

Article

# Measurement and Quantification of Effective Slip Length at Solid–Liquid Interface of Roughness-Induced Surfaces with Oleophobicity

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**Featured Application:** Our study focuses on inhibiting hydrodynamic drag in many applications of micro-/nano-fluidic channels, including micro-/nano-electromechanical systems (MEMS/NEMS), micro-/nano-fluidic systems, confined biological system, etc.

**Abstract:** Boundary conditions of the liquid–solid interface of micro/nano fluid flow are of great interest, as slippage is linked with decreased drag. However, previous studies have seldom included a systematic analysis of the effect of roughness on the measurement and quantification of slip length. For the measurement of slip length using atomic force microscopy (AFM), which is believed to be the most accurate method, a theoretical description of the drainage of thin liquid films between sphere and surface, with realistic roughness, is yet to be published. This study focuses on the measurement and quantification of slip length on rough surfaces immersed in liquids, based on AFM and laser confocal scanning microscopy. A reformulation of the boundary condition is presented, taking into account the effect of surface roughness. The correction to the effective slip length is analyzed, then surfaces with various degrees of spacing roughness  $R_{sm}$  were fabricated. Quantitative analysis of the effective slip length is presented. Results show that the corrected effective slip length remains constant with increased spacing roughness  $R_{sm}$  of surfaces. The results are discussed for the coagulation process of colloids and measurement of slip lengths on roughness-induced surfaces with AFM.

**Keywords:** hydrodynamic drag; boundary slip; roughness; drainage; superoleophilic; superoleophobic

## 1. Introduction

At the micro or nano scale, fluid flow is subjected to high drag with decreasing dimensions and increasing surface-to-volume ratio in confined systems. Reducing hydrodynamic drag is a crucial issue in many applications of micro-/nano-fluidic channels, including micro-/nano-electromechanical systems (MEMS/NEMS), micro-/nano-fluidic systems, confined biological systems, etc., and has been of wide scientific interest [1]. It is obvious that boundary conditions at the solid–liquid interface have a direct influence on hydrodynamic drag, as published studies show that boundary slip is believed to inhibit hydrodynamic drag [2–5].

Slippage of fluid flow at the solid–liquid interface, the so-called boundary slip, is of great importance in hydrodynamics. Boundary slip is characterized by slip length according to Navier’s slip condition [6], via  $v = b \frac{dv}{dy} \Big|_{y=0}$ , where  $b$  is the slip length,  $v$  is the tangential velocity, and  $y$  is the axis perpendicular to the wall. At the micro or nano scale, slip lengths of various surfaces immersed in liquid have been investigated in theoretical and experimental studies [7–17]. For the measurement technique,

slip length can be derived via measurement of surface force or hydrophobic force using surface force apparatus (SFA) or atomic force microscopy (AFM). Vinogradova [18–20] investigated the drainage of a thin liquid film confined between two spheres, where hydrophobic force could apply to obtain slip length by employing Navier’s slip condition for liquid flow near the surface. Fang and Mi [21] presented a reformulation of the hydrodynamic conditions based on Vinogradova’s work, taking into account the boundary curvature effects of spheres. The Reynolds equation for hydrodynamic lubrication is generalized to obtain analytic expressions of the pressure and drag force for arbitrary values of slip length and for arbitrary radii of the approaching sphere, which has been widely used. Zhu and Granick [22] studied boundary slip on chemically modified octadecyltrichlorosilane (OTS) and octadecyltriethoxysilane (OTE) samples by using SFA. The Craig group [23] utilized AFM to measure the slip length of deionized (DI) water on silicon wafers roughened by treatment with KOH. The Bhushan group [24,25] studied boundary slip on SiO<sub>2</sub> particle composite-coated surfaces with varying degrees of roughness by using AFM.

Roughness is believed to have an effect on measurement. For the technique using hydrodynamic forces to derive slip length on a rough surface, the measured slip length should be replaced by the effective slip length. However, previous studies have not included the effect of roughness on measurement and quantification, and the positions of the “reference surface,” i.e., the surface from which the slip velocity is determined, in boundary slip measurement are ambiguous. For the technique using hydrodynamic forces to derive the slip, different choices of reference surface can lead to a shift of the fitting force curve and result in different calculated values of slip length, as pointed out by the Vinogradova group [20] and Craig group [26]. Studies have focused on smooth surfaces, and set the reference surface at the peak of the surface. If the reference surface is located on the peak of the rough surface, the calculated value of the measured slip length will tend to be larger than the true value, as the liquid molecules can still flow between the peaks and valleys. Thus, studies on the boundary slip of surfaces with various degrees of roughness must locate the position of the reference surface. Kunert and Harting [27] investigated slippage lengths on randomly generated surfaces with Gaussian distribution heights, and reported that slippage was independent of detailed surface profile, and they suggested that the location of the reference surface was related to  $R_a$  roughness. A complete theoretical description of reference surface on realistic surface roughness to derive effective slip length is yet to be published. Surface roughness most commonly refers to the average height and width of the topography relative to a reference plane, and it can be characterized by amplitude roughness and spacing roughness. Studies have reported the effect of amplitude roughness on slip length; however, there is no experimental data on the effect of spacing roughness. Investigating the boundary conditions for the flow of liquids on surfaces with varying spacing roughness can provide a fundamental understanding of the interaction of solid and liquid at interfaces.

In this paper, the effect of roughness on effective slip length at the solid–liquid interface was investigated. We reformulate the theory of thin liquid film drainage between sphere and superoleophobic/superoleophilic surfaces, taking into account the roughness effect. A measurement technique is established to obtain effective slip length on roughness-induced surfaces immersed in oil by using AFM and laser confocal scanning microscopy. Due to the wide application of hexadecane and ethylene glycol in the lubrication and antifreeze of MEMS/NEMS, these two kinds of oil were selected. A series of multilayered compositing surfaces with adjusted roughness and the same chemical properties were fabricated, and then were used to investigate the effect of spacing roughness on effective slip length. The results and mechanisms are discussed in this paper.

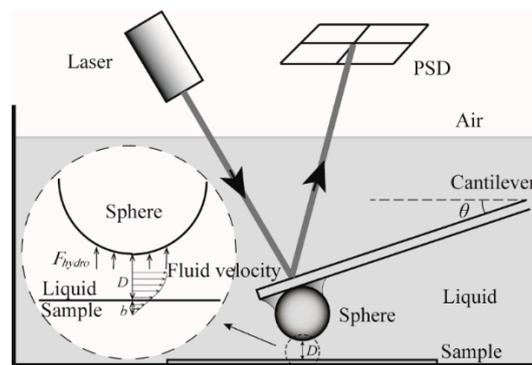
## 2. Experiment

The measurement and quantification technique of effective slip length on roughness-induced superoleophilic/superoleophobic surfaces is described first. The location of the reference surface is discussed and the calculation of effective slip length is presented, followed by the procedures for preparing the superoleophilic and superoleophobic surfaces with varying degrees of spacing roughness

and the oils used for the experimental study. Finally, measurement techniques of surface roughness and wetting properties are presented.

### 2.1. Measurement of Slip Length by AFM

An AFM in contact mode under liquid was used to measure slip length [18]. A colloidal AFM probe was prepared by gluing a borosilicate sphere to the end of a rectangular AFM cantilever (ORC 8, Bruker, Billerica, MA, USA). As shown in Figure 1, the borosilicate sphere was driven toward the surface immersed in liquid at a certain driving velocity, and the hydrodynamic force detected on the probe as a function of deflection was recorded. The measured deflection data of the probe was used to calculate the hydrodynamic force data using Hooke’s law ( $F_{hydro} = k \times Def$ , where  $F_{hydro}$  is the hydrodynamic force,  $k$  is the stiffness of the AFM probe, and  $Def$  is the deflection of the probe).



**Figure 1.** Schematic illustration of slip length measurement on a rough surface by using a colloidal atomic force microscopy (AFM) probe in contact mode. As the sphere approaches the sample, liquid is driven and drained to become fluid flow. The arrows above and below the solid–liquid interface represent magnitude and direction of fluid flow with boundary slip.

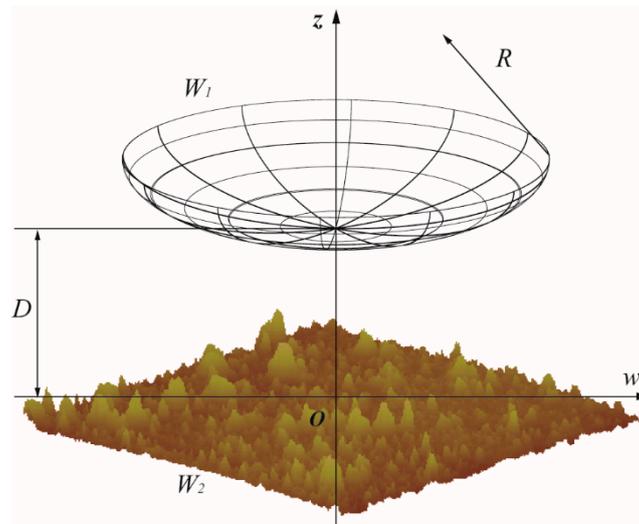
For smooth surfaces, the hydrodynamic force can be written in the limit of large separation distance ( $D \gg b$ ) as [28]:

$$\frac{V}{F_{hydro}} = \frac{1}{6\pi\mu R^2}(D + b), \tag{1}$$

where  $V$  is the approaching velocity of the sphere,  $\mu$  is the dynamic viscosity of the liquid,  $R$  is the radius of the sphere, and  $D$  is the separation distance between the surface and the bottom of the sphere. By analyzing the hydrodynamic force, electrostatic force, van der Waals force, and Stokes’ force obtained on the probe, the boundary slip can be calculated.

### 2.2. Quantitation of Effective Slip Length on the Rough Surface

For rough surfaces, drainage of the thin film between sphere and surface is investigated in order to determine the effective slip length, as shown in Figure 2. Consider a spherical particle  $W_1$  having radius  $R$  and a flat particle  $W_2$  immersed in the Newtonian liquid.  $W_2$  is located on the peak of the rough surface. We assume that the particles are sufficiently rigid that any deformation due to hydrodynamic pressure is negligible. The distance  $D$  between two particles is assumed to be much less than radius  $R$  ( $D \ll R$ ). The particle  $W_1$  approaches  $W_2$  along the line connecting their centers with velocity  $v$  (the Reynolds problem). The origin of cylindrical coordinates ( $w, z$ ) coincides with the  $W_2$  particle, with the  $z$ -axis oriented in the direction of  $W_1$ .



**Figure 2.** Schematic illustration of drainage of a thin liquid film between sphere and rough surface. The distance of closest approach between the two surfaces is  $D$ , and the approaching velocity of surfaces is  $v$ . The appropriate cylindrical coordinate system  $(w, z)$  is established as shown.

In the inner region, which is close to the origin of the coordinates, the surfaces  $W_1$  and  $W_2$  can be expressed as follows:

$$\begin{cases} z = D + \frac{1}{2} \frac{w^2}{R} + O(w^4) & W_1 \\ z = 0 & W_2 \end{cases} \quad (2)$$

The steady-state flow between particles develops while in the approaching process, and the motion of liquid is axisymmetric and follows the continuity equation:

$$\frac{\partial p}{\partial w} = \mu \frac{\partial^2 v_w}{\partial z^2}, \quad \frac{\partial p}{\partial z} = 0, \quad (3)$$

where  $p$  is the pressure of the liquid flow,  $\mu$  is dynamic viscosity, and  $v_w$  is the projection of the liquid flow rate on the  $w$ -axis. If the thin flow is incompressible liquid, then the system of motion equation takes the form:

$$\frac{1}{w} \frac{\partial}{\partial w} (w \cdot v_w) + \frac{\partial v_z}{\partial z} = 0, \quad (4)$$

where  $v_z$  is the projection of the liquid flow rate on the  $z$ -axis.

The quantity of motion follows the  $w$ -component and  $z$ -component hydrodynamic equations:

$$\begin{cases} \rho \left( v_z \frac{\partial v_w}{\partial z} + v_w \frac{\partial v_w}{\partial w} \right) = -\frac{\partial p}{\partial w} + \mu \left[ \frac{\partial^2 v_w}{\partial z^2} + \frac{1}{w} \frac{\partial}{\partial w} \left( w \frac{\partial v_w}{\partial w} \right) - \frac{v_w}{w^2} \right] \\ \qquad \qquad \qquad = \frac{\mu}{w} \frac{\partial}{\partial w} \left( w \frac{\partial v_w}{\partial w} \right) - \mu \frac{v_w}{w^2} \\ \rho \left( v_z \frac{\partial v_z}{\partial z} + v_w \frac{\partial v_z}{\partial w} \right) = -\frac{\partial p}{\partial z} + \mu \left[ \frac{\partial^2 v_z}{\partial z^2} + \frac{1}{w} \frac{\partial}{\partial w} \left( w \frac{\partial v_z}{\partial w} \right) \right] \\ \qquad \qquad \qquad = \mu \frac{\partial^2 v_z}{\partial z^2} + \frac{\mu}{w} \frac{\partial}{\partial w} \left( w \frac{\partial v_z}{\partial w} \right) \end{cases} \quad (5)$$

where  $\rho$  is the density of the liquid.

In order to characterize the state of the fluid flow, the boundary conditions of two surfaces are set. We assume that the solid–liquid interface of two surfaces is a Navier slip condition, and the slip

lengths for surfaces  $W_1$  and  $W_2$  are  $b_1 = b$  and  $b_2 = k(b + 1)$ , respectively. Therefore, the boundary condition of  $W_1$  is given by:

$$\begin{cases} z = D + \frac{1}{2} \frac{w^2}{R} + O(r^4) \\ v_z = \frac{zv_z}{R} + v = v \\ v_w = -b(k + 1) \frac{\partial v_w}{\partial z} \end{cases}, \tag{6}$$

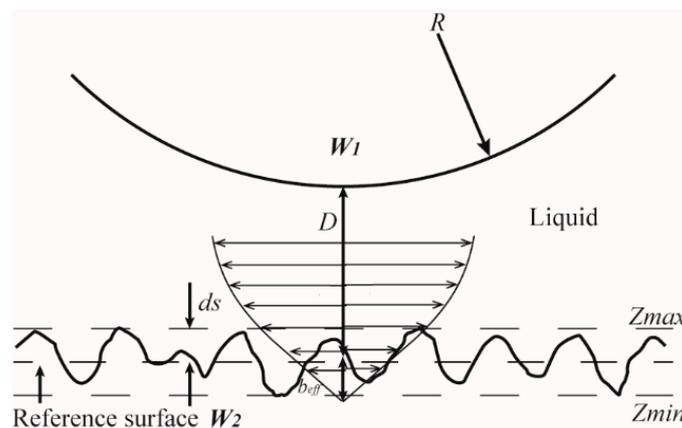
and the boundary condition of  $W_2$  is given by:

$$\begin{cases} z = 0 \\ v_z = 0 \\ v_w = b \frac{\partial v_w}{\partial z} \end{cases}. \tag{7}$$

Assume the reference surface is located on the position below surface  $W_1$  at a distance  $d_s$ , as shown in Figure 3, and parallel to surface  $W_1$ . The effective slip length for the reference surface is  $b_{eff}$ . Therefore, the boundary condition of the reference surface is given by:

$$\begin{cases} z = -d_s \\ v_z = 0 \\ v_w = b_{eff} \frac{\partial v_w}{\partial z} \end{cases}. \tag{8}$$

In addition, assume that the pressure of the fluid outside the two surfaces is negligible, while  $w \rightarrow \infty, p = 0$ .



**Figure 3.** Schematic illustrating possible definitions of the reference at a rough surface and the boundary condition when the reference surface is located between the peak and valley of sample.

The solution of Equation (3), taking into account boundary conditions (6) and (8), leads to an expression about  $v_w$ :

$$v_w = \frac{1}{2\mu} \frac{\partial p}{\partial w} \left[ z^2 - zH \left( \frac{H + 2b_{eff}(1+k)}{H + b_{eff}(2+k)} \right) - bH \left( \frac{H + 2b_{eff}(1+k)}{H + b_{eff}(2+k)} \right) \right], \tag{9}$$

where  $H = D + \frac{1}{2} \frac{w^2}{R}$ . The solution of Equation (4), taking into account Equation (9) and integrating, leads to an expression about the relationship between  $v$  and  $z$ . This formula determines the

differential equation for pressure. Integrating this formula two times, we obtain the expression for the hydrodynamic force of surface  $W_1$ :

$$\begin{aligned} F_{hydro} &= -2\pi w \int_0^{+\infty} \left[ -p(w) + 2\mu \frac{dv_z}{dz} \right] dw, \\ &= -\frac{6\pi\mu R^2 v}{D+d_s} f^* \end{aligned} \quad (10)$$

where

$$f^* = \frac{b_{eff} b_2 (D + d_s)}{6} \left\{ \left[ 1 + b_{eff} b_2 (D + d_s) \right] \ln \left[ 1 + \frac{3}{b_{eff} b_2 (D + d_s)} \right] - 1 \right\}.$$

As the effective slip  $b_{eff}$  is much less than the distance between two surfaces, Equation (10) can be simplified as:

$$\begin{aligned} F_{hydro} &= -\frac{6\pi\mu R^2 v}{(D+d_s)} \left( -\frac{D+d_s}{D+d_s+b_2+b_{eff}} \right) \\ &= \frac{6\pi\mu R^2 v}{(D+d_s+b_2+b_{eff})} \end{aligned} \quad (11)$$

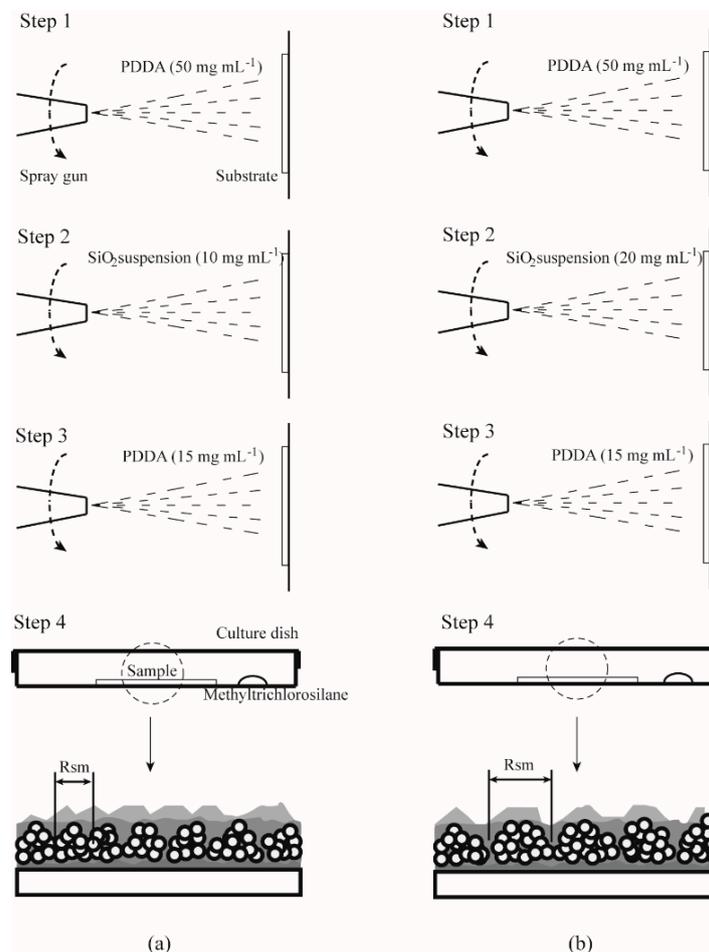
Note that the effective slip length is obtained by analyzing the velocity of liquid flow at the reference surface. Therefore, the velocity at the reference surface shall be representative of the average velocity of liquid flow between the peaks and valleys. According to the study of Pan et al. on the correction of slip length [29], the  $R_q$  roughness of the profile is a typical case to describe surface roughness based on the standard of International Organization for Standardization (ISO), and is suitable to describe the average velocity of liquid flow. The  $R_q$  roughness, which is defined as the Root Mean Square (RMS) value of the ordinate values within a sampling length, is selected to describe the amplitude of roughness in this paper, as it is more sensitive than  $R_a$  roughness, via  $R_q = \sqrt{\frac{1}{l} \int_0^l z(x)^2 dx}$ . The position within the surface near the height of  $R_q$  on the surface is also a more reasonable choice than the tops of peaks. Thus, the reference surface is defined as the position of  $R_q$  roughness, and the height of asperities  $d_s$  is defined by  $b_{eff} = b - b_2 - d_s$ , via  $d_s = R_z - R_q$ .

### 2.3. Preparation of Superoleophilic and Superoleophobic Surfaces

To prepare the superoleophilic surface, layer-by-layer compositing surfaces were fabricated to prepare samples with varying spacing roughness [30]. Soda–lime glass (Cat. No. 7101, Sail Brand, Yancheng, China) with 1.0 mm thickness was used as a substrate.  $\text{SiO}_2$  nanoparticles with a diameter of 7 nm (Aerosil RX50, Evonik Industries, Essen, Germany) were used to form a layer of roughness-induced nanostructure. Methyltrichlorosilane was used to obtain a functional layer for the property of superoleophilicity. Polydiallyldimethylammonium chloride (PDDA) was used to adsorb particles of each layer. The procedure was applied three times to the substrates with a spray-coating method using a spray gun (Airbrush-S130, U-star Company, Hong Kong, China) at a distance of about 15 cm and a pressure of 200 kPa, as shown in Figure 4a. Then the samples were annealed in an oven at 140 °C for 1 h. For the chemical vapor deposition (CDV) process, a drop of methyltrichlorosilane (methylsilane, Sigma Aldrich, St. Louis, MO, USA) was deposited near the samples to form a functional layer, which was then sealed and left for 10 h. Figure 4b shows that the  $\text{SiO}_2$  nanoparticles coalesced to a larger group and enhanced volume with increasing concentration from 10 mg mL<sup>-1</sup> to 15 mg mL<sup>-1</sup>. Therefore, pitches with increasing average width of the roughness pitch ( $R_{sm}$  roughness) were formed on the surfaces. There were five groups of samples (*a1* to *a5*) for superoleophilic surface.

To prepare the superoleophobic surface, the same substrate and processes as for the superoleophilic samples were used, except for the final step. The fluorosurfactant solution (1 mL) was coated as a functional layer with spray deposition, and the samples were allowed to air-dry for 10 h. When the  $\text{SiO}_2$  nanoparticles increased from 10 mg mL<sup>-1</sup> to 15 mg mL<sup>-1</sup>, a topography

with increasing  $R_{sm}$  was formed on the surfaces. There were five groups of samples ( $b1$  to  $b5$ ) for superoleophobic surface.



**Figure 4.** Schematic illustration of the preparation procedures for superoleophilic samples (a)  $a1$  and (b)  $a2$ . The dashed arrow is the moving direction of the spray gun, which is parallel to the samples. With increasing concentration from  $10 \text{ mg mL}^{-1}$  to  $15 \text{ mg mL}^{-1}$ , the  $\text{SiO}_2$  nanoparticles coalesce together into larger groups, leading to increased  $R_{sm}$  roughness.

## 2.4. Characterization of Surfaces

### 2.4.1. Morphology of Roughness

To measure effective slip length on the rough surfaces, the morphology of the superoleophilic and superoleophobic surfaces was measured using a laser confocal scanning microscope (OLS 3000, Olympus, Tokyo, Japan) with a magnification of  $100\times$  in 3D scanning mode. The surfaces were imaged with a scan size of  $128 \mu\text{m} \times 128 \mu\text{m}$  at a step length of  $20 \text{ nm}$ . Then surface roughness, including amplitude roughness and spacing roughness, was obtained by image processing.

### 2.4.2. CA and CAH Measurement

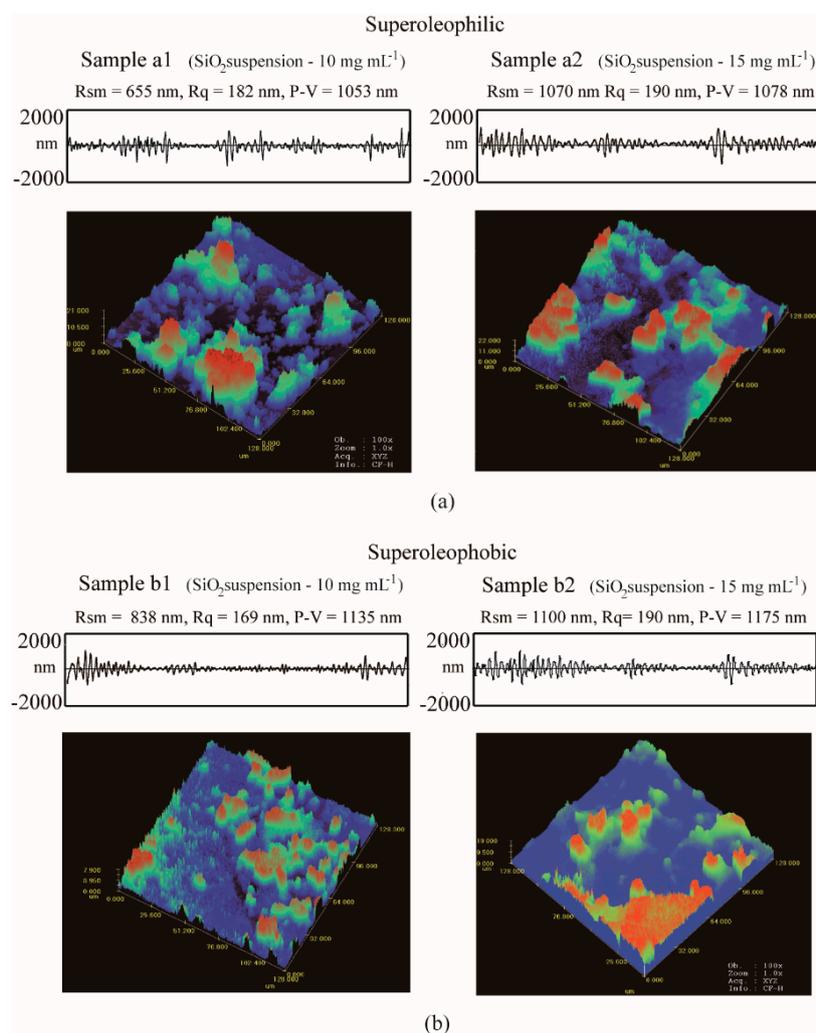
Surface wettability is believed to affect boundary slip. Therefore, to distinguish the individual effects of roughness and wettability on slip length, the contact angle (CA) and contact angle hysteresis (CAH) are should be constant. CAs and CAHs were measured by using a goniometer (DropMeter<sup>TM</sup> Element A-60, MAIST Vision Inc., Ningbo, China). A  $5 \mu\text{L}$  droplet each of hexadecane and ethylene glycol was deposited on the superoleophilic and superoleophobic surfaces, respectively, and images of

the droplets on the surfaces were captured and analyzed to obtain the CAs by Dropmeter software. Reproducibility of all CA and CAH data was obtained from measurements.

### 3. Results and Discussion

#### 3.1. Morphology and Surface Roughness

Figure 5a,b shows the laser confocal scanning microscopy images of samples *a1*, *a2* and *b1*, *b2* in air with calculated RMS and  $R_z$  roughness, respectively. A  $128 \mu\text{m} \times 128 \mu\text{m}$  scan size was used to present data. For both the superoleophilic and superoleophobic surfaces, the  $\text{SiO}_2$  nanoparticles coalesced together to form a random morphology with certain roughness. It can be noted that the  $R_{sm}$  roughness of sample *a2* was larger than that of *a1*. This result can be explained by the  $\text{SiO}_2$  nanoparticles with increasing concentration coalescing together into a larger group, which enhanced the spacing parameters of the surfaces. Therefore, the  $R_{sm}$  roughness increased from *a1* to *a5* and *b1* to *b5*, as shown in Table 1, and the  $R_z$  roughness kept consistent at  $\sim 1100 \pm 100 \text{ nm}$  for all samples.



**Figure 5.** Confocal laser scanning images in the air, and measured  $R_{sm}$ ,  $R_z$  roughness of (a) superoleophilic surface samples *a1* and *a2*, and (b) superoleophobic surface samples *b1* and *b2*.

**Table 1.**  $R_z$ ,  $R_{sm}$ , contact angle (CA), and contact angle hysteresis (CAH) of superoleophilic and Superoleophobic surfaces.

Type	$R_z$ (nm)	$R_{sm}$ (nm)	Hexadecane		Ethylene Glycol	
			CA (°)	CAH (°)	CA (°)	CAH (°)
<i>a1</i>	1040 ± 150	620 ± 90	0	–	10 ± 1	–
<i>a2</i>	1100 ± 100	1080 ± 100	0	–	10 ± 1	–
<i>a3</i>	1160 ± 100	1480 ± 110	0	–	10 ± 1	–
<i>a4</i>	1050 ± 80	2050 ± 100	0	–	10 ± 1	–
<i>a5</i>	1110 ± 100	2740 ± 100	0	–	10 ± 1	–
<i>b1</i>	1100 ± 100	760 ± 100	150 ± 3	10 ± 2	159 ± 5	7 ± 1
<i>b2</i>	1120 ± 80	1170 ± 150	150 ± 3	8 ± 1	160 ± 3	5 ± 1
<i>b3</i>	1150 ± 100	1690 ± 100	152 ± 2	6 ± 1	158 ± 3	6 ± 1
<i>b4</i>	1150 ± 80	2050 ± 150	151 ± 2	8 ± 1	160 ± 3	5 ± 2
<i>b5</i>	1180 ± 100	2670 ± 100	155 ± 3	8 ± 2	158 ± 5	5 ± 1

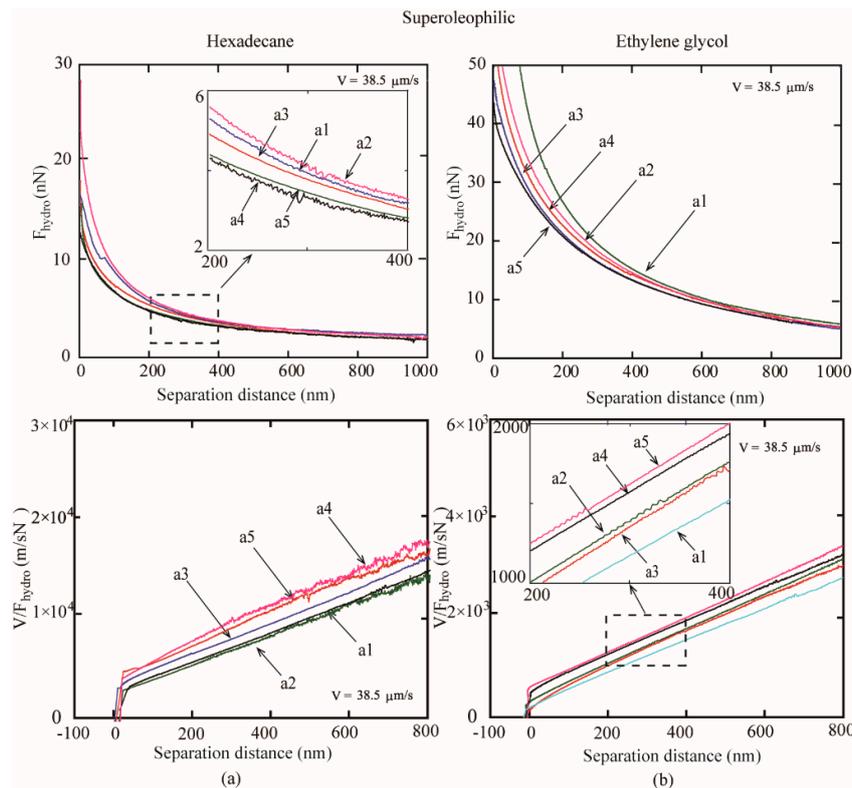
### 3.2. CA and CAH

Table 1 shows the CAs and CAHs of hexadecane and ethylene glycol on the superoleophilic and superoleophobic surfaces. For the superhydrophilic surfaces, the CAs and CAHs of the hexadecane droplets on the surfaces remained  $\sim 0^\circ$  and were smaller than that of ethylene glycol, which was  $\sim 10^\circ$  with increasing  $R_{sm}$  roughness from *a1* to *a5*. For the superhydrophobic surfaces, the CAs of the hexadecane droplets on the surfaces remained  $\sim 150^\circ$ , and were smaller than that of ethylene glycol, which was  $\sim 160^\circ$  with increasing  $R_{sm}$  roughness from *b1* to *b5*, since the surface tension of ethylene glycol is larger than that of hexadecane, leading to a larger contact angle. For each type of sample, the CAs and CAHs kept constant with increasing roughness, and the effect of wettability on the slip length was decoupled.

### 3.3. Effective Boundary Slip

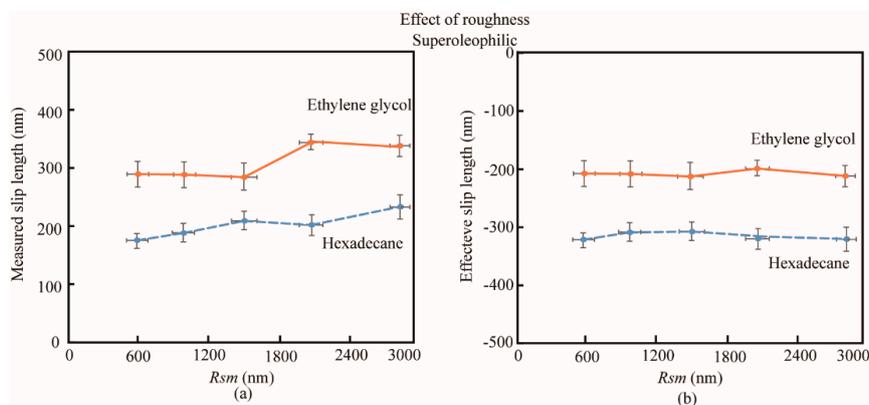
#### 3.3.1. Superoleophilic Surfaces

- Hydrodynamic forces.** Figure 6a shows the measured hydrophobic forces  $F_{hydro}$  applied on the AFM probe approaching the superoleophilic surface immersed in hexadecane with varying  $R_{sm}$  roughness as a function of separation distance  $D$ . The plots of experimental data exhibit nonlinear behavior at separation distances of 0 nm to 400 nm and are indicative of a slip boundary condition. In order to obtain the slip length, the  $V/F_{hydro}$  applied on the AFM probe is used for superoleophilic surfaces immersed in hexadecane and ethylene glycol as a function of separation distance  $D$ , as shown in Figure 6a. In the case of hexadecane, the plots of  $V/F_{hydro}$  on superoleophilic surfaces exhibit linear behavior at separation distances of 0 nm to 800 nm, and show a trend of the linear parts shifting to the left with increasing  $R_{sm}$  from samples *a1* to *a5*. This means that the interceptions of  $V/F_{hydro}$  on the horizontal ordinate shift to the left, and lead to an increasing slip length from samples *a1* to *a5*. For ethylene glycol, the plots of  $V/F_{hydro}$  are similar to those of hexadecane. This means that the increasing  $R_{sm}$  roughness leads to a larger slip length, as shown in Figure 6b. It can be noted that the tendencies are more obvious, because the surface tension of ethylene glycol is greater than that of hexadecane.



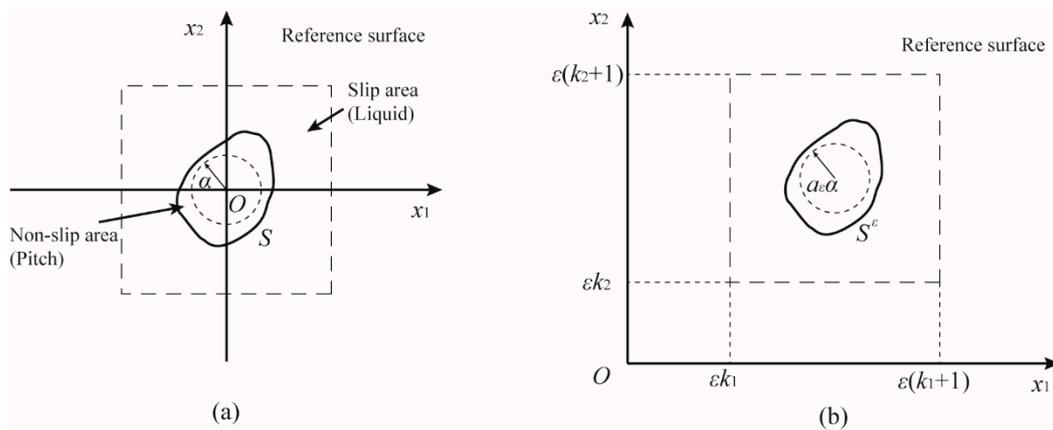
**Figure 6.** Hydrodynamic force  $F_{hydro}$  and  $V/F_{hydro}$  of a borosilicate sphere on superoleophilic surfaces immersed in (a) hexadecane and (b) ethylene glycol with various  $Rsm$  roughness at a sphere velocity of  $38.5 \mu\text{m/s}$ .

- Slip length.** Measured slip length was obtained from the hydrophobic forces according to Equation (1). Figure 7a shows the measured slip length data as a function of  $Rsm$  roughness. For samples  $a1$  to  $a5$ , the slip length of the superoleophilic surface immersed in hexadecane and ethylene glycol increased with increasing  $Rsm$  roughness. The effective slip length was obtained according to Equation (11). Figure 7b shows the effective slip length data as a function of  $Rsm$  roughness. Results show that all of the slip lengths are negative and remain constant from samples  $a1$  to  $a5$  after correction by compensation  $f^*$ . This means that the flow velocity at the reference surface is discontinuous due to the rough structure, and the slippage is independent of spacing roughness, where the slip length of the sphere and the location of the reference surface are taken into account.



**Figure 7.** (a) Measured slip length and (b) effective slip length on superoleophilic surfaces with varied  $Rsm$  roughness.

- Discussion.* It should be noted that slip boundary conditions at the reference surface are complex, as there is rough topography, and slip length at the interface of liquid, and rough superoleophilic surface is discontinuous, which should be studied by the average hydrodynamic forces detected using AFM. The effect of spacing roughness on slip length can be described by the following model, shown in Figure 8. The boundary of rough topography were replaced by a flat plane of reference surface, and the pitches were divided into square zones, where the average length of side  $\varepsilon$  was the value of  $Rsm$  roughness. We assumed that each zone was divided into two areas: (i) the no-slip area  $S^\varepsilon$ , corresponding to a cross-section of the pitch of the rough surface, containing a circle of radius  $\alpha$  centered in the origin, which is relative to the area of  $S^\varepsilon$ ; and (ii) the slip area, corresponding to a cross-section of the slippery part of fluid flow.



**Figure 8.** Mechanism of effect of spacing roughness on effective slip length on superoleophilic and superoleophobic surfaces with varied  $Rsm$  roughness. The cross-section of the surface was obtained by cutting at a height of reference surface  $h = R_q$  in the horizontal direction. (a)  $S$  is the no-slip area; and (b)  $S^\varepsilon$  is the average no-slip area.

We assume that the average no-slip area  $S^\varepsilon$  contains a circle of radius  $a_\varepsilon\alpha$ , via  $a_\varepsilon\alpha = \frac{1}{m} \sum_{i=1}^m \alpha_i$ , where  $\alpha_\varepsilon$  is a numerical prefactor. The no-slip area  $S^\varepsilon$  is defined by:

$$S^\varepsilon = \left( \begin{matrix} \varepsilon k_1 + \frac{\varepsilon}{2} \\ \varepsilon k_2 + \frac{\varepsilon}{2} \end{matrix} \right) + a_\varepsilon S, \tag{12}$$

where  $S^\varepsilon$  is expected to depend on the underlying geometry of the surface, and  $(\varepsilon k_1 + \frac{\varepsilon}{2}, \varepsilon k_2 + \frac{\varepsilon}{2})$  is the center of the average no-slip area  $S^\varepsilon$ .

The slip length can be estimated by the solid friction  $\Phi_s$  between solid and liquid, which is defined by the relative area of the no-slip area  $S^\varepsilon$  in the square of  $(\varepsilon k, \varepsilon k + 1)^2$ . It can be found that solid friction at the no-slip area  $S^\varepsilon$  is  $\Phi_s \sim \infty$ . The expression of solid friction  $\Phi_s$  is given by Bonnivard et al. [31]:

$$\Phi_s = \left( \frac{a_\varepsilon}{\varepsilon} \right)^2 |S^\varepsilon|,$$

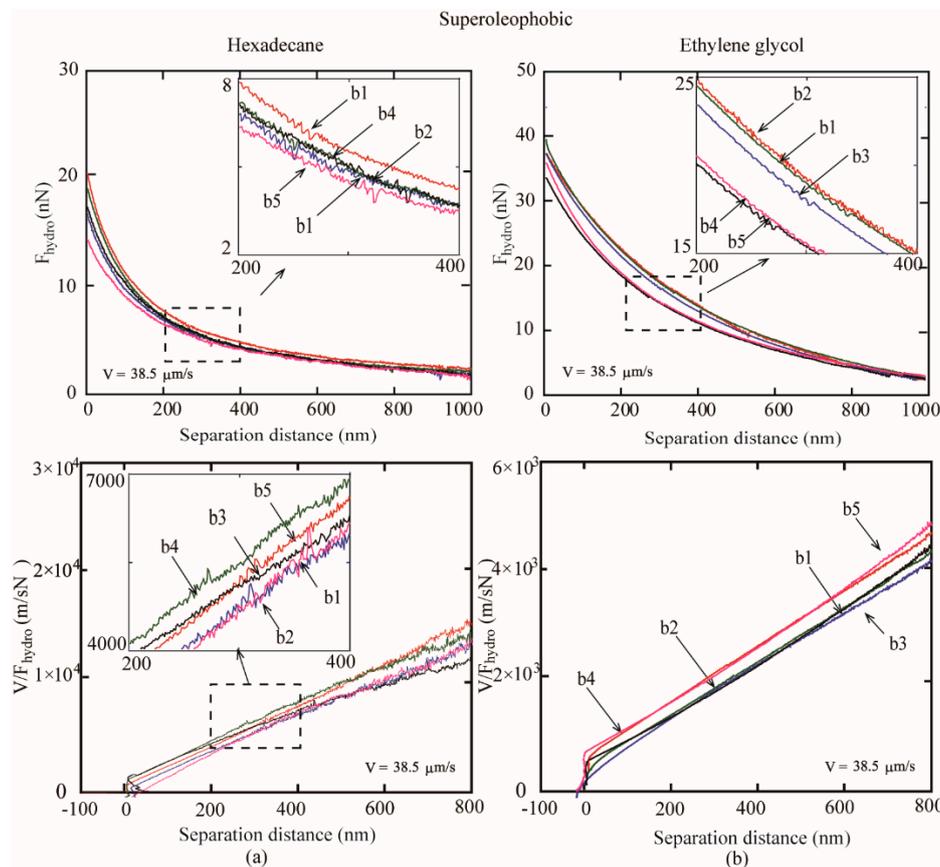
where  $|S^\varepsilon|$  is the area of the average no-slip area  $S^\varepsilon$ . Since  $\lim_{\varepsilon \rightarrow 0} \Phi_s = 0$ , the slip length can be obtained by:

$$b = \frac{\alpha}{\sqrt{\Phi_s}} = \frac{\alpha}{\left( \frac{a_\varepsilon}{\varepsilon} \right) \sqrt{|S^\varepsilon|}} = \frac{\alpha}{a_\varepsilon} \left( \frac{\varepsilon}{\sqrt{|S^\varepsilon|}} \right), \tag{13}$$

where  $\frac{\alpha}{a_e}$  is the constant and remains unchanged. Thus, the effect of spacing roughness on the effective slip length depends on the value of  $\frac{\epsilon}{\sqrt{|S^e|}}$ . With increased  $Rsm$ , the values of  $\frac{\epsilon}{\sqrt{|S^e|}}$  remain constant, therefore the results of effective slip length remain constant.

### 3.3.2. Superoleophobic Surfaces

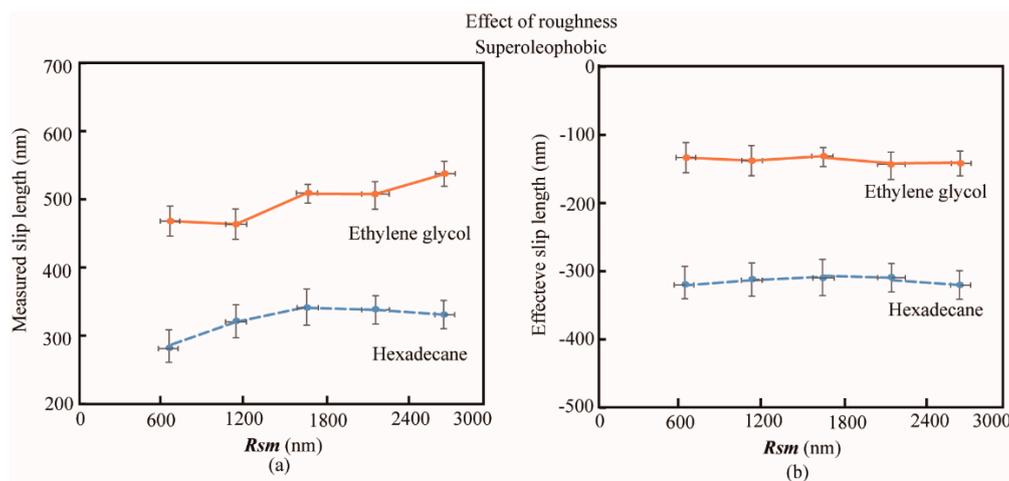
- Hydrodynamic forces.** The plots of measured hydrodynamic forces  $F_{hydro}$  between the colloidal AFM probe and the superoleophobic surfaces immersed in hexadecane and ethylene glycol, as a function of separation distance  $D$ , are shown in Figure 9. In order to obtain slip length, the  $V/F_{hydro}$  applied on the AFM probe is used for superoleophobic surfaces immersed in hexadecane and ethylene glycol as a function of separation distance. In the case of superoleophobic surfaces, it can be noted that the plots of  $V/F_{hydro}$  shift to the left with increasing  $Rsm$  from samples  $a1$  to  $a5$ . The results are similar to those of superoleophilic surfaces. This means that the interception of  $V/F_{hydro}$  on the axis of separation distance shifts to the left from  $b1$  to  $b5$  and leads to increased slip length. The change of hydrodynamic forces  $F_{hydro}$  can be expressed by the varying  $R_q$  roughness of surfaces, by the effect of the morphology of surfaces on the measured hydrodynamic forces.



**Figure 9.** Hydrodynamic forces  $F_{hydro}$  and  $V/F_{hydro}$  of a borosilicate sphere on superoleophobic surfaces immersed in (a) hexadecane and (b) ethylene glycol with varied  $Rsm$  roughness at a sphere velocity of  $38.5 \mu\text{m/s}$ .

- Slip length.** Measured slip length of the superoleophobic surface is obtained from the hydrophobic forces  $F_{hydro}$  and  $V/F_{hydro}$  according to Equation (1). Figure 10a shows the data of measured slip length as a function of  $Rsm$  roughness. With increased roughness from  $b1$  to  $b5$ , the slip length of the superoleophilic surface in hexadecane and ethylene glycol increases with increasing  $Rsm$  roughness. Then the effective slip length is obtained according to Equation (11). Figure 10b

shows the data of effective slip length as a function of  $R_{sm}$  roughness. The results are similar to those of the superoleophilic surface, and show that all slip lengths are negative and remain constant from  $b_1$  to  $b_5$ . This also can be explained by the existence of rough topography, leading to a discontinuity of boundary slip, and the values of  $\frac{\varepsilon}{\sqrt{|S^\varepsilon|}}$  remain constant with varying  $R_{sm}$ . For the superoleophobic surfaces, the reference surface of the morphology in a Cassie regime remains an open question. Consider the case of drainage between sphere and rough surface; the reference surface should be located at the height of  $R_q$ , as in a Wenzel regime. In this paper, application in micro-/nano-fluidic channels with rough walls on both sides has been considered, so the reference surface should still be considered as  $R_q$  of the roughness profile, which leads to a discontinuity of boundary slip.



**Figure 10.** (a) Measured slip length and (b) effective slip length on superoleophobic surfaces with varied  $R_{sm}$  roughness.

#### 4. Conclusions

Although numerous investigations addressing the question of drainage of the thin film between two surfaces represent an improvement over Reynolds' theory, the effects of surface roughness were ignored; thus, it could not be applied to obtain slip length on rough surfaces, such as superoleophilic/superoleophobic surfaces. Roughness is known to be a considerable parameter influencing the flow aptitude of liquids at the solid–liquid interface on surfaces. We have further improved the quantitation and measurement of effective slip length by using a colloidal probe AFM and laser confocal scanning microscopy. We conducted experiments with hexadecane and ethylene glycol, two kinds of oil, to study slip length on superoleophilic and superoleophobic surfaces with varying surface  $R_{sm}$  roughness. We also addressed the issues of experimental studies of boundary slip on rough surfaces. Negative slip length was found on superoleophilic and superoleophobic surfaces immersed in hexadecane and ethylene, as the viscosity of the liquids at reference surface were discontinuous. According to the results, the effective slip lengths kept constant with increasing  $R_{sm}$  roughness, as they depend on the value of  $\varepsilon/\sqrt{|S^\varepsilon|}$ , which is constant. These results contribute to further study on the behavior of liquid flowing near a rough solid interface, and the inhibition of hydrodynamic drag in micro-/nano-fluidic systems with omiphobic surfaces.

**Author Contributions:** Y.L. conceived the idea to perform this research. X.Z. and Y.P. guided the research scientifically and technically throughout. Y.L. performed all experiments and analyzed data. Y.L. and Y.P. wrote the paper. All authors discussed the content of this work and reviewed the manuscript. The manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript.

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