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Analytical Assessment of the Structural Behavior of a Specific Composite Floor System at Elevated Temperatures Using a Newly Developed Hybrid Intelligence Method

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Abstract: The aim of this paper is to study the performance of a composite floor system at different heat stages using artificial intelligence to derive a sustainable design and to select the most critical factors for a sustainable floor system at elevated temperatures. In a composite floor system, load bearing is due to composite action between steel and concrete materials which is achieved by using shear connectors. Although shear connectors play an important role in the performance of a composite floor system by transferring shear force from the concrete to the steel profile, if the composite floor system is exposed to high temperature conditions excessive deformations may reduce the shearbearing capacity of the composite floor system. Therefore, in this paper, the slip response of angle shear connectors is evaluated by using artificial intelligence techniques to determine the performance of a composite floor system during high temperatures. Accordingly, authenticated experimental data on monotonic loading of a composite steel-concrete floor system in different heat stages were employed for analytical assessment. Moreover, an artificial neural network was developed with a fuzzy system (ANFIS) optimized by using a genetic algorithm (GA) and particle swarm optimization (PSO), namely the ANFIS-PSO-GA (ANPG) method. In addition, the results of the ANPG method were compared with those of an extreme learning machine (ELM) method and a radial basis function network (RBFN) method. The mechanical and geometrical properties of the shear connectors and the temperatures were included in the dataset. Based on the results, although the behavior of the composite floor system was accurately predicted by the three methods, the RBFN and ANPG methods represented the most accurate values for split-tensile load and slip prediction, respectively. Based on the numerical results, since the slip response had a rational relationship with the load and geometrical parameters, it was dramatically predictable. In addition, slip response and temperature were determined as the most critical factors affecting the shear-bearing capacity of the composite floor system at elevated temperatures.

Keywords: extreme learning machine; radial basis function network; neural network; shear connector; floor system; elevated temperature; metaheuristic algorithms

1. Introduction

Fire safety is a major concern that has not been well developed in recent years. Many studies have been conducted on a range of approaches to mitigate fire-induced damage to steel and concrete members [1–3]. Some research studies have also focused on improving



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Copyright: © 2023 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). the safety of occupants during and after fire occurrences and on reducing the refurbishment and retrofitting costs.

Composite beams have been widely used in a variety of structures and buildings due to a number of positive features such as lower thickness, considerable span length and high stiffness [4,5]. The development of different composite beams is highly valued to mitigate some shortcomings of specific composite structures [6–8]. Steel-concrete composite beams are one of the critical components of high rise and multi-story structures, and different studies have been conducted to improve their performance [9,10]. Moreover, shear connectors (SCs) are one of the most practical elements that are extensively utilized in steelconcrete composite beams to increase shear strength and the integrated behavior of concrete and steel. There are different types of SCs such as channel, angle, stud and perfobond sections. Concrete is cast in different shapes and types such as self-consolidating [11], porous [12], high strength, lightweight and green concrete [13]. Concrete characteristics are divided into two major categories namely fresh and hardened properties. Fresh properties include the most primitive properties of concrete such as slump and workability. On the contrary, hardened properties refer to a range of critical features such as compressive strength, flexural strength, shear strength and corrosion resistance, where many attempts have been made to enhance these properties by surface protection [14,15], the inclusion of fibers and cementitious replacement powders [16].

A few studies have considered push-out tests with various loading patterns to evaluate slip and failure load in channel SCs [17]. Channel SCs have been shown to exhibit ductile performance when exposed to a series of load patterns while equipped with c-shaped connectors; however, this behavior was amplified in more extended channel SCs [18]. In another study, composite beams showed brittle behavior when channel SCs were embedded in plain concrete with no confinement [19]. In contrast, when the channel SCs were embedded in high-strength concrete, the behavior of the composite beam was ductile. In addition, more extended channel SCs demonstrated better flexibility than lower channels [19]. Bearing capacity has a direct linear relationship with length, and therefore, a C-shaped channel SC with 150 mm length has almost 60 percent higher load-carrying capacity compared to a 100 mm channel SC. In addition, failure modes are governed by concrete properties when a C-shaped channel SC is embedded in high-strength concrete [20]. Despite the inevitable slip between an I-beam and slab, this slip can be negligible with appropriate design of the shear connector. Thick channel connectors result in reducing slip and consequently increasing load capacity [21].

Angle SCs present suitable ductility but a noticeable stiffness loss [22]. Using angle shear connectors at elevated temperatures has been shown to protect strength loss by up to 50% of the initial strength [23]. Three main failure modes have occurred during tests: (1) shear connector fracture, (2) concrete crushing and (3) concrete shear plane failure. Based on experimental results, connectors' strength loss and deterioration while exposed to fire can be changed in different situations [24,25]. Several methods have been employed for data validation such as artificial neural networks, whereas extreme learning machine [21,26], genetic programming, neural network and other natural basis functional networks have been reported to be the best methods [27]. Finite element and finite strip methods have also been proven to be reliable approaches for data authentication and prediction [28–33].

The role of AI techniques has recently been highlighted in the. development of engineering goals [25,34,35]. A raw model of artificial neural networks (ANNs) can generally be developed by training and optimization techniques such as backpropagation algorithms [36]. Then, ANNs are able to solve three types of problems: (1) classification, (2) function approximation and (3) time series prediction. However, not being able to proceed with local extrema and complications in crossing plateaus of error function landscape are common defects of classic approaches [37]. Neural networks and some optimization techniques have recently been applied to solve nonlinear and sophisticated engineering problems. In some cases, the performance of an ANN can be improved by using the global search feature of classic methods such as GA and PSO [26]. As a remedy for ANN problems,

a fuzzy technique has been integrated with neural networks, and other algorithms have been developed such as the artificial neuro fuzzy inference system (ANFIS) [38], which has been used for different types of applications including the prediction of experimental results with nonlinear relationships and parameter identification of the test data. Studies have shown that an ANFIS alone has some shortcomings which could be annihilated by incorporating metaheuristic algorithms [39]. Due to the relatively conventional approach of laboratory data in the steel-concrete composite sector, in addition to the studies on different SC applications to develop the structural strength of composite floor systems and raise their ductility, AI techniques can be employed to optimize and to evaluate the structural characteristics of steel-concrete composite structures [19].

In addition, several studies have used different AI techniques in comparative studies to challenge the main algorithm results and to achieve reliable outcomes [40]. In a study, the RBFN approach was selected as a secondary method to challenge the main algorithm prediction which was stochastic gradient descent. The RBFN results were also used to detect landslide susceptibility [41]. The machine learning method is another useful approach as a secondary algorithm for prediction of data and assessment of structural behavior [42]. The ELM method has been performed on data from steel-concrete composite floors at different heat stages along with an ANN and genetic programming technique. Based on the results, the ELM method accurately predicted the target outcomes and achieved superior performance indices [43]. In this study, a comparative AI assessment on data derived from a composite floor system at different heat stages was performed to predict the failure load and to obtain the most critical parameters for slip response.

In this study, we conducted a comparative AI assessment of the behavior of a composite floor system at different temperatures. In addition, three different AI methods were performed which was profoundly helpful to identify the most susceptible characteristics of the composite floor system at elevated temperatures. Predicting values for split-tensile and shear connector slip of a steel-concrete composite floor system subjected to a monotonic loading scenario at different heat stages is complicated since empirical testing is difficult and time-consuming and because the effective parameters are somehow hidden from the researchers or the outcomes of test results do not have enough consistency. Therefore, in this study, we aimed to overcome the prediction difficulties by employing an integrating neural network and fuzzy system with a multi-hybrid metaheuristic technique, called the ANPG method. The main algorithm was a hybrid AI technique carried out to predict the shear response in angle shear connectors simultaneously with an investigation of the effect of various inputs on the structural performance of a composite floor system at elevated temperatures. For this purpose, we developed the ANPG algorithm by using a hybrid metaheuristic (combination of PSO-GA) technique which was based on a neuro-fuzzy algorithm (ANFIS) due to the diverse nature of the employed data and its ability to predict the shear behavior of composite systems at high temperatures. Accordingly, some validated data from Davoodnabi et al. [23] were derived from a previous laboratory research study to delineate the shear behavior of the angle shear connectors at different temperatures. In soft computing methods, the above-mentioned methods can provide a compact solution for multi-variable method drawbacks since knowledge of the internal system is not necessary. Two proven and effective artificial intelligence algorithms, i.e., the RBFN and ELM methods, were also employed to verify and to compare the obtained results. In addition, the affect of different parameters on the shear-bearing capacity of the composite floor system were evaluated and the parameters that were the most critical factors were selected.

2. Materials and Methods

For this research, the database was obtained from the study by Davoodnabi et al. [23] regarding a monotonic push-out test on SCs at elevated temperatures to achieve reliable structural behavior of a composite system at high temperatures. The aforementioned shear connectors are shown in Figure 1.

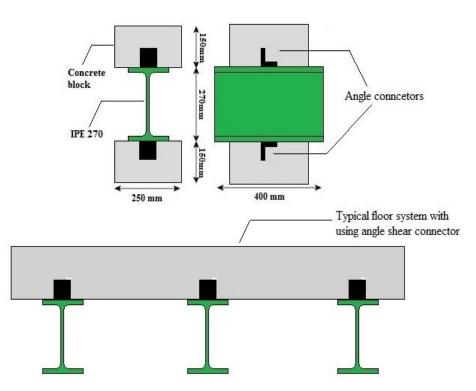


Figure 1. Composite floor system and shear connectors.

2.1. Statistical Data of Samples

In this study, the dataset was the information of experiments that eventually consisted of 584 test results (the specifications of the dataset are shown in Appendix A). The statistical properties of the whole dataset and input variables are indicated in Table 1.

| Inputs | Variables | Min | Max | Mean Value | Std |
|----------|------------------|------|-------|------------|-------|
| Input 1 | Slip (mm) | 0.00 | 73.70 | 22.87 | 39.2 |
| Input 2 | Length (mm) | 30.0 | 50.0 | 40.0 | 10.0 |
| Input 3 | Thickness (mm) | 5.0 | 7.0 | 6.0 | 0.8 |
| Input 4 | Height (mm) | 65.0 | 100.0 | 80.4 | 14.8 |
| Input 5 | Temperature (°C) | 25.0 | 850.0 | 568.2 | 311.9 |
| Input 6 | Load (kN) | 0.00 | 126.7 | 36.8 | 27.6 |
| Outputs | | | | | |
| Output 1 | Slip (mm) | 0.00 | 73.70 | 22.87 | 39.2 |
| Output 2 | Load (kN) | 0.00 | 126.7 | 36.8 | 27.6 |

Table 1. Details of input variables.

As shown in Table 1, the concrete's compressive strength along with the steel properties remained at constant values with no involvement in the dataset. The database was set for variables such as the height, length and thickness of the shear connectors, which directly affect the split-tensile capacity of the composite floor system, especially at elevated temperatures. Load and slip could be replaced by each other in the placement order either as an input or an output.

2.2. Analytical Assessment

Recently, some research studies have been conducted on the performance of welded built-up steel members using AI techniques [25]. The following sections describe the architecture and some background of the employed algorithms in the current study.

2.2.1. ANFIS Algorithm and Architecture

In an adaptive network (AN), nodes are directly connected by links, and every node acts in a defined performance on its receiving signals to produce a single node output; therefore, this procedure is made up of a multi-layer feed-forward system [34]. Notably, the configuration of an AN acts as a static node function on its receiving signals to produce a single node output, and every node performance is a parameterized function with changeable parameters. With any alteration of these parameters, the node functions are altered such as the overall behavior of the AN, Figure 2. In a fuzzy inference system (FIS), membership function parameters are tuned by a specific technique. Indeed, an ANFIS is utilized to delineate the optimal amounts of equivalent FIS parameters through a learning algorithm [44]. Across the training session(s), parameter optimization is performed in a way that the error between actual output and target decreases. A hybrid algorithm is utilized for the optimization that is a combination of gradient descent and the least square estimate method. The optimized parameters are called premise parameters that specify the shape of the membership functions (MFs). To minimize the error measure, each optimization routine could be used after the MFs are generated. The parameter set of the AN permits the fuzzy systems to learn from the modeling data.

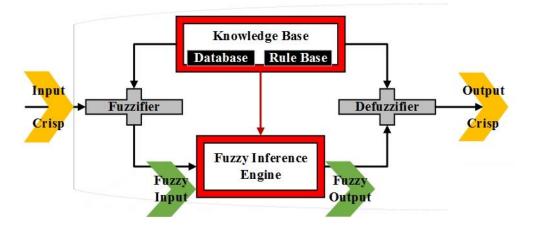


Figure 2. Flowchart of the ANFIS network concept.

The ANFIS network has five layers called the fuzzy layer, normalized layer, product layer, total output layer and de-fuzzy layer, as shown in Figure 3 [45]. During this technique, a threshold value between the output and the actual value is set and the following parameters are obtained by the least-squares model, while an error for all data is also received. If the threshold value exceeds the deliberated threshold, using the gradient descent method the premise parameters are updated. This continues until the error turns out to be less than the threshold. Because the parameters are simultaneously obtained by using two algorithms (the decent gradient and least-squares algorithms), the utilized algorithm during this procedure is called a hybrid algorithm.

2.2.2. Particle Swarm Optimization (PSO)

The PSO algorithm is another member of the swarm intelligence algorithms initially generated by Kennedy and Eberhart [46] while sharing many aspects with evolutionary computation models such as GA. Similar to other population-based intelligence models, PSO needs an initial population of random resolutions. The search for optimal values is gained by updating the generations without evolution operators such as mutation and crossover. The potential decisions are generally called particles in PSO, flying through the resolution space by following their own experiences and the current optimal particles. Thus, the performance of PSO is comparable with GA and may be regarded as an alternative approach for GA. Figure 4 indicates the systematic sequences of the PSO algorithm.

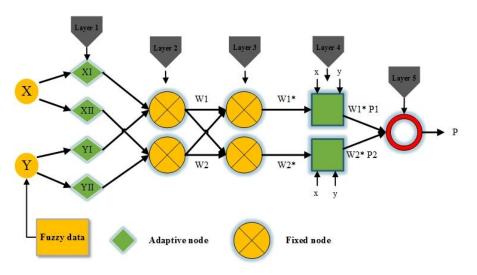


Figure 3. The underlying architecture of the ANFIS.

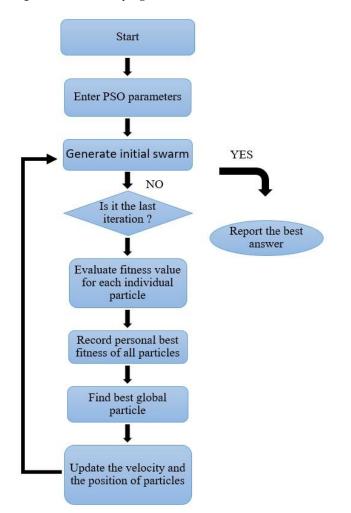


Figure 4. Flowchart of sequential steps of the PSO algorithm.

2.2.3. Genetic Algorithm (GA)

Holland (1992) [47] introduced the GA based on the extended evolution theory of Darwin that was developed by Goldberg and Holland (1988) [48]. As a member of the larger group of evolutionary algorithms (EAs), the GA is a metaheuristic algorithm based on the principles of biological evolution in nature. After many evolutions, the best individual is

obtained. Compared with other optimizing methods, the GA includes good robustness and convergence. With the same accuracy of calculation, the GA takes the least time to find an optimal resolution [49]. Figure 5 represents the step-by-step platform of the GA algorithm.

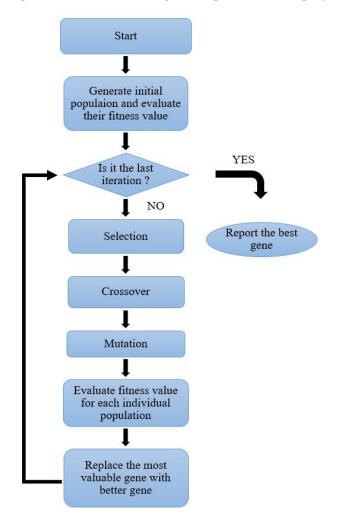


Figure 5. Flowchart of the sequential steps of the GA algorithm.

2.2.4. Hybrid ANPG Architecture

For the first time, a hybridized ANFIS using PSO and GA techniques was applied to solve a composite floor system problem. The combination of the sequential PSO-GA and ANFIS is depicted in Figure 6. In order to identify the best weights and to select suitable functions, the ANPG method was performed several times to predict one specific outcome with a variety of input scenarios. First, in PSO, swarm is initiated by a group of random resolutions as a particle, while showing the particle's position. Then, the specific velocity is identified, the transmitting function is triggered, and the GA procedure initiates to optimize the final problem space. Finally, a particular velocity is gained for any *i*th particle in every cycle by using Equation (1) where w represents the inertia weight.

$$v_i(t+1) = wv_i(t) + c_1\phi_1(p_i(t) - x_i(t)) + c_2\phi_2(p_i(t) - x_i(t))$$
(1)

 c_1 and c_2 represent the positive acceleration coefficients. $\vec{\phi}_1$ and $\vec{\phi}_2$ show uniformly distributed random vectors [0, 1], in which a random value is tried for each dimension. \vec{v}_i limited to $\left[-\vec{v}_{\max}, \vec{v}_{\max}\right]$ series is reliant on the problem. In some cases, the velocity

exceeds the mentioned curb and is rearranged within its suitable limits. Based on their velocities, every particle alters its position based on the following Equation (2):

$$s(t+1) = s(t) + v(t+1)$$
 (2)

Based on \vec{v}_i and \vec{s}_i , the particle population tends to cluster around the best number.

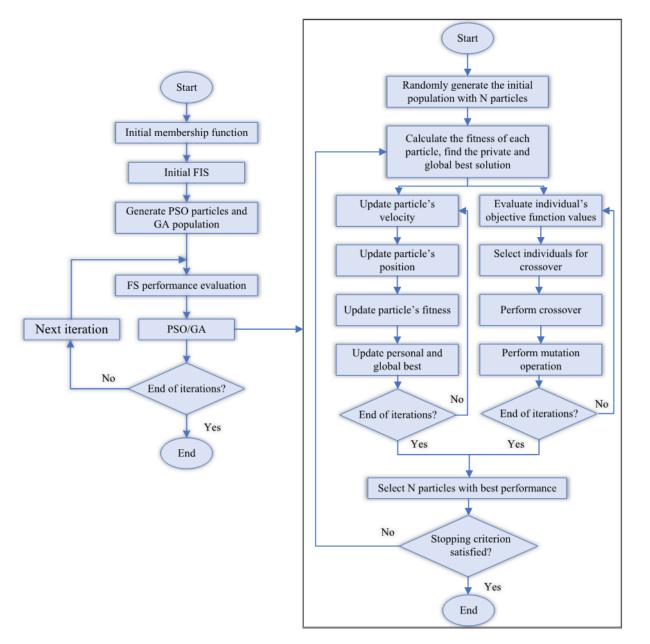


Figure 6. The sequential combination of the hybrid ANPG algorithm.

The ANPG hybrid method operates in regard to random population generation and is based on avian mass flight behavior modeling and simulation of fish mass movement. A global minimization method can deal with questions whose answers are a point or surface in n-dimensional space. A random population is assumed in this space, and an elementary velocity is defined for it and between the particles to the communication channels. The particles move through the response space, and the outcomes are computed on a "merit basis" after each time interval. Then, particles speed up toward the particles of higher competence that are in matching communication groups. Although each method is performed satisfactorily in a range of problems, it demonstrates pronounced capability in resolving continuous problems in optimization. The GA, by using evolutionary biology methods, tries to find the optimum formula for predicting or pattern matching. The GA could be an effective choice for regression-based prediction techniques, while its modeling is a programming technique based on genetic evolution to problem resolutions. The solved problem possesses inputs converted into solutions through a patterned process of genetic evolution. Afterward, by using the fitness function, the solutions are verified as candidates.

2.2.5. Extreme Learning Machine (ELM)

As a single-layer learning tool, the ELM method was introduced which is similar to a feed-forward neural network [50]. In the ELM method, the output weights are analytically determined while the weights of input are defined randomly. The superiority of the ELM method is its extremely fast ability to find target weights. Additionally, without exterior interference, the ELM method is able to determine all the network parameters. In the case of prediction and characteristic estimation for concrete products, the ELM method is efficient and reliable [51] and because of these benefits it has gained high popularity and applicability.

The ANPG algorithm terminates in case the condition of problem exit is arranged. Generally,

it is an iteration-based algorithm in which most of its parts are randomly selected.

2.2.6. Radial Basis Function Network (RBFN) Method

Generally, in each RBFN architecture, a set of D-dimensional radial activation functions estimate the input function $f_{(x)}$. The architecture consists of the D neuron input layer, the P neuron output layer and the M neuron hidden layer. The biases at each output neuron and adjustable weights between the hidden and output layers are shown in Figure 7 [52,53]. The system is represented by the *n*th input vector, and as described in Equation (3), the approximation function $f_{(x)}$ can be represented as a linear combination of radial basis functions in which the output of the *k*th network consists of the sum of weighted hidden layer neurons plus the bias [41]:

$$\hat{f}(X) = wh(X) + w, k = 1, 2, \dots, P$$
 (3)

where:

 w_{kj} = weight of the *j*th basis function and *k*th output; $h_j(X^n)$ = output of *j*th hidden neuron for the input vector (x^n) ; $w_{(k0)}$ = bias term at *k*th output neuron.

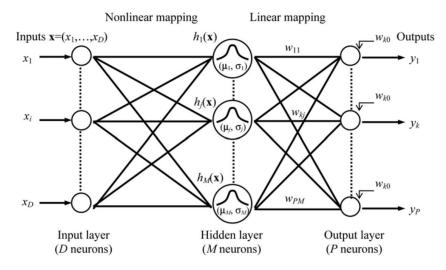


Figure 7. The architecture of the RBF network.

2.2.7. Performance Evaluation

Models of all the developed methods were evaluated by using evaluation criteria namely, root mean squared error (RMSE), determination coefficient (R^2) and Pearson correlation coefficient (r) as follows:

$$RMSE = \sqrt{\frac{\sum\limits_{i=1}^{n} (P_i - O_i)^2}{n}}$$
(4)

$$\mathbf{r} = \frac{n\left(\sum_{i=1}^{n} O_i \cdot P_i\right) - \left(\sum_{i=1}^{n} O_i\right) \cdot \left(\sum_{i=1}^{n} P_i\right)}{\sqrt{\left(n\sum_{i=1}^{n} O_i^2 - \left(\sum_{i=1}^{n} O_i\right)^2\right) \cdot \left(n\sum_{i=1}^{n} P_i^2 - \left(\sum_{i=1}^{n} P_i\right)^2\right)}}$$

$$\mathbf{R}^2 = \frac{\left[\sum_{i=1}^{n} \left(O_i - \overline{O_i}\right) \cdot \left(P_i - \overline{P_i}\right)\right]^2}{\sum_{i=1}^{n} \left(O_i - \overline{O_i}\right) \cdot \sum_{i=1}^{n} \left(P_i - \overline{P_i}\right)}$$
(5)

where P_i and O_i are the predicted and observed variables, and n is the total number of considered data. Alternatively, MATLAB (2019) was used to compare the code performance of the ANPG, RBFN and ELM methods in one computer system with no external compiler or toolbox implementation.

3. Results

In this study, the employed algorithms (the ANPG, RBFN and ELM methods) were separately tuned. To optimize the coefficients of specific parameters for each algorithm, the other parameters were considered to remain constant. By changing the coefficient value, the best value was determined and used for different parameters. Therefore, all the algorithms were repeatedly used and revised to develop the algorithms, as explained below.

3.1. ANFIS-PSO-GA (ANPG) Method

The parameters of the ANPG method were adjusted and are summarized in Table 2. The inputs of the dataset were initially defined and predicted, while the predition values of split-tensile load and slip were obtained separately in different analyses (Table 2). The results of the regression and comparative graphs are shown in Figures 8 and 9, respectively. As shown in Figure 8 and Table 3, the ANPG method is more successful for predicting values of slip than for predicting tensile load, which could be due to the properties of this type of NN or simply to the output being more predictable. In addition, the test results of slip and load prediction demonstrate good consistency with the training results, indicating the reliability of this method for predicting complex and nonlinear test results. Despite the acceptability of the outputs of the other employed ELM method, the inconsistent test and training results reduced the reliability of the output(s).

Table 2. Parameter characteristics used for the ANPG method.

| FIS | Population | PSO- | GA-Sub- | MAX- | Inertia | Damping | Learning C | oefficient | Conducted |
|----------|------------|------------|-----------|-----------|---------|---------|------------|------------|----------------|
| Clusters | Size | Iterations | Iteration | Iteration | Weight | Ratio | Personal | Global | Fuzzy Function |
| 10 | 90 | 50 | 45 | 150 | 1.00 | 0.988 | 1 | 2 | bell-shaped |

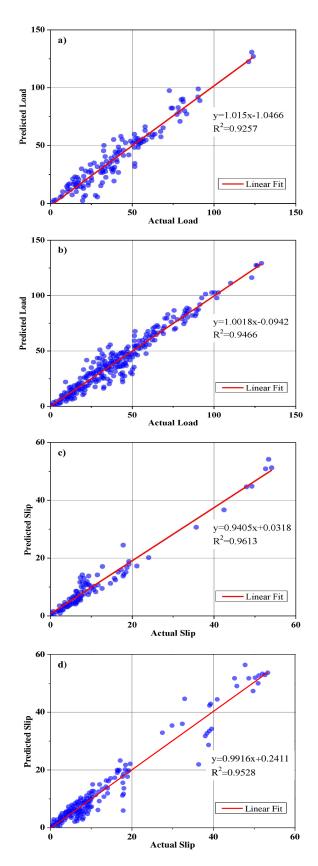


Figure 8. ANPG vs. experimental results regression for: (**a**) Ultimate shear load test phase; (**b**) ultimate shear load training phase; (**c**) slip test phase; (**d**) slip training phase.

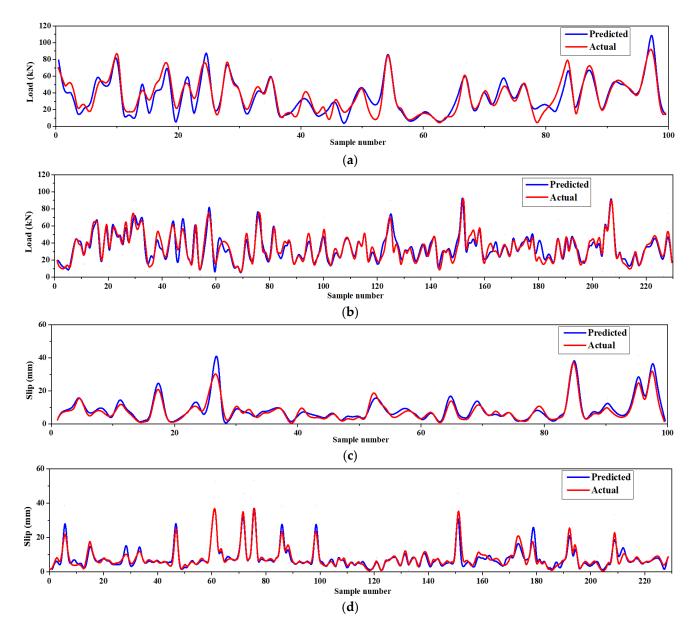
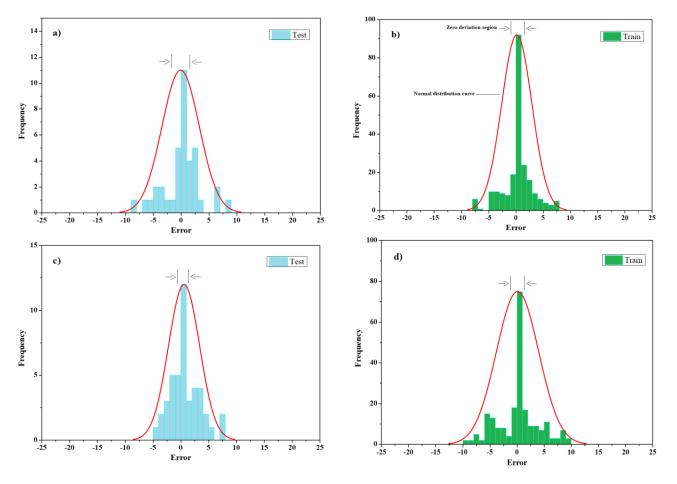


Figure 9. ANPG vs. experimental diagram for: (a) Ultimate shear load test phase; (b) ultimate shear load training phase; (c) slip test phase; (d) slip training phase.

| Table 3. Output and input database. | |
|-------------------------------------|--|
|-------------------------------------|--|

| | | Test | Train |
|-------------------------------|-------------------|--------|--------|
| | Std * | 3.869 | 3.1884 |
| Split-tensile load prediction | e _{mean} | -0.014 | -0.081 |
| opini tenenie nous presidenti | R ² | 0.925 | 0.946 |
| | r | 0.962 | 0.973 |
| | RMSE | 3.869 | 4.868 |
| | | Test | Train |
| | Std * | 0.954 | 1.136 |
| Slip prediction | e _{mean} | -0.012 | -0.049 |
| | umean | 0.0 | 0.017 |
| Ship prediction | R ² | 0.961 | 0.953 |
| Shp prediction | | | |
| Shp prediction | R ² | 0.961 | 0.953 |

* Std, standard deviation.



For the tensile load, the standard deviation of the two test and training phases is 18%, and the standard deviation is 16% for slip value outputs, indicating less error concentration in the first output than the second output, Figure 10.

Figure 10. ANPG vs. experimental results regression for: (**a**) Split-tensile load test phase; (**b**) split-tensile load training phase; (**c**) slip test phase; (**d**) slip training phase.

3.2. RBFN

Table 4 shows the settings used for the combination of a hybrid grid. The results of the RBFN method are presented in Table 5 and Figures 11 and 12. In this method, the results for the lateral load output were much better than the compressive strength. In addition, the test and training phase results for the first output were very similar.

| Table 4. The parame | er characteristics use | ed for the RBFN method. |
|---------------------|------------------------|-------------------------|
|---------------------|------------------------|-------------------------|

| FIS | Population | MAX- | Cross over | | Mutation | Selection |
|----------|------------|-----------|------------|-----|----------|-----------|
| Clusters | Size | Iteration | Percentage | | Rate | Pressure |
| 10 | 180 | 200 | 1.00 | 0.5 | 0.1 | 8 |

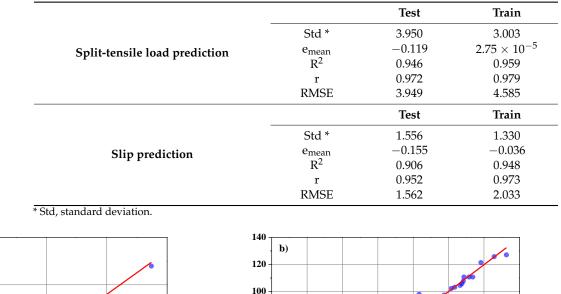


Table 5. Analytical prediction results through the RBFN method.

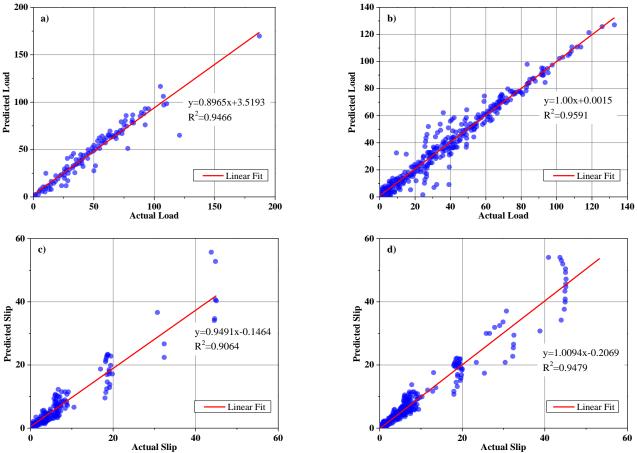


Figure 11. RBFN vs. experimental results regression for: (a) Ultimate shear load test phase; (b) ultimate shear load training phase; (c) slip test phase; (d) slip training phase.

The results of this neural network approximation for the tensile e-load value output indicated more concentration at the boundary. In particular, during the training phase, the reliable evaluation criteria results are approximate. Another point to note from the graphs in Figure 12 is the relatively low error for tensile-load data below 5 MPa for both the training and test phases and relatively high error for data above 20 MPa, especially during the training phase (Figure 12). Furthermore, slip value outputs indicate higher irregularities above 10 mm. The standard deviation of the test and training phases for the tensile load is 24% and the standard deviation is 15% for slip value outputs, indicating a better concentration of errors in slip output than load output (Figure 13).

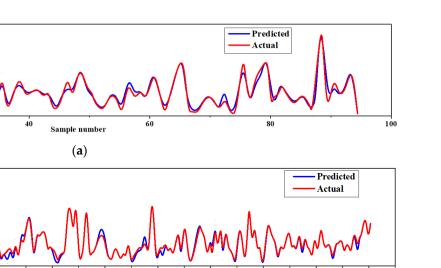
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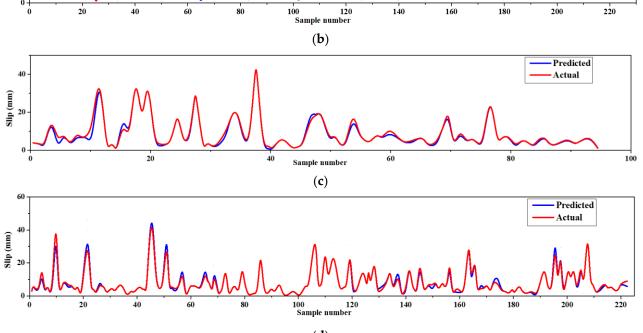
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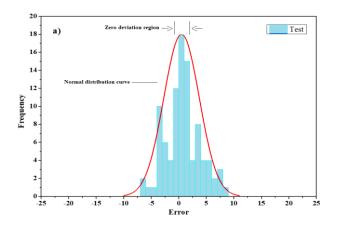
100





(**d**)

Figure 12. RBFN vs. experimental diagram for: (**a**) Split-tensile load test phase; (**b**) split-tensile load training phase; (**c**) slip test phase; (**d**) slip training phase.



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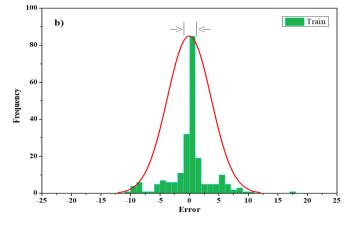


Figure 13. Cont.

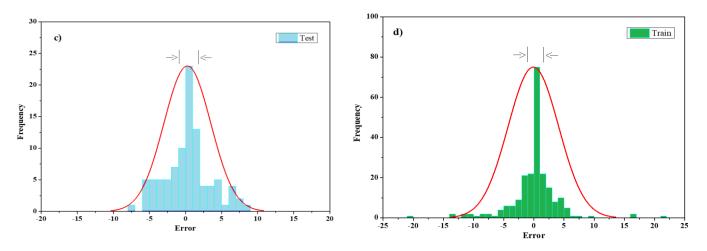


Figure 13. RBFN error histogram for: (**a**) Split-tensile load test phase; (**b**) split-tensile load training phase; (**c**) slip test phase; (**d**) slip training phase.

3.3. ELM Method

The last neural network is the ELM method and the settings and are summarized in Table 6. The results are also acceptable for both outputs, as shown in Figures 14 and 15. However, by comparing the load output evaluation criteria to those of the slip value outputs and by comparing the test and training results, the load outputs show more consistency. At the same time, it is different for other products, as shown in Table 7.

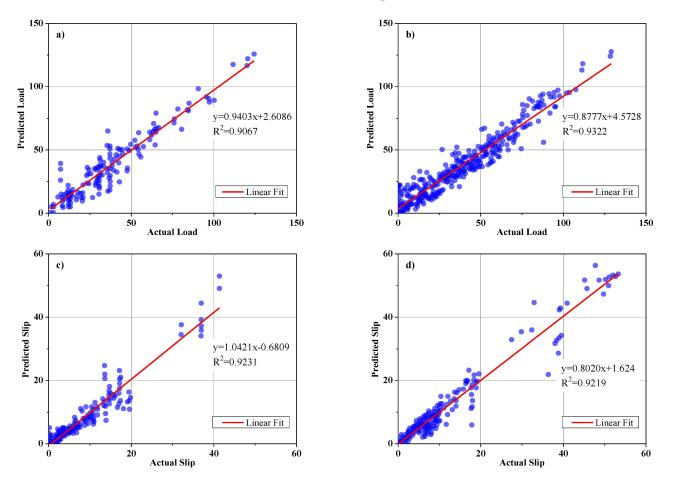


Figure 14. ELM vs. experimental results regression for: (**a**) Ultimate shear load test phase; (**b**) ultimate shear load training phase; (**c**) slip test phase; (**d**) slip training phase.

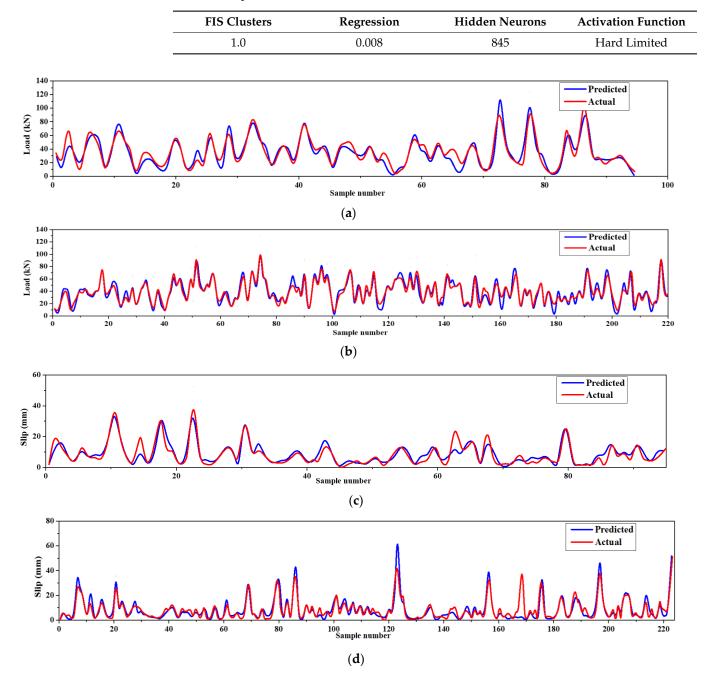


Table 6. The parameter characteristics used for the ELM method.

Figure 15. ELM vs. experimental diagram for: (**a**) Split-tensile load test phase; (**b**) split-tensile load training phase; (**c**) slip test phase; (**d**) slip training phase.

Regarding the standard deviation and error histogram in Figure 16, errors have a greater focus on slip value outputs which make the outputs more reliable. The tensile-load outputs presented are probably good results; however, due to the lack of focus on the errors of the center axis, an unprecedented response could be high with unacceptable errors.

| | | Test | Train |
|-------------------------------|--|--|-------|
| | Std * | 4.341 | 3.949 |
| Split-tensile load prediction | e _{mean} | 0.128 | |
| opin tensile iouu preutenon | R ² | 0.906 | 0.932 |
| | $\begin{array}{ccccc} e_{mean} & 0.128 & 0.02 \\ R^2 & 0.906 & 0.93 \\ r & 0.9522 & 0.96 \\ RMSE & 4.339 & 6.03 \\ \hline & {\bf Test} & {\bf Trai} \\ \hline \\ Std * & 1.454 & 1.85 \\ e_{mean} & -0.086 & 0.04 \\ R^2 & 0.923 & 0.92 \\ \hline \end{array}$ | 0.965 | |
| | RMSE | 4.339 | 6.030 |
| | | Test | Train |
| | Std * | 4.341 3.94 0.128 0.02 0.906 0.93 0.9522 0.96 4.339 6.03 Test Trai 1.454 1.85 -0.086 0.04 0.923 0.92 0.961 0.96 | 1.851 |
| Slip prediction | e _{mean} | -0.086 | 0.044 |
| Ship prediction | \mathbb{R}^2 | 0.923 | 0.922 |
| | r | 0.961 | 0.960 |
| | RMSE | 1 455 | 2 827 |

Table 7. Analytical prediction results through the ELM algorithm.

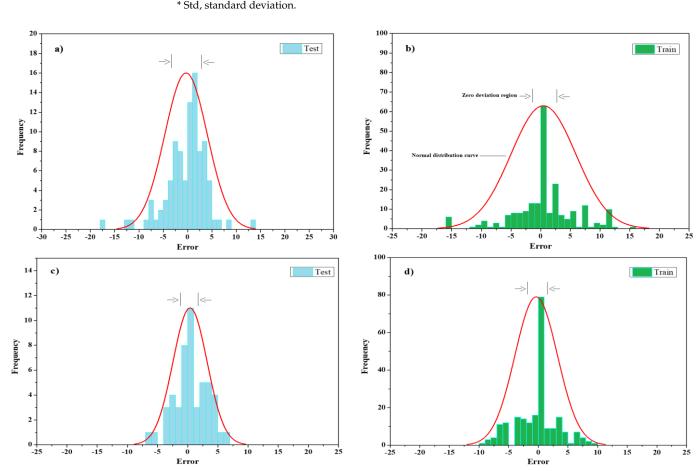


Figure 16. ELM error histogram for: (**a**) Split-tensile load test phase; (**b**) split-tensile load training phase; (**c**) slip test phase; (**d**) slip training phase.

4. Discussion

To define the inputs of RMSE, R^2 and r, an ANFIS was individually trained for every input. The effect of every input on the output could be delineated based on the determined analytical parameters for any input. Inputs with the smallest training RMSE had the most effect or relevance to the output. To identify the overfitting between test data and training, RMSE testing was applied. If the testing RMSE is very high, the regression of data is not beneficial. According to the RMSE training, the optimum combination is PSO and the GA with an ANFIS, with the most substantial accuracy on the output evaluation parameters. By examining the results of all methods, it is concluded that both split-tensile load and slip value outputs indicate a likely predictable trend due to the described inputs and useful employed NNs. A comparison of the best results for each method is shown in Figure 17, where the RBFN prediction is stronger compared to the others with R^2 (test) = 0.9466, R^2 (train) = 0.9591; r (test) = 0.973, r (train) = 0.973; and RMSE (test) = 3.949, RMSE (train) = 4.585. By evaluating the test phase error histograms shown in Figures 10, 13 and 16, due to the minor error interval in the ANPG method, the three graphs show reasonable concentration around the center, and the chance of obtaining a high error response is relatively low compared to the other methods. From the normal distribution point of view in each rectangular histogram of error, 68% of the data are within one time of the standard deviation of the mean value, 95% of the data are within two times of the standard deviation, and 99.7% of the data are within three times of the standard deviation [54–56]. Based on the results and discussion, all of the represented histograms in this paper are in agreement with the mentioned fact. Nevertheless, the charts (load error histograms) are consistent with the normal distribution paradigm, but according to Tables 3–5, different standard deviations and mean values lead to different shapes of the bell curves of load charts compared to the slip charts.

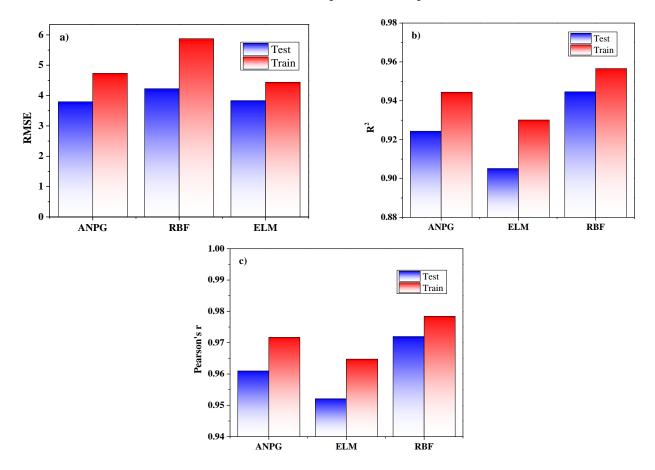


Figure 17. The comparison of performed algorithm results of split-tensile load based on: (a) RMSE; (b) \mathbb{R}^2 ; (c) r.

For slip value output, the ANPG method also provides the best result, as shown in Figure 18. The evaluation of the test phase for the ANPG method is R^2 (test) = 0.961, R^2 (train) = 0.952; r (test) = 0.980, r (train) = 0.976; and RMSE (test) = 0.962, RMSE (train) = 1.735. Thus, in the test phase, the result presented by the ANPG method is more acceptable.

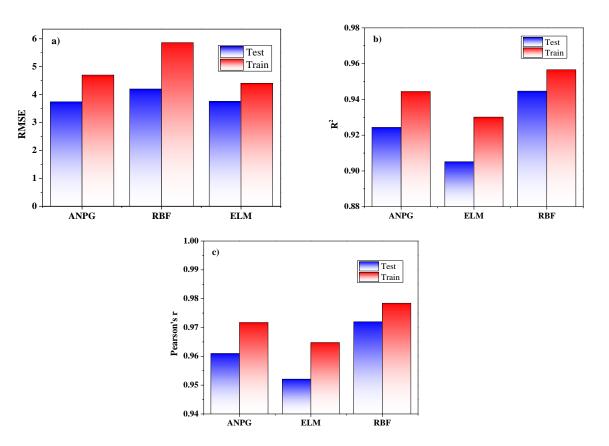


Figure 18. The comparison between the results of the performed algorithms of slip based on the analytical parameters: (a) RMSE; (b) R^2 ; (c) r.

The calculated equations from the linear regressions are summarized in Tables 8 and 9 where the most decisive equations for both split-tensile load and slip value output of specific steel-concrete specimens manufactured by angle shear connector are highlighted.

Table 8. The calculated tensile-load regression equation of the implemented models.

| | Networ | k Result |
|------------|--|--|
| Model | Train Phase | Test Phase |
| | Regression Equation | Regression Equation |
| ANPG | y = 1.015x - 1.0466 | y = 1.0018x - 0.0942 |
| RBF ELM | y = 0.8965x + 3.5193 * y = 0.9403x + 2.6086 | y = 1.0x - 0.0015 ** y = 0.8777x - 4.5728 |

* and ** are the best-achieved equations.

Table 9. The calculated slip value regression equation of the implemented models.

| | Networ | k Result |
|-------|----------------------------|----------------------------|
| Model | Train Phase | Test Phase |
| | Regression Equation | Regression Equation |
| ANPG | y = 0.9405x - 0.0318 * | y = 0.9916x - 0.2411 ** |
| RBF | y = 0.9491x - 0.1464 | y = 1.0094x - 0.2069 |
| ELM | y = 1.0421x - 0.6809 | y = 0.802x - 1.624 |

* and ** are the best-achieved equations.

5. Conclusions

In this study, a comparative AI study was conducted to identify the most susceptible structural characteristics of a composite floor system at elevated temperatures and to predict

critical strength factors such as failure load and slip value of shear connectors. The main algorithm was a hybridized ANFIS technique with PSO and a GA called the ANPG method. The RBFN and ELM methods were also employed as subsidiary evaluation methods. In addition, this study utilized data from 584 test results which included width (mm), height (mm), thickness (mm), shear load (kN), temperature stages (°C) and slip value (mm). The major findings are as follows:

- Based on the results for slip value output, the ANPG method provided the best result. In this method, the test and training phase evaluation criteria were R² (test) = 0.961, R² (train) = 0.952; r (test) = 0.980, r (train) = 0.976; and RMSE (test) = 0.962, RMSE (train) = 1.736. Based on the tolerance charts, the test and training phases both represented suitable compatibility, while envelope curves dramatically maintained the same tolerance. According to the error histograms, the normal distribution shapes confirmed appropriate deviation from the mean value, and slip predictions had the least error value among other predictions.
- In general, the RBFN method is an iteration-based algorithm in which most parts are randomly selected. For tensile-load output, the best result was obtained using the RBFN method with the performance parameters of R² (test) = 0.946, R² (train) = 0.959; r (test) = 0.973, r (train) = 0.973; and RMSE (test) = 3.949, RMSE (train) = 4.585. Tolerance curves in the load section illustrated the best coverage, and error histograms showed the least value in load prediction.
- The ELM method recorded the most suitable results in training phases for slip and split-tensile load prediction. In addition, the ELM method represented the lowest sensitivity against parameter contractions and performed a stable paradigm. For load, the results were R² (test) = 0.906, R² (train) = 0.932; r (test) = 0.952, r (train) = 0.965; and RMSE (test) = 4.339, RMSE (train) = 6.030. Furthermore, the slip results were R² (test) = 0.923, R² (train) = 0.922; r (test) = 0.961, r (train) = 0.960; RMSE (test) = 1.455, RMSE (train) = 2.877.
- For the identification study to determine the most critical factors on the shear-bearing capacity of a composite floor system at elevated temperatures, the ANPG method was performed on two subdata models, where slip and temperature were selected as the most significant parameters on the quality of the shear-bearing capacity. Based on the results, it could also be concluded that by restricting slip, the shear-bearing capacity could be improved at elevated temperatures, and conversely.

Finally, although all three methods (ELM, ANPG and RBFN) resulted in satisfactory prediction results, the ANPG method provided the best slip prediction results and the RBFN method achieved better load prediction results; nevertheless, all the above-mentioned methods are suitable for load and slip prediction.

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Conflicts of Interest: The authors declare no conflict of interest.

Appendix A

 Table A1. Description of the dataset for analysis.

| No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) | No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) | No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) |
|-----|---------------|----------------|----------------|----------------|--------------|--------------|-----|---------------|----------------|----------------|----------------|--------------|--------------|-----|---------------|----------------|----------------|----------------|--------------|--------------|
| 1 | 25 | 65 | 500 | 5 | 0.000 | 0.000 | 31 | 550 | 65 | 50 | 5 | 0.677 | 33.071 | 61 | 700 | 65 | 50 | 5 | 7.641 | 41.313 |
| 2 | 25 | 65 | 50 | 5 | 0.021 | 0.642 | 32 | 550 | 65 | 50 | 5 | 0.846 | 42.382 | 62 | 700 | 65 | 50 | 5 | 8.303 | 40.356 |
| 3 | 25 | 65 | 50 | 5 | 0.063 | 5.458 | 33 | 550 | 65 | 50 | 5 | 0.972 | 51.051 | 63 | 700 | 65 | 50 | 5 | 8.838 | 39.236 |
| 4 | 25 | 65 | 50 | 5 | 0.084 | 8.508 | 34 | 550 | 65 | 50 | 5 | 1.077 | 57.794 | 64 | 850 | 65 | 50 | 5 | 0.000 | 0.000 |
| 5 | 25 | 65 | 50 | 5 | 0.083 | 13.805 | 35 | 550 | 65 | 50 | 5 | 1.332 | 67.266 | 65 | 850 | 65 | 50 | 5 | 0.235 | 0.483 |
| 6 | 25 | 65 | 50 | 5 | 0.124 | 17.818 | 36 | 550 | 65 | 50 | 5 | 1.524 | 69.996 | 66 | 850 | 65 | 50 | 5 | 0.406 | 1.287 |
| 7 | 25 | 65 | 50 | 5 | 0.166 | 24.881 | 37 | 550 | 65 | 50 | 5 | 1.758 | 70.801 | 67 | 850 | 65 | 50 | 5 | 0.598 | 2.252 |
| 8 | 25 | 65 | 50 | 5 | 0.165 | 27.610 | 38 | 550 | 65 | 50 | 5 | 2.015 | 70.321 | 68 | 850 | 65 | 50 | 5 | 0.918 | 3.539 |
| 9 | 25 | 65 | 50 | 5 | 0.164 | 30.338 | 39 | 550 | 65 | 50 | 5 | 2.293 | 68.879 | 69 | 850 | 65 | 50 | 5 | 1.174 | 4.825 |
| 10 | 25 | 65 | 50 | 5 | 0.227 | 35.957 | 40 | 550 | 65 | 50 | 5 | 2.871 | 65.673 | 70 | 850 | 65 | 50 | 5 | 1.664 | 10.447 |
| 11 | 25 | 65 | 50 | 5 | 0.290 | 44.946 | 41 | 550 | 65 | 50 | 5 | 3.277 | 64.232 | 71 | 850 | 65 | 50 | 5 | 1.984 | 14.302 |
| 12 | 25 | 65 | 50 | 5 | 0.309 | 55.380 | 42 | 550 | 65 | 50 | 5 | 3.961 | 61.990 | 72 | 850 | 65 | 50 | 5 | 2.304 | 18.478 |
| 13 | 25 | 65 | 50 | 5 | 0.349 | 64.529 | 43 | 550 | 65 | 50 | 5 | 4.538 | 60.550 | 73 | 850 | 65 | 50 | 5 | 2.453 | 18.960 |
| 14 | 25 | 65 | 50 | 5 | 0.432 | 79.939 | 44 | 550 | 65 | 50 | 5 | 5.201 | 58.950 | 74 | 850 | 65 | 50 | 5 | 2.965 | 23.940 |
| 15 | 25 | 65 | 50 | 5 | 0.473 | 85.237 | 45 | 550 | 65 | 50 | 5 | 6.163 | 57.032 | 75 | 850 | 65 | 50 | 5 | 3.583 | 29.563 |
| 16 | 25 | 65 | 50 | 5 | 0.558 | 88.287 | 46 | 550 | 65 | 50 | 5 | 7.831 | 52.711 | 76 | 850 | 65 | 50 | 5 | 3.882 | 31.492 |
| 17 | 25 | 65 | 50 | 5 | 0.708 | 86.041 | 47 | 550 | 65 | 50 | 5 | 8.451 | 50.630 | 77 | 850 | 65 | 50 | 5 | 4.202 | 33.581 |
| 18 | 25 | 65 | 50 | 5 | 0.902 | 80.906 | 48 | 700 | 65 | 50 | 5 | 0.000 | 0.000 | 78 | 850 | 65 | 50 | 5 | 4.672 | 36.474 |
| 19 | 25 | 65 | 50 | 5 | 1.180 | 76.254 | 49 | 700 | 65 | 50 | 5 | 0.149 | 1.767 | 79 | 850 | 65 | 50 | 5 | 5.099 | 38.083 |
| 20 | 25 | 65 | 50 | 5 | 1.694 | 70.479 | 50 | 700 | 65 | 50 | 5 | 0.362 | 5.621 | 80 | 850 | 65 | 50 | 5 | 5.590 | 39.050 |
| 21 | 25 | 65 | 50 | 5 | 2.337 | 65.187 | 51 | 700 | 65 | 50 | 5 | 0.724 | 11.242 | 81 | 850 | 65 | 50 | 5 | 6.402 | 39.377 |
| 22 | 25 | 65 | 50 | 5 | 2.615 | 62.942 | 52 | 700 | 65 | 50 | 5 | 0.916 | 15.417 | 82 | 850 | 65 | 50 | 5 | 7.770 | 38.104 |
| 23 | 25 | 65 | 50 | 5 | 2.829 | 60.215 | 53 | 700 | 65 | 50 | 5 | 1.171 | 20.876 | 83 | 850 | 65 | 50 | 5 | 9.030 | 37.312 |
| 24 | 25 | 65 | 50 | 5 | 3.107 | 58.291 | 54 | 700 | 65 | 50 | 5 | 1.852 | 33.402 | 84 | 850 | 65 | 50 | 5 | 10.398 | 36.520 |
| 25 | 550 | 65 | 50 | 5 | 0.000 | 0.000 | 55 | 700 | 65 | 50 | 5 | 2.427 | 43.037 | 85 | 850 | 65 | 50 | 5 | 11.317 | 35.725 |
| 26 | 550 | 65 | 50 | 5 | 0.042 | 1.124 | 56 | 700 | 65 | 50 | 5 | 3.088 | 46.253 | 86 | 850 | 65 | 50 | 5 | 12.236 | 35.251 |
| 27 | 550 | 65 | 50 | 5 | 0.127 | 5.458 | 57 | 700 | 65 | 50 | 5 | 3.815 | 46.580 | 87 | 850 | 65 | 50 | 5 | 13.134 | 34.937 |
| 28 | 550 | 65 | 50 | 5 | 0.254 | 12.522 | 58 | 700 | 65 | 50 | 5 | 4.755 | 46.266 | 88 | 850 | 65 | 50 | 5 | 13.732 | 34.621 |
| 29 | 550 | 65 | 50 | 5 | 0.359 | 19.104 | 59 | 700 | 65 | 50 | 5 | 6.016 | 44.671 | 89 | 850 | 65 | 50 | 5 | 14.501 | 34.145 |
| 30 | 550 | 65 | 50 | 5 | 0.486 | 25.205 | 60 | 700 | 65 | 50 | 5 | 7.064 | 42.432 | 90 | 850 | 65 | 50 | 5 | 15.164 | 33.830 |
| 91 | 850 | 65 | 50 | 5 | 15.912 | 33.354 | 126 | 550 | 65 | 30 | 5 | 1.538 | 27.722 | 161 | 850 | 65 | 30 | 5 | 0.818 | 0.142 |
| 92 | 850 | 65 | 50 | 5 | 16.296 | 33.357 | 127 | 550 | 65 | 30 | 5 | 1.993 | 35.697 | 162 | 850 | 65 | 30 | 5 | 1.318 | 0.564 |
| 93 | 850 | 65 | 50 | 5 | 16.766 | 33.521 | 128 | 550 | 65 | 30 | 5 | 2.447 | 43.367 | 163 | 850 | 65 | 30 | 5 | 2.050 | 0.946 |
| 94 | 850 | 65 | 50 | 5 | 17.108 | 33.364 | 129 | 550 | 65 | 30 | 5 | 2.793 | 49.276 | 164 | 850 | 65 | 30 | 5 | 2.718 | 1.509 |
| 95 | 850 | 65 | 50 | 5 | 17.215 | 32.401 | 130 | 550 | 65 | 30 | 5 | 3.173 | 56.738 | 165 | 850 | 65 | 30 | 5 | 5.007 | 5.747 |
| 96 | 25 | 65 | 30 | 5 | 0.000 | 0.000 | 131 | 550 | 65 | 30 | 5 | 3.164 | 57.952 | 166 | 850 | 65 | 30 | 5 | 6.560 | 8.699 |
| 97 | 25 | 65 | 30 | 5 | 0.021 | 0.038 | 132 | 550 | 65 | 30 | 5 | 2.983 | 56.900 | 167 | 850 | 65 | 30 | 5 | 8.215 | 11.972 |

| No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) | No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) | No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) |
|------------|---------------|----------------|----------------|----------------|----------------|-----------------|------------|---------------|----------------|----------------|----------------|-----------------|------------------|------------|---------------|----------------|----------------|----------------|------------------|------------------|
| 98 | 25 | 65 | 30 | 5 | 0.059 | 3.441 | 133 | 550 | 65 | 30 | 5 | 2.695 | 54.393 | 168 | 850 | 65 | 30 | 5 | 8.519 | 12.033 |
| 99 | 25 | 65 | 30 | 5 | 0.078 | 5.827 | 134 | 550 | 65 | 30 | 5 | 2.320 | 50.752 | 169 | 850 | 65 | 30 | 5 | 10.624 | 15.568 |
| 100 | 25 | 65 | 30 | 5 | 0.073 | 11.160 | 135 | 550 | 65 | 30 | 5 | 1.528 | 42.980 | 170 | 850 | 65 | 30 | 5 | 13.042 | 19.445 |
| 101 | 25 | 65 | 30 | 5 | 0.113 | 13.831 | 136 | 550 | 65 | 30 | 5 | 1.025 | 38.327 | 171 | 850 | 65 | 30 | 5 | 13.958 | 20.530 |
| 102 | 25 | 65 | 30 | 5 | 0.149 | 19.572 | 137 | 550 | 65 | 30 | 5 | 0.190 | 30.676 | 172 | 850 | 65 | 30 | 5 | 14.946 | 21.715 |
| 103 | 25 | 65 | 30 | 5 | 0.147 | 22.320 | 138 | 550 | 65 | 30 | 5 | 0.483 | 24.673 | 173 | 850 | 65 | 30 | 5 | 16.341 | 23.282 |
| 104 | 25 | 65 | 30 | 5 | 0.145 | 25.067 | 139 | 550 | 65 | 30 | 5 | 1.253 | 17.834 | 174 | 850 | 65 | 30 | 5 | 17.283 | 23.685 |
| 105 | 25 | 65 | 30 | 5 | 0.204 | 28.670 | 140 | 550 | 65 | 30 | 5 | 2.344 | 8.311 | 175 | 850 | 65 | 30 | 5 | 18.083 | 23.265 |
| 106 | 25 | 65 | 30 | 5 | 0.260 | 35.666 | 141 | 550 | 65 | 30 | 5 | 4.300 | 9.192 | 176 | 850 | 65 | 30 | 5 | 19.000 | 21.300 |
| 107 | 25 | 65 | 30 | 5 | 0.272 | 45.486 | 142 | 550 | 65 | 30 | 5 | 5.060 | 16.176 | 177 | 850 | 65 | 30 | 5 | 19.961 | 16.165 |
| 108 | 25 | 65 | 30 | 5 | 0.307 | 53.328 | 143 | 700 | 65 | 30 | 5 | 0.000 | 0.000 | 178 | 850 | 65 | 30 | 5 | 20.968 | 11.812 |
| 109 | 25 | 65 | 30 | 5 | 0.379 | 66.104 | 144 | 700 | 65 | 30 | 5 | 0.384 | 1.869 | 179 | 850 | 65 | 30 | 5 | 22.082 | 7.158 |
| 110 | 25 | 65 | 30 | 5 | 0.417 | 70.068 | 145 | 700 | 65 | 30 | 5 | 1.108 | 5.870 | 180 | 850 | 65 | 30 | 5 | 22.747 | 3.768 |
| 111 | 25 | 65 | 30 | 5 | 0.500 | 70.400 | 146 | 700 | 65 | 30 | 5 | 2.217 | 11.739 | 181 | 850 | 65 | 30 | 5 | 23.514 | 0.699 |
| 112 | 25 | 65 | 30 | 5 | 0.652 | 63.344 | 147 | 700 | 65 | 30 | 5 | 2.963 | 16.046 | 182 | 850 | 65 | 30 | 5 | 24.311 | 2.149 |
| 113 | 25 | 65 | 30 | 5 | 0.848 | 52.011 | 148 | 700 | 65 | 30 | 5 | 3.943 | 21.680 | 183 | 850 | 65 | 30 | 5 | 24.808 | 4.155 |
| 114 | 25 | 65 | 30 | 5 | 1.130 | 38.423 | 149 | 700 | 65 | 30 | 5 | 6.287 | 34.674 | 184 | 850 | 65 | 30 | 5 | 25.426 | 6.803 |
| 115 | 25 25 | 65 (F | 30 20 | 5 5 | 1.648 | 16.172 9.703 | 150 | 700 700 | 65 (F | 30 20 | 5 5 | 8.141 | 44.704 | 185 | 850 850 | 65 (F | 30 | 5 5 | 25.987 26.583 | 8.989 |
| 116 117 | 25 25 | 65 65 | 30 30 | 5 5 | 2.294 2.573 | 9.703 2.867 | 151 152 | 700 | 65 65 | 30 30 | 5 5 | 9.230 10.000 | 48.374 49.200 | 186 187 | 850 850 | 65 65 | 30 30 | 5 5 | 26.583 | 11.577 12.660 |
| 117 | 25 25 | 65 | 30 30 | 5 | 2.373 | 0.461 | 152 | 700 | 65 | 30 30 | 5 | 10.000 | 49.200 | 187 | 850 | 65 | 30 30 | 5 | 20.908 | 13.822 |
| 118 | 25 25 | 65 | 30 30 | 5 | 3.069 | 0.401 | 155 | 700 | 65 | 30 30 | 5 | 10.899 | 49.332 | 188 | 850 | 65 | 30 30 | 5 | 27.491 | 13.822 |
| 119 | 550 | 65 | 30 30 | 5 | 0.000 | 0.415 | 154 | 700 | 65 | 30 | 5 | 12.698 | 47.284 | 190 | 850 | 65 | 30 | 5 | 27.582 | 14.940 |
| 120 | 550 | 65 | 30 | 5 | 0.033 | 0.788 | 155 | 700 | 65 | 30 | 5 | 13.127 | 46.562 | 191 | 25 | 75 | 30 | 6 | 0.000 | 0.000 |
| 121 | 550 | 65 | 30 | 5 | 0.239 | 4.454 | 150 | 700 | 65 | 30 | 5 | 13.662 | 46.059 | 192 | 25 | 75 | 30 | 6 | 0.019 | 0.040 |
| 123 | 550 | 65 | 30 | 5 | 0.585 | 10.516 | 158 | 700 | 65 | 30 | 5 | 14.048 | 45.307 | 193 | 25 | 75 | 30 | 6 | 0.054 | 3.636 |
| 124 | 550 | 65 | 30 | 5 | 0.920 | 16.265 | 159 | 850 | 65 | 30 | 5 | 0.000 | 0.000 | 194 | 25 | 75 | 30 | 6 | 0.071 | 6.158 |
| 125 | 550 | 65 | 30 | 5 | 1.202 | 21.362 | 160 | 850 | 65 | 30 | 5 | 0.390 | 0.180 | 195 | 25 | 75 | 30 | 6 | 0.067 | 11.794 |
| 196 | 25 | 75 | 30 | 6 | 0.103 | 14.616 | 231 | 550 | 75 | 30 | 6 | 0.937 | 40.504 | 266 | 850 | 75 | 30 | 6 | 12.757 | 21.696 |
| 197 | 25 | 75 | 30 | 6 | 0.136 | 20.684 | 232 | 550 | 75 | 30 | 6 | 0.174 | 32.419 | 267 | 850 | 75 | 30 | 6 | 13.661 | 22.948 |
| 198 | 25 | 75 | 30 | 6 | 0.134 | 23.588 | 233 | 550 | 75 | 30 | 6 | 0.442 | 26.074 | 268 | 850 | 75 | 30 | 6 | 14.936 | 24.605 |
| 199 | 25 | 75 | 30 | 6 | 0.132 | 26.491 | 234 | 550 | 75 | 30 | 6 | 1.145 | 18.847 | 269 | 850 | 75 | 30 | 6 | 15.796 | 25.031 |
| 200 | 25 | 75 | 30 | 6 | 0.186 | 30.298 | 235 | 550 | 75 | 30 | 6 | 2.142 | 8.783 | 270 | 850 | 75 | 30 | 6 | 16.528 | 24.587 |
| 201 | 25 | 75 | 30 | 6 | 0.238 | 37.691 | 236 | 550 | 75 | 30 | 6 | 3.931 | 9.715 | 271 | 850 | 75 | 30 | 6 | 17.366 | 22.510 |
| 202 | 25 | 75 | 30 | 6 | 0.249 | 48.069 | 237 | 550 | 75 | 30 | 6 | 4.625 | 17.095 | 272 | 850 | 75 | 30 | 6 | 18.244 | 17.083 |
| 203 | 25 | 75 | 30 | 6 | 0.281 | 56.357 | 238 | 700 | 75 | 30 | 6 | 0.000 | 0.000 | 273 | 850 | 75 | 30 | 6 | 19.165 | 12.483 |
| 204 | 25 | 75 | 30 | 6 | 0.346 | 69.859 | 239 | 700 | 75 | 30 | 6 | 0.351 | 1.976 | 274 | 850 | 75 | 30 | 6 | 20.183 | 7.565 |
| 205 | 25 | 75 | 30 | 6 | 0.381 | 74.048 | 240 | 700 | 75 | 30 | 6 | 1.013 | 6.203 | 275 | 850 | 75 | 30 | 6 | 20.791 | 3.982 |
| 206 | 25 | 75 | 30 | 6 | 0.457 | 74.399 | 241 | 700 | 75 | 30 | 6 | 2.026 | 12.406 | 276 | 850 | 75 | 30 | 6 | 21.492 | 0.739 |

| No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) | No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) | No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) |
|-----|---------------|----------------|----------------|----------------|--------------|--------------|-----|---------------|----------------|----------------|----------------|--------------|--------------|-----|---------------|----------------|----------------|----------------|--------------|--------------|
| 207 | 25 | 75 | 30 | 6 | 0.595 | 66.942 | 242 | 700 | 75 | 30 | 6 | 2.708 | 16.957 | 277 | 850 | 75 | 30 | 6 | 22.220 | 2.271 |
| 208 | 25 | 75 | 30 | 6 | 0.775 | 54.965 | 243 | 700 | 75 | 30 | 6 | 3.604 | 22.912 | 278 | 850 | 75 | 30 | 6 | 22.675 | 4.391 |
| 209 | 25 | 75 | 30 | 6 | 1.033 | 40.605 | 244 | 700 | 75 | 30 | 6 | 5.746 | 36.643 | 279 | 850 | 75 | 30 | 6 | 23.239 | 7.189 |
| 210 | 25 | 75 | 30 | 6 | 1.506 | 17.090 | 245 | 700 | 75 | 30 | 6 | 7.441 | 47.243 | 280 | 850 | 75 | 30 | 6 | 23.752 | 9.499 |
| 211 | 25 | 75 | 30 | 6 | 2.096 | 10.254 | 246 | 700 | 75 | 30 | 6 | 8.436 | 51.122 | 281 | 850 | 75 | 30 | 6 | 24.297 | 12.234 |
| 212 | 25 | 75 | 30 | 6 | 2.352 | 3.029 | 247 | 700 | 75 | 30 | 6 | 9.140 | 51.995 | 282 | 850 | 75 | 30 | 6 | 24.649 | 13.379 |
| 213 | 25 | 75 | 30 | 6 | 2.550 | 0.487 | 248 | 700 | 75 | 30 | 6 | 9.961 | 52.346 | 283 | 850 | 75 | 30 | 6 | 25.127 | 14.608 |
| 214 | 25 | 75 | 30 | 6 | 2.805 | 0.436 | 249 | 700 | 75 | 30 | 6 | 10.920 | 51.576 | 284 | 850 | 75 | 30 | 6 | 25.393 | 15.795 |
| 215 | 550 | 75 | 30 | 6 | 0.000 | 0.000 | 250 | 700 | 75 | 30 | 6 | 11.606 | 49.970 | 285 | 850 | 75 | 30 | 6 | 25.210 | 17.131 |
| 216 | 550 | 75 | 30 | 6 | 0.030 | 0.833 | 251 | 700 | 75 | 30 | 6 | 11.998 | 49.206 | 286 | 25 | 75 | 50 | 6 | 0.000 | 0.000 |
| 217 | 550 | 75 | 30 | 6 | 0.218 | 4.707 | 252 | 700 | 75 | 30 | 6 | 12.487 | 48.675 | 287 | 25 | 75 | 50 | 6 | 0.017 | 0.708 |
| 218 | 550 | 75 | 30 | 6 | 0.535 | 11.114 | 253 | 700 | 75 | 30 | 6 | 12.840 | 47.880 | 288 | 25 | 75 | 50 | 6 | 0.051 | 6.015 |
| 219 | 550 | 75 | 30 | 6 | 0.841 | 17.189 | 254 | 850 | 75 | 30 | 6 | 0.000 | 0.000 | 289 | 25 | 75 | 50 | 6 | 0.068 | 9.376 |
| 220 | 550 | 75 | 30 | 6 | 1.099 | 22.575 | 255 | 850 | 75 | 30 | 6 | 0.356 | 0.190 | 290 | 25 | 75 | 50 | 6 | 0.067 | 15.213 |
| 221 | 550 | 75 | 30 | 6 | 1.406 | 29.296 | 256 | 850 | 75 | 30 | 6 | 0.747 | 0.150 | 291 | 25 | 75 | 50 | 6 | 0.101 | 19.635 |
| 222 | 550 | 75 | 30 | 6 | 1.821 | 37.725 | 257 | 850 | 75 | 30 | 6 | 1.205 | 0.596 | 292 | 25 | 75 | 50 | 6 | 0.134 | 27.419 |
| 223 | 550 | 75 | 30 | 6 | 2.237 | 45.830 | 258 | 850 | 75 | 30 | 6 | 1.874 | 1.000 | 293 | 25 | 75 | 50 | 6 | 0.134 | 30.426 |
| 224 | 550 | 75 | 30 | 6 | 2.553 | 52.075 | 259 | 850 | 75 | 30 | 6 | 2.484 | 1.595 | 294 | 25 | 75 | 50 | 6 | 0.134 | 33.433 |
| 225 | 550 | 75 | 30 | 6 | 2.900 | 59.960 | 260 | 850 | 75 | 30 | 6 | 4.576 | 6.073 | 295 | 25 | 75 | 50 | 6 | 0.185 | 39.625 |
| 226 | 550 | 75 | 30 | 6 | 2.892 | 61.244 | 261 | 850 | 75 | 30 | 6 | 5.996 | 9.193 | 296 | 25 | 75 | 50 | 6 | 0.235 | 49.531 |
| 227 | 550 | 75 | 30 | 6 | 2.727 | 60.132 | 262 | 850 | 75 | 30 | 6 | 7.509 | 12.652 | 297 | 25 | 75 | 50 | 6 | 0.251 | 61.028 |
| 228 | 550 | 75 | 30 | 6 | 2.463 | 57.482 | 263 | 850 | 75 | 30 | 6 | 7.787 | 12.717 | 298 | 25 | 75 | 50 | 6 | 0.284 | 71.111 |
| 229 | 550 | 75 | 30 | 6 | 2.120 | 53.635 | 264 | 850 | 75 | 30 | 6 | 9.711 | 16.452 | 299 | 25 | 75 | 50 | 6 | 0.350 | 88.093 |
| 230 | 550 | 75 | 30 | 6 | 1.396 | 45.421 | 265 | 850 | 75 | 30 | 6 | 11.920 | 20.549 | 300 | 25 | 75 | 50 | 6 | 0.384 | 93.931 |
| 301 | 25 | 75 | 50 | 6 | 0.453 | 97.292 | 336 | 700 | 75 | 50 | 6 | 0.588 | 12.388 | 371 | 850 | 75 | 50 | 6 | 9.936 | 38.846 |
| 302 | 25 | 75 | 50 | 6 | 0.575 | 94.817 | 337 | 700 | 75 | 50 | 6 | 0.743 | 16.989 | 372 | 850 | 75 | 50 | 6 | 10.664 | 38.500 |
| 303 | 25 | 75 | 50 | 6 | 0.732 | 89.159 | 338 | 700 | 75 | 50 | 6 | 0.951 | 23.006 | 373 | 850 | 75 | 50 | 6 | 11.150 | 38.152 |
| 304 | 25 | 75 | 50 | 6 | 0.958 | 84.031 | 339 | 700 | 75 | 50 | 6 | 1.504 | 36.809 | 374 | 850 | 75 | 50 | 6 | 11.775 | 37.628 |
| 305 | 25 | 75 | 50 | 6 | 1.376 | 77.668 | 340 | 700 | 75 | 50 | 6 | 1.970 | 47.427 | 375 | 850 | 75 | 50 | 6 | 12.313 | 37.280 |
| 306 | 25 | 75 | 50 | 6 | 1.897 | 71.836 | 341 | 700 | 75 | 50 | 6 | 2.508 | 50.970 | 376 | 850 | 75 | 50 | 6 | 12.920 | 36.756 |
| 307 | 25 | 75 | 50 | 6 | 2.123 | 69.362 | 342 | 700 | 75 | 50 | 6 | 3.098 | 51.331 | 377 | 850 | 75 | 50 | 6 | 13.233 | 36.760 |
| 308 | 25 | 75 | 50 | 6 | 2.297 | 66.357 | 343 | 700 | 75 | 50 | 6 | 3.861 | 50.985 | 378 | 850 | 75 | 50 | 6 | 13.614 | 36.941 |
| 309 | 25 | 75 | 50 | 6 | 2.523 | 64.237 | 344 | 700 | 75 | 50 | 6 | 4.885 | 49.228 | 379 | 850 | 75 | 50 | 6 | 13.892 | 36.767 |
| 310 | 550 | 75 | 50 | 6 | 0.000 | 0.000 | 345 | 700 | 75 | 50 | 6 | 5.736 | 46.760 | 380 | 850 | 75 | 50 | 6 | 13.979 | 35.706 |
| 311 | 550 | 75 | 50 | 6 | 0.035 | 1.239 | 346 | 700 | 75 | 50 | 6 | 6.204 | 45.527 | 381 | 25 | 100 | 30 | 7 | 0.000 | 0.000 |
| 312 | 550 | 75 | 50 | 6 | 0.103 | 6.015 | 347 | 700 | 75 | 50 | 6 | 6.742 | 44.472 | 382 | 25 | 100 | 30 | 7 | 0.171 | 4.947 |
| 313 | 550 | 75 | 50 | 6 | 0.206 | 13.799 | 348 | 700 | 75 | 50 | 6 | 7.176 | 43.238 | 383 | 25 | 100 | 30 | 7 | 0.512 | 11.484 |
| 314 | 550 | 75 | 50 | 6 | 0.292 | 21.053 | 349 | 850 | 75 | 50 | 6 | 0.000 | 0.000 | 384 | 25 | 100 | 30 | 7 | 0.938 | 19.611 |
| 315 | 550 | 75 | 50 | 6 | 0.395 | 27.775 | 350 | 850 | 75 | 50 | 6 | 0.191 | 0.533 | 385 | 25 | 100 | 30 | 7 | 1.279 | 36.749 |
| 316 | 550 | 75 | 50 | 6 | 0.549 | 36.444 | 351 | 850 | 75 | 50 | 6 | 0.329 | 1.419 | 386 | 25 | 100 | 30 | 7 | 1.791 | 47.703 |

| No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) | No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) | No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) |
|-----|---------------|----------------|----------------|----------------|--------------|--------------|-----|---------------|----------------|----------------|----------------|--------------|--------------|-----|---------------|----------------|----------------|----------------|--------------|--------------|
| 317 | 550 | 75 | 50 | 6 | 0.687 | 46.705 | 352 | 850 | 75 | 50 | 6 | 0.485 | 2.482 | 387 | 25 | 100 | 30 | 7 | 2.217 | 55.654 |
| 318 | 550 | 75 | 50 | 6 | 0.789 | 56.258 | 353 | 850 | 75 | 50 | 6 | 0.745 | 3.900 | 388 | 25 | 100 | 30 | 7 | 2.900 | 69.081 |
| 319 | 550 | 75 | 50 | 6 | 0.875 | 63.689 | 354 | 850 | 75 | 50 | 6 | 0.953 | 5.317 | 389 | 25 | 100 | 30 | 7 | 3.326 | 75.972 |
| 320 | 550 | 75 | 50 | 6 | 1.081 | 74.127 | 355 | 850 | 75 | 50 | 6 | 1.352 | 11.512 | 390 | 25 | 100 | 30 | 7 | 3.753 | 82.156 |
| 321 | 550 | 75 | 50 | 6 | 1.237 | 77.136 | 356 | 850 | 75 | 50 | 6 | 1.611 | 15.760 | 391 | 25 | 100 | 30 | 7 | 4.606 | 86.042 |
| 322 | 550 | 75 | 50 | 6 | 1.428 | 78.022 | 357 | 850 | 75 | 50 | 6 | 1.871 | 20.362 | 392 | 25 | 100 | 30 | 7 | 5.203 | 86.749 |
| 323 | 550 | 75 | 50 | 6 | 1.636 | 77.494 | 358 | 850 | 75 | 50 | 6 | 1.992 | 20.894 | 393 | 25 | 100 | 30 | 7 | 5.885 | 83.569 |
| 324 | 550 | 75 | 50 | 6 | 1.862 | 75.904 | 359 | 850 | 75 | 50 | 6 | 2.408 | 26.382 | 394 | 25 | 100 | 30 | 7 | 7.249 | 72.792 |
| 325 | 550 | 75 | 50 | 6 | 2.331 | 72.372 | 360 | 850 | 75 | 50 | 6 | 2.910 | 32.579 | 395 | 25 | 100 | 30 | 7 | 7.164 | 66.431 |
| 326 | 550 | 75 | 50 | 6 | 2.661 | 70.783 | 361 | 850 | 75 | 50 | 6 | 3.152 | 34.704 | 396 | 25 | 100 | 30 | 7 | 7.079 | 57.244 |
| 327 | 550 | 75 | 50 | 6 | 3.216 | 68.313 | 362 | 850 | 75 | 50 | 6 | 3.412 | 37.006 | 397 | 25 | 100 | 30 | 7 | 7.164 | 56.007 |
| 328 | 550 | 75 | 50 | 6 | 3.685 | 66.726 | 363 | 850 | 75 | 50 | 6 | 3.793 | 40.194 | 398 | 550 | 100 | 30 | 7 | 0.000 | 0.000 |
| 329 | 550 | 75 | 50 | 6 | 4.223 | 64.963 | 364 | 850 | 75 | 50 | 6 | 4.140 | 41.967 | 399 | 550 | 100 | 30 | 7 | 0.171 | 1.060 |
| 330 | 550 | 75 | 50 | 6 | 5.004 | 62.849 | 365 | 850 | 75 | 50 | 6 | 4.539 | 43.033 | 400 | 550 | 100 | 30 | 7 | 0.597 | 5.830 |
| 331 | 550 | 75 | 50 | 6 | 6.358 | 58.088 | 366 | 850 | 75 | 50 | 6 | 5.198 | 43.394 | 401 | 550 | 100 | 30 | 7 | 1.023 | 13.428 |
| 332 | 550 | 75 | 50 | 6 | 6.862 | 55.794 | 367 | 850 | 75 | 50 | 6 | 6.309 | 41.991 | 402 | 550 | 100 | 30 | 7 | 1.365 | 20.318 |
| 333 | 700 | 75 | 50 | 6 | 0.000 | 0.000 | 368 | 850 | 75 | 50 | 6 | 7.333 | 41.117 | 403 | 550 | 100 | 30 | 7 | 2.047 | 29.859 |
| 334 | 700 | 75 | 50 | 6 | 0.121 | 1.947 | 369 | 850 | 75 | 50 | 6 | 8.443 | 40.245 | 404 | 550 | 100 | 30 | 7 | 2.388 | 37.633 |
| 335 | 700 | 75 | 50 | 6 | 0.294 | 6.194 | 370 | 850 | 75 | 50 | 6 | 9.190 | 39.369 | 405 | 550 | 100 | 30 | 7 | 3.241 | 49.117 |
| 406 | 550 | 100 | 30 | 7 | 4.606 | 58.834 | 441 | 700 | 100 | 30 | 7 | 16.461 | 34.452 | 476 | 850 | 100 | 30 | 7 | 63.642 | 30.052 |
| 407 | 550 | 100 | 30 | 7 | 6.482 | 67.138 | 442 | 700 | 100 | 30 | 7 | 17.058 | 32.862 | 477 | 850 | 100 | 30 | 7 | 64.665 | 29.524 |
| 408 | 550 | 100 | 30 | 7 | 7.761 | 70.848 | 443 | 700 | 100 | 30 | 7 | 18.081 | 30.035 | 478 | 850 | 100 | 30 | 7 | 66.198 | 29.704 |
| 409 | 550 | 100 | 30 | 7 | 8.102 | 71.378 | 444 | 850 | 100 | 30 | 7 | 0.000 | 0.000 | 479 | 850 | 100 | 30 | 7 | 66.880 | 29.175 |
| 410 | 550 | 100 | 30 | 7 | 8.870 | 69.965 | 445 | 850 | 100 | 30 | 7 | 0.511 | 0.886 | 480 | 850 | 100 | 30 | 7 | 67.732 | 29.530 |
| 411 | 550 | 100 | 30 | 7 | 9.126 | 63.428 | 446 | 850 | 100 | 30 | 7 | 1.874 | 3.544 | 481 | 850 | 100 | 30 | 7 | 70.288 | 29.005 |
| 412 | 550 | 100 | 30 | 7 | 9.126 | 59.187 | 447 | 850 | 100 | 30 | 7 | 3.408 | 6.910 | 482 | 850 | 100 | 30 | 7 | 73.695 | 27.774 |
| 413 | 550 | 100 | 30 | 7 | 9.126 | 53.534 | 448 | 850 | 100 | 30 | 7 | 4.601 | 8.506 | 483 | 25 | 100 | 50 | 7 | 0.000 | 0.000 |
| 414 | 550 | 100 | 30 | 7 | 9.126 | 48.410 | 449 | 850 | 100 | 30 | 7 | 5.708 | 9.570 | 484 | 25 | 100 | 50 | 7 | 0.012 | 6.257 |
| 415 | 550 | 100 | 30 | 7 | 9.126 | 45.936 | 450 | 850 | 100 | 30 | 7 | 6.986 | 11.874 | 485 | 25 | 100 | 50 | 7 | 0.088 | 15.414 |
| 416 | 550 | 100 | 30 | 7 | 9.126 | 43.110 | 451 | 850 | 100 | 30 | 7 | 8.775 | 14.887 | 486 | 25 | 100 | 50 | 7 | 0.214 | 26.816 |
| 417 | 550 | 100 | 30 | 7 | 9.126 | 39.576 | 452 | 850 | 100 | 30 | 7 | 10.650 | 17.900 | 487 | 25 | 100 | 50 | 7 | 0.077 | 46.573 |
| 418 | 550 | 100 | 30 | 7 | 9.126 | 36.749 | 453 | 850 | 100 | 30 | 7 | 12.439 | 20.736 | 488 | 25 | 100 | 50 | 7 | 0.030 | 61.457 |
| 419 | 700 | 100 | 30 | 7 | 0.000 | 0.000 | 454 | 850 | 100 | 30 | 7 | 14.228 | 22.863 | 489 | 25 | 100 | 50 | 7 | 0.163 | 72.682 |
| 420 | 700 | 100 | 30 | 7 | 0.171 | 1.237 | 455 | 850 | 100 | 30 | 7 | 15.676 | 24.813 | 490 | 25 | 100 | 50 | 7 | 0.349 | 91.349 |
| 421 | 700 | 100 | 30 | 7 | 0.768 | 5.124 | 456 | 850 | 100 | 30 | 7 | 17.039 | 25.347 | 491 | 25 | 100 | 50 | 7 | 0.522 | 101.514 |
| 422 | 700 | 100 | 30 | 7 | 1.365 | 7.420 | 457 | 850 | 100 | 30 | 7 | 18.062 | 27.297 | 492 | 25 | 100 | 50 | 7 | 0.720 | 110.973 |
| 423 | 700 | 100 | 30 | 7 | 2.303 | 15.724 | 458 | 850 | 100 | 30 | 7 | 20.021 | 29.602 | 493 | 25 | 100 | 50 | 7 | 1.429 | 121.409 |
| 424 | 700 | 100 | 30 | 7 | 3.156 | 24.205 | 459 | 850 | 100 | 30 | 7 | 22.066 | 30.845 | 494 | 25 | 100 | 50 | 7 | 2.000 | 126.700 |
| 425 | 700 | 100 | 30 | 7 | 3.923 | 32.156 | 460 | 850 | 100 | 30 | 7 | 23.855 | 32.088 | 495 | 25 | 100 | 50 | 7 | 2.800 | 128.759 |
| 426 | 700 | 100 | 30 | 7 | 4.947 | 40.106 | 461 | 850 | 100 | 30 | 7 | 27.348 | 34.220 | 496 | 25 | 100 | 50 | 7 | 4.562 | 128.461 |

| 427 700 100 30 7 5.714 45.838 462 850 100 30 7 27.74 33.868 497 25 100 50 428 700 100 30 7 6.482 50.000 463 850 100 30 7 33.568 463.858 499 25 100 50 429 700 100 30 7 6.452 50.0071 463 850 100 30 7 35.64 35.34 401 550 100 50 431 700 100 30 7 12.576 62.544 466 850 100 30 7 41.576 37.240 50 100 50 433 700 100 30 7 14.528 63.530 469 850 100 30 7 41.576 37.260 50 100 50 433 700 100 | No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) | No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) | No. | Temp. (°C) | Height (mm) | Length (mm) | Thick. (mm) | Slip (mm) | Load (kN) |
|--|-----|---------------|----------------|----------------|----------------|--------------|------------------|-----|---------------|----------------|----------------|----------------|--------------|--------------|-----|---------------|----------------|----------------|----------------|------------------|------------------|
| 429 700 100 30 7 7.676 55.654 464 850 100 30 7 34.420 35.474 499 25 100 50 430 700 100 30 7 85.55 60.071 465 850 100 30 7 35.612 36.716 500 550 100 50 431 700 100 30 7 16.776 37.848 501 550 100 50 433 700 100 30 7 13.646 56.360 469 850 100 30 7 46.603 39.041 504 550 100 50 435 700 100 30 7 14.328 50.333 471 850 100 30 7 53.419 39.056 557 50 100 50 436 700 100 30 7 53.441 39.405 506 | 427 | 700 | 100 | 30 | 7 | 5.714 | 45.583 | 462 | 850 | 100 | 30 | 7 | 27.774 | 33.867 | 497 | 25 | 100 | 50 | 7 | 4.712 | 121.445 |
| 430 700 100 30 7 8,955 60,071 465 850 100 30 7 35,612 36,716 500 550 100 50 431 700 100 30 7 10,576 62,544 466 850 100 30 7 36,976 35,834 501 500 50 433 700 100 30 7 12,623 61,307 468 850 100 30 7 43,280 37,972 503 550 100 50 434 700 100 30 7 13,464 56,360 469 850 100 30 7 43,689 505 550 100 50 435 700 100 30 7 15,437 45,583 472 850 100 30 7 51,148 39,405 506 550 100 50 437 700 100 | 428 | 700 | 100 | 30 | | 6.482 | 50.000 | 463 | 850 | 100 | 30 | 7 | 33.568 | 36.358 | 498 | 25 | 100 | 50 | 7 | 4.966 | 111.603 |
| 431 700 100 30 7 10.576 62.544 466 850 100 30 7 36.976 35.834 501 550 100 50 432 700 100 30 7 12.23 61.307 468 850 100 30 7 41.576 37.26 502 550 100 50 433 700 100 30 7 13.646 56.360 469 850 100 30 7 47.199 38.89 505 550 100 50 436 700 100 30 7 15.437 45.83 472 850 100 30 7 53.419 39.405 506 550 100 50 433 700 100 30 7 15.437 45.63 474 850 100 30 7 55.48 39.416 508 550 100 50 433 700 | 429 | 700 | 100 | 30 | | | 55.654 | 464 | 850 | 100 | 30 | 7 | 34.420 | 35.474 | 499 | | 100 | 50 | 7 | 5.097 | 111.021 |
| 432 700 100 30 7 12.111 63.251 467 850 100 30 7 41.576 37.260 502 550 100 50 433 700 100 30 7 12.623 61.307 468 850 100 30 7 44.280 37.972 503 550 100 50 434 700 100 30 7 14.283 50.353 471 850 100 30 7 47.199 38.689 505 550 100 50 437 700 100 30 7 15.437 45.53 472 850 100 30 7 53.419 39.416 508 550 100 50 439 700 100 30 7 15.643 47.633 475 850 100 30 7 58.96 37.830 509 550 100 50 410 | 430 | 700 | | | | | | 465 | | | | - | | | 500 | | | | 7 | 0.000 | 0.000 |
| 433 700 100 30 7 12,623 61,307 468 850 100 30 7 43,280 37,972 503 550 100 50 434 700 100 30 7 13,646 56,360 469 850 100 30 7 44,603 39,041 504 550 100 50 436 700 100 30 7 14,328 50,353 471 850 100 30 7 51,118 39,405 506 550 100 50 437 700 100 30 7 15,437 45,583 472 850 100 30 7 53,419 39,056 507 550 100 50 440 700 100 30 7 15,467 105,700 536 700 100 50 7 11,320 92,359 561 850 100 50 511 | | | | | | | | | | | | - | | | | | | | 7 | 0.131 | 1.783 |
| 434 700 100 30 7 13.646 56.360 469 850 100 30 7 46.603 39.041 504 550 100 50 435 700 100 30 7 13.902 54.240 470 850 100 30 7 47.199 38.689 505 550 100 50 437 700 100 30 7 15.437 45.883 472 850 100 30 7 53.419 39.056 507 550 100 50 433 700 100 30 7 15.678 40.636 474 850 100 30 7 55.84 39.416 508 550 100 50 440 700 100 30 7 15.864 37.633 475 850 100 30 7 11.320 92.359 561 850 100 50 511 | | | | | | | | | | | | | | | | | | | 7 | 0.382 | 8.359 |
| 435 700 100 30 7 13.902 54.240 470 850 100 30 7 47.199 38.689 505 550 100 50 436 700 100 30 7 14.328 50.353 471 850 100 30 7 51.118 39.405 506 550 100 50 437 700 100 30 7 15.437 47.858 472 850 100 30 7 55.804 39.416 508 550 100 50 439 700 100 30 7 15.784 40.636 474 850 100 30 7 51.18 508 509 550 100 50 511 550 100 50 7 54.67 105.700 536 700 100 50 7 11.63 99.914 56 850 100 50 511 550 | 433 | | | | | | | | | | | | | | | | | | 7 | 0.528 | 17.763 |
| 436 700 100 30 7 14.328 50.353 471 850 100 30 7 51.118 39.405 506 550 100 50 437 700 100 30 7 15.437 45.583 472 850 100 30 7 53.419 39.056 507 550 100 50 439 700 100 30 7 15.778 40.636 474 850 100 30 7 58.956 37.830 509 550 100 50 440 700 100 50 7 54.67 105.700 536 700 100 50 7 61.880 100 50 51 100 50 7 61.661 86.99 50 100 50 512 550 100 50 7 6.287 100.30 7 13.208 88.152 563 850 100 50 | | | | | | | | | | | | | | | | | | | 7 | 0.615 | 26.099 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | | | | | | | | | | | | | | 7 | 0.945 | 38.529 |
| 438 700 100 30 7 15.693 43.463 473 850 100 30 7 55.804 39.416 508 550 100 50 440 700 100 30 7 15.778 40.636 474 850 100 30 7 58.956 37.830 509 550 100 50 440 700 100 50 7 15.864 37.633 475 850 100 30 7 61.086 36.949 510 550 100 50 512 550 100 50 7 61.287 107.538 537 700 100 50 7 11.633 90.91 62 850 100 50 511 550 100 50 7 62.850 100 50 51 550 100 50 7 13.556 86.307 564 850 100 50 516 550 | | | | | | | | | | | | - | | | | | | | 7 | 0.999 | 47.748 |
| 439 700 100 30 7 15.778 40.636 474 850 100 30 7 58.956 37.830 509 550 100 50 440 700 100 30 7 58.956 37.830 509 550 100 50 511 550 100 50 7 5.467 105.700 536 700 100 50 7 11.320 92.359 561 850 100 50 513 550 100 50 7 6.784 102.085 538 700 100 50 7 13.556 86.307 564 850 100 50 513 550 100 50 7 7.439 87.067 541 700 100 50 7 13.856 86.307 564 850 100 50 516 550 100 50 7 7.439 87.067 541 | | | | | | | | | | | | - | | | | | | | 7 | 1.428 | 62.845 |
| 44070010030715.86437.63347585010030761.08636.949510550100505115501005075.467105.70053670010050711.32092.359561850100505125501005076.287107.53853770010050711.66390.914562850100505135501005076.784102.08553870010050713.55686.307564850100505145501005077.14992.19154070010050713.89984.862565850100505155501005077.33987.06754170010050714.31079.481567850100505165501005077.43084.59454270010050714.31079.481567850100505185501005077.76975.40654570010050715.03877.876568850100505205501005077.76975.40654570010050716.84177.734570850< | | | | | | | | | | | | - | | | | | | | 7 | 2.434 | 78.343 |
| 511 550 100 50 7 5.467 105.700 536 700 100 50 7 11.360 92.359 561 850 100 50 512 550 100 50 7 6.287 107.538 537 700 100 50 7 11.363 90.914 562 850 100 50 513 550 100 50 7 6.784 102.085 538 700 100 50 7 11.325 563 850 100 50 514 550 100 50 7 6.941 97.845 539 700 100 50 7 13.356 86.307 564 850 100 50 516 550 100 50 7 7.430 84.594 542 700 100 50 7 14.101 82.260 566 850 100 50 516 550 < | | | | | | | | | | | | | | | | | | | 7 | 4.003 | 94.595 |
| 512 550 100 50 7 6.287 107.538 537 700 100 50 7 11.663 90.914 562 850 100 50 513 550 100 50 7 6.784 102.085 538 700 100 50 7 12.250 88.152 563 850 100 50 513 550 100 50 7 6.941 97.845 539 700 100 50 7 13.556 86.307 564 850 100 50 516 550 100 50 7 7.149 92.191 540 700 100 50 7 14.310 79.481 567 850 100 50 516 550 100 50 7 7.430 84.594 542 700 100 50 7 14.310 79.481 567 850 100 50 518 550 100 50 7 7.534 81.767 543 700 100 | 440 | | 100 | 30 | | | | 475 | | 100 | | | 61.086 | | 510 | 550 | 100 | 50 | 7 | 5.146 | 103.725 |
| 5135501005076.784102.08553870010050712.25088.152563850100505145501005076.94197.84553970010050713.55686.307564850100505155501005077.14992.19154070010050713.89984.862565850100505165501005077.33987.06754170010050714.10182.260566850100505185501005077.43084.57454270010050714.31079.481567850100505185501005077.65481.76754370010050715.70177.876568850100505195501005077.76975.40654570010050716.84177.734570850100505217001005070.30110050716.84177.734570850100505227001005070.5667.14954885010050716.154.17857385010050523 <t< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>7</th><th>8.301</th><th>38.313</th></t<> | | | | | | | | | | | | | | | | | | | 7 | 8.301 | 38.313 |
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