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# The Preparation of H13 Steel for TBM Cutter and the Performance Test Close to Working Condition

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**Abstract:** The material of disc cutters is important to full-face tunnel boring machines (TBM). In recent years, disc cutters were optimized and tested by many scholars all around the world. H13(4Cr5MoSiV1) steel is widely used due to its excellent properties, especially in TBM disc cutters. In this paper, H13 steel with optimized composition was prepared and heat treatment. The high temperature compression of H13 steel was conducted at the temperatures ranging from  $100~^{\circ}$ C to  $700~^{\circ}$ C, with strain rate at  $0.01~\text{s}^{-1}$ . The stress-strain curves, Rockwell hardness and microstructure of H13 steel after compression were obtained and analyzed. The results showed that the compression strength and hardness decreased as the temperature increased; and the compression strength, hardness and ductility decreased rapidly between  $600~^{\circ}$ C and  $700~^{\circ}$ C, HR<sub>700</sub> (the hardness of H13 steel at  $700~^{\circ}$ C) only reached 33.23 HRC. It is not recommended for TBM disc cutters to work in an environment over  $600~^{\circ}$ C.

Keywords: H13 steel; TBM disc cutter; high temperature compression; hardness

# 1. Introduction

A Full-face tunnel boring machine (TBM) is a large tunnel construction operating system integrating mechanical, hydraulic, electronic, and laser technologies. Compared with the traditional method of drilling and blasting, TBM has the characteristics of fast construction, a short construction period, good working environment and high comprehensive benefits, so it has been widely used in tunnel construction [1–4].

The main tool for TBM rock breaking is the disc cutters, which are mounted on the cutter head, and the consumption is extremely high due to the poor working conditions, in such conditions, the partial temperature could exceed 600 °C [5–7]. In order to reduce the consumption of the cutters, the cutter material needs to have high hardness, high wear resistance, good impact toughness, a certain resistance to tempering performance and a good processing performance [8].

H13 steel is a C-Cr-Mo-Si-V steel, which is widely used around the world [9–11]. Meanwhile, Extensive research have been conducted to explore the optimization of the chemical composition of H13 steel. H13 steel has high thermal strength, hardenability, wear resistance and hardness, and has good toughness and thermal fatigue at moderate temperatures [12–14]. Many TBM companies have produced H13 steel as a cutter material.

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In this study, the H13 steel was prepared and the working condition was simulated at high temperature compression. The effects of temperature, compression stress-strain curves, hardness and microstructure on H13 steel were analyzed. It is believed that the results will serve as a guide for efficient selection and production of TBM disc cutters.

## 2. Materials and Methods

# 2.1. The Initial Microstructure and Heat Treatment

The as-cast H13 steel in this study was smelted by the Medium frequency induction furnace (Atmosphere Protection) (Zhuzhou Shuangling Technology Co., Ltd., Zhuzhou, China) and the Vacuum electroslag furnace (Zhuzhou Shuangling Technology Co., Ltd., Zhuzhou, China) [15]. The chemical composition (wt.%) of as-received H13 steel is shown in Table 1.

	C:	N /	D	С.	C	N/-	<b>T</b> 7		NT:
	Si	MIN	P	S	Cr	IVIO	V	Со	IN1
0.44	0.93	0.46	0.018	0.007	5.02	1.37	1.02	0.03	0.13

**Table 1.** The chemical composition of H13 steel (wt.%).

The heat treatment process application is shown in Figure 1. The as-cast H13 steel was firstly preheated and retained at  $700\,^{\circ}\text{C}$  for  $60\,^{\circ}\text{C}$  min inside a vacuum furnace, then it was heated up to  $1050\,^{\circ}\text{C}$ , and held up for  $45\,^{\circ}\text{min}$  for quenching, followed by oil-cooling to  $60\,^{\circ}\text{C}$ . After the quenching process, the steel was reheated and retained at  $580\,^{\circ}\text{C}$  for  $120\,^{\circ}\text{min}$ , followed by air-cooling to room temperature inside the furnace [16,17].

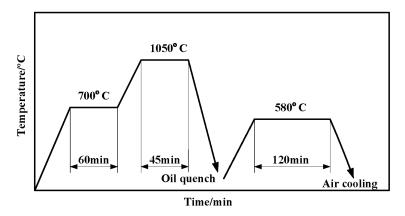


Figure 1. Quenching-tempering heat treatment process curve.

The specimens for compression and metallographic observation were machined from as-casted steel and heat treatment steel mentioned above. The metallographic specimens were polished and corrosion in the concentration 4% of nitric alcohol solution for about 1 min at room temperature, which was observed by OLYMPUS DSX500 microscope (Olympus Corporation, Tokyo, Japan).

Figure 2 shows the microstructure of initial as-cast and heat treatment H13 steel. It can be seen in Figure 2a, there exists segregation in the as-cast H13 steel. The microstructure was not uniform, and pseudo-eutectic carbides were present in the segregation zone of the black alloy elements [18]. After quenching and tempering of H13 steel, the coarse columnar crystals and dendrites in the as-cast microstructure were crushed, and the pseudo-eutectic carbides were broken and partially dissolved in the matrix. By comparing Figure 2a,b, it could be seen that under the effect of temperature and pressure, the diffusion rate of atoms was accelerated, the segregation was effectively improved, and the chemical composition became uniform after a long time of thermal insulation. The organization was mainly based on small lath tempered martensite.

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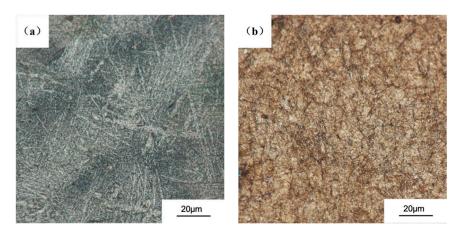


Figure 2. Microstructure of H13 steel: (a) As-cast; (b) heat treatment.

# 2.2. The Condition of High Temperature Compression Test

Figure 3 is an illustration of the high temperature compression tester produced by Sinotest Equipment Co., ltd. (DDL10, Changchun, China). A special plate with a hardness greater than 65 HRC was adopted during compression. The test procedure and specimens for high temperature compression are also shown in Figure 3.

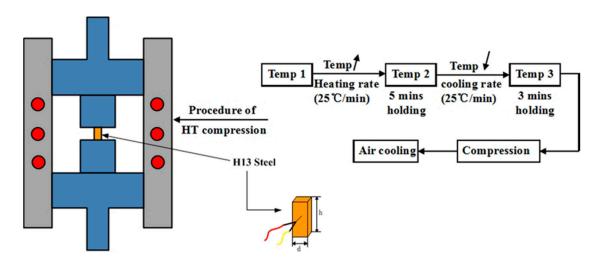


Figure 3. Compression tester and specimen for high temperature compression.

The size of specimens for compression is  $5 \times 5 \times 10$  mm, considering the work and failure conditions of TBM cutter comprehensively, the specimens were compressed to a strain of 0.25. First, the specimens (as-cast and heat treatment) were placed in the compression tester and compressed under room temperature. Then, the high temperature compression tests started, the steps of each test showed as follows: Temp 1 indicates the room temperature, Temp 2 indicates the temperature after heated and Temp 3 indicates the test temperature. The specimens (heat treatment) were heated to Temp 2 (50 °C higher than Temp 3 of 100–700 °C with a 100 °C interval at 25 °C/min and held for 5 min), after that, the temperature was adjusted back to Temp 3 at 25 °C/min and held for 3 min to get a uniform temperature distribution. Finally, the specimens were compressed to a strain of 0.25 under Temp 3 and strain rates of 0.01 s<sup>-1</sup>, followed by air-cooling to Temp 1 inside the compression tester and the test ended. After the high temperature compression, the specimens were cut lengthwise, polished and corrosion, then, optical microscopes were used to observe the structural changes in the specimens.

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## 2.3. Mechanical Properties

The mechanical strength of the specimens was measured through hardness tests and the high temperature compression tests above. Hardness was measured in terms of Rockwell hardness, taking several points in the upper, the middle and lower part of specimens after high temperature compression, and the average was obtained by measuring specimens for 5 times per test condition.

#### 3. Results

# 3.1. Analysis of Compression Curve

The stress-strain curves of H13 specimens (as-cast and heat treatment) at room temperature are shown in Figure 4. It could be seen from Figure 4 that the mechanical properties of the H13 steel after heat treatment have been significantly improved. Its maximum compression strength ( $\sigma_c$ ) is about four times that of the as-cast steel, which reached 2700 MPa, and shows that the elastic limit has also been greatly improved. However, the ductility of the H13 steel after heat treatment is poor, the reason leading to this phenomenon is the high hardness and high strength of the mechanical properties of tempered martensite, while due to the brittle phase of the tempered martensite, it resulted in the increased strength but decreased the ductility. At the same time, due to the presence of tempered troostite, the elastic limit and yield limit of the material were increased, and a certain degree of toughness also appeared. This meets the requirements of the high strength and high elastic limit of the TBM cutter.

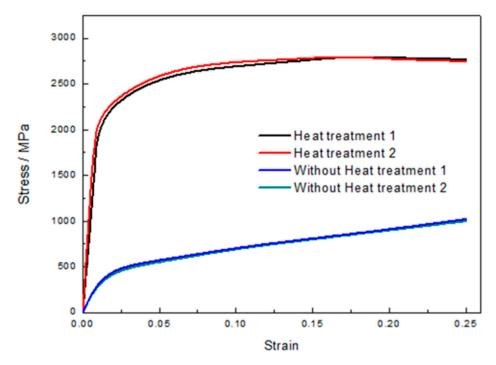


Figure 4. Stress-strain curve of H13 steel at room temperature.

The stress-strain curves of H13 specimens (heat treatment) at high temperature are shown in Figure 5. It could be seen from Figure 5 that the compression strength, overall, decreased as the temperature increased, and the reduction of the stress between 100 °C and 500 °C was relatively small; when the temperature was raised to 600 °C, the compression strength, the elastic limit and ductility decreased rapidly, and the brittleness appeared. The brittleness of H13 steel resulted in serious deterioration of the mechanical properties of steel, making it difficult to be used in the range of brittle temperatures and would easily get damaged which will affect practical work; when the temperature was raised to 700 °C, the  $\sigma_{c700}$  only reached 480 MPa, but ductility of the material was restored.

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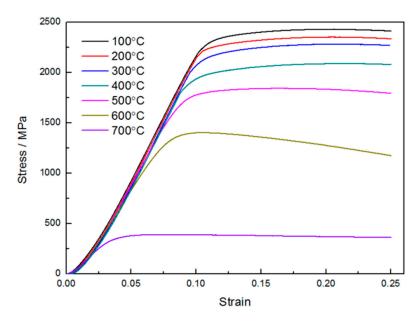
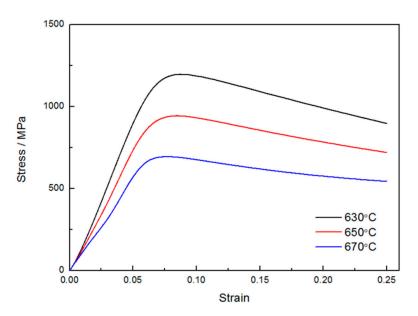


Figure 5. Stress-strain curve of H13 steel at high temperature.

In order to explore the mechanical properties of H13 steel between 600–700  $^{\circ}$ C, three groups of compression tests (630  $^{\circ}$ C, 650  $^{\circ}$ C and 670  $^{\circ}$ C) were added. The results of curves are shown in Figure 6.



**Figure 6.** Stress-strain curve of H13 steel at 630  $^{\circ}$ C, 650  $^{\circ}$ C and 670  $^{\circ}$ C.

As shown in Figure 6, the overall trend of the compression strengths at  $630\,^{\circ}\text{C}$ ,  $650\,^{\circ}\text{C}$  and  $670\,^{\circ}\text{C}$  were similar to the one at  $600\,^{\circ}\text{C}$ , which decreased rapidly as the temperature increased, as the ductility also decreased rapidly.

The reason which might cause the above phenomenon could be the high temperature compression of H13 steel leading to the tempered martensite decomposition, the continuous precipitation of carbide and the decrease of the ductility and strength.

# 3.2. Analysis of Hardness

The results of the Rockwell hardness of H13 specimens after high temperature compression are shown in Figure 7. As shown in Figure 7, the hardness decreased with the increase of compression

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temperature, which showed the reduction of the hardness between 100  $^{\circ}$ C and 500  $^{\circ}$ C was relatively small. In this test, the HR<sub>100</sub> reached 58.21 HRC, and HR<sub>500</sub> reached 55.46 HRC. When the temperature was raised to 600  $^{\circ}$ C, the hardness decreased rapidly, and when the temperature was raised to 700  $^{\circ}$ C, HR<sub>700</sub> only reached 33.23 HRC, and the organization is mainly based on tempered sorbite.

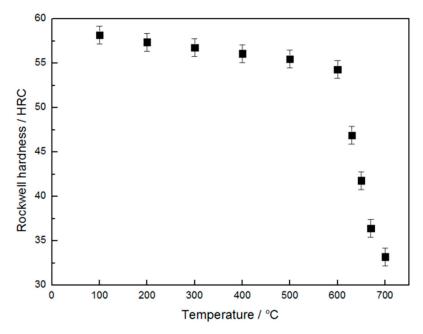


Figure 7. Rockwell hardness of H13 steel at high temperature.

# 3.3. Analysis of Microstructure

In order to further analyze the results, Figure 8 shows the microstructure of H13 steel compressed to a strain of 0.25 under a strain rate of 0.01 s $^{-1}$  from 500 °C to 700 °C. Due to the excellent alloy ratio, tissues and grains were refined. Meanwhile, special carbides were formed because of alloying elements, the expansion of carbon atoms was hindered, and the decomposition of martensite was delayed. It could be seen that as the temperature increased, the martensite content gradually decreased. When the temperature reached 600 °C, as shown in Figure 8b, the alloying elements in the sample were segregated at the grain boundary, so that the grain boundary embrittled, and led to a decrease in material ductility. As the temperature continued to rise, the segregation grew, aggregated, and spheroidized, which restored the ductility of the material.

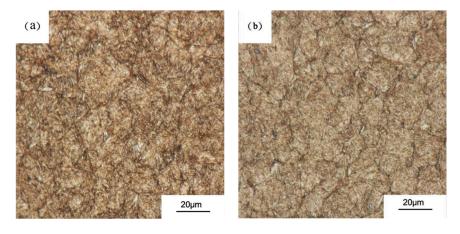
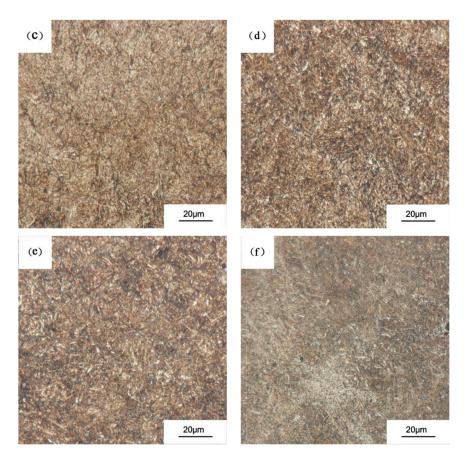


Figure 8. Cont.

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**Figure 8.** Microstructure of H13 steel after high temperature compression (a) 500 °C, (b) 600 °C, (c) 630 °C, (d) 6500 °C, (e) 670 °C, (f) 700 °C.

## 4. Conclusions

The high temperature compression of H13 steel was conducted at the compression temperatures ranging from  $100 \,^{\circ}\text{C}$  to  $700 \,^{\circ}\text{C}$ , with the strain rate at  $0.01 \, \text{s}^{-1}$ . The following conclusions could be summarized through the analysis on the compression curves, Rockwell hardness and microstructure:

During the high temperature compression, the compression strength decreased as the temperature increased. The reduction of the stress between 100 °C and 500 °C was relatively small, the compression strength, the elastic limit and ductility decreased rapidly between 600 °C and 700 °C, and when the temperature was raised to 700 °C, the ductility of the H13 steel was restored.

The hardness decreased with the increase of compression temperature, and the reduction of the hardness between 100  $^{\circ}$ C and 500  $^{\circ}$ C was relatively small. When the temperature reached over 600  $^{\circ}$ C, the hardness decreased rapidly, and HR<sub>700</sub> only reached 33.23 HRC.

The martensite in the material was decomposed when the temperature increased, the grain boundary segregation started to occur after  $600\,^{\circ}$ C, which decreased the strength and ductility of the material. As the temperature continued to rise, the segregation grew, aggregated, spheroidized, and the ductility recovered.

Since H13 steel showed a sharp deterioration in properties after 600  $^{\circ}$ C, it is not recommended for TBM cutters to work in an environment of temperature over 600  $^{\circ}$ C.

**Author Contributions:** Y.H., H.Z and J.T. conceived and designed the experiments; M.X. and M.W. (Mingze Wang) performed the experiments; M.W. (Maosen Wang) and A.Z. analyzed the data; J.T. wrote the paper.

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