

Article

# Cutting Force Prediction and Experiment Verification of Paper Honeycomb Materials by Ultrasonic Vibration-Assisted Machining

Wenjun Cao <sup>1</sup>, Jun Zha <sup>1,2</sup>  and Yaolong Chen <sup>1,\*</sup>

<sup>1</sup> School of Mechanical Engineering, Xi'an Jiaotong University, Xi'an 710049, China; caowenjun17@stu.xjtu.edu.cn (W.C.); jun\_zha@xjtu.edu.cn (J.Z.)

<sup>2</sup> Shenzhen Research School, Xi'an Jiaotong University, Hi-Tech Zone, Shenzhen 518057, China

\* Correspondence: chenzwei@mail.xjtu.edu.cn; Tel.: +86-029-83-39-95-11

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**Abstract:** The disc-cutter is a finishing tool for the ultrasonic-cutting of paper honeycomb-core material. The cutting state directly affects the machining accuracy and surface quality of the workpiece. The cutting force is an important physical quantity and the cause of ultrasonic cutting defects of the honeycomb-core material. Due to differences in the mechanical properties and cutting performance of honeycomb-core materials and commonly used metal materials, existing metal-cutting-force models cannot be applied to the calculation of ultrasonic cutting forces in the processing of honeycomb-core materials. In response to this problem—combined with actual working conditions using the ABAQUS finite element analysis software—a finite element simulation model of the ultrasonic vibration-assisted cutting force of the disc-cutter on the honeycomb-core material was established, and the cutting curves and values were obtained. The experiment of ultrasonic vibration cutting of the disc-cutter proves that from the surface morphology of the honeycomb core, the milling-width has the greatest influence on the cutting force, and the cutting-depth has the smallest influence on the cutting force. The maximum error between the cutting force experimental results and the finite element simulation results under the same cutting conditions was 13.2%, which means that the established cutting-force finite element model is more accurate and can be used to predict the cutting in honeycomb ultrasonic vibration-assisted cutting-force value. Finally, based on the response surface method, a three-dimensional cutting force prediction model of the ultrasonic cutting honeycomb core of the disc-cutter was established by using the simulation model data. The results of this study can provide a useful basis for the improvement of cutting performance and processing efficiency in the processing of paper honeycomb-core materials.

**Keywords:** honeycomb core; disc-cutter; ultrasonic vibration-assisted; finite element analysis

## 1. Introduction

Honeycomb-core material is a kind of high-stiffness, light-quality, heat-resistant, impact-resistant, fatigue-resistant, good-insulating soundproof stays-engineering composite material. Zuhri, Gomet and Castanea analyzed the mechanical properties and excellent qualities of honeycomb-core materials through theoretical modeling and experimental verification [1–3]. Alix and Tauhiduzzaman introduced honeycomb parts used in the aerospace field such as helicopter power plant fairings, large aircraft wings, liquid fuel barriers in rockets, etc. [4,5]. In order to meet the requirements of assembly and connection, the honeycomb-core material must be cut after it is formed. However, the honeycomb-core material is a typical difficult to machine material, it brings great challenges to the CNC machining of honeycomb-core material due to the particularity of honeycomb core structure and cutting mechanism.

Rinker, Malek and Hohe proposed related process optimization methods for processing defects such as honeycomb core fracture and collapse, increased surface burrs and dust pollution during the CNC high-speed milling process of honeycomb core, which greatly reduces the performance of the honeycomb core structure and improves the product Safety and service life [6–8].

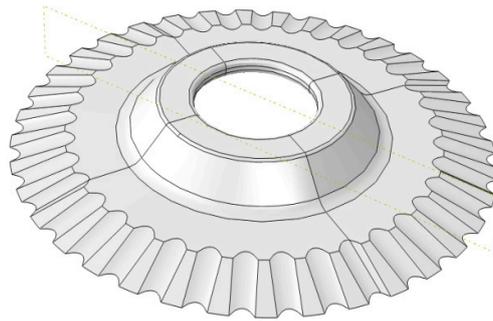
Oriented to the manufacturing requirements of honeycomb-core material parts, in view of the problems existing in CNC high-speed milling processing, scholars are constantly exploring new processing methods and improving the existing processing technology. Ultrasonic vibration-assisted cutting technology as a new advanced processing technology has been applied in the field of CNC machining of honeycomb core workpiece [9]. Compared with high speed milling, this machining method has significant advantages in machining accuracy, quality, efficiency and environmental friendliness [10,11]. In the ultrasonic vibration-assisted machining of honeycomb-core material, there still have surface damage problems such as core tearing and machining surface burr. There is little research on the ultrasonic vibration-assisted cutting force of the disc-cutter. Heimbs and Aminanda studied the failure behavior of the honeycomb core through experimental means and concluded that the cutting force is an important physical parameter that causes defects in the honeycomb core workpiece [12,13]. The research of rotating vibration cutting of honey comb core components with disc-cutter is only focusing on the test verification; mechanism study must be carried out to reveal the influence of the cutting parameters on machining quality. Potlkuri measured the elastic properties of the hexagonal honeycomb-core material through experiments [14]. Based on brittle fracture mechanics, Hu studied the cutting mechanism of the ultrasonic cutting of the honeycomb core with a sharp knife and derived a theoretical model of cutting force [15]. However, the entire process of ultrasonic vibration-assisted cutting of disk cutters is time-consuming, the processing quality is unstable, the surface burrs on the processing, and the core damage are still outstanding.

In order to solve the problem of cutting damage of the honeycomb core workpiece in ultrasonic vibration-assisted cutting, this study used finite element analysis software to establish a 3D honeycomb-core material model and a disc-cutter model according to the actual working conditions. A method of ultrasonically cutting the honeycomb-core material with a disk milling cutter is proposed. At the same time, the correctness of the finite element model is verified through experiments. The influence of process parameters on cutting quality was studied. At the same time, based on the response surface method, a simulation model was used to construct a cutting force prediction model for the honeycomb core of the disc-cutter ultrasonic machining, which provided a theoretical basis for the optimization of the cutting technology of the honeycomb-core material and the reasonable selection of processing parameters.

## **2. Establishment and Verification of Finite Element Simulation Model for Honeycomb Core Ultrasonic Vibration-Assisted Cutting**

### *2.1. Disc-cutter Geometry Model*

Due to the structure difference between Nomex honeycomb-core composite material and the metal material, a corresponding special tool must be used for machining, and the structural shape and geometric angle of the tool are greatly different from the metal cutter. Nomex honeycomb-core composites material can be machined due to the tool forms a sharp cutting edge with a small wedge angle, which is the key to the material being cut. The rotary-vibration-cutting disc-cutter model studied in this paper is shown in Figure 1. Due to the complex structure of the tool, the model was built by the CATIA V5R21 and imported into the ABAQUS, the geometric parameters of disc-cutter are shown in Table 1.



**Figure 1.** Disc-cutter geometry model.

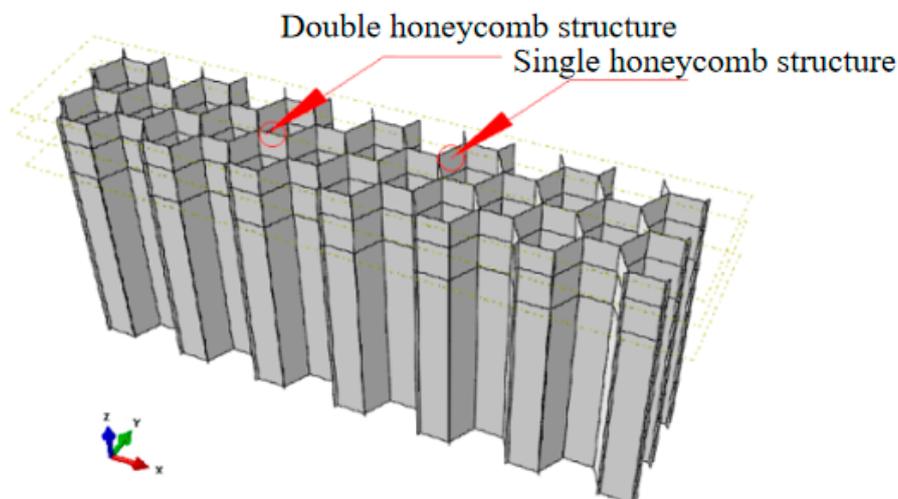
**Table 1.** Geometric parameters of disc-cutter.

Features of the Model	Parameter
Cutter diameter	50.8 mm
Angle of wedge	14°
Height of tool	5 mm
inner diameter of tool	12 mm

The tool material is W18Cr4 V, material density  $\rho = 7900 \text{ kg/m}^3$ , elasticity modulus  $E = 205 \text{ Gpa}$ , Poisson's ratio  $\mu = 0.3$ . Due to the low hardness of the Nomex honeycomb-core material, the tool wear is neglected in the simulation, and the tool is defined as a rigid body.

## 2.2. Honeycomb Core Geometry Model and Material Model

The honeycomb-core material is structurally different from the conventional metal-processing material. It is a porous thin-walled structure with a hexagonal shape, the hole has a side length of 3–6 mm and a single-layer-wall thickness of 0.05–0.15 mm. Honeycomb core geometry modeling is performed in ABAQUS/CAE, where a single core is drawn, then the entire sketch is completed by mirroring and arraying, and finally stretched vertically along the aperture according to the height of the desired honeycomb core. When the wall thickness of the shell unit is set, the thickness of the single layer is set to 0.1 mm, and the thickness of the double layer joint is 0.2 mm. The geometric model of the Nomex honeycomb-core composite material established in the finite element analysis is shown in Figure 2.



**Figure 2.** Nomex honeycomb-core composite geometry model.

The main structure of Nomex honeycomb core is aramid paper. The molding of aramid paper material is made by arranging aramid fibers randomly distributed in XYZ direction in any ratio and combining them. Due to the flexibility and randomness of fiber arrangement, the mechanical properties of Nomex honeycomb-core materials cannot be directly measured by researchers using conventional measurement methods. To date, the more commonly used is derived from the empirical formula of the fiber modulus at random. The research shows that the mechanical properties of the aramid fiber in the vertical direction are basically consistent with the main direction of the material. In this paper, the honeycomb material and tool material used in cutting simulation processing The attributes are shown in Table 2 below.

**Table 2.** Tool and honeycomb material properties [16,17].

Material	Density $\rho$ (kg/m <sup>3</sup> )	Elastic Modulus E/Gpa	Poisson's Ratio $\sigma$	Thermal Expansion Coefficient 10 <sup>-6</sup> /°C	Thermal Conductivity W/(m·°C)	Specific Heat Capacity J/(kg·°C)
W18Cr4 V high speed steel	7800	210	0.3	4.5	24	420
Nomex honeycomb core	1334	2.01	0.25	4	0.123	1300

### 2.3. Separation and Fracture Failure Criteria

The ultrasonic vibration-assisted cutting process of honeycomb-core material is the separation process of chip and workpiece under the action of blade and ultrasonic vibration-assisted. Therefore, the determination of chip separation and fracture failure criteria is critical to achieving finite element simulation of the honeycomb core cutting process. The separation criteria depend on the mechanical and physical properties of the material. Common separation criteria are geometric and physical criteria. The shear-failure criterion is applied in this study, which is provided by the finite element software. Depending on the plastic strain value of the element node reaches a predetermined critical value to determining failure occurs or not. By the calculation, when the destruction coefficient  $\omega$  reaches the set value, the unit is considered to be "killed", which means the material is destroyed and chips are formed. The value of the failure coefficient  $\omega$  can be obtained from the following formula:

$$\omega = \sum \frac{\Delta \bar{\epsilon}^{pl}}{\bar{\epsilon}_f^{pl}} \quad (1)$$

where  $\Delta \bar{\epsilon}^{pl}$  is the equivalent plastic strain increment;  $\bar{\epsilon}_f^{pl}$  is the total strain when the material is damaged;  $w$  is the shaping limit value or destruction coefficient.

### 2.4. Meshing, Boundary Conditions and Load Settings

In this paper—based on the Hypermesh software—the honeycomb-core material in the processing path of the disc-cutter was locally refined and sharpened. The honeycomb core was is meshed with C3D8T eight-node thermal coupling hexahedron, and the disc-cutter uses C3D10MT ten-node thermal coupling second-order tetrahedron meshing. The divided honeycomb core is imported into ABAQUS. Since the calculation of cutting heat is considered, an explicit temperature–displacement algorithm is selected. Before the model is submitted to the calculation, carefully check the setting of nonlinear parameters that may lead to nonconvergence or difficult convergence, Such as material settings, contact settings, etc.

During the simulation, the disk cutter and the honeycomb core must be subjected to load and boundary condition constraints according to the actual working conditions. Since the stiffness of the disc-cutter is much greater than that of the honeycomb core, the cutter is used as a rigid body during the simulation. In terms of boundary constraints, due to the poor local strength of the honeycomb core, it is not possible to use the traditional method of holding. In actual working conditions, the part is

held by vacuum suction through adhesive tape on the bottom surface of the part. In the simulation model, it is assumed that the part is held firmly. All joints on the bottom of the part are fully fixed.

The disc-cutter has three directions of motion synthesis relative to the honeycomb material, which are the feed movement, rotary movement of the cutter along its cutting trajectory and the vibration of the cutter along its axis. Velocity/angular velocity was adopted in ABAQUS The disc-cutter defines the feed velocity ( $v_f$ ) along the  $x$ -axis and the rotary motion along the  $z$ -axis, while applying a reciprocating ultrasonic wave up and down to the periodic amplitude function of the Fourier series in the  $z$ -axis direction of the disc-cutter vibration. Set the initial temperature of parts, disc-cutter and environment to room temperature. The simulation model of Nomex honeycomb core with ultrasonic vibration of disc-cutter is shown in Figure 3.

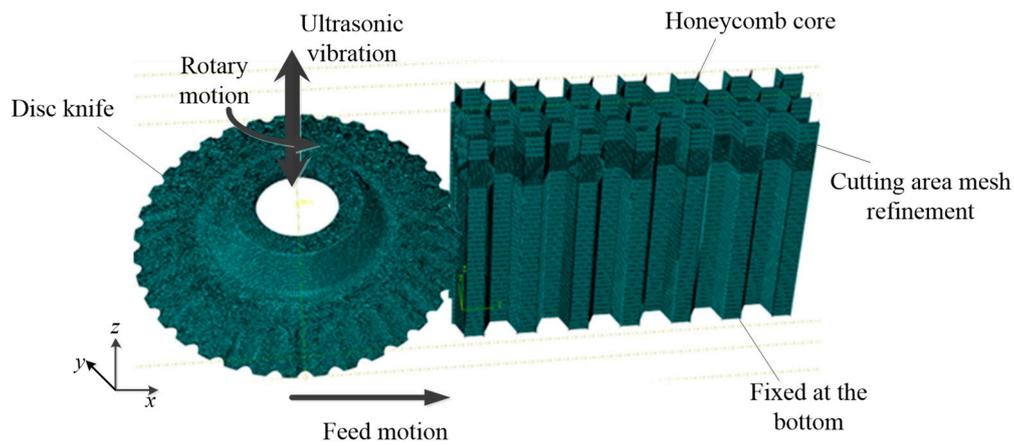


Figure 3. Nomex simulation model of ultrasonic vibration cutting of disk cutter.

In the direction of the  $z$ -axis of the tool, the vibration equation of any node of the disc-cutter during rotary-vibration-cutting is:

$$z_i = A \sin(2\pi ft) \tag{2}$$

where  $A$  is the amplitude ( $\mu\text{m}$ );  $f$  is the frequency (Hz).

The periodic amplitude function in the formula is expressed by Fourier series, and loaded in ABAQUS in the form of Figure 4, the expression is:

$$a = A_0 + \sum_{n=1}^N [A_n \cos n\omega(t - t_0) + B_n \sin n\omega(t - t_0)] \tag{3}$$

where  $A_0$  is the initial amplitude ( $\mu\text{m}$ );  $\omega$  is the circular frequency (rad/s);  $A_n$  is the coefficient of the  $\cos$  function;  $B_n$  is the coefficient of the  $\sin$  function.

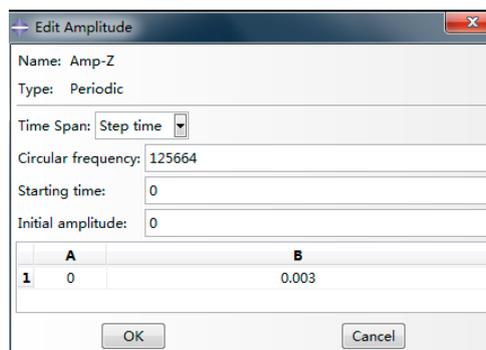
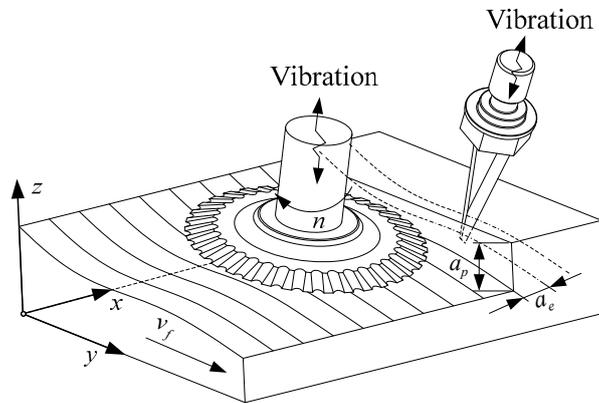


Figure 4. Schematic diagram of the rotary vibration amplitude loading of disc-cutter.

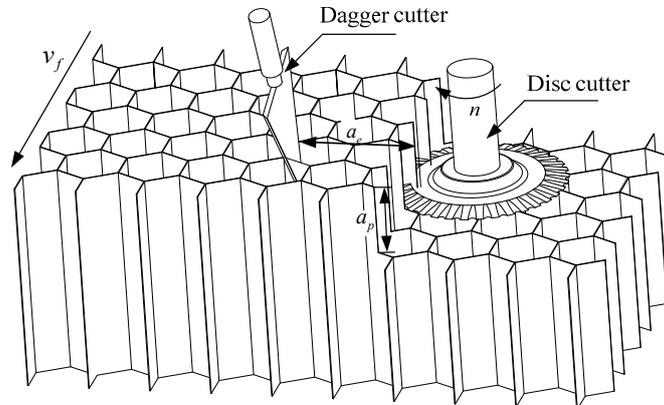
### 2.5. Simulation Scheme Design

In actual cutting, the disc-cutter cannot cut with large margin in the radial direction without crushing chip, otherwise the residual material cannot be cut off, the workpiece will be pulled up and causing cutting damage. The disc-cutter must be processing according to the depth and width produced by knife cutting. The specific cutting is shown in Figure 5.



**Figure 5.** Schematic diagram of ultrasonic vibration-assisted cutting of Nomex honeycomb-core composite material.

In order to ensure the feasibility of the experiment, first, use the knife cutter to produce the cutting thickness and width for disk cutter processing, and then use the disk cutter to machine the profile. The cutting process is shown in Figure 6.



**Figure 6.** Disc-cutter ultrasonic vibration-assisted cutting scheme.

In order to ensure the consistency of the cutting simulation and the cutting experiment parameters, as well as the accuracy of subsequent test verification. Since the follow-up test is verified on the designated ultrasonic processing equipment, the spindle speed and amplitude must be kept constant. According to the actual processing conditions on site, technicians usually adjust the cutting width range from 5 to 20 mm. The cutting depth ranges from 5 to 20 mm, and the feed speed ranges from 3000 to 6000 mm/min under the conditions of speed  $n = 1500$  r/min and amplitude  $A = 30$   $\mu\text{m}$ , may wish to obtain the single-factor simulation program shown in Table 3 through reasonable design and planning.

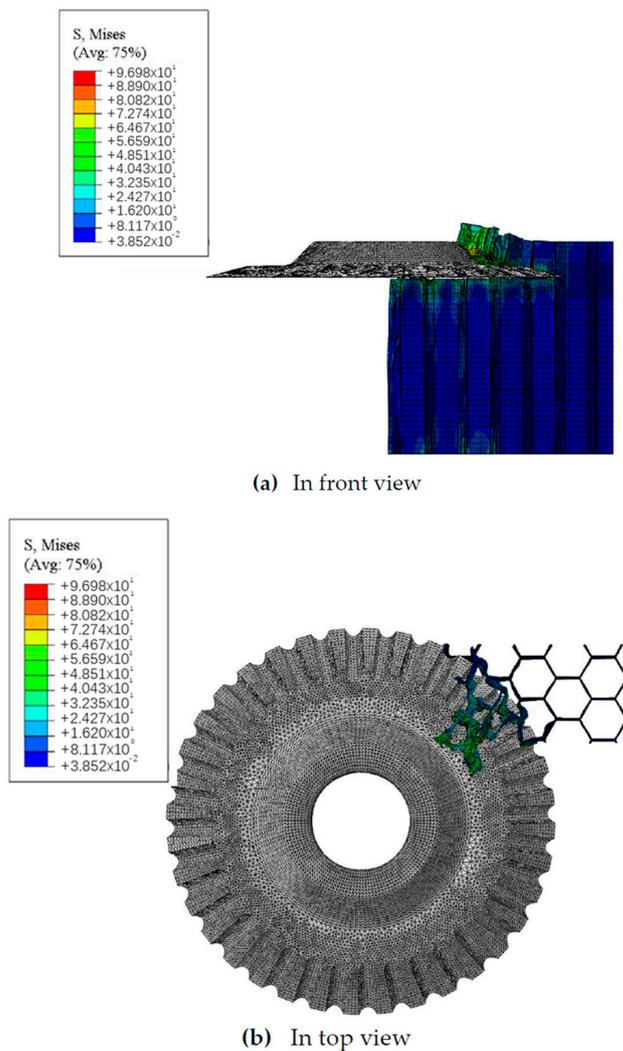
**Table 3.** Single factor simulation scheme for ultrasonic vibration-assisted cutting of disk cutter.

Number	Cutting Width (mm)	Cutting Depth (mm)	Feed Speed (mm/min)
1	5	5	3000
2	8.75	8.75	3750
3	12.5	12.5	4500
4	16.25	16.25	5250
5	20	20	6000

### 3. Results

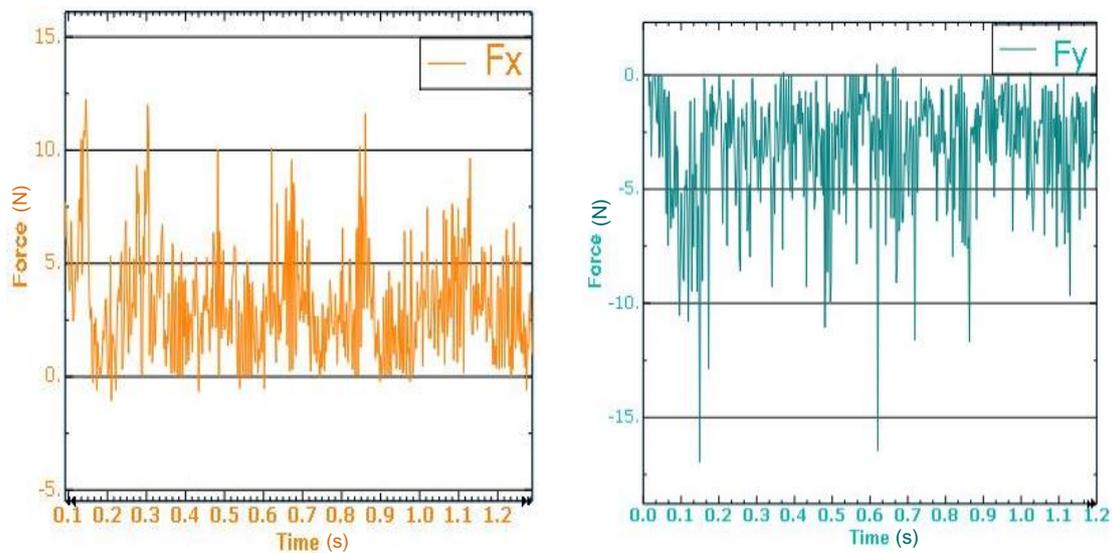
#### 3.1. Simulation Results and Verification Analysis

In addition to the above key links, the rotational vibration simulation analysis of the disc-cutter must set the field output results and historical output results in the software, such as stress, strain, displacement, energy, temperature, etc. At the same time, in order to improve the calculation efficiency, the honeycomb-core composite material is scaled by 5 times in the simulation to reduce the calculation time. The finite element simulation process of Nomex honeycomb-core composite disc-cutter rotating vibration cutting is shown in Figure 7.



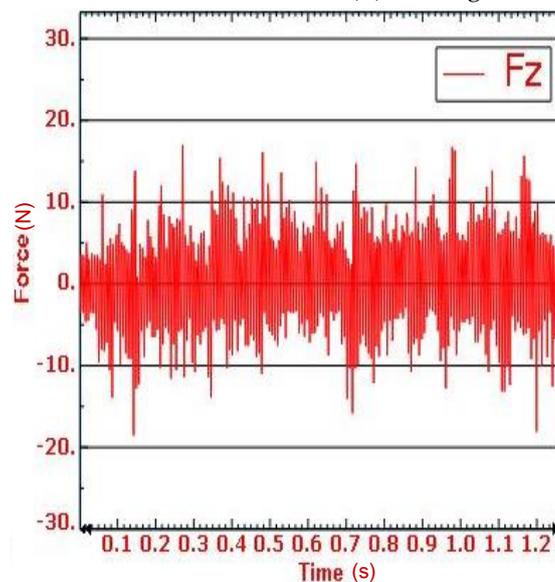
**Figure 7.** Rotary-vibration-cutting simulation of disc-cutter.

Figure 8 is a schematic diagram showing the cutting force variation curve. Where the spindle speed is 1500 r/min, the cutting depth  $a_p = 5$  mm, the cutting width  $a_e = 10$  mm, Feeding speed  $v_f = 3000$  mm/min, the vibration frequency is 20,000 Hz, the ultrasonic vibration-assisted amplitude  $A = 30$   $\mu$ m, and the simulation acquisition frequency is 600 Hz. It can also be seen from figure that during the cutting process, the maximum and minimum values of the cutting force in three directions fluctuate greatly. On one hand, the reason is that the Nomex honeycomb core is not a completely homogeneous structure. When the tool is processed to the honeycomb hole At the time, the required cutting force is small, and when the tool is processed to the bonding point of the honeycomb hole wall, the required cutting force is large. The other reason is that due to the frictional resistance of the upper and lower surfaces of the disc-cutter and the honeycomb core, the cutting direction of the cutter is different from the direction of the reaction force of the honeycomb core in the feed direction, so that each cutting The conditions for chip removal are also different at all times.



(a) Cutting force variation in X direction

(b) Cutting force variation in Y direction



(c) Cutting force variation in Z direction

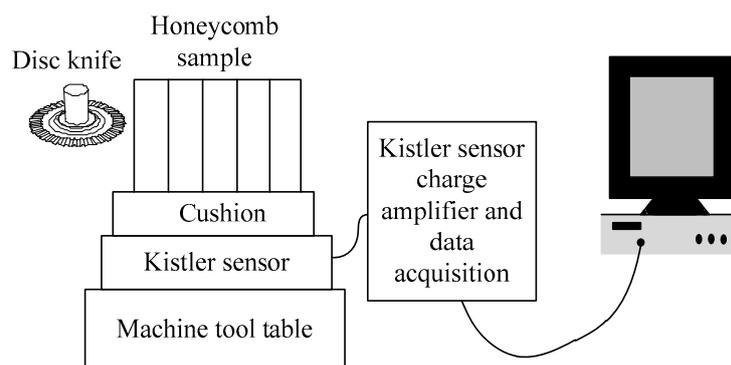
Figure 8. Simulation of cutting force changing curve by rotating vibration of the disc-cutter.

### 3.2. Verification of Ultrasonic Vibration-Assisted Cutting Simulation Model

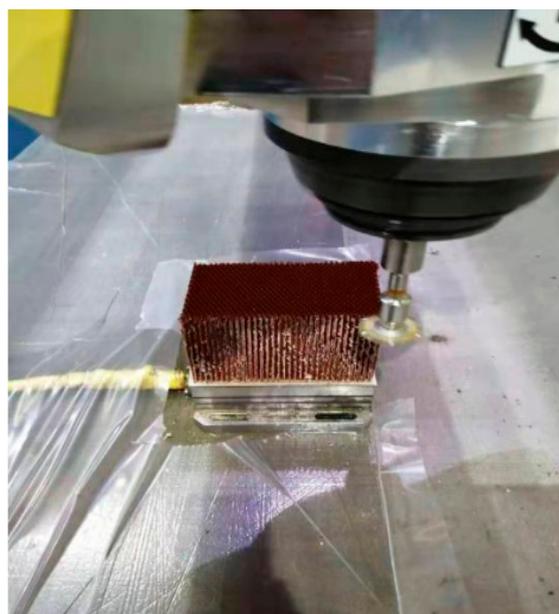
In order to verify the accuracy of the finite element model, the simulation scheme in Table 3 was used to conduct cutting experiments on honeycomb-core materials, and the simulation resulted of cutting force were compared with the experimental results.

The ultrasonic vibration cutting experiment of the Nomex honeycomb-core composite material was carried out on the advanced ultrasonic processing machine US-50 produced by the Austrian GFM company. The measurement of the cutting force in the experiment was performed by the Kistler9257B dynamic force measurement system. In the test, the data acquisition frequency was 4000 Hz, the Nomex honeycomb-core material used in the test was NRH-3-48, and the sample size was 100 mm × 80 mm × 60 mm.

The cutting force measurement principle is shown in Figure 9. The basic principle is that the voltage analog signal of the cutting force in three directions is first measured by the Kistler9275B three-way dynamometer, and then the signal is collected by the quasi-static charge amplifier, data acquisition card and chassis. Then, it is converted into numeric signals by data-acquisition virtual instrument software for data storage and analysis by the computer, and finally the average value of the collected cutting force signals is used as the cutting force during the processing. During the experiment, each group of process parameters are tested twice, and the average value is taken to ensure the reliability of the experimental data. The specific processing environment is shown in Figure 10.



**Figure 9.** Cutting-force measurement principle.



**Figure 10.** Overview of experimental devices.

During the experiment, the spindle speed was 1500 r/min and the feed rate was 4500 mm/min. There were 8 groups of experiments, 4 groups of cutting width experiments and 4 groups of cutting depth experiments.

As shown in Figure 11, the surface topography of  $a_e = 5$  mm was obviously better than that of  $a_e = 10$  mm. There were a large number of burrs on the surface when the constant was 10 mm, in addition to a large number of burrs; the regular hexagon on the surface also had serious distortion. It could be seen, with the increase of cutting depth  $a_p$ , the surface morphology of honey comb core material became better. When  $a_p = 40$  mm the surface of the material had almost no burrs, and the surface hexagon was regular.

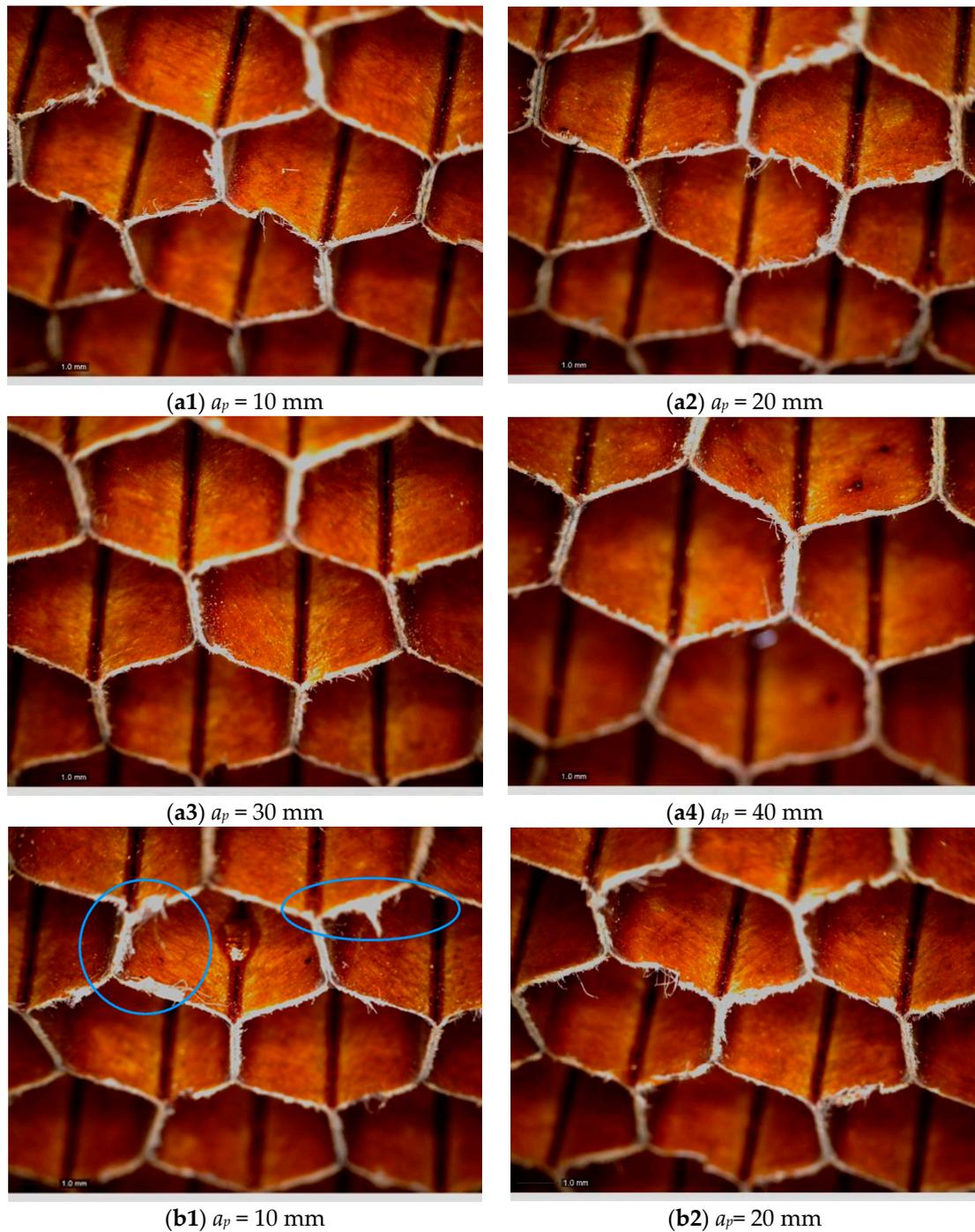
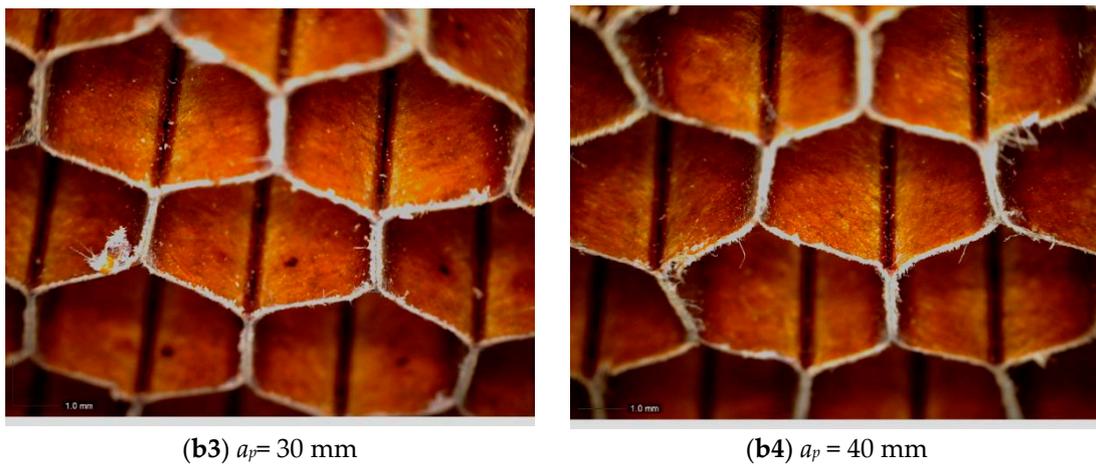


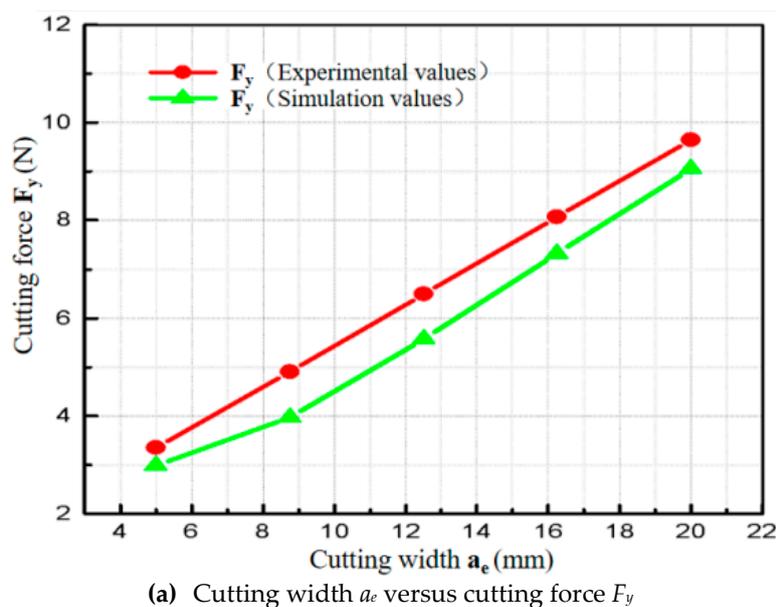
Figure 11. Cont.



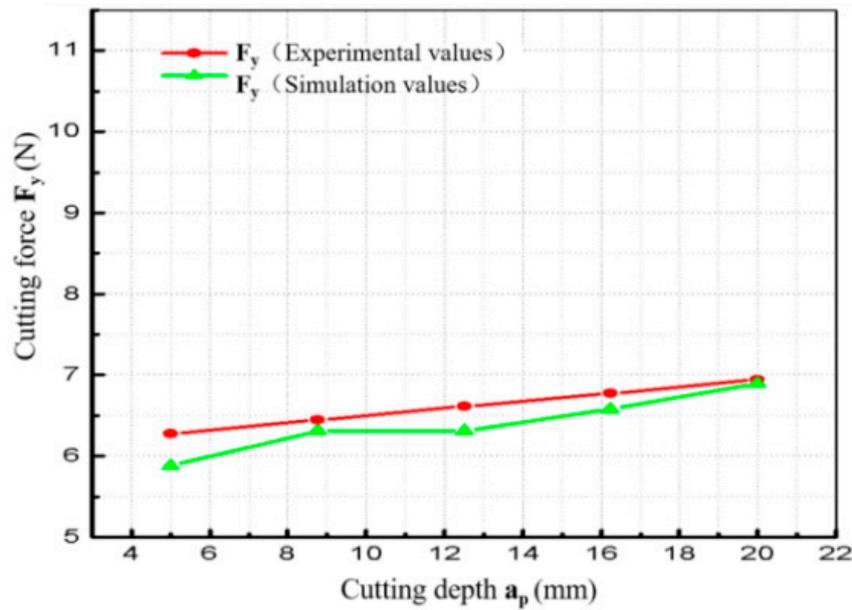
**Figure 11.** Honeycomb-core material topography. (a) Honeycomb-core material morphology (cutting width  $a_e = 5$  mm); (b) honeycomb-core material morphology (cutting width  $a_e = 10$  mm).

Based on the change curve of the cutting force under different machining parameters obtained by actual cutting experiments, the simulation data of the vibration cutting of the disc-cutter was compared and analyzed. The experimental data were obtained by the three-dimensional dynamometer. The simulation data were obtained by the reaction force of the tool reference point in the ABAQUS software.

In the verification data, two sets of cutting data were selected, as shown in Figure 12. Among them, under the conditions of feed speed  $v_f = 4000$  mm/min, cutting depth  $a_p = 10$  mm, spindle speed  $n = 1500$  r/min and amplitude  $\mu = 30$   $\mu$ m, Figure 12a shows the cutting width  $a_e$  versus cutting force  $F_y$ . With the increase of the cutting width, the experimental value of the rotary-vibration-cutting force component of the disc-cutter increased linearly. This was mainly because the increase of the cutting width will increase the contact area between the tool and the workpiece surface. Thus, the cutting force increased. Under the conditions of feed speed  $v_f = 4000$  mm/min, cutting depth  $a_e = 10$  mm, spindle speed  $n = 1500$  r/min and amplitude  $\mu = 30$   $\mu$ m, Figure 12b showed the effect of cutting depth  $a_p$  on cutting force  $F_y$ . The regular curve, with the increase of the cutting depth, the cutting force tends to increase, but the increase of the entire cutting force was also gentler. Because the disc-cutter did not made the contact area between the tool and the workpiece surface increase during the cutting process.



**Figure 12.** Cont.



(b) Cutting depth  $a_p$  versus cutting force  $F_y$

Figure 12. Simulation and test data verification.

Comparing the experiment results with the simulation results, the error is less than 13.2%. It can be verified that the finite element model proposed in this paper is basically reasonable. The tool wear and the phenolic resin coating outside the Nomex honeycomb-core composite material are neglected in the simulation process. The simulation data are slightly smaller than the measured data, but the simulation results can be applied to the actual Nomex honeycomb-core composite disc-cutter rotary-vibration-cutting.

#### 4. Construction of Cutting Force Prediction Model Based on Response Surface Method

Based on the verified simulation model of disc-cutter cutting, a three-dimensional cutting force prediction model of Nomex honeycomb-core material disc-cutter rotating vibration cutting was established by using the response surface method.

##### 4.1. Design of Cutting Simulation Test Scheme

In this test, the center complex response surface method is adopted, the cutting depth  $a_p$ , cutting width  $a_e$  and feed speed  $v_f$  are setting as independent variables and cutting forces  $F_x$ ,  $F_y$  and  $F_z$  as response values. Each factor in the three-factor center composite design has 5 levels, namely  $\pm 1$  level, 0 level and  $\pm 0.5$  level. The coding and level of test factors are shown in Table 4.

Table 4. Test factors and encoding level.

Factor	Encoding Level				
	-1	-0.5	0	0.5	+1
$a_p$ (mm)	5	8.75	12.5	16.25	20
$a_e$ (mm)	5	8.75	12.5	16.25	20
$v_f$ (mm/min)	3000	3750	4500	5250	6000

The Nomex honeycomb core disc-cutter rotary-vibration-cutting simulation test scheme is shown in Table 5.

**Table 5.** Scheme of cutting simulation center composite design.

Sequence	Coded Values			Actual Values		
	$a_p$ (mm)	$a_e$ (mm)	$v_f$ (mm/min)	$a_p$ (mm)	$a_e$ (mm)	$v_f$ (mm/min)
1	0.5	0.5	-0.5	16.25	16.25	3750
2	0	0	0	12.5	12.5	4500
3	0	0	1	12.5	12.5	6000
4	0	0	0	12.5	12.5	4500
5	-0.5	0.5	-0.5	8.75	16.25	3750
6	0	0	0	12.5	12.5	4500
7	-0.5	-0.5	0.5	8.75	8.75	5250
8	-1	0	0	5	12.5	4500
9	0	1	0	12.5	20	4500
10	0.5	-0.5	-0.5	16.25	8.75	3750
11	0	0	0	12.5	12.5	4500
12	0	0	-1	12.5	12.5	3000
13	1	0	0	20	12.5	4500
14	0	0	0	12.5	12.5	4500
15	0.5	-0.5	0.5	16.25	8.75	5250
16	-0.5	-0.5	-0.5	8.75	8.75	3750
17	0	-1	0	12.5	5	4500
18	-0.5	0.5	0.5	8.75	16.25	5250
19	0.5	0.5	0.5	16.25	16.25	5250
20	0	0	0	12.5	12.5	4500

#### 4.2. Output Cutting Simulation Results

Based on ABAQUS simulation platform, the simulation test was carried out in accordance with the cutting simulation center composite design scheme in Table 5, and the simulation test results were obtained, as shown in Table 6.

**Table 6.** Test parameters and simulation results of cutting force.

Sequence	Experimental Combination			Response Value		
	$a_p$ (mm)	$a_e$ (mm)	$v_f$ (mm/min)	$F_x$ (N)	$F_y$ (N)	$F_z$ (N)
1	16.25	16.25	3750	5	7.17	8.31
2	12.5	12.5	4500	4.56	6.49	7.34
3	12.5	12.5	6000	6.01	6.48	7.63
4	12.5	12.5	4500	5.9	6.87	8
5	8.75	16.25	3750	5.92	7.92	9.29
6	12.5	12.5	4500	5.9	6.56	7.67
7	8.75	8.75	5250	4.6	4.96	7.45
8	5	12.5	4500	4.53	6.03	9.03
9	12.5	20	4500	8.67	9.4	10.55
10	16.25	8.75	3750	5.1	5.21	6.25
11	12.5	12.5	4500	5.02	6.68	7.22
12	12.5	12.5	3000	4.21	5.74	6.59
13	20	12.5	4500	6.87	7.2	8
14	12.5	12.5	4500	6.01	6.5	7.74
15	16.25	8.75	5250	5.58	5.3	6.65
16	8.75	8.75	3750	3.95	4	5.65
17	12.5	5	4500	4.03	4.07	6.53
18	8.75	16.25	5250	7.36	9.65	11.32
19	16.25	16.25	5250	9.12	9.2	10.85
20	12.5	12.5	4500	6.1	6.6	7.84

#### 4.3. Construction of Cutting Force Prediction Model

Based on the experimental design method and response value, combined with the analysis software Design-Expert, the regression analysis was used to analyze the data. When the regression equation was established, some items may have no significant effect on the response. In order to obtain an optimal regression equation, these items should be removed without affecting the accuracy of the equation. The following equations are quadratic regression models for the rotational vibration cutting of the Nomex honeycomb-core composite material with disc-cutter.

$$\left\{ \begin{array}{l} F_x = +7.215 - 0.153a_p - 0.47a_e - 1.139 \times 10^{-3}v_f + 0.086 \times 10^{-3}a_p v_f \\ \quad + 0.117 \times 10^{-3}a_e v_f + 0.012a_e^2 - 0.065 \times 10^{-6}v_f^2 \\ F_y = -5.03 + 0.536a_p + 0.253a_e + 0.994 \times 10^{-3}v_f - 0.014a_p a_e \\ \quad - 0.049 \times 10^{-3}a_p v_f + 0.061 \times 10^{-3}a_e v_f - 0.077 \times 10^{-6}v_f^2 \\ F_z = +2.576 - 0.225a_e + 1.004 \times 10^{-3}v_f - 0.086 \times 10^{-3}a_p v_f + 0.065 \times 10^{-3}a_e v_f \\ \quad + 0.015a_p^2 + 0.011a_e^2 \end{array} \right. \quad (4)$$

where  $a_p$  is the cutting depth (mm),  $a_e$  is the cutting width (mm) and  $v_f$  is the feed rate (mm/min).

#### 4.4. Variance Analysis

Table 7 is variance analysis of disc-cutter Nomex honeycomb composites ultrasonic vibration-assisted cutting force prediction model. As can be seen from the results of variance analysis, in the regression model of  $F_x$  and  $F_y$ ,  $P < 0.0001$  and in regression model of  $F_z$ ,  $P < 0.005$ , which indicating that the regression model established for  $F_x$ ,  $F_y$  and  $F_z$  was extremely significant. The feed speed  $v_f$ , cutting depth  $a_p$  and cutting width  $a_e$  had a great influence on the cutting force of rotary vibration of the disc-cutter. The lack of fit of  $F_x$  ( $P = 0.7098 > 0.05$ ), the lack of fit of  $F_y$  ( $P = 0.1271 > 0.05$ ) and the lack of fit of  $F_z$  ( $P = 0.0767 > 0.05$ ), indicating that the lack of fit of regression models of  $F_x$ ,  $F_y$  and  $F_z$  was not significant. According to the credibility analysis of the quadratic regression equation, the coefficient of determination of the regression model of  $F_x$  was  $R^2 = 0.9510$  and the adjustment of  $R^2 = 0.9069$ , indicating that the model could explain 90.69% of the experimental data; the coefficient of determination of the regression model of  $F_y$  was  $R^2 = 0.9568$ , adjust  $R^2 = 0.9179$ , indicating that the model could explain 91.79% of the experimental data;  $F_z$  regression model decision coefficient  $R^2 = 0.8916$ , adjust  $R^2 = 0.7940$ , indicating that the model could explain 79.40% of the experimental data.

Combining the above analysis of variance and model significance tests, it is shown that the predicted values of  $F_x$ ,  $F_y$  and  $F_z$  fit well with the experimental values; the regression effect of the model was great, and it had a high credibility. Therefore, the regression model of the disc-cutter rotary-vibration-cutting force of the honeycomb-core material established by the response surface method was effective, and it could be used to analyze and predict the cutting force.

**Table 7.** Regression model analysis of variance.

	Sources of Variance	Sum of Squares	Degrees of Freedom	Mean Square	F	P (Prob > F)
F <sub>x</sub>	Model	27.71	9	3.08	21.56	<0.0001
	residual	1.43	10	0.14		
	Loss of quasi	0.53	5	0.11	0.59	0.7098
	Pure error	0.90	5	0.18		
	Sum	29.14	19			
R <sup>2</sup> = 0.9510, After the adjustment: R <sup>2</sup> = 0.9069						
F <sub>y</sub>	Model	37.66	9	4.18	24.61	<0.0001
	residual	1.7	10	0.17		
	Loss of quasi	1.27	5	0.25	2.99	0.1271
	Pure error	0.43	5	0.085		
	Sum	39.36	19			
R <sup>2</sup> = 0.9568, After the adjustment: R <sup>2</sup> = 0.9179						
F <sub>z</sub>	Model	32.27	9	3.59	9.14	0.0009
	residual	3.92	10	0.39		
	Loss of quasi	3.14	5	0.63	4.01	0.0767
	Pure error	0.78	5	0.16		
	Sum	36.19	19			
R <sup>2</sup> = 0.8916, After the adjustment: R <sup>2</sup> = 0.7940						

## 5. Conclusions

In order to improve the processing quality such as surface burrs and cutting damage caused by the cutting force during rotary-vibration-cutting honeycomb-core material, several key technologies involved in finite element simulation of honeycomb-core material model were studied in this paper, following conclusions could be obtained:

- (1) The three-dimensional finite element simulation model of disc-cutter which used in honeycomb-core material ultrasonic vibration-assisted cutting process was established, the material properties and material failure criteria were studied in detail;
- (2) The validation experiment was executed in order to verify the simulation resulted, the relative error between simulation results and experimental results was less than 13.2%;
- (3) The cutting force prediction model was established though the regression analysis based on the simulation results. According to the cutting force model, the influence of cutting parameters on cutting force could be predicted; the processing quality and the processing efficiency could be improved due to cutting parameters regulation;
- (4) By analyzing the influence of cutting parameters on the cutting force, it was concluded that larger cutting depth and smaller cutting width had better cutting performance which was reflected in less burrs and better surface integrity.

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