, and again precipitated in ethanol. After repeating this procedure two more times, the final aqueous solution was lyophilized. The methacrylation reaction was evaluated and confirmed by proton and carbon nuclear magnetic resonance (¹H-NMR, ¹³C-NMR), and fourier transform infrared (FTIR) spectroscopy (The characterization of methacrylated starch was reported in reference [32]).

2.3. Casting and Photocuring of Methacrylated Starch Coating

Methacrylated starch was suspended in de-ionized water (10 wt.% MS). After the complete solubilization, LAP as a photoinitiator in the content of 1 wt.% with respect to the starch weight was added. Then, the solution was immediately casted on a glass substrate.

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The solution was completely dried in air and subsequently irradiated with a DYMAX UV static lamp (125 mW/cm²) (Dymax, Torrington, USA) to fabricate the methacrylated starch cured film (MSC, $100 \mu m$).

2.4. Characterization

2.4.1. Attenuated Total Reflectance-Fourier Transform Infrared Spectroscopy (ATR-FTIR)

The FTIR spectra of starch and methacrylated starch were recorded by Perkin Elmer Spectrum 2000 FTIR spectrometer (Perkin Elmer, Norwalk, CT, USA) equipped with a single reflection attenuated total reflectance (ATR) accessory. For each sample, 16 scans were recorded with 4 cm⁻¹ resolution.

2.4.2. Gel Content

The gel content percentage (G%) of the cured films was determined by measuring the weight loss after 24 h extraction with hot water at 60 °C. G% was calculated according to Equation (1):

$$G\% = \frac{W_i}{W_0} \times 100\% \tag{1}$$

where W_i is the weight of the dry film after the treatment with water and W_0 is the weight of the dry sample before the treatment.

2.4.3. Differential Scanning Calorimetry (DSC)

Differential scanning calorimetric analysis was carried out on a Mettler Toledo DSC instrument (Mettler-Toledo, Stockholm, Sweden) at a heating rate of 10 $^{\circ}$ C/min using a nitrogen atmosphere. Samples (10–12 mg) were sealed in a 100 μ L aluminium pan with pierced lids.

2.4.4. Tensile Test

Tensile tests were performed on dry rectangular specimens (1 cm \times 10 cm) with 600 µm thickness using MTS QTestTM/10 Elite controller (MTS Systems Corporation, Edan Prairie, Minnesota, USA) using TestWorks[®] 4 software (Edan Prairie, Minnesota, USA). The traction force was applied along the length of the samples at a constant cross-head displacement rate of 2 mm/min. The Young's modulus (E) of each sample was calculated from the slope of the initial linear portion of the stress–strain curve. The ultimate tensile strength and elongation at break were calculated as the maximum stress value in the stress-strain curve. Five samples for each film were tested.

2.4.5. Pencil Hardness

The pencil hardness test was performed using pencils of different grades starting from the 6 H and continuing down the scale, testing with softer and softer pencils according to ASTM D 3363-74 [39]. The pencils were maintained at 45° and pushed for at least 6 mm with uniform pressure and speed onto the coating surface. The hardness of the coating was taken as that of the hardest pencil, which caused a cut less than 3 mm long out of the 6 mm test push on the surface of the coating.

2.4.6. Adhesion Measurement

The coating adhesion measurements were performed according to the ASTM D3359-B [40]. The surface of each coating was scratched both vertically and horizontally with a blade holding 6 teeth, separated from each other by a 2 mm distance. A strip of adhesive tape was then applied and subsequently pulled away with a 180° angle. The percentage of squares where the coating was still intact was reported.

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2.4.7. Solvent Rub Resistance test

The coating chemical resistance was evaluated by methyl ethyl ketone (MEK) double rub test according to the ASTM D5402 [41]. Double rubs were performed until the substrate was exposed, or for a maximum of 200 rubs.

2.4.8. Contact Angle

Contact angle measurements were performed with a Kruss DSA10 instrument (Hamburg, Germany), equipped with a video camera. Analyses were conducted using the sessile drop technique at room temperature. Ten measurements were performed on each sample. The surface free energy (γ) was determined based on Owens–Wendt–Rabel–Kaelble (WORK) method. [42] The measuring liquids were double distilled water (γ = 72.8 mN/m) and hexadecane (γ = 27.6 mN/m).

2.4.9. Enzymatic Degradation

The enzymatic degradation test was carried out by using α -amylase from bacillus *licheniformis*. Pre-weighted samples (4 mm \times 6 mm \times 0.4 mm) were incubated in phosphate buffer saline (PBS) solution containing 0.6 mg/mL of the enzyme at 37 °C for 2 weeks. At different time points (2, 5, 7 and 14 days), supernatants were collected. The enzymatic degradation of MS and MSC was quantified by measuring the amount of maltose and glucose using The Maltose and Glucose Assay kit provided by Sigma Aldrich. Briefly, 50 µL of supernatants were mixed with 50 µL of master reaction mix containing a glucose probe, which quantifies the amount of glucose generating a colorimetric product (570 nm). To measure the amount of maltose, an additional 50 µL of supernatants were mixed with 50 μL of master reaction mix containing a glucose probe and a-D-Glucosidase enzyme able to degrade maltose into two glucose units. The absorbance at 570 nm was detected using a multimode plate reader (SYNERGY, BioTeK, Wimooski, VT, USA). Three samples for each condition were used and experiments were performed three times. GraphPad Prism[®] software (Graph Pad Prism 8.3.0) was used for one or two way analysis of variance (ANOVA). Values * p < 0.05 were considered statistically significant. To monitor the α amylase activity over time, a control solution containing only the enzyme in PBS was prepared and stored at 37 °C.

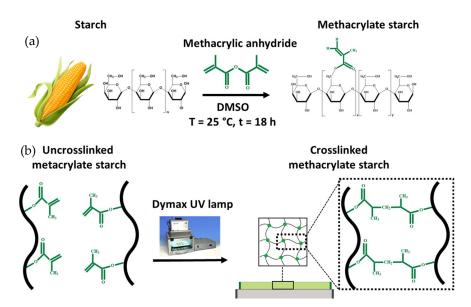
3. Results and Discussion

Starch was modified with methacrylic anhydride (Scheme 1, as already reported in a previous paper from our group [32]) in order to exploit the methacrylic functional groups in UV-curing process. Fully transparent tack-free crosslinked coatings were achieved, and thermal, mechanical, and surface properties of the crosslinked networks were evaluated.

3.1. Confirmation of Starch Methacrylation and Photocuring Process

The FTIR spectra of starch (S) and methacrylate starch (MS) are reported in Figure 1a. The starch spectrum shows the characteristic functional groups of starch. In the fingerprint region, the peaks at 760 and 859 cm $^{-1}$ represent the C–C stretching vibration and C(1)–H, CH $_2$ deformation, respectively. The peaks at 929, and 995 cm $^{-1}$ represent the skeletal vibration of C–O–C α -1–4 glycosidic linkage, while the peak at 1076 cm $^{-1}$ is the C–H bending vibration. The peak at 1149 cm $^{-1}$ corresponds to the C–O–C stretching vibrations of the cyclic ether group. The peaks at 1300 and 1360 cm $^{-1}$ are attributed to the –CH $_2$ – and C–O vibrations. The band at 1638 cm $^{-1}$ corresponds to the absorbed water in starch. The peak at 2925 cm $^{-1}$ is the –CH $_2$ – stretching vibration, while the broad peak at 3270 cm $^{-1}$ is assigned to the –OH vibration [43,44]. In the MS spectrum, it is possible to observe the appearance of new peaks that confirm the success of the methacrylation reaction. The peaks at 1300 and 1710 cm $^{-1}$ represent the C–O and C=O stretching vibrations, respectively. It is also possible to observe an enhancement and sharpness of the 1638 cm $^{-1}$ peak intensity, which can be due to the C=CH $_2$ out of plane bending vibrations [32,45].

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Scheme 1. (a) Methacrylation reaction; (b) schematic representation of the photo-crosslinking reaction.

The MS was dissolved in water and films were achieved by solvent-casting. Photocrosslinking reaction was performed, after water evaporation, by UV-irradiation under inert atmosphere.

Since the methacrylic peak signal at 1638 cm⁻¹ is overlapped with the peak of tightly bound water (already present in the native starch), FTIR analysis to follow the UV-Curing process kinetics was not possible. For this reason, the efficiency of curing was evaluated by measuring the insoluble content (Gel%) at different irradiation time. As shown in Figure 1b, the increase of irradiation time leads to an increment of the gel fraction, thus confirming the network formation. The equilibrium Gel% value (83%) was reached after 15 min. However, it can be stressed that after 10 min, the insoluble fraction is already above 78%. The obtained Gel% values are comparable with those reported in literature for the cross-linked starch with sodium benzoate (85%) [34]. Nevertheless, previous works used DMSO as a solvent to estimate the film insoluble fraction. However, DMSO requires several washes to be completely removed. In this work, to avoid those passages, water was used as an extraction solvent in which MS was originally soluble.

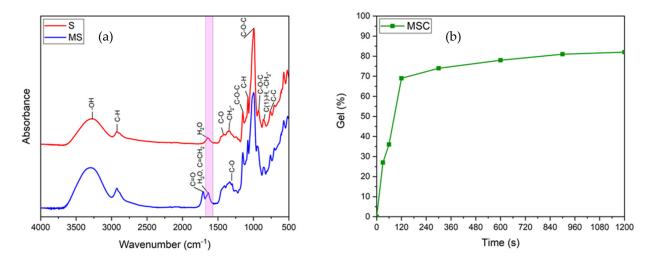
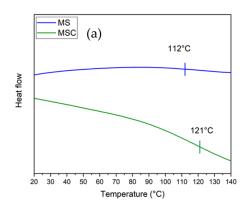


Figure 1. (a) FTIR spectra of Starch (S) and methacrylated starch (MS); (b) Evaluation of gel content after different UV-curing times for MSC films.

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3.2. Thermal and Mechanical Properties

Thermal and mechanical properties of both uncured casted films of methacrylated starch (MS) and UV-cured methacrylated starch coatings (MSC) were evaluated in order to show the effect of crosslinking reaction on the final performance of the coatings. The DSC and tensile test are presented in Figure 2a,b, respectively, and the properties are summarized in Table 1.



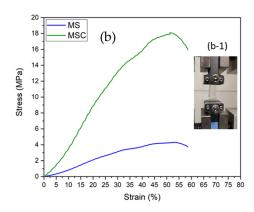


Figure 2. (a) DSC thermogram of MS and MSC; (b) Stress-strain curve of MS and MSC. (b-1) tensile fracture image.

Table 1. Thermal and mechanical properties of the MSC.

Sample	T _g (°C)	Young's Modulus (MPa)	Elongation at Break (%)	Ultimate Tensile Strength (MPa)
MS	112	9.4 ± 0.9	49 ± 12 48 ± 15	4.3 ± 1.2
MSC	121	39.3 ± 5.7		18.1 ± 2.9

In Figure 2a the DSC thermograms are reported respectively for MS and MSC, showing an important enhancement of the glass transition temperature (T_g) in the case of the UV-cured coatings. This can be attributed to the network formation upon UV-irradiation which hindered the chain mobility with the consequent enhancement of the T_g value. Those T_g values are similar to the ones obtained in literature for other crosslinked high amylose maize starch systems [46].

The Young's modulus (*E*) of both MS and MSC was evaluated by the slope of the initial part of the stress–strain curve (Figure 2b). It can be clearly seen that after the irradiation, the mechanical properties of the starch films were enhanced. In fact, for the MSC films the Young's modulus and the ultimate tensile strength are increased by 420%, while the elongation at break remains unchanged. These results can also be ascribed to the cross-linking reaction. These achieved values are comparable with the reported one of gellan/gelatin composite films [47] and higher than those reported for the crosslinked neat cassava and wheat starch with sodium benzoate [34,36]. By observing the data reported in Table 1 we can conclude that the crosslinking reaction improves the final performance of the starch-based coatings, and the UV-curing process is quite efficient.

3.3. Surface Properties of the UV-Cured Coatings

The UV-cured MSC coatings were visually perfectly transparent (Figure 3a). The surface properties of the MSC UV-cured coating were evaluated by means of pencil hardness, surface adhesion, solvent resistance and surface tension.

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Figure 3. (a) The fully transparent MSC coating on a glass substrate; (b) images of water and hexadecane drops on the surface of MSC.

MSC illustrated high pencil hardness corresponding to 7H (Table 2). This value is higher than the ones reported in literature for other fully biobased coatings [48,49]. Since it was previously reported that the pencil hardness depends on the flexibility of the polymeric chains, the high values obtained by MSC can be ascribed to the presence of a large quantity of rigid glucose rings in the starch polymer. Furthermore, the crosslinking reaction may have contributed to enhancing the film hardness [50].

Table 2. Surface properties of the UV-cured MSC coating.

Sample	Pencil Hardness	Adhesion (%)	MEK Resistance	Water Contact Angle (°)	Hexadecane Contact Angle (°)	γ (mN/m)
MSC	7H	99	>200	85 ± 5	24.8 ± 4	29.8

The MSC coating adhesion was evaluated with the scratch test following the ASTM D3359-B process. MSC coatings showed excellent surface adhesion on glass (Table 2). Different works have previously investigated the possible adhesion mechanisms. The most common mechanisms are mechanical coupling, molecular bonding, and thermodynamic adhesion. The molecular bonding mechanism is based on intermolecular forces such as dipole-dipole and Van der Waals forces [51]. The very good adhesion of UV-cured MSC coatings on glass substrate could be explained considering the high number of hydroxyl groups present in the starch chains able to form a large number of hydrogen bonding with the substrate.

The chemical resistance of the UV-cured MSC was evaluated by the solvent rub resistance test. This type of test correlates, in a qualitatively way, the resistance of the coating to a specific solvent (MEK) with the curing degree. MEK is a suitable solvent for many polymers, including starch. This method is commonly used in industry where the crosslinking degree of coatings cannot be evaluated by conventional laboratory instruments, such as FTIR. MSC coatings possessed high MEK resistance (Table 2), which could be attributed to a high curing degree. As mentioned before the degree of curing could not be evaluated by FTIR analysis, but both MEK resistance and the high gel content values previously discussed as well as the important enhancement of $T_{\rm g}$ and modulus upon UV-irradiation, support the formation of a tightly crosslinked network.

The MSC water contact angle value was around 85° (see Figure 3b), which is higher than the values reported in literature for starch-based films [52]. This hydrophobicity enhancement can be ascribed to the crosslinking reaction. The hexadecane contact angle was also evaluated (Figure 3b) to quantitatively characterize the surface energy of the coating (γ) . The fabricated MSC coating possessed quite a low surface tension value: $29.8 \, \text{mN/m}$, calculated using OWRK model (Table 2). The low γ value indicates poor wetting capability. This may result in improved antifouling properties [53].

3.4. Enzymatic Degradation

In order to assess the effect of curing on the biodegradability, the MS and MSC coatings were subjected to an enzymatic degradation test. The term biodegradation may be defined as "gradual breakdown of a material mediated by a specific biological activity" [54].

In particular, this work evaluated the susceptibility of starch-based coatings to enzymatic degradation by α -amylase (from *Bacillus licheniformis*) enzyme. *B. licheniformis* is a gram-positive thermophilic bacterium commonly present in soil [55]. The choice of this

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particular enzyme aims to lay the foundations for further composting experiments for the crosslinked coatings.

 α -amylases are enzymes able to split the α -1,4 glycosidic linkage in polysaccharides leading to low-molecular-weight products like glucose, maltose, and maltotriose [56]. For this reason, the starch films degradation was evaluated by quantifying the concentration of glucose and maltose present in the starch–enzyme solution at different time points. The results for the uncured MS film and for the UV-cured MSC are collected in Figure 4a,b, respectively, showing the glucose and maltose formation upon enzymatic degradation. The tested films started to fragment already after 4 days of incubation.

The concentrations of both glucose and maltose were quite similar in the MS and MSC supernatants. Indeed, significant differences (* p < 0.05) were observed only for maltose concentration at 7 days, where a higher amount was measured in MSC supernatants. This strongly indicates that the effect of the crosslinking reaction on the enzymatic degradation kinetics of starch-based film was negligible. In Figure 4b, it is possible to observe a sharp decrease of maltose concentration after 14 days of incubation, while the glucose concentration shows a constant linear increase (with significant differences—p > 0.05—among each time point). It thus seems that the α -amylase can ultimately degrade maltose to glucose if left to react for a longer period. After 14 days, no solid films remained.

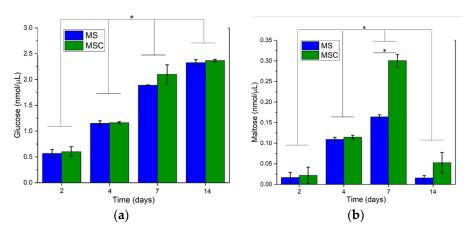


Figure 4. The amount of (a) glucose and (b) maltose formed during enzymatic degradation of MS and MSC. Significant increase of maltose and glucose was observed at the different time points. The sample MSC did not show any significant difference compared to MS except for values of maltose at 7 days (* p < 0.05).

4. Conclusions

Starch was successfully methacrylated with methacrylic anhydride and the methacrylate functionalities were exploited during the UV-curing process. The UV-curing resulted in stable starch-based coatings. The efficiency of UV-curing was evaluated by measuring the insoluble content (Gel%) after different irradiation time. A plateau corresponding to the formation of an almost insoluble network (79%) was reached after about 10 min of irradiation. The UV-crosslinking reaction improved the final performance of the starch-based MSC coating, with a 10 °C enhancement of T_g (121 °C) and 420% increase in Young's modulus (39 MPa) and the ultimate tensile strength (18 MPa) with respect to the uncured MS.

The MSC coating possesses high pencil hardness (7H), excellent adhesion (99%), and good solvent MEK resistance (>200). The susceptibility of MS and MSC to biodegradation by α -amylase (from *Bacillus licheniformis*) was evaluated and compared. The results show that the degradation velocity was not affected by the crosslinking reaction.

Therefore, we have demonstrated the possibility to exploit methacrylic functionalization of starch to achieve new types of UV-cured coatings. The preliminary enzymatic degradation results are encouraging and will be further implemented by compostability evaluation.

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