

Article

Finite Element Analysis of Thermo-Diffusion and Multi-Slip Effects on MHD Unsteady Flow of Casson Nano-Fluid over a Shrinking/Stretching Sheet with Radiation and Heat Source

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Abstract: In this article, we probe the multiple-slip effects on magnetohydrodynamic unsteady Casson nano-fluid flow over a penetrable stretching sheet, sheet entrenched in a porous medium with thermo-diffusion effect, and injection/suction in the presence of heat source. The flow is engendered due to the unsteady time-dependent stretching sheet retained inside the porous medium. The leading non-linear partial differential equations are transmuted in the system of coupled nonlinear ordinary differential equations by using appropriate transformations, then the transformed equations are solved by using the variational finite element method numerically. The velocity, temperature, solutal concentration, and nano-particles concentration, as well as the rate of heat transfer, the skin friction coefficient, and Sherwood number for solutal concentration, are presented for several physical parameters. Next, the effects of these various physical parameters are conferred with graphs and tables. The exact values of flow velocity, skin friction, and Nusselt number are compared with a numerical solution acquired with the finite element method (FEM), and also with numerical results accessible in literature. In the end, we rationalize the convergence of the finite element numerical solution, and the calculations are carried out by reducing the mesh size.

Keywords: MHD; FEM; Casson nano-fluid; heat source; multiple slip; porous medium

1. Introduction

The basic idea of the non-slip condition is concerned with the Navier Stokes theory. To study the temperature and velocity, numerous authors have found both the analytical and numerical solution by the implementation of non-slip boundary conditions. The utmost significance of slip-conditions in nano-channels has stimulated, to a great extent, interest in the study of vibrating values [1]. Now it is not unknown that if fluid contains concentrated suspensions, in that case the slip could be stirring. Soltani and Yilmazer [2] have performed by parallel disk rheometer with prominence on the wall slip phenomena on the rheological characterization of extremely filled suspensions consisting of Newtonian matrix and diverse with two different power sizes of aluminum and two different sizes of bed glass. In the articulations of fluid-like as suspension, emulsion foams, and polymer solution,



partial velocity slip can occur on the stretching boundary. In an assortment of industry procedures, the influences of slip can crop-up at the boundary of pipes, surfaces, and walls. The Navier Stoke velocity slip conditions are customary to approach in the study of slip phenomenon.

There are hundreds of applications in industries and engineering, and magneto-hydrodynamic fluid flows through stretching sheet have achieved much importance in recent days, according to Mabbod et al. [3]. Applications as well as the liquid coating on the photographic films, boundary layers throughout the liquid film in the concentration procedure, and the aerodynamic excrescence of plastic sheets exist. With this, the extensive range of applications of magnetohydrodynamic flow that can be found in copious fields like in electronic cooling process, in boilers, heat lagging, and metal extrusion, geothermal system, nuclear process, micro-magnetohydrodynamic pumps, underground water system, in energy storage units, biological conveyance, and in the thermal energy procedure has played a very important role. Unsteady flow due to the stretching sheet has been scrutinized by Pop and Na [4]. Afterward, Sheridan et al. [5] investigated the significance of variable wall temperature and variable heat flux in the boundary layer flow over the unsteady stretching surface with similarity transformation. An unsteady stagnation point flow of the viscous fluid caused by a stretching sheet under the influence of slip condition has been reported by Bhattacharyya et al. [6]. The impact of the magnetic field on the two-dimensional flow of nano-fluid with and without slip condition was conferred by Khan et al. [7] and Mohyud-Din et al. [8,9], correspondingly. Khan et al. [10] investigated two-dimensional electrically conducting a flow of nano-fluid due to the stretching sheet under the impact of convective boundary condition.

The wide-ranging applications of non-Newtonian liquids in numerous industries such as molten plastics, nuclear waste disposal, artificial fibers, foodstuffs, transpiration cooling, and petroleum reservoirs have gained fascination to analyze their characteristic comportment. Casson fluid is one sort of fluid model for non-Newtonian fluid. Casson fluid has an inestimable viscosity at zero rates of shear and have zero viscosity at an infinite rate of shear and the yield stress under which there is no flow occurs. Consequently, Casson-fluid could be defined such as shear-thinning liquid or pseudo-plastic fluid. The flow characteristic of blood can precisely be defined by Casson fluid at the small shear rates. Sharada and Shankar [11] scrutinized numerically Soret and Dufour effects, thermal radiation, and chemical reaction on fluid flow, and heat and mass transfers of Casson fluid over an exponentially stretching surface. Ullah et al. [12] observed that unsteady MHD diverse convection slip flow of Casson fluid towards non-linearly stretching sheet soaked in a porous medium in existence of slip and convective boundary conditions occurs. Furthermore, Ullah et al. [13] acquired numerical results for hydro-magnetic Falkner Skan flow of the Casson fluid past a moving wedge, along with heat transfer. Pushpalatha et al. [14] deliberated thermal diffusion effects and radiation on Casson-fluid flow with convective boundary conditions. Pushpalatha et al. [15] deliberated the thermos-diffusion consequences on the Casson fluid over an unsteady stretching surface in the existence of thermal radiations and the magnetic field. They found that the Casson parameters and unsteadiness parameter have the propensity to denigrate the velocity dissemination. Uddin et al. [16] studied the free convective boundary layer flow of nano-fluid over a penetrable upward horizontal plate in a porous medium with thermal convective boundary conditions.

Recently, Rahman et al. [17] explored the hydro-magnetic slip flow of water-based nano-fluid over a wedge with a convective surface in the existence of heat generation or absorption. Ibrahim and Shankar [18] analyzed magneto-hydrodynamic boundary layer flow and heat transfer of nano-fluid past over penetrable stretching sheet using velocity, thermal, and solute slip boundary conditions. Das [19] presented an imperative numerical inquiry on the convective heat transfer performance of nanofluids over a penetrable stretching surface in the presence of partial slip, thermal buoyancy, and internal heat generation/absorption. The transfer of heat, investigated through the thermal radiation, has enormous applications in different technical processes, satellites, nuclear power-plants, astronomical vehicles, gas turbines, comprising missiles, and in several propulsion devices for jets. Linear radiations are not systematically in effect for the enormous temperature alteration. Abbas et al. [20] deliberated the consequences of radiation in the existence of a uniform magnetic field of nano-fluid on the curved stretching surface by integrating the slip effect. In recent times, Makinde et al. [21] deliberated a numerical study of the effects of radiation on chemically reacting MHD nano-fluid prejudiced by the heat source/sink, and the collective heat and mass transfer analysis aimed at mixed convection flow over the vertical surface, with radiation and chemical reaction explained by Ibrahim et al. [22]. Prasannakumara et al. [23] deliberated the velocity slip effects, temperature jump, solutal slip, and thermal radiation, on steady flow, and the transfer of heat and mass of incompressible Jeffrey nano-fluid over the horizontal stretching surface. Imtiaz et al. [24] scrutinized the unsteady MHD flow of the curved stretching surface.

The literature remains silent whether we have to investigate the impact of multiple slips on MHD unsteady Casson nano-fluid flow, heat, and mass transfer in the presence of heat source with thermo-diffusion effect over a stretching/shrinking sheet. The objective of this article was to prolong the recent work of Fazle Mabood and Standford Shateyi [25]. Appropriate similarities have been used for transformation, and the governing non-linear partial differential equations are rendered in the non-dimensional and non-linear system of ODEs. The resulting system of non-linear ODEs has been solved numerically with an efficient and validated variational finite element method (FEM) with the boundary conditions. We also use a special case for the existing model to compare our outcomes along with previous studies. A parametric study has been performed to inquire into the mass and heat transfer characteristics and also the impact of different parameters of the flow. After that, we have provided a numerical comparison of our results and discussed them with graphs. In future studies, transient flow with slip effects in the presence of mixed convection and chemical reaction at the sheet can be examined.

2. Mathematical Modeling

The unsteady two-dimensional MHD flow of an incompressible fluid and Casson nano-fluid viscous flow over an electrically conducted stretching/shrinking sheet in the presence of heat source was considered. We choose an xy-ordinate system as the measurement of the sheet will be taken with x-, y-axis, and the y-axis along the vertical direction of the sheet, as given in Figure 1. The sheet is moving with non-uniform velocity $U(x, t) = ax/(1 - \lambda t)$ since *a* is the stretching rate along the *x*-axis but λt is positively constant, as by property $\lambda t < 1$. The transverse magnetic field is supposed be the function of distance from the origin and is defined as $B(x) = B_0\sqrt{x}$ with $B_0 \neq 0$, where B_0 is the strength of the magnetic field. The induced magnetic field is negligible as compared to the applied magnetic field. The free stream temperature is supposed to be T_{∞} , the free mass concentration is C_{∞} , and the nano-particle concentration is E_{∞} . The governing equations for flow can be put into the form as in ([25,26])

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \tag{1}$$

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = v(1 + \frac{1}{\beta}) \frac{\partial^2 u}{\partial u^2} - \frac{\sigma B^2(x)u}{\rho} + g\beta_T(T - T_\infty) + g\beta_C(C - C_\infty) + g\beta_E(E - E_\infty) - \frac{v}{\kappa'}u$$
(2)

$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \left(1 + \frac{16T_{\infty}^3 \sigma^*}{3k^* \kappa}\right) \frac{\partial^2 T}{\partial y^2} + \tau \left[D_B \frac{\partial E}{\partial y} \frac{\partial T}{\partial y} + \frac{D_T}{T_{\infty}} \left(\frac{\partial T}{\partial y}\right)^2\right] + \frac{Q(T - T_{\infty})}{\rho C_p} + D_{TC} \frac{\partial^2 C}{\partial y^2}$$
(3)

$$\frac{\partial C}{\partial t} + u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} = D_m \frac{\partial^2 C}{\partial y^2} + D_T \frac{\partial^2 T}{\partial y^2}$$
(4)

$$\frac{\partial E}{\partial t} + u \frac{\partial E}{\partial x} + v \frac{\partial E}{\partial y} = D_B \frac{\partial^2 E}{\partial y^2} + \frac{D_T}{T_\infty} \frac{\partial^2 T}{\partial y^2}$$
(5)

where *x* and *y* are the co-ordinates in the *x*-axis and *y*-axis; *u* and *v* are the velocity components along the *x*-axis and *y*-axis respectively; α , ν , σ , ρ are the thermal diffusivity, kinetic viscosity,

electrical conductivity, and density of fluid, respectively; *g* is the acceleration due to gravity; β_T is the thermal expansion coefficient; β_C is the solutal concentration expansion coefficient; β_E is the nano-particle concentration expansion coefficient; *T* is the temperature; *C* is the solutal concentration; *E* is the nano-particle concentration; D_M is the molecular diffusivity; D_T is the thermal diffusivity; D_B is the Brownian diffusivity; σ^* is the Stefan-Boltzmann constant; k^* is the mean absorption coefficient; T_{∞} is the stream temperature; *Q* is the uniform volumetric heat generation/absorption; C_p is the specific heat of fluid; C_s is the concentration of susceptibility; and K_T is the thermal diffusion ratio. The boundary conditions for the above mathematical model are (see [25]):

$$u = U(x,t) + U_{slip}, v = v_w, T = T_w(x,t) + T_{slip}, C = C_w(x,t) + C_{slip}, E = E_w(x,t) + E_{slip},$$

$$as \quad y = 0$$
(6)

$$u \to 0, T \to T_{\infty}, C \to C_{\infty}, E \to E_{\infty}, \quad as \quad y \to \infty,$$
 (7)

where *x* and *y* are the co-ordinates; *u* and *v* are the velocity components along the *x*-axis and *y*-axis, respectively; α , ν , σ , ρ are the thermal diffusivity, kinetic viscosity, electrical conductivity and density of fluid, respectively; *g* is the acceleration due to gravity; β_T is thermal expansion coefficient; β_C is the solutal concentration expansion coefficient; β_E is the nano-particle concentration expansion coefficient; *T* is the temperature; *C* is the solutal concentration; *E* is the nano-particle concentration; *D*_M is the molecular diffusivity; *D*_T is the thermal diffusivity; *D*_B is the Brownian diffusivity; σ^* is the Stefan-Boltzmann constant; k^* is the mean absorption coefficient; *T*_∞ is the stream temperature; *Q* is the uniform volumetric heat generation/absorption; *C*_p is the specific heat of fluid; *C*_s is the concentration of susceptibility; and *K*_T is the thermal diffusion ratio.

Where the injection/suction velocity as $v_w = v_0/\sqrt{x}$, $T_w(x,t)$ is the temperature of sheet and $C_w(x,t)$, $E_w(x,t)$ are concentrations at surface of the below form (see [25]):

$$T_w(x,t) = T_{\infty} + T_0 \left(\frac{ax}{2\nu(1-\lambda t)^2}\right)$$
$$C_w(x,t) = C_{\infty} + C_0 \left(\frac{ax}{2\nu(1-\lambda t)^2}\right)$$
$$E_w(x,t) = E_{\infty} + E_0 \left(\frac{ax}{2\nu(1-\lambda t)^2}\right)$$

where T_0 , C_0 , and E_0 are the reference temperature, reference solutal concentration, and reference nano-particle concentration respectively, such that $0 \le T_0 \le T_w$, $0 \le C_0 \le C_w$ and $0 \le E_0 \le E_w$, with these above expressions being valid if $(1 - \lambda t) > 0$.

Usually, the stream function Ψ is defined as $u = \frac{\partial \Psi}{\partial y}$ and $v = -\frac{\partial \Psi}{\partial x}$ that the Equation (1) is satisfied. We introduce similarity transformations to solve the above equations (see [25,26]):

$$\eta = \sqrt{\frac{a}{\nu(1-\lambda t)}} y, \quad \psi = \sqrt{\frac{a\nu}{(1-\lambda t)}} x f(\eta), \quad \theta(\eta) = \frac{T-T_{\infty}}{T_w - T_{\infty}},$$
$$\phi(\eta) = \frac{C-C_{\infty}}{C_w - C_{\infty}}, \quad \xi(\eta) = \frac{E-T_{\infty}}{E_w - E_{\infty}}$$
(8)

In view of the above similarity transformations of Equation (7), PDEs from (1)–(5) transform into the following system of nonlinear ODEs:

$$(1+\frac{1}{\beta})f''' + ff'' - f'^2 - \sigma(\frac{\eta}{2}f'' + f') - Mf' + \lambda_1\theta + \lambda_2\phi + \lambda_3\xi - k_pf' = 0,$$
(9)

$$(1+R)\frac{1}{Pr}\theta'' - f'\theta + f\theta' - \sigma\left(\frac{\eta}{2}\theta' + 2\theta\right) + Nb\phi'\theta' + Nt\theta'^2 + Q\theta + N_d\phi'' = 0$$
(10)

$$\frac{1}{Sc}\phi'' - f'\phi + f\phi' - \sigma\left(\frac{\eta}{2}\phi' + 2\phi\right) + S_r\theta'' = 0$$
(11)

$$\xi'' - Le\left[f'\xi - f\xi' + \sigma\left(\frac{\eta}{2}\xi' + 2\xi\right)\right] + \frac{Nt}{Nb}\theta'' = 0$$
(12)

for the above problem the transformed boundary conditions are:

$$f(0) = f_w,$$

$$f'(0) = 1 + S_f f''(0),$$
(13)

$$\theta(0) = 1 + S_{\theta} \theta'(0), \tag{14}$$

$$\phi(0) = 1 + S_{\phi} \phi'(0), \tag{15}$$

$$\xi(0) = 1 + S_{\xi}\xi'(0), \tag{16}$$

$$f'(\infty) \to 0, \theta(\infty) \to 0, \phi(\infty) \to 0, \xi(\infty) \to 0,$$
 (17)

where unsteadiness parameter $\sigma = \lambda/a$, M is the magnetic field parameter, Pr is the Prandtl number, Nb is the Brownian motion parameter, Nt is the thermo-phoresis parameter, β is the Deborah number, Sc is the Schmidt number, R is the thermal radiation parameter, λ_1 , λ_2 , and λ_3 are the buoyancy parameters, k_p is the permeability parameter, Nd is the Dufour parameter, Sr is the Soret parameter, and f_w is the Suction/injection parameter.

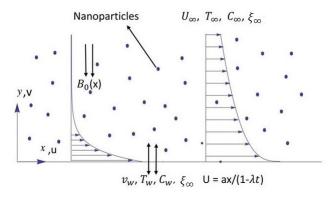


Figure 1. Physical sketch with xy-coordinates.

The primes show the differentiation with respect to η . The parameters used in Equations (8)–(11) are explained as:

 $M = \left[\frac{\sigma(1-\lambda t)}{\rho a}B_{0}\right]^{1/2}, Pr = \nu/\alpha, Nb = \tau D_{B}(C_{w}-C_{\infty})/\nu, Nt = (\tau D_{T}(T_{w}-T_{\infty})/\nu T_{\infty}, \beta = k_{0}a/(1-\lambda t), Sc = \frac{\nu}{D_{m}}, Le = \frac{\sigma}{D_{B}}, R = (16\sigma^{*}T_{\infty}^{3})/(3k^{*}K), \sigma = \lambda/a, \lambda_{1} = (g\beta_{T}T_{0})/(2a\nu), \lambda_{2} = (g\beta_{C}C_{0})/(2a\nu), \lambda_{3} = (g\beta_{E}E_{0})(2a\nu), Sr = (D_{T}T_{0})/\nu C_{0}, N_{d} = (D_{m}K_{T}C_{0})/(C_{s}C_{p}T_{0}), k_{p} = \nu(1-\lambda t)/a, f_{w} = -v_{w}(1-\gamma t)^{1/2}/(\nu a)^{1/2},$

Also, the local skin friction co-efficient, local Nusselt number, and local Sherwood number are explained as below

$$C_f = \frac{\mu}{\rho(U_w)^2} \left(\frac{\partial u}{\partial y}\right)_{y=0} \tag{18}$$

$$N_{u} = \frac{x}{k(T - T_{\infty})} \left[k \left(\frac{\partial T}{\partial y} \right)_{y=0} - \frac{4\sigma_{*}}{3k_{*}} \left(\frac{\partial T^{4}}{\partial y} \right)_{y=0} \right]$$
(19)

$$Sh = -\frac{x}{(C - C_{\infty})} \left(\frac{C}{\partial y}\right)_{y=0}$$
(20)

when Equation (7) is substituted into Equations (17)–(19), the final dimensionless form is obtained; $C_{fr} = (Re_x)^{1/2} = f''(0), N_{ur} = N_u/(Re_x)^{1/2} = -(1+R)\theta'(0), Shr = Sh/(Re_x)^{1/2} = -\phi'(0)$ where the local Reynolds number is Re_x , reduced skin friction is Cfr, reduced Nusselt number is Nur, and the reduced Sherwood number is *Shr*.

3. Finite Element Method Solutions

We solve the system of non-linear boundary value problem that is given in Equations (8)–(11) numerically by applying the finite element method (FEM) subjected with the boundary conditions (12)–(16). The FEM is extremely effectual and has been applied to study different problems in fluid mechanics, CFD, mass transfer, heat transfer, solid mechanics, and also in many other fields. The general detail of the finite element method (FEM) can be found in Raddy [26–28]. Reddy [29] gives a general detail of the variational finite element method, which also found that the finite element method (FEM) is employed in commercial software like ADINA, ANSYS, MATLAB, and ABAQUS. Swapna et al. and Rana et al. [30,31] explain that the variational finite element method solves the boundary value problem very efficiently and accurately. To solve the non-linear boundary value problem (8)–(11) by using finite element method (FEM), along with boundary conditions (12)–(16), to apply FEM, first we have to consider:

$$f' = g. \tag{21}$$

The Equations (8)–(11) take the form

$$(1+\frac{1}{\beta})g'' + fg' - g^2 - \sigma(\frac{\eta}{2}g' + g) - Mg + \lambda_1\theta + \lambda_2\phi + \lambda_3\xi - k_pg = 0,$$
 (22)

$$(1+R)\frac{1}{Pr}\theta'' - g\theta + f\theta' - \sigma\left(\frac{\eta}{2}\theta' + 2\theta\right) + Nb\phi'\theta' + Nt\theta'^2 + Q\theta + N_d\phi'' = 0$$
(23)

$$\frac{1}{Sc}\phi'' - g\phi + f\phi' - \sigma\left(\frac{\eta}{2}\phi' + 2\phi\right) + S_r\theta'' = 0$$
(24)

$$\xi'' - Le\left[g\xi - f\xi' + \sigma\left(\frac{\eta}{2}\xi' + 2\xi\right)\right] + \frac{Nt}{Nb}\theta'' = 0,$$
(25)

The corresponding boundary conditions now reduce to the following form:

$$f(0) = f_w, g(0) = 1 + S_f g'(0), \theta(0) = 1 + S_\theta \theta'(0), \quad \phi(0) = 1 + S_\phi \phi'(0),$$

$$\zeta(0) = 1 + S_{\xi}\zeta'(0), \tag{26}$$

$$h(\infty) \to 0, \theta(\infty) \to 0, \phi(\infty) \to 0, \xi(\infty) \to 0,$$
 (27)

3.1. Variational Formulations

The variational formulation is associated with Equations (20)–(24) over a linear element (η_c , η_{c+1}) is given by

$$\int_{\eta_c}^{\eta_{c+1}} w_1\{f'-g\}d\eta = 0,$$
(28)

$$\int_{\eta_c}^{\eta_{c+1}} w_2\{(1+\frac{1}{\beta})g'' + fg' - g^2 - \sigma(\frac{\eta}{2}g' + g) - Mg + \lambda_1\theta + \lambda_2\phi + \lambda_3\xi - k_pg\}d\eta = 0,$$
(29)

$$\int_{\eta_c}^{\eta_{c+1}} w_3\{(1+R)\frac{1}{Pr}\theta'' - g\theta + f\theta' - \sigma\left(\frac{\eta}{2}\theta' + 2\theta\right) + Nb\phi'\theta' + Nt\theta'^2 + Q\theta + N_d\phi''\}d\eta = 0, \quad (30)$$

$$\int_{\eta_c}^{\eta_{c+1}} w_4 \{ \frac{1}{Sc} \phi'' - g\phi + f\phi' - \sigma \left(\frac{\eta}{2} \phi' + 2\phi \right) + S_r \theta'' \} d\eta = 0,$$
(31)

$$\int_{\eta_c}^{\eta_{c+1}} w_5\{\xi'' - Le\left[g\xi - f\xi' + \sigma\left(\frac{\eta}{2}\xi' + 2\xi\right)\right] + \frac{Nt}{Nb}\theta''\}d\eta = 0,$$
(32)

where w_1, w_2, w_3, w_4 , and w_5 are weight functions and maybe viewed as variations in f, g, θ , ϕ , ξ resp.

3.2. Finite Element Formulations

The equation of finite element model that is gained from the Equations (27)–(31) by exchanging the FEM approximation in the form:

$$\bar{f} = \sum_{j=1}^{3} \bar{f}_{j}^{e} \psi_{j}^{e}, \ \bar{g} = \sum_{j=1}^{3} \bar{g}_{j}^{e} \psi_{j}^{e}, \ \bar{\theta}' = \sum_{j=1}^{3} \bar{\theta}_{j}'^{e} \psi_{j}^{e}, \ \bar{\phi}' = \sum_{j=1}^{3} \bar{\phi}_{j}'^{e} \psi_{j}^{e}$$
(33)

with $w_1 = w_2 = w_3 = w_4 = w_5 = \psi_i^e$ (*i* = 1, 2, 3), where the shape function ψ_i^e are the shape functions for the element (η_c , η_c + 1) and are taken as

$$\psi_{1}^{e} = \frac{(\eta_{c+1} - \eta_{c} - 2\eta)(\eta_{c+1} - \eta)}{(\eta_{c+1} - \eta_{c})^{2}}, \quad \psi_{2}^{e} = \frac{4(\eta - \eta_{c})(\eta_{c+1} - \eta)}{(\eta_{c+1} - \eta_{c})^{2}}, \quad (34)$$
$$\psi_{3}^{e} = -\frac{(\eta_{c+1} - \eta_{c} - 2\eta)(\eta - \eta_{c})}{(\eta_{c+1} - \eta_{c})^{2}}, \quad \eta_{c} \le \eta \le \eta_{c+1}.$$

Therefore, the finite element model equations are given by

$$\begin{bmatrix} W^{11} & [W^{12}] & [W^{13}] & [W^{14}] & [W^{15}] \\ [W^{21}] & [W^{22}] & [W^{23}] & [W^{24}] & [W^{25}] \\ [W^{31}] & [W^{32}] & [W^{33}] & [W^{34}] & [W^{35}] \\ [W^{41}] & [W^{42}] & [W^{43}] & [W^{44}] & [W^{45}] \\ [W^{51}] & [W^{52}] & [W^{53}] & [W^{54}] & [W^{55}] \end{bmatrix} \begin{bmatrix} f \\ g \\ \theta \\ \xi \end{bmatrix} = \begin{bmatrix} b_1 \\ b_2 \\ b_3 \\ b_4 \\ b_5 \end{bmatrix}$$
(35)

where $[W^{mn}]$ and b^m (m,n = 1,2,3,4,5) are the matrices and are given as:

$$\begin{split} [W_{ij}^{11}] &= \int_{\eta_c}^{\eta_{c+1}} \psi_i^e \frac{d\psi_j^e}{d\eta} d\eta, \\ W_{ij}^{12} &= -\int_{\eta_c}^{\eta_{c+1}} \psi_i^e \psi_j^e d\eta, \\ [W_{ij}^{22}] &= -(1+\frac{1}{\beta}) \int_{\eta_c}^{\eta_{c+1}} \frac{d\psi_i^e}{d\eta} \frac{d\psi_j^e}{d\eta} d\eta + \int_{\eta_c}^{\eta_{c+1}} \bar{f} \psi_i^e \frac{d\psi_j^e}{d\eta} d\eta - \int_{\eta_c}^{\eta_{c+1}} \bar{g} \psi_i^e \psi_j^e d\eta - A \frac{\eta}{2} \int_{\eta_c}^{\eta_{c+1}} \psi_i^e \frac{d\psi_j^e}{d\eta} d\eta \\ &- \int_{\eta_c}^{\eta_{c+1}} \bar{g} \psi_i^e \psi_j^e d\eta - A \int_{\eta_c}^{\eta_{c+1}} \psi_i^e \psi_j^e d\eta - M \int_{\eta_c}^{\eta_{c+1}} \psi_i^e \psi_j^e d\eta - k_p \int_{\eta_c}^{\eta_{c+1}} \psi_i^e \psi_j^e d\eta \\ [W_{ij}^{23}] &= \lambda_1 \int_{\eta_c}^{\eta_{c+1}} \psi_i^e \psi_j^e d\eta, \\ W_{ij}^{24} &= \lambda_2 \int_{\eta_c}^{\eta_{c+1}} \psi_i^e \psi_j^e d\eta, \\ W_{ij}^{25} &= \lambda_3 \int_{\eta_c}^{\eta_{c+1}} \psi_i^e \psi_j^e d\eta, \\ \end{split}$$

$$\begin{split} [W_{ij}^{31}] &= 0, \quad [W_{ij}^{32}] = 0, [W_{ij}^{33}] = -(1+R)\frac{1}{Pr}\int_{\eta_c}^{\eta_{c+1}}\frac{d\psi_i^e}{d\eta}\frac{d\psi_j^e}{d\eta}d\eta - \int_{\eta_c}^{\eta_{c+1}}\bar{g}\psi_i^e\psi_j^ed\eta + \int_{\eta_c}^{\eta_{c+1}}\bar{f}\psi_i^e\frac{d\psi_j^e}{d\eta}d\eta \\ &- A\frac{\eta}{2}\int_{\eta_c}^{\eta_{c+1}}\psi_i^e\frac{d\psi_j^e}{d\eta}d\eta - 2A\int_{\eta_c}^{\eta_{c+1}}\psi_i^e\psi_j^ed\eta + Nb\int_{\eta_c}^{\eta_{c+1}}\bar{\phi}'\psi_i^e\frac{d\psi_j^e}{d\eta}d\eta \\ &+ Nt\int_{\eta_c}^{\eta_{c+1}}\bar{\theta}'\psi_i^e\frac{d\psi_j^e}{d\eta}d\eta + Q\int_{\eta_c}^{\eta_{c+1}}\psi_i^e\psi_j^ed\eta, \quad [W_{ij}^{34}] = -Nd\int_{\eta_c}^{\eta_{c+1}}\frac{d\psi_i^e}{d\eta}\frac{d\psi_j^e}{d\eta}d\eta, [W_{ij}^{35}] = 0, \end{split}$$

$$\begin{split} [W_{ij}^{41}] &= [W_{ij}^{42}] = 0, \quad [W_{ij}^{43}] = -Sr \int_{\eta_c}^{\eta_{c+1}} \frac{d\psi_i^e}{d\eta} \frac{d\psi_j^e}{d\eta} d\eta, \\ [W_{ij}^{44}] &= -\frac{1}{Sc} \int_{\eta_c}^{\eta_{c+1}} \frac{d\psi_i^e}{d\eta} \frac{d\psi_j^e}{d\eta} d\eta + \int_{\eta_c}^{\eta_{c+1}} \bar{f}\psi_i^e \frac{d\psi_j^e}{d\eta} d\eta - \int_{\eta_c}^{\eta_{c+1}} \bar{g}\psi_i^e \psi_j^e d\eta d\eta \\ &- A\frac{\eta}{2} \int_{\eta_c}^{\eta_{c+1}} \psi_i^e \frac{d\psi_j^e}{d\eta} d\eta - 2A \int_{\eta_c}^{\eta_{c+1}} \psi_i^e \psi_j^e d\eta, \\ [W_{ij}^{45}] &= [W_{ij}^{51}] = [W_{ij}^{52}] = [W_{ij}^{54}] = 0, \\ [W_{ij}^{53}] = -\frac{Nt}{Nb} \int_{\eta_c}^{\eta_{c+1}} \frac{d\psi_i^e}{d\eta} \frac{d\psi_j^e}{d\eta} d\eta \end{split}$$

$$[W_{ij}^{55}] = -\int_{\eta_c}^{\eta_{c+1}} \frac{d\psi_i^e}{d\eta} \frac{d\psi_j^e}{d\eta} d\eta + Le \int_{\eta_c}^{\eta_{c+1}} \bar{f} \psi_i^e \frac{d\psi_j^e}{d\eta} d\eta - Le \int_{\eta_c}^{\eta_{c+1}} \bar{g} \psi_i^e \psi_j^e d\eta d\eta - LeA \frac{\eta}{2} \int_{\eta_c}^{\eta_{c+1}} \psi_i^e \frac{d\psi_j^e}{d\eta} d\eta - 2LeA \int_{\eta_c}^{\eta_{c+1}} \psi_i^e \psi_j^e d\eta,$$
(36)

and

$$b_{i}^{1} = 0, \ b_{i}^{2} = -(\psi \frac{dg}{d\eta})_{\eta_{c}}^{\eta_{c}+1}, \ b_{i}^{3} = -(1+R) \frac{1}{Pr} (\psi \frac{d\theta}{d\eta})_{\eta_{c}}^{\eta_{c}+1} - Nd(\psi \frac{d\phi}{d\eta})_{\eta_{c}}^{\eta_{c}+1}, b_{i}^{4} = -\frac{1}{Sc} (\psi \frac{d\phi}{d\eta})_{\eta_{c}}^{\eta_{c}+1} - Sr(\psi \frac{d\theta}{d\eta})_{\eta_{c}}^{\eta_{c}+1}, b_{i}^{5} = -(\psi \frac{d\xi}{d\eta})_{\eta_{c}}^{\eta_{c}+1} - \frac{Nt}{Nb} (\psi \frac{d\theta}{d\eta})_{\eta_{c}}^{\eta_{c}+1},$$

where $\bar{f} = \sum_{j=1}^{3} \bar{f}_{j} \psi_{j}^{e}$, $\bar{g} = \sum_{j=1}^{3} \bar{g}_{j} \psi_{j}^{e}$, $\bar{\theta}' = \sum_{j=1}^{3} \bar{\theta}'_{j} \psi_{j}^{e}$, and $\bar{\phi}' = \sum_{j=1}^{3} \bar{\phi}'_{j} \psi_{j}^{e}$ are assumed to be known.

After the assemblage of element equations, a consequential system of non-linear equations is obtained, after that, it requires an iterative scheme to solve it for an efficient solution. The calculation of f, g, θ , and ϕ are then conceded out for a higher level, and then proceeding until the required 0.00005 is not obtained. The results in Table 1 show the convergency, as we computed, for the increasing number of elements, n = 300, 500, 1000, 1300, 1500, 1800, 1900, 2100. From the results, it is clear that as the number of elements increases further, no significant difference in the values of f, g, θ , ϕ , and ξ can be seen as the number of elements increases beyond 1800, so the outcomes at n = 1800 elements are reported.

Table 1. The convergence of the results of finite element method (FEM) when Pr = 1, $M = \sigma = 0.2$, $\beta = 0.1$, $\lambda_1 = \lambda_2 = \lambda_3 = 0.2$, $S_f = S_{\theta} = S_{\phi} = S_{\xi} = Sr = R = S_g = S_p = 0.5$, $k_P = Nu = Nt = Nb = 0.1$, Sc = 10, Le = 5, $f_w = 0.3$.

Number of Elements	<i>f</i> (3)	g(3)	$\theta(3)$	φ(3)	$\xi(3)$
300	0.82439	0.16241	0.16733	0.06876	0.03046
500	0.82455	0.16250	0.19729	0.06875	0.03046
1000	0.82466	0.16257	0.19726	0.06874	0.03045
1300	0.82469	0.16259	0.19726	0.06873	0.03045
1500	0.82470	0.16260	0.19725	0.06873	0.03045
1800	0.82471	0.16260	0.19725	0.06873	0.03045
1900	0.82472	0.16261	0.19725	0.06874	0.03045
2100	0.82472	0.16261	0.19725	0.06874	0.03045

4. Results and Discussion

The numerical calculations have been performed for the velocity, temperature, solutal, and Casson nano-fluid volume fraction functions for a different assessment of physical parameters, as magnetic parametre M, Prandtl number Pr, Unsteadiness σ , permeability k_p , Brownian motion Nb, thermophoresis Nt, thermal radiation R, Dufour Nd, Schmidt Sc, buoyancy $\lambda_1, \lambda_2, \lambda_3$, Suction/Injection f_w , Soret Sr, Lewis number Le, hydro-dynamic slip S_f , thermal slip S_θ , solutal slip S_ϕ , and nano-particles concentration slip S_{ξ} .

The detail of the present results and the appraisal of flow velocity is made with the exact solution that is given by Crane [32] as $f(\eta) = 1 - e^{(-\eta)}$ under the special case $(M = 0, \sigma = 0, \beta \rightarrow \infty, \lambda_1 = \lambda_2 = \lambda_3 = 0, S_f = 0, f_w = 0, kp = 0)$. The finite element method's outcomes have decent concurrence with the exact solution, which approves the validity of the finite element method. It can be seen clearly in Table 2, and in Table 3, that the skin friction coefficient attained by the finite element method is equivalent to the numerical outcomes of Gireesha et al. [33] and the exact solution of Mudassar et al. [34] under special case $\sigma = 0, \beta = 0, \lambda_1 = \lambda_2 = \lambda_3 = 0, S_f = 0, f_w = 0, kp = 0$. To confirm the accuracy of the presented numerical results, the results obtained by the finite element method for skin friction co-efficient for steady and unsteady flow have been compared with the numerical results that have previously been reported in studies and shown in Table 4. Regarding our results, there is admirable conformity among our outcomes and previously available research articles, which approves the cogency and the accuracy of the current results that are obtained by the finite element method (FEM). Table 5 describes the results of the heat transfer rate that are acquired by the finite element method, which are compared with the results of earlier studies and with the accurate solution of Ishak et al. [35] in a special case (Nt = Nb = 0). We observe that our results are in complete agreement and the grid invariance test has performed to sustain accuracy for 4 decimal points. In Table 6, local skin friction coefficient -f''(0), the rates of heat transfer $-\theta'(0)$, and mass transfer $-\phi'(0)$ that are acquired by FEM, which are also compared with the published research work, show excellent correlation.

η	Crane [32]	FEM	η	Crane [32]	FEM
0	1	1	7	0.0009	0.0009
1	0.1379	0.1379	8	0.0003	0.0003
2	0.1353	0.1353	9	0.0001	0.0001
3	0.0498	0.0498	10	0.0000	0.0000
4	0.0183	0.0018	11	0.0000	0.0000
5	0.0067	0.0067	12	0.0000	0.0000
6	0.0025	0.0025	13	0.0000	0.0000

Table 3. Assessment of skin friction coefficient for different values of M.

М	Gireesha et al. [33] $\beta = 0$	Mudassar et al. [34] Exact Solution (a)	FEM (Our Results) (b)	Error in % $ (\frac{b-a}{a}) \times 100$
0.0	1.000	1.000000	1.0000078	0.00078
0.2	1.095	1.095445	1.0954462	0.00010
0.5	1.224	1.224745	1.2247452	0.00001
1.0	1.414	1.414214	1.4142142	0.00001
1.2	1.483	1.483240	1.4832385	0.00010
1.5	1.581	1.581139	1.5811392	0.00001
2.0	1.732	1.732051	1.7320515	0.00002

Table 4. Assessment of skin friction coefficient for various values of M and σ when $f_w = \lambda_1 = \lambda_2 = \lambda_3 = k_p = S_f = 0$.

Μ	Mabood and Das [36]	Fazle and Stanford [25]	FEM (Our Results)	σ	Chamkha et al. [37]	Fazle and Stanford [25]	FEM (Our Results)
0	-1.000008	-1.0000084	-1.0000082	0.2	-	-	1.068027
1	1.4142135	1.41421356	1.41421353	0.4	-	-	1.134687
5	2.4494897	2.44948974	2.44948963	0.6	-	-	1.199118
10	3.3166247	3.31662479	3.31662463	0.8	1.261512	1.261042	1.261042
50	7.1414284	7.14142843	7.14142839	1.0	-	-	1.320522
100	10.049875	10.0498756	10.0498751	1.2	1.378052	1.377724	1.377724
500	22.383029	22.3830293	22.3830283	1.4	-	-	1.432836
1000	31.638584	31.6385840	31.6385833	1.6	-	-	1.486039

Table 5. Comparison of $-\theta'(0)$ for various values of Pr when $M = f_w = S_\theta = \sigma = \lambda_1 = \lambda_2 = \lambda_3 = R = Nd = k_p = S_f = 0.$

Pr	Ali [38]	Fazle and Stanford [25]	Ishak et al. [35]	Dulal Pal. [39]	Haile et al. [40]	Ishak et al. [35] (a) Exact Solution	FEM (b) Our Results	Error in % $ (\frac{b-a}{a}) \times 100$
0.72	0.8058	0.8088	-	-	-	0.8086313498	0.8086339299	0.0003
1.00	0.9691	1.0000	1.0000	1.0000	1.0004	1.000000000	1.0000080213	0.0008
3.00	1.9144	1.9237	1.9237	1.9236	1.9234	1.923682594	1.9236777221	0.0003
10.0	3.7006	3.7207	3.7207	3.7207	3.7205	3.720673901	3.7206681683	0.0002
100	-	-	12.2941	12.2940	12.2962	12.294083260	12.294051659	0.0003

Pr	Sc -	Cha	mkha et al.	[37]	FEM(Our Results)			
<i></i>	50	-f''(0),	- heta'(0),	$-\phi'(0), -\phi'(0) -f''(0)$		- heta'(0)	$-\phi'(0)$	
0.71	0.22	0.27377	1.158393	0.740140	0.27371	1.158389	0.740160	
	0.60	0.49677	1.101087	1.312248	0.49669	1.101082	1.312192	
	0.94	0.59941	1.076931	1.713443	0.59935	1.076899	1.713358	
0.3	0.62	0.38639	0.621980	1.355045	0.38655	0.621892	1.355036	
0.71		0.50438	1.099032	1.337571	0.50429	1.099018	1.337267	
1.0		0.55244	1.384875	1.331027	0.55237	1.384753	1.331856	
3.0		0.69042	2.966999	1.316710	0.69036	2.966894	1.316382	

Table 6. Comparison of -f''(0), $-\theta'(0)$, and $-\phi'(0)$ for different values of Pr, and Sc when $M = \sigma = \lambda_3 = \beta = R = Nb = Nt = Nd = Sr = 0$, $f_w = 0.5$, $\lambda_1 = k_p = 1$, $\lambda_2 = 2$, $S_f = S_{\theta} = S_{\varphi} = S_{\xi} = 0$.

Figure 2 shows the effect of M on the velocity function with no hydro-dynamic slip and with hydro-dynamic slip. The results show that in both cases the velocity component decreases as the value of the magnetic parameter M increases. Physically, the magnetic parameter M produced Lorentz force like a drag force, which causes the motion of the fluid to decelerate. Figure 2 also shows that in both cases the suction f_w decelerates the momentum boundary layer thickness. The boundary layer thickness can be controlled with the help of suction f_w .

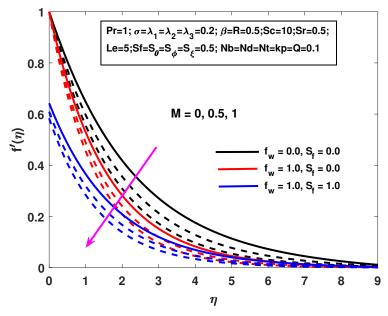


Figure 2. Effects of *M*, f_w , and S_f on f'.

Figures 3 and 4 exemplify that the velocity boundary layer thickness increases with enhancing the thermal buoyancy parameter λ_1 and the nano-particles concentration buoyancy parameter λ_3 in the non-existence of hydro-dynamic slip and the existence of hydro-dynamic slip. In these two cases, we have to perceive that the momentum boundary layer is prolonged with the increasing values of buoyancy λ_1 and λ_3 . Also in Figures 3 and 4, the velocity profile is increasing in the case of steady and unsteady flow and alike behavior of solutal buoyancy has been observed in Figure 5. It is observed that increasing the value of radiation parameter *R* is the reason to improve the velocity profile and incentive of instability in parameter k_p , and the velocity profile is explained in Figure 6.

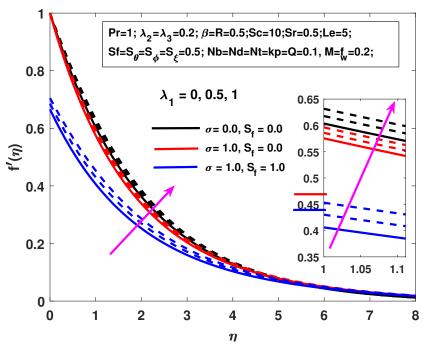


Figure 3. Effects of λ_1 , σ , and $S_f = 0$ on f'.

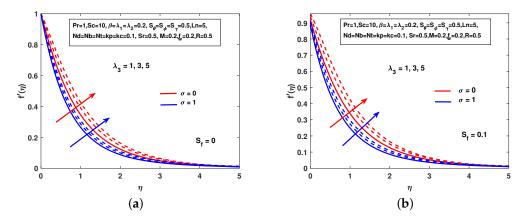


Figure 4. Effects of λ_3 and σ on f'. (a) $S_f = 0$ (b) $S_f = 0.1$.

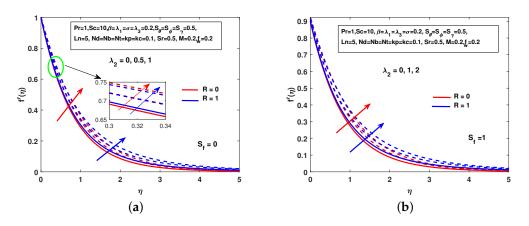


Figure 5. Effects of λ_2 and *R* on f'. (a) $S_f = 0$ (b) $S_f = 1$.

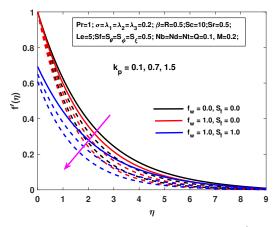


Figure 6. Effects of kp, f_w , and S_f on f'.

Also, we perceive in both cases that as the permeability of k_p increases, this causes a decline in the velocity profile with no hydro-dynamic slip and with hydro-dynamic slip. Furthermore, we also perceive in Figure 6 that the suction decreases the momentum boundary layer thickness. Similar behavior of the Deborah number β has been perceived on the velocity profile in Figure 7. Figure 8 indicates the impact of M on the temperature profile with the non-existence of thermal slip and with existence thermal slip. In the figure, it is clear that with an increasing value of M the temperature profile also increases in both cases. From Figure 8 it is also clear that suction f_w decreases the thermal boundary layer thickness in both cases and the thickness of the thermal boundary layer can be controlled with the help of suction f_w . Figure 9 depicts the similar behavior of M. It is perceived that the temperature increases with the discrepancy in parameter R.

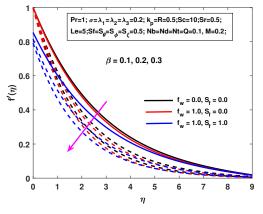


Figure 7. Effects of β , f_w , and S_f on f'.

Figure 10 demonstrates the influence of σ and Pr on the temperature profile with and without the existence of thermal slip, with increasing Pr, σ , and S_{θ} causing the thermal boundary layer to decrease. The description of the effect of N_b , f_w , and S_{θ} with the temperature profile is explained in Figure 11. It is clear that with the increase in N_b , the thermal boundary layer of fluid flow increases in both cases. It can also be perceived that f_w decreases the thermal boundary layer thickness in both cases. In Figure 12, there is the influence of M and Sc on the solutal profile with the non-existence of solutal slip and with the existence of solutal slip. From the figure, it is clear that with the increasing value of M, the solutal profile also increases in both cases. Furthermore, the effect of S_c over the solutal profile declines the profile. The impact of the existence and non-existence of solutal slip and increasing values of S_r is depicted in Figure 13. It is seen that increasing the value of the Soret parameter increases the solutal profile in both the steady and unsteady cases. It is also seen that increasing the value of the slip results in decreasing the thickness of the solutal profile boundary.

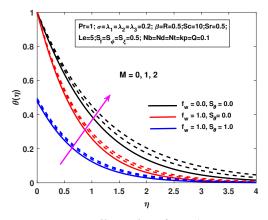


Figure 8. Effects of *M*, f_w , and S_θ on θ .

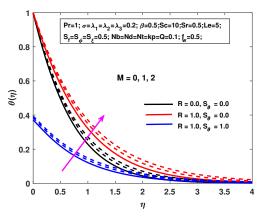


Figure 9. Effects of *M*, *R*, and S_{θ} on θ .

Figure 14 indicates the impact of N_t on the nano-particle volume fraction profile without the existence of nano-particles concentration slip and with the existence of nano-particles concentration slip. It is clear from the figure that in both the steady and unsteady cases, increasing values of N_t cause a decline in the nano-particle volume fraction profile. The impacts of σ and S_{γ} over the nano-particle volume fraction profile have been illustrated in Figure 14. It is noticed that the nano-particle volume fraction profile decreases in increments in the values of σ and S_{γ} . Figures 15 and 16 show the impact of Lewis number *Le*, unsteadiness parameter σ , and suction parameter f_w on the nano-particle volume fraction profile, and interpretations about the nano-particle volume fraction profile are made. It is seen that increasing values of *Le* and f_w in the boundary layer of nano-particles causes the volume fraction profile to decline. In addition, it is clear from the figures that the nano-particle volume fraction profile volume fraction profile volume fraction profile volume fraction profile to decline. In addition, it is clear from the figures that the nano-particle volume fraction profile to decline. In addition, it is clear from the figures that the nano-particle volume fraction profile to decline. In addition, it is clear from the figures that the nano-particle volume fraction profile decreases both with and without the existence of nano-particles concentration slip.

Figure 17 shows the impact of M, σ , and S_f on the skin friction co-efficient and also shows that the skin friction co-efficient decreases with the increase of slip parameter, magnetic and unsteadiness parameter. In Figure 18, the skin friction coefficient increases with the increment in the thermal buoyancy, suction parameters, and solutal buoyancy. Figure 19 represents the increment in the value of Nusselt number with increasing values of magnetic, radiation and thermal slip parameters. As perceive in Figure 20 that when the values of solutal buoyancy and suction intensity increases with the existence and the non-existence absence of thermal buoyancy. Figure 21 demonstrates that the impact of *Sc*, *Sr*, and S_{ϕ} on the reduced Sherwood number. Also from the Figure 22, it clear that the reduced Sherwood number decreases with increment in the values of the unsteadiness parameter σ , magnetic parameter *M* and the suction parameters f_w .

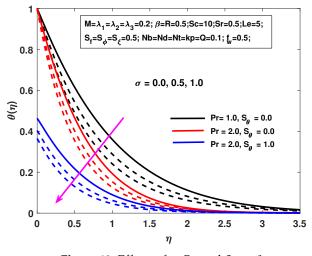


Figure 10. Effects of σ , *Pr*, and S_{θ} on θ .

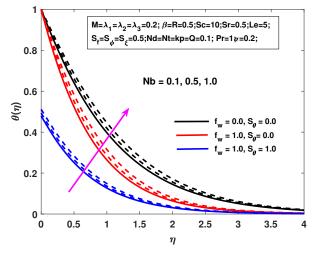


Figure 11. Effects of *Nb*, f_w , and S_θ on θ .

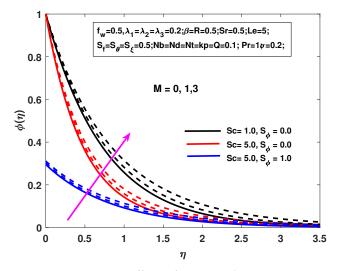


Figure 12. Effects of *M*, *Sc*, and S_{ϕ} on ϕ .

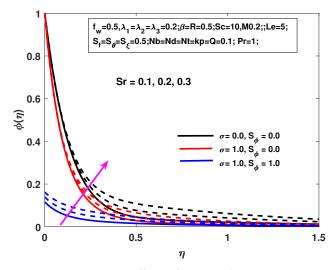


Figure 13. Effects of *Sr*, σ , and *S*_{ϕ} on ϕ .

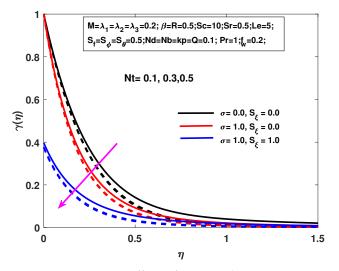


Figure 14. Effects of Nt, σ , and S_{ξ} on ξ .

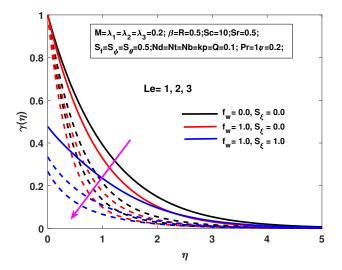


Figure 15. Effects of *Le*, f_w , and S_{ξ} on ξ .

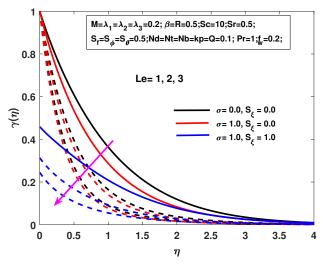


Figure 16. Effects of *Le*, σ , and S_{ξ} on ξ .

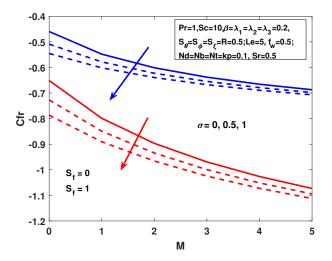


Figure 17. Effects of *M*, σ , and *S*_{*f*} on the skin friction coefficient.

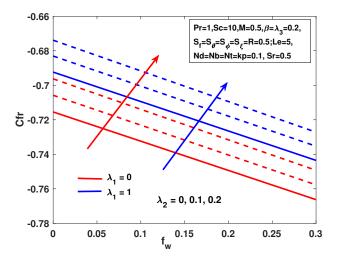


Figure 18. Effects of f_w , λ_1 , and λ_2 on the skin friction coefficient.

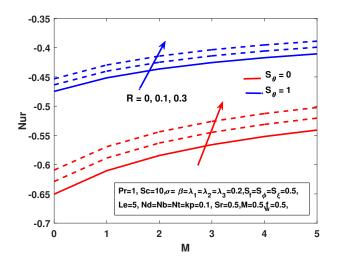


Figure 19. Effects of *M*, *R*, and S_{θ} on the reduced nusselt number.

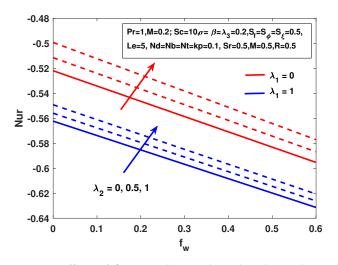


Figure 20. Effects of f_w , λ_1 , and λ_2 on the reduced nusselt number.

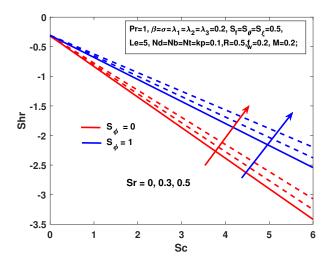


Figure 21. Effects of *Sc*, *Sr*, and S_{ϕ} on the reduced Sherwood number.

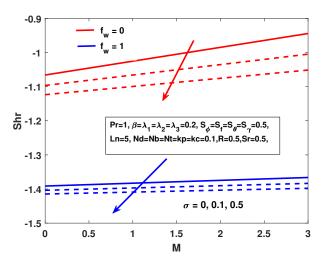


Figure 22. Effects of *M*, σ , and f_w on the reduced Sherwood number.

In Table 7 we analyze the variation of physical parameters M, λ_1 , λ_2 , λ_3 , σ , P_r , L_e on skin friction co-efficient -f''(0), Nusselt number $-\theta'(0)$, and Sherwood number $-\xi'(0)$.

The following results are concluded from Table 7:

(i) The skin-friction coefficient is increasing while reducing the local Nusselt and Sherwood numbers through improvement in the Magnetic parameter; (ii) The increment in thermal buoyancy parameters λ_1 , λ_2 , λ_3 causes the skin-friction coefficient to decrease while increasing the local Nusselt number and Sherwood number; (iii) With the increasing unsteadiness parameter σ , the skin-friction coefficient, local Nusselt, and Sherwood numbers are also increasing; (iv) The skin-friction coefficient is increasing with the increment in Prandtl number and the local Nusselt number and Sherwood number also increase; (v) The skin-friction coefficient is increasing with the increasing Lewis number and also increment in the local Nusselt number and Sherwood number.

М	λ_1	λ_2	λ_3	σ	Pr	Le	-f''(0)	$-\theta'(0)$	$-\xi'(0)$
0.5	0.2	0.2	0.2	0.5	1	5	0.43564	0.70863	1.33066
1.0	•				-	-	0.47695	0.70192	1.32746
1.5							0.51239	0.69612	1.32468
0.5	0.2	0.2	0.2	0.5	1	5	0.43564	0.70863	1.33066
	0.5						0.42223	0.71052	1.33163
	0.8						0.40901	0.71237	1.33258
0.5	0.2	0.2	0.2	0.5	1	5	0.43564	0.70863	1.33066
		0.5					0.43095	0.70928	1.33099
		0.8					0.42628	0.70993	1.33133
0.5	o.2	0.2	0.2	0.5	1	5	0.43564	0.70863	1.33066
			0.5				0.43217	0.70906	1.33089
			0.8				0.42870	0.70949	1.33113
0.5	0.2	0.2	0.2	0.5	1	5	0.43564	0.70863	1.33066
				1.0			0.46926	0.79556	1.37699
				1.5			0.49903	0.86094	1.41349
0.5	0.2	0.2	0.2	0.5	1	5	0.43564	0.70863	1.33066
					3		0.43819	0.88813	1.28962
					5		0.43925	1.00288	1.25652
0.5	0.2	0.2	0.2	0.5	1	5	0.43564	0.70863	1.33066
						7	0.43635	0.70919	1.44132
						10	0.43689	0.70993	1.54699

Table 7. Various mathematical values of physical constraints M, λ_1 , λ_2 , λ_3 , σ , P_r , L_e when $R = f_w = S_r = S_t = S_f = S_p = S_g = 0.5$, $k_p = 0.1$, $N_u = N_b = N_t = Q = 0.1$, $\beta = 0.2$, $S_c = 10$.

5. Conclusions

In this paper, we have developed a mathematical model to investigate the unsteady two-dimensional magnetohydrodynamic (MHD) flow and heat transfer of an incompressible electrically conducted fluid. This study was conducted to analyze the multiple slip effects on magneto-hydrodynamic unsteady Casson nano-fluid flow over a non-linear porous shrinking/stretching sheet in the presence of a heat source with Soret effect. Appropriate similarities have been used for transformations and the governing partial differential equations (PDEs) are rendered into a system of ordinary differential equations (ODEs). The resulting system of ordinary differential equations was solved numerically with an efficient and validated finite element method (FEM). We also use a special case of the present model to compare our results with previous studies. A parametric study has been performed to explore the mass and heat transfer characteristics, and also the impact of different parameters, of the flow. The following are the results that can be concluded from the present study.

- The cause of reducing the fluid velocity near the region of the boundary layer is the increment in values of slip, suction, magnetic field, and unsteady parameters.
- The increment in thermal buoyancy parameters $\lambda_1, \lambda_2, \lambda_3$ and slip parameters cause decreasing the skin-friction coefficient while increasing the local Nusselt number and Sherwood number.
- Decreasing the value of the Sherwood number causes an increasing value of the solutal slip parameter, Schmidt number, and Soret number, but the effect is the opposite with increasing values of the unsteadiness, magnetic, and suction parameters.
- With the increasing value of the magnetic parameter *M*, the slip velocity parameter and suction parameter are found to be reduced in the velocity profile.
- The skin-friction coefficient decreases with the increasing value of slip, magnetic, and unsteadiness parameters, but the effect is the opposite for increasing values of thermal buoyancy, suction parameter, and solutal buoyancy.
- The increment of the values of buoyancy parameter, injection parameter, and heat source parameter cause an increase in the velocity profile.

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