

Article

Detection of Concrete Cover of Reinforcements in Reinforced Concrete Wall by Microwave Thermography with Transmission Approach

Sam Ang Keo ^{1,*}, Franck Brachelet ², Didier Defer ² and Florin Breaban ²¹ Cerema, Research Team ENDSUM, 23 Amiral Chauvin Avenue, 49130 Les Ponts-de-Cé, France² Univ. Artois, IMT Nord Europe, Junia, Univ. Lille, ULR 4515, Laboratoire de Génie Civil et Géo-Environnement (LGCgE), 62400 Béthune, France

* Correspondence: keo_samang@yahoo.com

Abstract: Concrete cover has an important role in reinforced concrete (RC) structures because it protects reinforcement bars from the bad effects of weather, fire, and bad environmental conditions that cause the corrosion of the reinforcements. Although it is an essential parameter to be considered for structural health monitoring (SHM), its detection by infrared thermography, especially in the heating phase, has not been accessed yet. The detailed analysis and discussions of physical phenomena, known as diffraction and interference, affecting the thermograms during the detection of the steel bars by microwave thermography have given an essential key for resolving this issue. The present paper proposes an innovative methodology with microwave thermography for determining the concrete cover thickness of one-layer reinforcements (12 mm in diameter and regularly placed at 10 cm) in an RC wall (1 m × 1 m × 6.5 cm). By using the transmission approach with five angles of microwave antenna direction (0°, 15°, 30°, 45°, and 60°) and the Snell–Descartes law and linear law, the proposed methodology leads us to deduce the approximate value of the concrete cover thickness (37.74 mm), which is close to the real value (38 mm), as well as the spacing of the steel bars and dielectric constant of the concrete. The detection of the concrete cover thickness is another new remarkable achievement of infrared thermography methods.

Keywords: structural health monitoring (SHM); electromagnetic nondestructive evaluation (NDE); microwave thermography; concrete cover thickness; steel reinforcements; reinforced concrete (RC) wall

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1. Introduction

Concrete cover has an important role in reinforced concrete (RC) structures. It protects reinforcement bars from the bad effects of weather, fire, and bad environmental conditions that cause the corrosion of the reinforcements and reduce the service life of the RC structures. Thus, it is an important durability indicator for RC structures, and an essential parameter to be considered for the structural health monitoring (SHM) of RC structures [1]. For this reason, the study on the concrete cover, as well as the development of different non-destructive evaluation (NDE) methods for detecting this parameter, have become crucial. The radar method is one of the NDE methods commonly used for the detection of the concrete cover [2,3]. This electromagnetic method has also been used for determining the location of reinforcements and assessing moisture in RC structures [4–8]. However, this method is a contact method (contact between the wave transmitter and the detected element) while the infrared thermography method is a non-contact one with a simple and rapid implementation.

The infrared thermography method is a temperature measurement technique based on heat transfer by thermal radiation. It is an NDE technique, that is based on measuring

the temperature difference at the surface of materials or structures to detect the presence of problems, defects, or variations of thermal conduction properties beneath the surface [9]. The detection by infrared thermography is classified into two approaches: active thermography and passive thermography. The development of active infrared thermography methods has been accompanied by the development of interpretation methods and adopted stimulation techniques (heating source or excitation) [9–17]. Active infrared thermography methods have been developed with different types of excitation (halogen lamps, CO₂ lasers, microwaves, etc.) for various applications, such as spot weld inspection [18] and the detection of a metal element behind a wooden plate [19]. Other applications for defect detection include defects of roll-to-roll printed conductors [20], defects in reinforcement with a carbon fiber-reinforced polymer (CFRP) [21–24], as well as defects in biomedical materials [25]. The latest development with a new microwave excitation system has enabled the detection of reinforcement in a reinforced concrete wall, which has highlighted the contributions of microwave excitation [26–30]. The microwave excitation is of great interest because of its volumetric heating, with a penetration depth of waves (which depends, in particular, on the dielectric constant of the detected material [31–34]), allowing the visualization of steel bars in the RC structure during the heating phase.

However, the detection of the concrete cover thickness (quantitative) by infrared thermography, especially in the heating phase, has not been accessed yet. The detailed analysis and discussions of the physical phenomena known as diffraction and interference affecting the thermograms during the detection of the steel bars by microwave thermography have given an essential key, leading to the resolution of this issue. As a result of the study, the effects of incident waves on the thermograms in both detection approaches (reflection and transmission) have also been clarified. On the thermograms in the reflection approach, concrete parts in the reflected areas are hotter than other areas, whereas the fractions in the areas of wave superposition (interference) are hotter than other areas in the transmission approach [35].

The present study shows an innovative methodology for determining the concrete cover thickness of one-layer reinforcements in a concrete wall with microwave thermography. In the methodology, the transmission approach (the infrared camera and the microwave antenna are situated on the same side) is used. It is a physical and mathematical methodology because it depends on a physical law called Snell–Descartes and the linear function of a non-linear relation between incident waves and shifts deduced from temperature profiles. The temperature profiles are obtained from the thermograms of the transmission approach with different incident waves. The details of the methodology are explained in the next part of the paper. At the end of the methodology, the values of the dielectric constant and the concrete cover thickness are deduced. This is a remarkable outcome of the application of physical law and mathematical analysis for detection by the microwave thermography method.

2. Methodology

The principle of the proposed methodology is illustrated by a flowchart, as shown in Figure 1. The methodology is divided into seven steps. From the first step to the fourth step, expertise in infrared thermography methods is applied. In the first step, five experimental campaigns with the microwave thermography method are carried out with five angles of the incident wave (θ_i): 0° (normal direction of the microwave antenna), 15°, 30°, 45°, and 60°. It is worth reminding that, in the transmission approach, the infrared camera and the heating source (and the antenna) are not situated on the same side. Details of the experimental set-up are shown in the next part of the present paper. In the second step, the thermograms are obtained from all the tests with the RC wall. Then, one thermogram at an instant is to be selected for each angle of the incident wave. The criteria for selecting the thermogram are based on the thermal contrast being optimal so that the corresponding temperature profile, to be drawn in the third step, gives clear peaks. Multiple choices are possible, but the selected thermogram must be in the heating phase to avoid thermal

contrast decrease on the thermogram due to thermal conduction in the detected materials. All the temperature profiles for all θ_i are drawn on the same axes to facilitate deducing the values of the shifts of the peaks on the temperature profiles (compared to the case of normal direction) in the fourth step. The shift value for the case of 15° of the incident wave angle is measured from the peaks of its temperature profile to the peaks of the temperature profile for the case of the normal incident waves. The same way of measurement is used to obtain the shift values for the other cases of incident wave angles. It is worth noticing that the shifts (Δ_i) are generated by the effect of the refraction of the waves after reaching the steel bars inside the detected RC wall, which was interpreted in the previous study [35]. From step five to step seven, which is the last step, a combination of a physical law and a mathematical analysis method is needed. In step five, a non-linear relation between θ_i and Δ_i is created by using the Snell–Descartes law (as presented in Figure 2) and a geometrical relation between the Δ_i , the transmitted waves in the concrete (θ_t), and the concrete cover thickness (e).

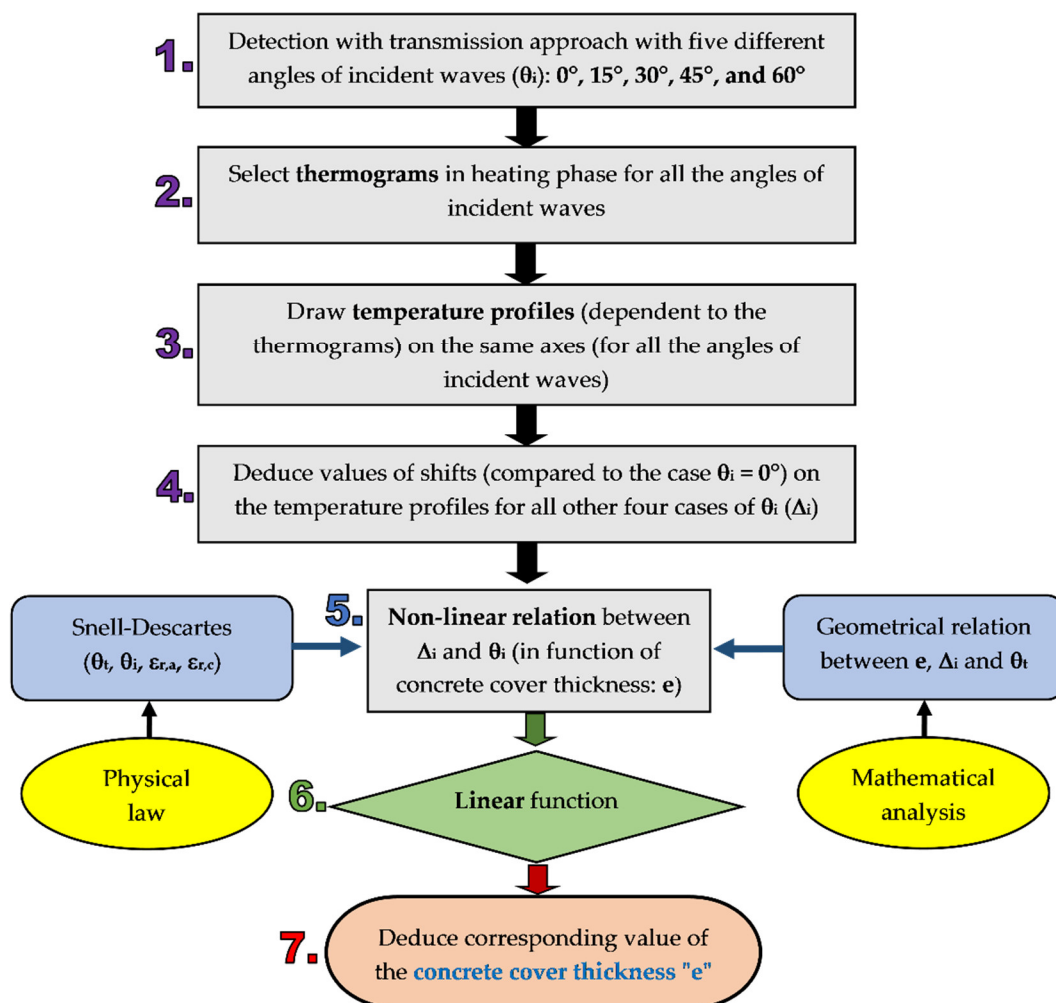


Figure 1. Methodology for detecting the concrete cover thickness of one-layer reinforcements in RC wall by microwave thermography method with transmission approach.

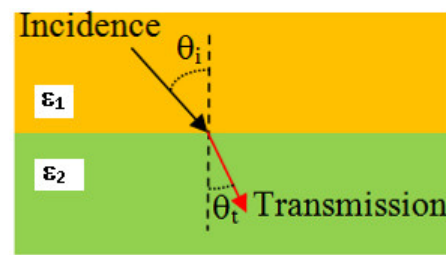


Figure 2. Refraction of wave by Snell–Descartes's law.

The theory gives the relation between the incident waves and refracted waves as the following equation:

$$\sqrt{\varepsilon_1} \times \sin \theta_i = \sqrt{\varepsilon_2} \times \sin \theta_t \quad (1)$$

where ε_1 is the dielectric constant of medium 1, ε_2 is the dielectric constant of medium 2, θ_i is the angle of the incident waves in medium 1, and θ_t is the angle of the transmitted waves in medium 2. In our study, medium 1 is the air, and medium 2 is the concrete. The dielectric constant of the air is equal to 1 ($\varepsilon_1 = 1$) [31].

The geometrical relation between Δ_i , θ_t , and the concrete cover (e) can be illustrated in Figure 3. As shown in Figure 3a, which was discussed in the previous study [35], the concrete in the areas of inference (superposition of the waves) of the refracted waves is hotter than in the other areas. The same study also showed that the steel bars in the detected wall play a role as an obstacle to the transmitted waves, which makes some fractions of the waves totally reflected to the concrete surface. The fractions of the refracted waves (with the transmitted angle θ_t) around a steel bar can be simplified, as shown in Figure 3b.

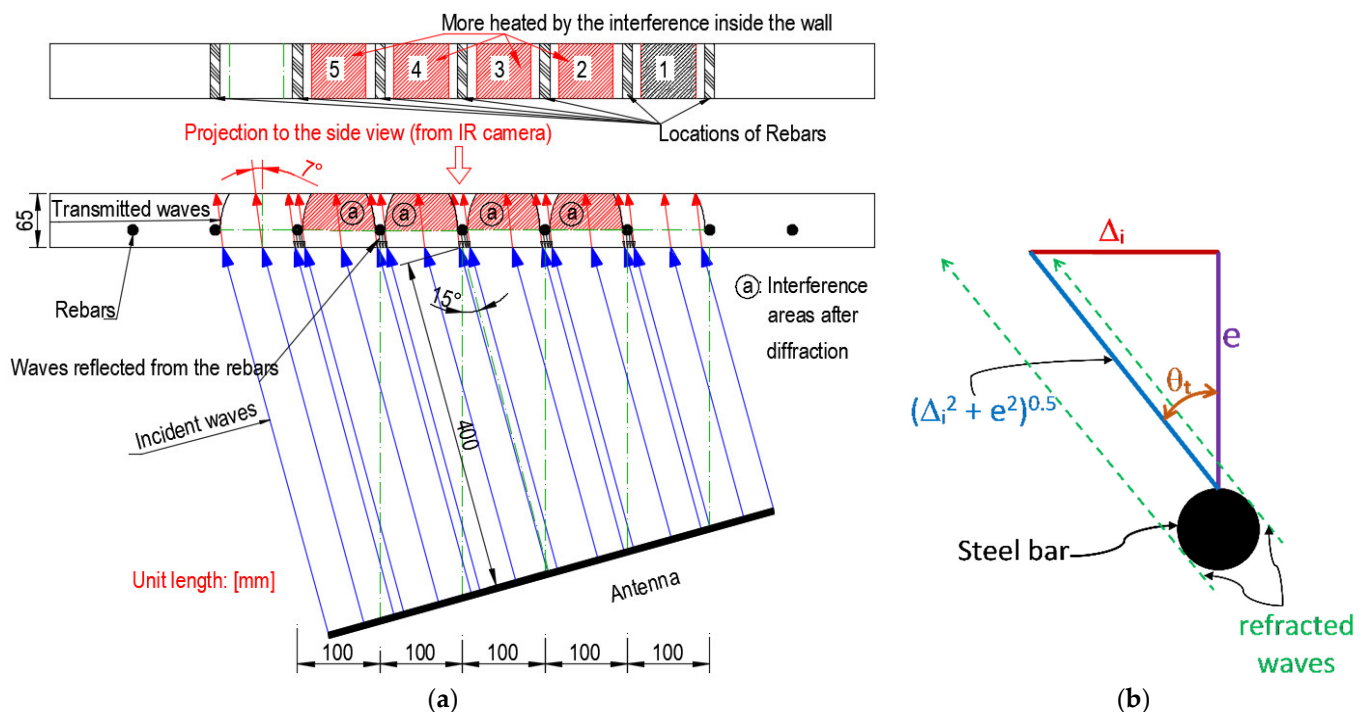


Figure 3. Schemas for geometrical relation between e , Δ_i , and θ_t : (a) Effect of the interference on the thermogram in transmission approach ($\alpha = 15^\circ$) [35]; (b) Simplified schema of refracted waves around a steel bar.

By applying the Pythagorean theorem and trigonometric formula to the simplified schema of the refracted waves in Figure 3b, the following equation is obtained:

$$\sin \theta_t = \frac{\Delta_i}{\sqrt{\Delta_i^2 + e^2}} \quad (2)$$

By combining Equations (1) and (2), we get the equation:

$$\frac{(\sin \theta_i)^2}{\varepsilon_2} = \frac{\Delta_i^2}{\Delta_i^2 + e^2} \quad (3)$$

Supposing that $X = (\sin \theta_i)^2$ and $Y = \Delta_i^2$, Equation (3) becomes:

$$X \times Y + e^2 \times X = \varepsilon_2 \times Y \quad (4)$$

Equation (4) is a non-linear relation in which the concrete cover (e) as a constant parameter is to be found. By dividing this non-linear equation by X , another form of the equation is obtained:

$$Y = \varepsilon_2 \times \left(\frac{Y}{X} \right) - e^2 \quad (5)$$

In the proposed methodology, the non-linear equation (of the X and Y variables) is to be converted to a linear equation (in step 6). For this purpose, we suppose that $X = \frac{Y}{X'}$ and $y = Y$. Then, Equation (5) becomes:

$$y = \varepsilon_2 \times X - e^2, \quad (6)$$

which is a linear function with ε_2 as the gradient constant, and a squared value of the concrete cover (e^2) is to be found.

Thus, the concrete cover thickness (e) can be deduced (at the final step of the methodology) from the line represented by linear Equation (6). It is worth noticing that two essential elements allowing us to detect the concrete cover (e) with the proposed methodology are: the angles of incident waves (θ_i) and the shift values (Δ_i).

3. Experimental Campaigns

The sample used for the tests was an RC wall of 1 m × 1 m dimensions and a 6.5 cm thickness, cast with a water/cement/sand/coarse aggregate mixing ratio of 1:1.6:4.45:4.7 (by weight). The reinforcements inside the RC wall were steel bars of 12 mm in diameter, regularly placed at 10 cm. As the reinforcements had one layer, there were two values of concrete cover thickness: 3.8 cm and 1.5 cm. The sample was subjected to testing at the age of 3 months. The experimental setup of the tests is shown in Figure 4.

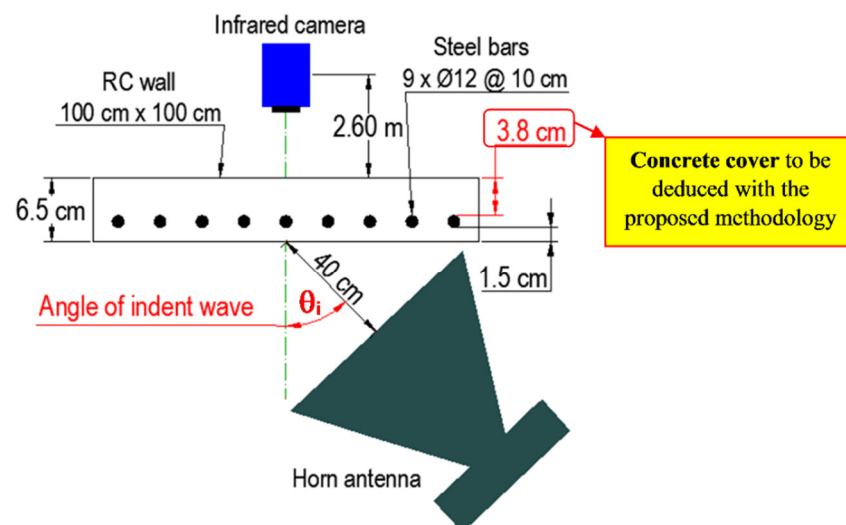


Figure 4. Experimental setup of the detection of RC wall by microwave thermography with transmission approach.

A mid-wavelength infrared camera of FLIR, sensitive to medium waves in the range of 3–5 μm , with a 320×256 matrix detector in InSb (indium antimonite), was placed at 2.6 m from the wall in the normal direction so as to detect the whole area of the wall to be heated by the microwaves. The microwaves used for the tests had a frequency of 2.45 GHz, and were guided onto the tested sample by a horn antenna with an opening of 40° , a gain of 21.67 dB in its main direction, and aperture dimensions of $59 \text{ cm} \times 56 \text{ cm}$. The sample was placed at 40 cm from the antenna's aperture.

Five tests were carried out for five different antennas' directions corresponding to the angles of the incident waves (θ_i): 0° (the normal direction of the microwave antenna), 15° , 30° , 45° , and 60° . The thermograms were recorded at regular intervals (one image per second). The sample was heated with an average power of 600 W for 5 min.

It is essential to note that the concrete cover deduced from the methodology (with the transmission approach) was behind the reinforcement layer, not exposed to the microwave antenna. The use of the normal direction of the infrared camera is an advantage for the transmission approach, compared to the reflection approach, which can give real dimensions to the thermograms.

4. Result Analysis and Discussion

4.1. Angles of Transmitted Waves

It is important to observe how the angle of the transmitted waves changed when the angle of the incident waves varied because it allows us to understand what happened inside the detected RC wall. Based on the Snell–Descartes law, the evolution of the angles of the refracted waves (θ_t) in the function of the direction of the microwave antenna used in the experimental campaigns for the proposed methodology is shown in Figure 5.

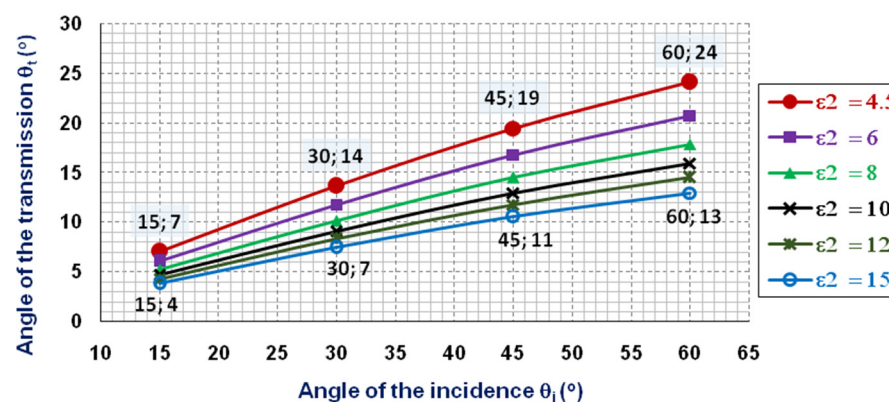


Figure 5. Angles of refracted waves (θ_t) in the function of the incident waves (θ_i) and the dielectric constant of the concrete (ϵ_2).

The evolution of the transmitted waves depends also on the dielectric constant of the concrete. As the real value of the dielectric constant of the tested concrete is unknown, the graphs for six different values of the dielectric constant of concrete (ϵ_2) are proposed. The proposed values of ϵ_2 are for common concrete, which vary from about 4.5 to 15 [31]. According to the graphs in Figure 5, we see that when the angle of the incident waves increases from 15° to 60° , the angle of the refracted waves also increases. However, the angles of the refracted waves are always smaller than the angles of the incident waves: they increase from 4° to 13° (the minimum angles) when $\epsilon_2 = 15$, and from 7° to 24° (the maximum angles) when $\epsilon_2 = 4.5$. The small values of the angles of the refracted waves also allow us to know that the shifts' values (Δ_i) to be determined for the proposed methodology are very small.

4.2. Determination of the Shifts' Values (Δ_i) from the Thermograms

As mentioned in the methodology section of this paper, the selection of the thermograms is very important in the procedure for determining the Δ_i . Five thermograms, selected from the detection of the RC wall, with five different angles of the incident waves (or the direction of the microwave antenna), are shown in Figure 6. All the selected thermograms were not obtained at the same instant of heating, although the same heating duration was used for the tests: 172 s when $\theta_i = 0^\circ$, 243 s when $\theta_i = 15^\circ$, 288 s when $\theta_i = 30^\circ$, 290 s when $\theta_i = 45^\circ$, and 281 s when $\theta_i = 60^\circ$.

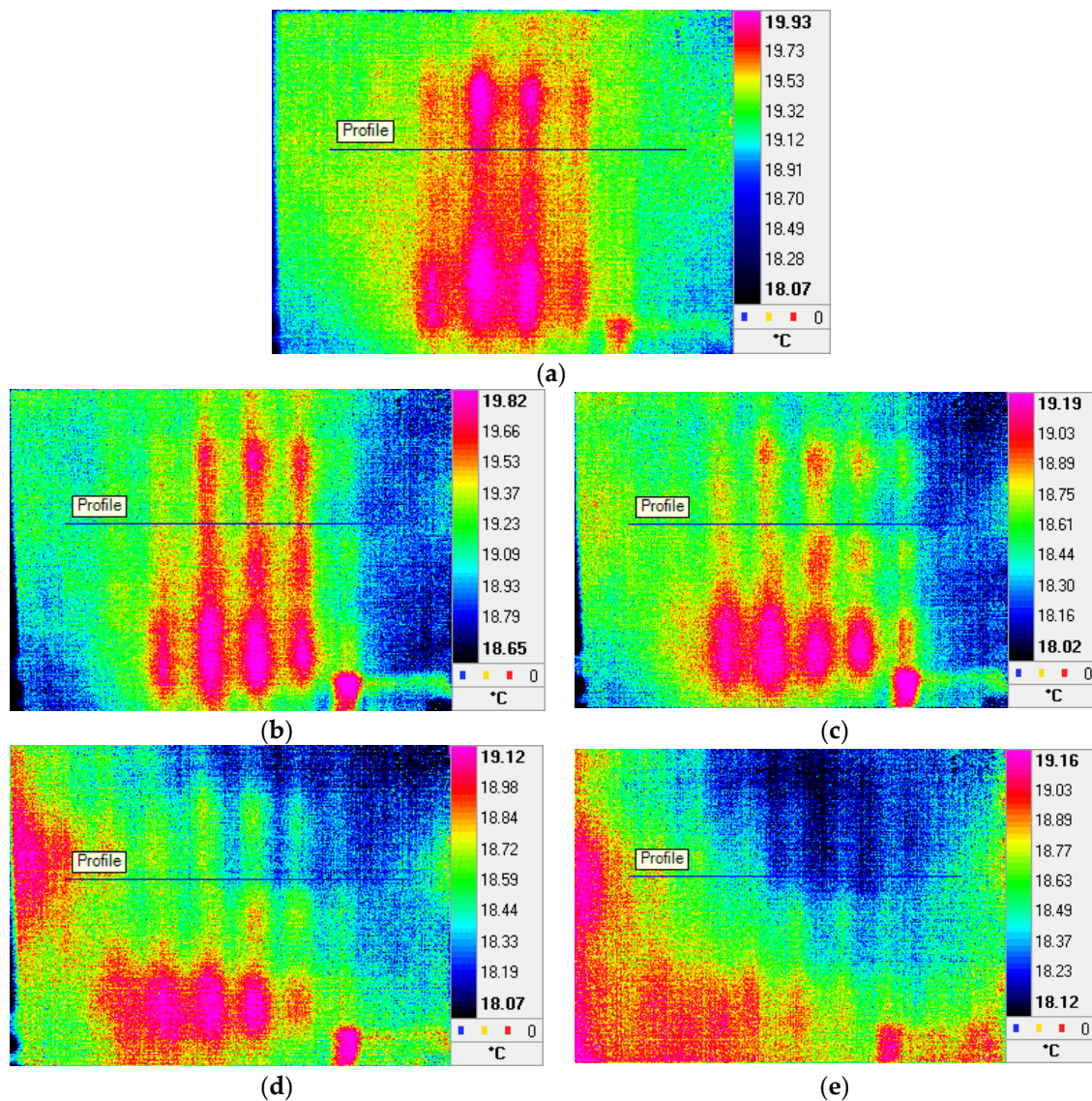


Figure 6. Thermograms from the detection of RC wall by transmission approach at different instants for different angles of incident waves (θ_i): (a) Thermogram at 172 s when $\theta_i = 0^\circ$; (b) Thermogram at 243 s when $\theta_i = 15^\circ$; (c) Thermogram at 288 s when $\theta_i = 30^\circ$; (d) Thermogram at 290 s when $\theta_i = 45^\circ$; (e) Thermogram at 281 s when $\theta_i = 60^\circ$.

On all the thermograms, we can see the heated areas due to the inference of the refracted waves between the steel bars inside the detected concrete wall. In order to obtain the temperature profiles for determining the shifts' values, a horizontal segment (the same length on all the thermograms) is placed at the same position (in the vertical and horizontal direction) on all the thermograms. The obtained temperature profiles for all the angles of the incident waves ($\theta = \theta_i$) are presented in Figure 7. The horizontal axis corresponds to the dimension (the length) of the detected RC wall.

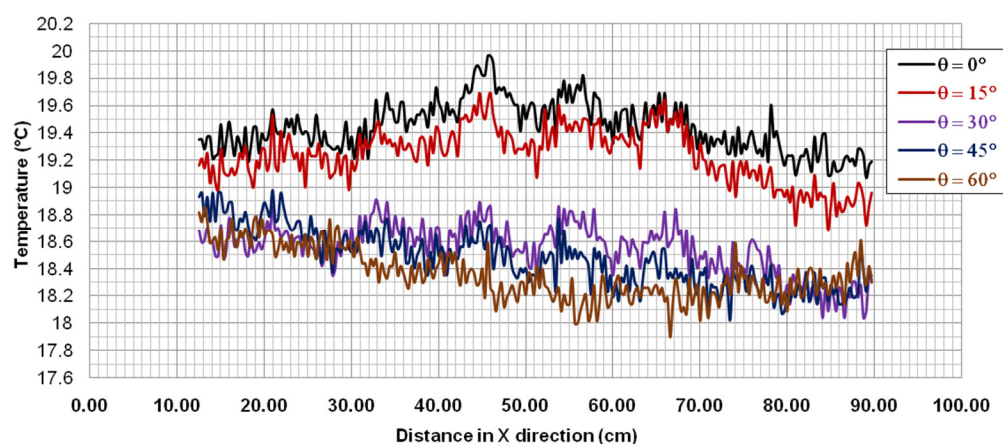


Figure 7. Temperature profiles for different angles of incident waves ($\theta = \theta_i$).

In order to deduce the shifts' values, the bottom peaks (which correspond to the real positions of the steel bars in case the normal direction of the microwave antenna is used) of the temperature profiles have to be defined. However, the forms of the temperature profiles do not facilitate the determination of the peaks' positions. For this reason, convenient fitting curves were needed for all the temperature profiles. In our study, moving the average with a period of 5 was used. Other fit functions (such as linear, exponential, logarithmic, polynomial, and power) have also been tried, but the moving average gives the best-fit curves. Other periods (3, 4, and 6) have also been tried, but period 5 gives the best-fit curves. It is necessary to note that the main objective of using the moving average fit curves is to facilitate the determination of the peaks on the temperature profile curves (after eliminating the multiple pulses) but to avoid a shift between the obtained fit curves and the original temperature profile curves. The peaks were hard to determine with period 3, while period 4 gave a better appearance of some peaks. Period 6 gave good peaks too (compared to period 5), but small shifts (compared to the initial temperature curves) started to appear, and the higher the period was used, the bigger shifts appeared. The fitted curves of the temperature profiles, after the application of the moving average, for all the angles of the incident waves are shown in Figure 8.

It is worth noting that 100 cm in the horizontal axis corresponds well to the 1 m width of the detected wall. The minor gridlines of 1 cm lead to a good observation of the shifts (from the peaks for different angles of the incident waves compared to those of the normal incident wave). On the new graphs of the temperature profiles, the peaks clearly appear. We can also observe the zoomed area (from 40 cm to 60 cm) to see the difference between both states of the temperature profiles: before and after the application of the moving average.

As there is no effect on the direction of the infrared camera, the temperature profile for the case of the normal direction of the antenna (the angle of the incident waves is equal to zero) can be used to deduce the position and spacing of the steel bars inside the RC wall. According to the graph, we can see that the spacing of the steel bars is approximately 10 cm (the distance between two peaks). As described in the methodology part (step 4), the shift value for the case of an incident wave is deduced by measuring the distance from the peaks of its temperature profile to the peaks of the temperature profile for the case of the normal incident waves. The temperature profiles used for determining the values of Δ_i are their fitted curves obtained after using the moving average with a period of 5. Finally, the values of the shifts (Δ_i) obtained from the fitted temperature curves are shown in Table 1.

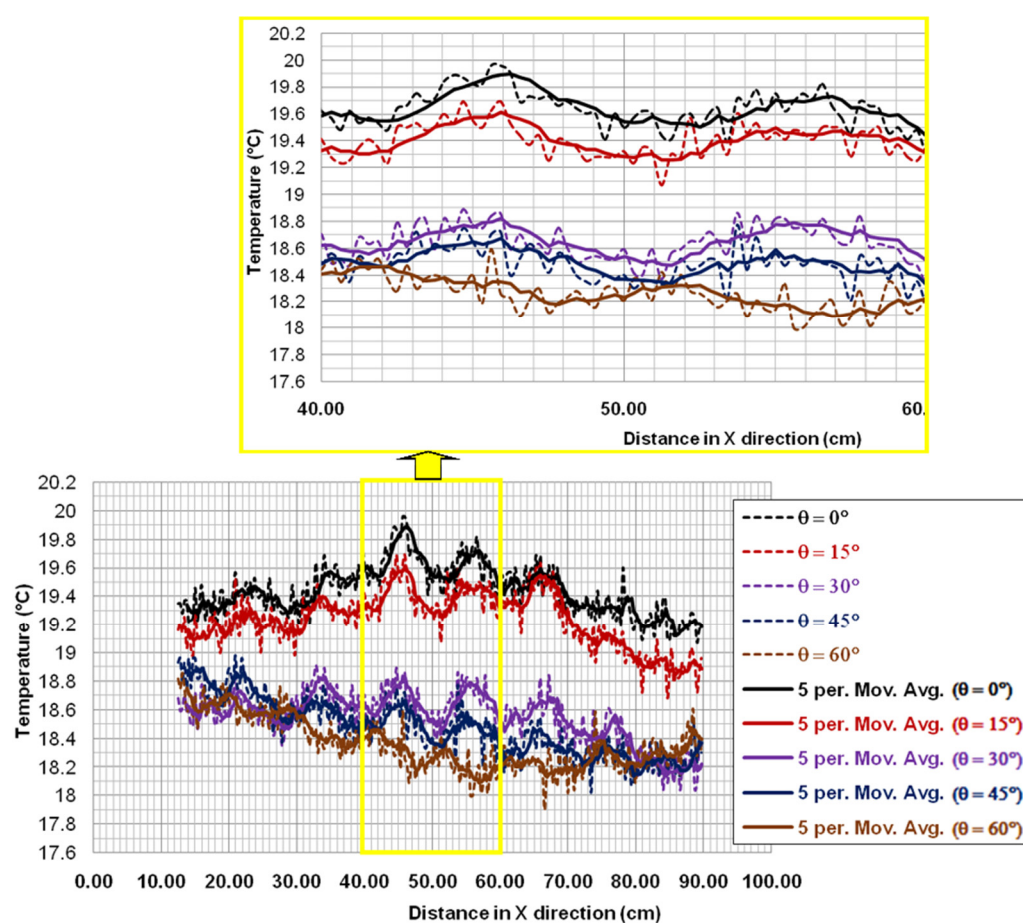


Figure 8. Temperature profiles with fitting curves by using the moving average for different angles of incident waves ($\theta = \theta_i$).

Table 1. Deduced values of the shifts (Δ_i) from the fitted temperature profiles.

θ_i (°)	$\sin(\theta_i)$	Δ_i (mm)
0	0	0
15	0.259	5
30	0.500	10
45	0.707	14.5
60	0.866	60

In the 2nd column of the table, the values of $\sin(\theta_i)$ are also given, as it is a parameter needed in the next step of the methodology.

4.3. Deduction of Concrete Cover Thickness

The last step, and also the essential one in the proposed methodology, is the use of linear law. In our case, the application of the linear law to the non-linear function (X, Y) in order to obtain the linear function (x, y) is illustrated in Figure 9.

Thus, the remaining problem to resolve is to find the equation representing the linear relation (x, y) in order to deduce the value of A and B (Figure 9). For this purpose, the graph (x, y) needs to be drawn by using the values in Table 2.

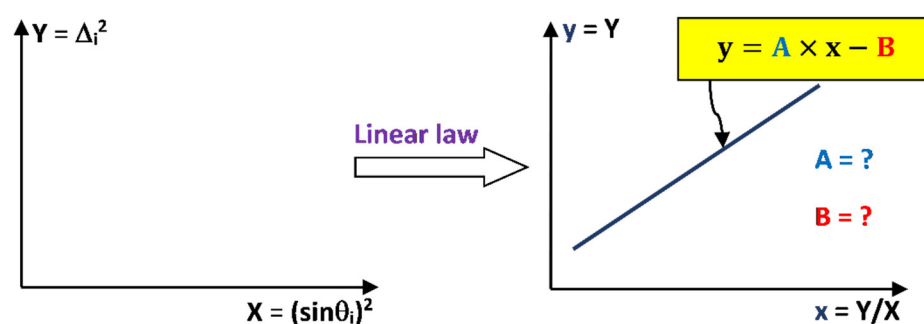


Figure 9. Application of linear law (x, y) for non-linear relation (X, Y).

Table 2. Values for drawing the linear function (x, y).

θ_i (°)	$X = (\sin\theta_i)^2$	$y = Y = \Delta_i^2(\text{mm}^2)$	$x = Y/X (\text{mm}^2)$
0	0	0	0
15	0.067	25	373.205
30	0.250	100	400
45	0.500	210.25	420.5
60	0.750	3600	4800 ¹

¹ Too large compared to the average value of x.

Note that the value of x when $\theta_i = 60^\circ$ is too large compared to the average value. For this reason, this point is not taken for determining the equation of the linear function. It can also allow us to see that this angle may be too large for detection with our microwave antenna due to the constraint related to its dimensions.

By using the values in Table 2, the graph of the linear function (x, y) is obtained (an approximation with $R^2 = 0.965$), as shown in Figure 10.

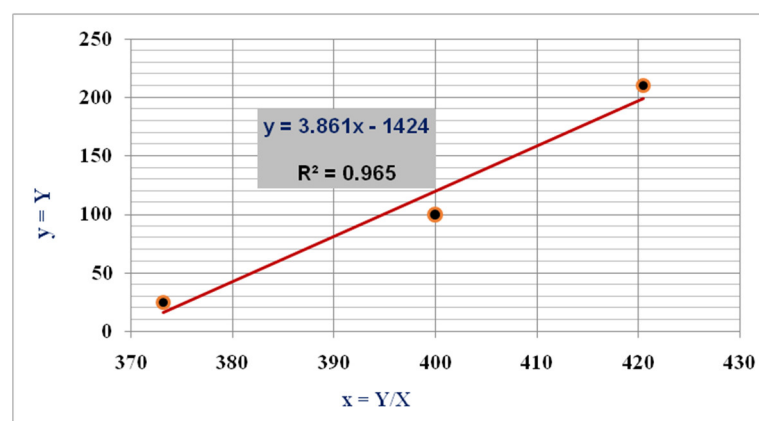


Figure 10. Graph of the linear function (x, y) for deducing the value of concrete cover thickness.

According to the equation of the fitting line: $y = 3.861 \times x - 1424$, and the Equation (6), the values of “ ϵ_2 ” and “e” can be deduced as follows:

$$\epsilon_2 = 3.861 \approx 4, e^2 = 1424 \Rightarrow e = \sqrt{1424} = 37.74 \text{ mm}$$

Therefore, the deduced value of the concrete cover thickness by the proposed methodology (37.74 mm) is acceptable compared to the real value (38 mm).

5. Conclusions

In this study, an innovative methodology with microwave thermography for determining the concrete cover thickness of one-layer reinforcements in an RC wall was presented. By using the transmission approach with five angles of microwave antenna

direction and the Snell–Descartes law (physical) and linear law (mathematical), the methodology led us to deduce the approximate value of the concrete cover thickness. The concrete cover detected by the proposed method was behind the reinforcement layer. This methodology expands the frontier of the infrared thermography method, which is a non-contact and simple method but capable of detecting the concrete cover thickness.

Perspectives of the present work can be the application of the reflection approach by taking into account the direction of the infrared camera, which would be more complicated for detecting the concrete cover facing the microwave antenna.

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