

Article **The Adhesive Force Measurement between Single μLED and Substrate Based on Atomic Force Microscope**

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Abstract: Compared with traditional liquid crystal and organic light emitting diode (OLED), micro light emitting diode (μ LED) has advantages in brightness, power consumption, and response speed. It has important applications in microelectronics, micro-electro-mechanical systems, biomedicine, and sensor systems. μ LED massive transfer method plays an important role in these applications. However, the existing μ LED massive transfer method is faced with the problem of low yield. To better transfer the μ LED, the force value detached from the substrate needs to be measured. Atomic force microscope (AFM) was used to measure the force of a single μ LED when it detached from the substrate. The μ LED was glued to the front of the cantilever. When a single μ LED was in contact with or detached from the Polydimethylsiloxane (PDMS), the maximum pull-off force can be obtained. The force at different peel speeds and preload was measured, and the experimental results show that the separation force between a single μ LED and PDMS substrate is not only related to the peel speeds, but also related to the preload. The force values under different peel speeds and preload were measured to lay a theoretical foundation for better design of μ LED massive transfer system.

Keywords: AFM; µLED; mass transfer; adhesive force measurement

1. Introduction

The main advantage of micro light emitting diode (μ LED) is that each LED can be controlled and driven independently, leading to excellent power consumption, brightness, resolution, contrast, heat dissipation, and other characteristics [1–3], and μ LED has important applications in microelectronics [4], biomedicine [5], and sensor systems [6].

 μ LED needs to be transferred to the circuit substrate in practical application. Currently, the most popular transfer method is the stamp method, which adjusts the adhesion force by adjusting the peeling parameters of Polydimethylsiloxane (PDMS) to complete the μ LED pickup and release. The design of stamp is one of the key technologies of μ LED transfer printing [7–9]. A comprehensive understanding of the adhesion between μ LED and PDMS is needed to achieve more efficient and high-yield transfer. Therefore, it is very important to measure the adhesion between the μ LED and the substrate under different peel speeds and preload.

Recently, many scholars have studied the adhesion between μ LED and substrate. Tian Yu et al. found that the peel angle can regulate the adhesion and friction through a theoretical model, which is the mechanism of gecko's strong adhesion and fast separation [10]. Xu Quan, Rogers et al. found that peel speed is an important factor affecting adhesion [11]. Rogers optimized the ground geometry of PDMS by using a sharp substrate, and the strength of adhesion can be switched from strong to weak in a reversible manner by more than three orders of magnitude [9].



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Copyright: © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). Chang Dong Yeo developed an instrument based on capacitive force sensor to measure the dynamic adhesion between rough surfaces [12]. Min sock Kim proposed a new instrument to measure the dynamic adhesion of the interaction surface on the flexible substrate, and proposed an optimal adhesion control strategy based on the analysis of adhesion [13]. In 2017, Lindsay Vasilak used strain gauge load cell to measure the normal adhesive force of OLED [14]. Chang-Dong Yeo used a high-resolution, high-dynamic bandwidth capacitive force transducer and two piezoelectric actuators to measure adhesive pull-off forces between nominally flat rough silicon surfaces under various dynamic conditions [15]. Jaeho Lee used Atomic Force Microscope (AFM) to measure the adhesion between the colloidal probe and silicon wafer. Two spherical colloids made of silicon dioxide and gold that were attached to an AFM cantilever were approached to and retracted from a silicon wafer specimen [16].

However, at present, none has been found in the literature regarding adhesion test between a single μ LED and the substrate and most of the experiments demonstrate the adhesion between a large area of PDMS and μ LED array, since it is hard to attach a single μ LED to the force sensor. In this paper, based on AFM, the adhesion between a single μ LED and the substrate was measured using cantilever, and the relationship between peel speeds, preloads, and adhesion was evaluated [17,18]. In Section 2, the theoretical relationship between pull-off forces to peel speeds and preload will be deduced. In Section 3, the theoretical results will be verified experimentally.

2. The Theoretical Relationship between Pull-Off Forces to Peel Speed and Preload 2.1. *The Image of µLED*

The size of μ LED is generally smaller than 100 μ m [19,20], as shown in Figure 1. A scanning electron microscope (SEM) image of μ LED is shown in Figure 1A. The surface of the μ LED array obtained by optical microscope is shown in Figure 1B.



Figure 1. Image of μ LED. (**A**) Scanning electron microscope (SEM) image of μ LED. (**B**) The surface of the μ LED array obtained by optical microscope.

2.2. The Theoretical Relationship between Pull-Off Forces and Peel Velocity

The relationship between peel speed and pull-off force has also been extensively studied [21], which can be expressed as:

$$G_{c}(v) = G_{0}[1 + \left(\frac{v}{v_{0}}\right)^{k}]$$
(1)

where G_0 is the critical energy release rate and corresponding detaching speed v_0 approaches zero, v is the peel speed, and the exponent k is a parameter that can be determined from experiments. The power–law relationship (Equation (1)) has been found applicable to low or high peel speed obtained from metal/polymer and polymer/polymer interfaces at various temperatures.

2.3. The Theoretical Relationship between Pull-Off Forces and Preload

According to the Hertzian contact theory, the actual contact occurs only on a small part of the apparent area due to the surface roughness when two solid surfaces are in contact. The size and distribution of the zone of contact exert a decisive influence on friction and wear. The shape of the rough peaks on the actual contact surface is usually elliptical. Since the size of the contact area of the ellipsoid is much smaller than its radius of curvature, the rough peak can be approximately regarded as a sphere. The contact of two flat surfaces can be regarded as a series of uneven spheres. The contact between two elastomer can be converted into the contact between an elastic sphere with equivalent radius of curvature *R* and equivalent modulus of elasticity *E* and a rigid smooth surface.

When μ LED contacts with PDMS, the Young's modulus of PDMS is much lower than that of μ LED, so it can be considered as elastic contact. When the two rough peaks contact each other, the normal deformation δ is produced under the action of load W, which makes the shape of the elastic sphere change from dotted line to solid line. The actual contact area is a circle of radius *a*, as shown in Figure 2. The relationship between load and contact area is given by Equation (2) [22].



Figure 2. Diagram of single peak elastic contact.

The ideal rough surface is composed of many orderly rough peaks with the same curvature radius and height, and the load and deformation of each peak are exactly the same and independent from each other. However, the rough peak height of the actual contact surface is randomly distributed in general, so the contact peak should be calculated according to the probability. The contact condition of two rough surfaces is shown in Figure 3.

Their contact can be converted into the situation where one smooth rigid surface touches another rough elastic surface. Since the surface of μ LED is very smooth, while the surface of PDMS is quite the opposite, this assumption is consistent with reality.

When the distance between the center lines is *h*, only the part of the contour height z > h contacts with. In the probability density distribution curve, the shading area of the z > h part is the surface contact probability, that is [23]

$$P(z > h) = \int_{h}^{\infty} \psi(z) dz$$
(3)

(2)



Figure 3. Contact of rough surfaces. The root mean square values of the roughness of the two surfaces are respectively σ_1 and σ_2 , *h* is the distance between the center lines, *z* is the part of the contour height z > h contacts with, and $\Psi(z)$ is the probability of the surface contact.

If the number of peaks on the rough surface is *n*, the number of peaks participating in the contact, *m*, is given by [23]:

$$m = n \int_{h}^{\infty} \psi(z) \mathrm{d}z \tag{4}$$

The normal phase deformation of each contact peak is *z*-*h*. From Equation (2), the actual contact area *A* is given by [23]:

$$A = m\pi R(z - h) = n\pi R \int_{h}^{\infty} (z - h)\psi(z)dz$$
(5)

The total load *W* is supported by the contact peak as [23]:

$$W = \frac{4}{3}mE^*R^{1/2}(z-h)^{3/2} = \frac{4}{3}nE^*R^{1/2}\int_h^\infty (z-h)^{3/2}\psi(z)dz$$
(6)

Usually, the contour height of the actual surface follows a Gaussian distribution [24], in which most of region near the *z*-score approximates an exponential distribution. Suppose that $\psi(z) = \exp(-z/\sigma)$, we get:

$$m = n\sigma \exp(-h/\sigma) \tag{7}$$

$$A = \pi n R \sigma^2 \exp(-h/\sigma) \tag{8}$$

$$W = \frac{3}{4}nE^*R^{1/2}\sigma^{3/2}\exp(-h/\sigma)$$
(9)

From the above equations, it can be derived that *W* is proportional to *A* and *W* is proportional to *m*. Thus, the actual contact area and the number of contact peaks have a linear relationship with the load in the elastic contact state of the two rough surfaces. Separating μ LEDs from PDMSs creates two new interfaces, and the force value *F*_{cr} required for this process is obtained as [10]:

$$F_{cr} = A\gamma \tag{10}$$

where γ is the viscosity coefficient of the two surfaces. From Equations (8)–(10), it can be concluded that the adhesive force increases with the increase of preload.

3. The Experimental Results and Discussion

3.1. Experimental Steps

To measure the adhesion between a single μ LED and the substrate, a cantilever measurement scheme is adopted, and the specific steps are shown in Figure 4A–C.



Figure 4. The adhesion measurement results based on cantilever between μLED and substrate. (A–C) Measurement steps. (A) The initial state. (B) The loading status. (C) The reverse motion. (D) Typical single measurement results.

Step 1: Apply glue to the tip of the tipless cantilever with a stiffness of 5.1 N/m.

Step 2: Move the cantilever above a μ LED.

Step 3: Lower the cantilever to contact the μ LED and wait for the glue (UV photoresist) to solidify.

Step 4: Raise the cantilever to make the µLED separate from the base.

Step 5: Move µLED above the PDMS substrate.

Step 6: Measure the relevant force value at different peel speeds and preload.

A typical adhesion–depth curve on a single μ LED with a flexible PDMS substrate (1:10 mixing ratio) measured by AFM is shown in Figure 4D. The tip of the cantilever is controlled at a speed of 10 μ m/s. The *x*-axis is the displacement of the μ LED. The measurement process is divided into two segments according to the direction of cantilever movement: approach (red line in Figure 4D) and retract (blue line in Figure 4D). The *y*-axis is force between the μ LED and PDMS.

The AFM has been well calibrated using thermal method. The relationship between the force acted on cantilever and PSD output has been obtained before measuring the adhesion force.

The μ LED on the cantilever was moved above a substrate PDMS, as shown in Figure 4A. Figure 4B is in a loading status. The μ LED is pressed on the PDMS and continuously moved through the precision stage. The laser spot moves as the cantilever bends. The cantilever will not stop until the pressure equals the set preload, as shown in section BC in Figure 4D. Figure 4C is in reverse motion. With the reverse movement, the pressure of μ LED on the PDMS substrate becomes smaller and smaller until the pressure reaches 0, as shown in the CD section.

Dynamic jumping behavior during approach (such as the BC segment) and measured jumping behavior during return (CF) were measured.

As can be seen from Figure 4D, the measurement process can be divided into four stages according to the contact status: (I) pressure down to contact with PDMS, (II) pressure to the maximum to reach preload, (III) reverse movement, and (IV) separation from PDMS.

I—Initial state: the cantilever is moved by a precision stage and is not in contact with the PDMS, as shown in Section AB.

II—Loading status: μ LED contact PDMS. The μ LED is pressed on the PDMS and continuously moved through the precision stage. The laser spot moves as the cantilever bends. The cantilever will not stop until the pressure equals the set preload, as shown in section BC.

III—Reverse motion: With the reverse movement, the pressure of μ LED on the PDMS substrate becomes smaller and smaller until the pressure reaches 0, as shown in the CD section. As the reverse motion continues, the PDMS deforms due to the tension between the μ LED and PDMS. At this point, the elastic force of the cantilever acting on μ LED is less than the critical adhesion force of PDMS, as shown in section DE.

IV—Exit stage: The elastic force of the cantilever on μ LED is greater than the critical adhesion force. A sudden jump in the position sensitive device (PSD) voltage output can be observed, as shown in the EF section.

The maximum pull-off force can be defined as the minimum force of the force-depth curve, as shown in Figure 4D.

3.2. Measurement of Adhesion under Different Detaching Velocities and Preload

As shown in Figure 5, the maximum pull-off force was measured at different peel velocities (detaching velocity) varying from $10 \,\mu\text{m/s}$ to $300 \,\mu\text{m/s}$, in which high peel speed ($300 \,\mu\text{m/s}$) resulted in strong adhesion, while low peel speed ($10 \,\mu\text{m/s}$) resulted in weak adhesion. Obviously, there is a strong correlation (proportional relationship) between the maximum pull-off force and the peel velocity.



Figure 5. The measured maximum pull-off forces with respect to peel velocity.

We measured the maximum adhesion force at different preload from 0.5 to 3 μ N (the peel speed was fixed at 10 μ m/s). The proportional relationship between the maximum pull-off force and the preload is shown in Figure 6.

The experimental results show that the preload has a great influence on the adhesion, which is different from the previous research: "Unlike the effects of material property of PDMS, the maximum pull-off force has similar value regardless of the initial indentation force between the tip and the flexible substrate". Our theoretical result is consistent with our experimental result but different from the literature.

It Is hard to compare the experimental results to results from Equations (8)–(10). The equations show a positive proportion relationship between contact area and the maximum pull-off force. However, the real contact area between the μ LED and PDMS or other

substrates could not be measured. Therefore, it is impossible to directly compare the quantity of theoretical value and experimental value absolutely, but only relatively.



Figure 6. Results for the maximum pull-off force at different preload.

4. Conclusions

In this paper, the adhesion force between the μ LED and substrate at different peel speeds and preload was measured by AFM. The experimental results show that the separation force between a single μ LED and PDMS substrate is not only related to the peel speed, but also related to the preload. Although it is hard to directly compare the absolute quantity of theoretical value and experimental value, the results find a new way to design an apparatus for μ LED transfer printing. Future research is required to reversibly change adhesion strength between strong and weak modes by more than two orders of magnitude so that the system can be applied in transfer printing. We will focus on the design of a novel substrate to achieve this target. This system would have broader impacts in transfer printing.

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