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Experimental Investigation of Phase Equilibria in the Co-Re-Ta Ternary System

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Received: 20 October 2018; Accepted: 31 October 2018; Published: 6 November 2018



Abstract: In this study, the isothermal sections of the Co-Re-Ta ternary system at 1100, 1200, and 1300 °C have been experimentally investigated by means of electron probe microanalysis and X-ray diffraction. The results indicated the following: (1) The solid solubilities of the λ_3 , (ϵ Co, Re), χ -Re₇Ta₃, and bcc-(Ta) phases were large and changed very little from 1100 to 1300 °C; (2) more interestingly, the λ_2 phase, with a very limited solubility of Re, was surrounded by the λ_3 phase; (3) the solubility of Re for the μ -Co₆Ta₇ phase increased slowly from 1100 to 1300 °C. These experimental results will be useful for Co-based high-temperature alloys, especially as a supplement for thermodynamic databases.

Keywords: Co-Re-Ta; phase diagram; high-temperature alloys; electron probe microanalysis

1. Introduction

It was first found by Sato et al. [1] that Co-based superalloys were strengthened by a stable ternary compound, $\gamma' Co_3(Al, W)$, with the L1₂ structure. Subsequently, the Co-based superalloys have been regarded as one of the promising high-temperature materials that exhibit better high-temperature strength than the conventional Ni-based superalloys [1]. To further improve high-temperature properties of Co-based superalloys, some refractory alloying elements, such as Re, Ta, W, and Mo, have been added to materials, which can improve high-temperature mechanical properties, creep properties, corrosion, and oxidation resistance [2–11]. Re does not randomly distribute in the alloy; it hinders dislocation movement by forming tiny clusters which act as obstacles during creep tests [2–5]. Thus, the addition of Re can effectively enhance the creep properties of superalloys. Meanwhile, as Re content increases, it refines the morphology and enhances the content of the alloy compound for Co-based superalloys [6]. Doping of Ta can maintain good microstructural stability and improve oxidation resistance [7,8]. The amount of Re and Ta additions is strictly restricted because excessive additions will cause the brittle and detrimental TCP (topologically close packed) phases to form at high stresses and temperatures [9–11]. Therefore, the knowledge of phase equilibria in the Co-Re-Ta ternary system is essential, which will provide significant basic data for the design of Co-based superalloys. However, there is no information on the experimental investigation of and thermodynamic data for the Co-Re-Ta ternary system. It is necessary to investigate the phase equilibria of the Co-Re-Ta ternary system.



The three binary systems, Co-Re, Re-Ta, and Co-Ta, that constitute the Co-Re-Ta ternary system are shown in Figure 1.

Elliott [12] has published the results for the Co-Re binary system. Later, Predel [13] reported the results for the Co-Re binary system based on experimental data. Recently, Liu et al. [14] and Guo et al. [15] estimated the Co-Re system and their findings were consistent with the experimental data. The newly assessed Co-Re phase diagram by Guo et al. [15] was applied in this work. The Co-Re system [15] is simple because there are two solid phases of (α Co) and (ϵ Co, Re) and no intermediate phases. The (ϵ Co, Re) phase has a wide homogeneity range.

The Re-Ta binary system was first studied by Greenfield and Beck [16]. They investigated alloys with Ta contents between 25 and 52 at. % and reported the composition range of the σ and χ phases. Cui and Jin [17] treated the σ phase as a stoichiometric phase and thermodynamically assessed the Re-Ta system. Afterwards, Liu and Chang [18] also evaluated the thermodynamic description of the Re-Ta system. Recently, Guo et al. [15] estimated the Re-Ta phase diagram with the latest thermodynamic description for pure Re, and this Re-Ta binary system was used in the paper. The two intermediate phases of χ -Re₇Ta₃ and σ -Re₃Ta₂ exist in the Re-Ta binary system [15]. The σ -Re₃Ta₂ phase forms from the peritectic reaction of liquid + χ -Re₇Ta₃ $\leftrightarrow \sigma$ -Re₃Ta₂. The melting point of the χ -Re₇Ta₃ phase is about 2832 °C.

The Co-Ta binary system has been investigated by many researchers [19–24]. Itoh et al. [19] investigated the homogeneity ranges, crystal structures, and magnetic properties of the three Laves phases in the Co-Ta system. Okamoto [20] assessed the Co-Ta phase diagram and treated C14 as a line compound. Liu and Chang [21] thermodynamically assessed the Co-Ta binary system. Shinagawa et al. [24] studied the Co-Ta binary system and revised the λ_1 phase as an intermetallic compound with a narrow composition range, and the phase diagram [24] was adopted in this work. There are three Laves phases of λ_1 (C14), λ_2 (C15), and λ_3 (C36), each with different polytypes. The other intermediate phases of CoTa₂, μ -Co₆Ta₇, and Co₇Ta₂, and solution phases of bcc-(Ta), (ϵ Co), and (α Co) also exist in the Co-Ta binary system. The λ_1 and λ_3 phases are obtained from peritectic reactions of liquid + $\lambda_2 \leftrightarrow \lambda_1$ and liquid + $\lambda_2 \leftrightarrow \lambda_3$, respectively. The λ_1 phase exists at ~1293–1587 °C and the λ_3 phase exists at ~947–1456 °C. The Co₇Ta₂ phase with the BaPb₃ [23] crystal structure is obtained from a peritectoid reaction: (α Co) + $\lambda_3 \leftrightarrow Co_7$ Ta₂. The information for the stable solid phases and their crystal structures in the three binary systems is listed in Table 1.

The temperatures of 1100, 1200, and 1300 °C were selected because the Co-based superalloys are widely used in high-temperature areas such as aircraft engines and turbine blades. Thus, it is more meaningful to investigate the phase equilibria at high temperatures. The present work aimed to experimentally investigate the phase equilibria of the Co-Re-Ta ternary system at 1100, 1200, and 1300 °C using electron probe microanalysis and X-ray diffraction techniques in order to understand the microstructures of the Co-Re-Ta ternary system and provide useful information for the development of Co-based high-temperature alloys.



Figure 1. Binary phase diagrams constituting the Co-Re-Ta ternary system [15,24].

System	Phase	Pearson Symbol	Space Group	Prototype	Structure Type	References
Re-Ta	(Re)	hP2	P63/mmc	Mg	A3	[15]
	χ-Re ₇ Ta ₃	cI58	I-43m	αMn	A12	[15]
	σ-Re ₃ Ta ₂	tP30	$P4_2/mnm$	σCrFe	$D8_b$	[15]
	bcc-(Ta)	cI2	Im-3m	W	A2	[15]
Co-Re	(aCo)	cF4	Fm-3m	Cu	A1	[15]
	(eCo, Re)	hP2	<i>P6₃/mmc</i>	Mg	A3	[15]
	(aCo)	cF4	Fm-3m	Cu	A1	[24]
	(εCo)	hP2	P63/mmc	Mg	A3	[24]
	λ_3 -Co ₂ Ta	hP24	P63/mmc	Ni ₂ Mg	C36	[24]
	λ_2 -Co ₂ Ta	cF24	Fd-3m	Cu ₂ Mg	C15	[24]
Co-Ta	λ_1 -Co ₂ Ta	hP12	P6 ₃ /mmc	Zn ₂ Mg	C14	[24]
	μ-Co ₆ Ta ₇	hR13	R-3m	Fe_7W_6	$D8_b$	[24]
	CoTa ₂	tI12	I4/mcm	Al ₂ Cu	C16	[24]
	bcc-(Ta)	cI2	Im-3m	W	A2	[24]
	Co ₇ Ta ₂	hR36	R-3m	BaPb ₃ [23]	-	[23,24]

Table 1. Crystal structures of each phase in the Co-Re-Ta ternary system [15,23,24].

2. Experimental Procedure

High-purity rhenium (99.9 wt %), tantalum (99.9 wt %), and cobalt (99.9 wt %) were used as raw materials. The required weights of the elements (with a total weight of about 20 g) were measured with a semi-micro analytical balance with an accuracy of at least 0.5 mg. During the whole sample preparation procedure, the mass loss was usually less than 1%. Therefore, the mass loss was assumed to make no significant effect on the sample composition.

All the bulk alloys were prepared in the form of atomic ratios (at. %). The bulk alloys with nominal compositions were melted by arc-melting in an argon atmosphere using a non-consumable tungsten electrode on a water-cooled plate. Titanium was used as a getter material. The buttons were re-melted at least five times to ensure that the ingots were homogeneous.

Afterwards, the specimens were cut into small pieces by a wire-cutting machine for heat treatment. The samples were cleaned by an ultrasonic cleaner and then encapsulated in quartz ampoules which were evacuated and flushed several times with purified argon. Heat treatments were performed at 1100, 1200, and 1300 °C, respectively. The time of the heat treatments ranged from 15 days to 65 days to reach phase equilibria based on the different temperatures and compositions of the samples. The samples containing over 20 at. % Re were heat-treated for a relatively long time. Subsequently, the specimens were quenched, mounted, grinded, and polished.

The microstructural observation and equilibrium composition analysis of specimens was characterized by electron probe microanalysis (EPMA) (JXA-8100R, JEOL, Tokyo, Japan). Pure elements were used as standards and the measurements were carried out at a voltage of 20 kV and a current of 1.0×10^{-8} A. To identify the crystal structures, powder X-ray diffraction (XRD) measurements were performed on a Philips Panalytical X-pert diffractometer (Bruker Daltonic Inc., Billerica, MA, USA) with Cu K α radiation at 40 kV and 40 mA. The scanning range of 20 was from 20° to 90° at a step size of 0.0167°.

3. Results and Discussion

3.1. Microstructure

The typical back-scattered electron (BSE) images of ternary Co-Re-Ta alloys annealed at 1100, 1200, or 1300 °C for different times are shown in Figure 2; there are three-phase equilibrium microstructures shown in Figure 2a–d and two-phase equilibrium microstructures shown in Figure 2e–j. The corresponding results of the XRD are presented in Figure 3.

For the Co₇₄Re₁₆Ta₁₀ alloy, the light grey phase ((ε Co, Re)), dark grey phase (λ_3), and black phase ((α Co)) were observed after annealing at 1100 °C for 50 days, as shown in Figure 2a. Figure 2b shows the three-phase equilibrium of the μ -Co₆Ta₇ phase, λ_3 phase, and bcc-(Ta) phase in the 1200 °C/35 days-annealed $Co_{44}Re_{14}Ta_{42}$ alloy. The white phase was bcc-(Ta), the light grey phase was μ -Co₆Ta₇, and the dark grey phase was λ_3 . Figure 3a shows that the corresponding XRD pattern, and the μ -Co₆Ta₇ phase, λ_3 phase, and bcc-(Ta) phase were clearly distinguished by the different symbols. The Co₃₁Re₃₅Ta₃₄ alloy annealed at 1300 °C for 25 days contained the three phases of χ -Re₇Ta₃ (light grey), bcc-(Ta) (dark grey), and λ_3 (black), which are shown in Figure 2c. The λ_3 phase was the matrix while the bcc-(Ta) phase was on the edge of the χ -Re₇Ta₃ phase. XRD identification, as shown in Figure 3b, confirmed the existence of the three phases of χ -Re₇Ta₃, bcc-(Ta), and λ_3 . Figure 2d shows the BSE image of the Co₄₅Re₃₀Ta₂₅ alloy annealed at 1300 °C for 25 days. There were three phases of λ_3 , χ -Re₇Ta₃, and (ε Co, Re) existing in an equilibrium. Figure 2e shows a two-phase microstructure constituted by a white (ϵ Co, Re) phase and a black λ_3 phase in the Co₅₄Re₂₅Ta₂₁ alloy quenched from 1100 °C. The two-phase equilibrium of bcc-(Ta) and CoTa₂ was identified in the annealed Co₂₂Re₅Ta₇₃ alloy (1100 °C/50 days), as shown in Figure 2f. In the $Co_{58}Re_3Ta_{39}$ alloy annealed at 1200 °C for 35 days, the white μ -Co₆Ta₇ phase and the dark grey λ_3 phase were observed in Figure 2g while their crystal structure was confirmed by the XRD pattern in Figure 3c. Figure 2h shows the BSE image of the bcc-(Ta) phase and the μ -Co₆Ta₇ phase in the Co₂₅Re₂₀Ta₅₅ alloy annealed at 1200 °C for 50 days. The white bcc-(Ta) phase was homogeneously distributed in the grey μ -Co₆Ta₇ phase. Figure 2i shows that the two phases of λ_3 and (α Co) were found in the Co₈₀Re₁₁Ta₉ alloy annealed at 1300 °C for 15 days. The light grey phase was λ_3 and the dark grey phase was (α Co). The two-phase microstructure of the λ_2 phase (dark grey) and μ -Co₆Ta₇ phase (light grey) was identified in the Co₆₀Re₁Ta₃₉ alloy annealed at 1300 °C for 15 days, as shown in Figure 2j. The corresponding XRD pattern is displayed in Figure 3d.



Figure 2. Back-scattered electron (BSE) images of the typical ternary Co-Re-Ta alloys: (a) The $Co_{74}Re_{16}Ta_{10}$ alloy annealed at 1100 °C for 50 days; (b) the $Co_{44}Re_{14}Ta_{42}$ alloy annealed at 1200 °C for 35 days; (c) the $Co_{31}Re_{35}Ta_{34}$ alloy annealed at 1300 °C for 25 days; (d) the $Co_{45}Re_{30}Ta_{25}$ alloy annealed at 1300 °C for 25 days; (e) the $Co_{54}Re_{25}Ta_{21}$ alloy annealed at 1100 °C for 65 days; (f) the $Co_{22}Re_{5}Ta_{73}$ alloy annealed at 1100 °C for 50 days; (g) the $Co_{58}Re_{3}Ta_{39}$ alloy annealed at 1200 °C for 35 days; (h) the $Co_{25}Re_{20}Ta_{55}$ alloy annealed at 1200 °C for 50 days; (i) the $Co_{80}Re_{11}Ta_{9}$ alloy annealed at 1300 °C for 15 days; (j) the $Co_{60}Re_{1}Ta_{39}$ alloy annealed at 1300 °C for 15 days.

In order to figure out the phase boundary between the λ_3 and λ_2 phases, several alloys were prepared. Unfortunately, all the compositions were located at single field region, which meant that the λ_2/λ_3 two-phase field was extremely narrow. This was consistent with that of the Co-Ta binary. The phase boundaries were then plotted with approximations based on the microstructure observation results of these single-phased compositions. Figure 4a,b shows the typical XRD patterns of the Co₆₆Re₅Ta₂₉ and Co₆₈Re₃Ta₂₉ alloys annealed at 1300 °C for 15 days, which were confirmed to be λ_3 and λ_2 single phases, respectively. The corresponding microstructure was consistent with the results.



Figure 3. X-ray diffraction patterns obtained from (**a**) the $Co_{44}Re_{14}Ta_{42}$ alloy annealed at 1200 °C for 35 days, (**b**) the $Co_{31}Re_{35}Ta_{34}$ alloy annealed at 1300 °C for 25 days, (**c**) the $Co_{58}Re_3Ta_{39}$ alloy annealed at 1200 °C for 35 days, and (**d**) the $Co_{60}Re_1Ta_{39}$ alloy annealed at 1300 °C for 15 days.



Figure 4. X-ray diffraction patterns obtained from (**a**) the $Co_{66}Re_5Ta_{29}$ alloy annealed at 1200 °C for 35 days and (**b**) the $Co_{68}Re_3Ta_{29}$ alloy annealed at 1300 °C for 15 days.

3.2. Isothermal Sections

All the equilibrium compositions of the Co-Re-Ta ternary system at 1100, 1200, and 1300 °C are listed in Tables 2–4, respectively. Figure 5a–c shows the isothermal sections at 1100, 1200, and 1300 °C based on the experimental data, respectively. The λ_2 single phase, λ_3 single phase, two-phase equilibrium, and three-phase equilibrium are characterized by different symbols. The solid triangle represents the determined three-phase equilibrium while the dashed triangle represents the undetermined three-phase equilibrium.

Table 2. Equilibrium compositions of the Co-Re-Ta ternary system at 1100 °C as determined in the
present work.

	Annealed Time (days)	Phase Equilibrium	Composition (at. %)					
Nominal Alloys (at. %)		Phase 1/Phase 2/Phase 3	Phase 1		Phase 2		Phase 3	
			Re	Ta	Re	Ta	Re	Та
Co ₃₁ Re ₃₅ Ta ₃₄	65	λ_3 /bcc-(Ta)/ χ -Re ₇ Ta ₃	19.7	26.5	46.5	45.5	52.7	34.8
Co45Re30Ta25	65	$\lambda_3/(\epsilon \text{Co}, \text{Re})/\chi$ -Re ₇ Ta ₃	20.1	25.5	30.4	22.0	60.1	26.0
Co ₆₀ Re ₂₀ Ta ₂₀	65	$(\varepsilon Co, Re)/\lambda_3$	27.3	16.6	16.5	20.5		
Co45Re20Ta35	65	bcc-(Ta)/ λ_3	41.4	48.4	13.1	30.9		
Co ₂₅ Re ₂₀ Ta ₅₅	65	μ-Co ₆ Ta ₇ /bcc-(Ta)	2.3	50.6	34.1	58.3		
Co ₅₄ Re ₂₅ Ta ₂₁	65	$(\epsilon Co, Re)/\lambda_3$	28.7	19.1	18.4	22.9		
Co ₇₈ Re ₅ Ta ₁₇	50	$(\alpha Co)/\lambda_3$	2.7	3.3	4.7	21.8		
Co44Re14Ta42	50	λ_3/μ -Co ₆ Ta ₇ /bcc-(Ta)	2.7	33.8	3.8	43.7	39.2	51.2
Co ₂₂ Re ₅ Ta ₇₃	50	CoTa ₂ /bcc-(Ta)	0.7	65.8	8.9	87.5		
Co ₅₈ Re ₃ Ta ₃₉	50	λ_3/μ -Co ₆ Ta ₇	1.9	33.6	3.2	43.4		
Co ₈₀ Re ₂ Ta ₁₈	50	$(\alpha Co)/\lambda_3$	0.9	3.5	1.8	22.7		
Co ₈₀ Re ₅ Ta ₁₅	50	$(\alpha Co)/\lambda_3$	3.5	3.6	5.7	20.8		
Co ₈₀ Re ₁₁ Ta ₉	50	$(\alpha Co)/\lambda_3$	9.2	2.7	13.8	17.2		
Co ₇₄ Re ₁₆ Ta ₁₀	50	$(\alpha Co)/\lambda_3/(\epsilon Co, Re)$	10.1	2.4	15.2	17.3	25.0	14.2
Co ₅₄ Re ₁₈ Ta ₂₈	50	λ_3	18.2	28.3				
Co ₈₉ Re ₅ Ta ₆	50	$(\alpha Co)/\lambda_3$	4.6	3.7	7.5	19.6		
Co ₃₃ Re ₅ Ta ₆₂	50	CoTa ₂ /bcc-(Ta)	1.7	59.2	18.0	77.3		
Co ₃₀ Re ₁₀ Ta ₆₀	50	μ-Co ₆ Ta ₇ /bcc-(Ta)	1.7	54.2	24.0	71.3		
Co ₆₉ Re ₉ Ta ₂₂	50	λ_3	9.3	22.3				
Co ₇₀ Re ₅ Ta ₂₅	50	λ_3	4.5	24.9				
Co ₇₁ Re ₁ Ta ₂₈	50	λ_2	0.8	28.2				
Co ₆₈ Re ₃ Ta ₂₉	50	λ_2	2.7	28.7				
Co ₆₆ Re ₅ Ta ₂₉	50	λ_3	4.7	28.5				
Co ₆₄ Re ₇ Ta ₂₉	50	λ_3	7.3	28.9				
Co ₆₀ Re ₁ Ta ₃₉	50	λ_2/μ -Co ₆ Ta ₇	0.7	32.3	1.2	43.7		
Co ₂₈ Re ₆ Ta ₆₆	50	CoTa ₂ /bcc-(Ta)	1.4	60.2	14.2	80.7		
Co ₄₃ Re ₁ Ta ₅₆	50	CoTa ₂ /µ-Co ₆ Ta ₇	0.9	57.8	1.1	54.8		

Table 3. Equilibrium compositions of the Co-Re-Ta ternary system at 1200 $^\circ C$ as determined in the present work.

	Annealed Time (days)	Phase Equilibrium	Composition (at. %)					
Nominal Alloys (at. %)		Phase 1/Phase 2/Phase 3	Phase 1		Phase 2		Phase 3	
			Re	Та	Re	Ta	Re	Ta
Co31Re35Ta34	50	λ ₃ /bcc-(Ta)/χ-Re ₇ Ta ₃	21.7	26.1	50.0	47.6	56.6	31.4
Co ₄₅ Re ₃₀ Ta ₂₅	50	$\lambda_3/(\epsilon Co, Re)/\chi$ -Re ₇ Ta ₃	21.7	25.4	31.3	24.3	59.9	26.8
Co ₆₀ Re ₂₀ Ta ₂₀	50	$(\epsilon Co, Re)/\lambda_3$	27.2	18.7	17.2	20.9		
Co ₄₅ Re ₂₀ Ta ₃₅	50	bcc-(Ta)/ λ_3	41.1	48.6	14.0	31.9		
Co ₂₅ Re ₂₀ Ta ₅₅	50	μ-Co ₆ Ta ₇ /bcc-(Ta)	2.8	51.1	35.3	58.7		
Co ₅₄ Re ₂₅ Ta ₂₁	50	$(\epsilon Co, Re)/\lambda_3$	28.0	20.9	20.1	22.9		
Co ₇₈ Re ₅ Ta ₁₇	35	$(\alpha Co)/\lambda_3$	2.7	4.4	4.3	21.9		
Co ₄₄ Re ₁₄ Ta ₄₂	35	λ_3/μ -Co ₆ Ta ₇ /bcc-(Ta)	3.5	35.3	4.0	44.2	39.4	50.4
Co ₂₂ Re ₅ Ta ₇₃	35	CoTa ₂ /bcc-(Ta)	0.8	65.2	8.9	86.5		
Co ₅₈ Re ₃ Ta ₃₉	35	λ_3/μ -Co ₆ Ta ₇	2.4	34.4	3.3	43.9		
Co ₈₀ Re ₂ Ta ₁₈	35	$(\alpha Co)/\lambda_3$	1.4	4.9	1.8	22.5		
Co ₈₀ Re ₅ Ta ₁₅	35	$(\alpha Co)/\lambda_3$	3.2	4.2	5.5	21.1		
Co ₈₀ Re ₁₁ Ta ₉	35	$(\alpha Co)/\lambda_3$	9.7	3.0	13.6	18.4		
Co ₇₄ Re ₁₆ Ta ₁₀	35	$(\alpha Co)/\lambda_3/(\epsilon Co, Re)$	11.2	2.8	15.5	17.6	24.9	15.3
Co ₅₄ Re ₁₈ Ta ₂₈	35	λ_3	18.3	28.2				
Co ₈₉ Re ₅ Ta ₆	35	$(\alpha Co)/\lambda_3$	4.3	4.5	7.1	20.6		
Co33Re5Ta62	35	CoTa ₂ /bcc-(Ta)	1.5	59.6	19.5	76.8		
Co ₃₀ Re ₁₀ Ta ₆₀	35	μ -Co ₆ Ta ₇ /bcc-(Ta)	2.0	55.1	23.5	72.2		
Co ₆₉ Re ₉ Ta ₂₂	35	λ_3	8.4	22.0				
Co ₇₀ Re ₅ Ta ₂₅	35	λ_3	4.5	24.8				
Co ₇₁ Re ₁ Ta ₂₈	35	λ_2	0.8	28.0				
Co68Re3Ta29	35	λ_2	2.6	28.8				
Co ₆₆ Re ₅ Ta ₂₉	35	$\overline{\lambda_3}$	4.8	29.0				
Co ₆₄ Re ₇ Ta ₂₉	35	λ_3	7.0	28.8				
Co ₆₀ Re ₁ Ta ₃₉	35	λ_2/μ -Co ₆ Ta ₇	0.5	32.4	1.0	44.1		
Co ₂₈ Re ₆ Ta ₆₆	35	CoTa ₂ /bcc-(Ta)	1.3	60.2	15.9	79.6		
Co ₄₃ Re ₁ Ta ₅₆	35	$CoTa_2/\mu$ - Co_6Ta_7	0.6	60.5	1.3	54.8		

		Phase Equilibrium	Composition (at. %)						
Nominal Alloys (at. %)	Annealed Time (days)	Phase 1/Phase 2/Phase 3	Phase 1		Phase 2		Phase 3		
			Re	Та	Re	Ta	Re	Та	
Co ₃₁ Re ₃₅ Ta ₃₄	25	λ_3 /bcc-(Ta)/ χ -Re ₇ Ta ₃	22.2	27.1	49.0	48.5	56.6	32.6	
Co45Re30Ta25	25	$\lambda_3/(\epsilon Co, Re)/\chi$ -Re ₇ Ta ₃	22.6	26.1	32.0	23.2	58.7	25.8	
Co ₆₀ Re ₂₀ Ta ₂₀	25	$(\epsilon Co, Re)/\lambda_3$	27.5	17.0	17.3	20.6			
Co45Re20Ta35	25	bcc-(Ta)/ λ_3	42.8	48.9	14.2	32.8			
Co ₂₅ Re ₂₀ Ta ₅₅	25	μ-Co ₆ Ta ₇ /bcc-(Ta)	3.9	51.2	35.5	58.9			
Co54Re25Ta21	25	$(\varepsilon Co, Re)/\lambda_3$	28.8	18.9	19.7	22.1			
Co ₇₈ Re ₅ Ta ₁₇	15	$(\alpha Co)/\lambda_3$	2.8	5.5	5.0	21.3			
Co44Re14Ta42	15	λ_3/μ -Co ₆ Ta ₇ /bcc-(Ta)	5.5	36.4	6.1	43.2	41.8	50.4	
Co ₂₂ Re ₅ Ta ₇₃	15	CoTa ₂ /bcc-(Ta)	0.8	65.2	8.7	87.6			
Co ₅₈ Re ₃ Ta ₃₉	15	λ_3/μ -Co ₆ Ta ₇	2.7	35.4	3.6	44.0			
Co ₈₀ Re ₂ Ta ₁₈	15	$(\alpha Co)/\lambda_3$	1.3	5.6	1.9	22.3			
Co ₈₀ Re ₅ Ta ₁₅	15	$(\alpha Co)/\lambda_3$	3.5	5.0	5.9	20.8			
Co ₈₀ Re ₁₁ Ta ₉	15	$(\alpha Co)/\lambda_3$	10.0	3.8	13.8	17.8			
Co ₇₄ Re ₁₆ Ta ₁₀	15	$(\alpha Co)/\lambda_3/(\epsilon Co, Re)$	13.0	2.6	16.2	17.8	26.0	14.2	
Co ₅₄ Re ₁₈ Ta ₂₈	15	λ_3	18.2	28.5					
Co ₈₉ Re ₅ Ta ₆	15	$(\alpha Co)/\lambda_3$	4.8	5.0	7.2	22.4			
Co ₃₃ Re ₅ Ta ₆₂	15	CoTa ₂ /bcc-(Ta)	2.1	59.2	19.2	76.2			
Co ₃₀ Re ₁₀ Ta ₆₀	15	μ -Co ₆ Ta ₇ /bcc-(Ta)	2.4	54.1	24.2	71.4			
Co ₆₉ Re ₉ Ta ₂₂	15	λ_3	8.9	22.0					
Co ₇₀ Re ₅ Ta ₂₅	15	λ_3	4.5	24.5					
Co ₇₁ Re ₁ Ta ₂₈	15	λ_2	0.7	27.8					
Co ₆₈ Re ₃ Ta ₂₉	15	λ_2	2.7	28.6					
Co ₆₆ Re ₅ Ta ₂₉	15	λ_3	4.6	28.4					
Co ₆₄ Re ₇ Ta ₂₉	15	λ_3	7.0	28.6					
Co ₆₀ Re ₁ Ta ₃₉	15	λ_2/μ -Co ₆ Ta ₇	0.8	32.3	1.3	44.2			
Co ₂₈ Re ₆ Ta ₆₆	15	CoTa ₂ /bcc-(Ta)	1.8	58.3	14.9	81.1			
Co ₄₃ Re ₁ Ta ₅₆	15	$CoTa_2/\mu$ -Co ₆ Ta ₇	0.6	59.7	1.3	54.9			

Table 4. Equilibrium compositions of the Co-Re-Ta ternary system at 1300 °C as determined in the present work.

Figure 5a shows the 1100 °C isothermal section of the Co-Re-Ta ternary system. There were three solid solution phases of (α Co), (ε Co, Re), and bcc-(Ta), two Laves phases of λ_2 and λ_3 , and the intermetallic compounds of the μ -Co₆Ta₇, CoTa₂, and χ -Re₇Ta₃ phases. Investigations of the Co₇₄Re₁₆Ta₁₀, Co₄₄Re₁₄Ta₄₂, Co₃₁Re₃₅Ta₃₄, and Co₄₅Re₃₀Ta₂₅ alloys were used to determine the three-phase equilibria of (α Co) + (ε Co, Re) + λ_3 , λ_3 + bcc-(Ta) + μ -Co₆Ta₇, λ_3 + χ -Re₇Ta₃ + bcc-(Ta), and (ε Co, Re) + λ_3 + χ -Re₇Ta₃, respectively. Seven alloys were confirmed to be single phases, two alloys (Co₇₁Re₁Ta₂₈ and Co₆₈Re₃Ta₂₉) were located in the λ_2 single-phase region, and five alloys (Co₅₄Re₁₈Ta₂₈, Co₆₉Re₉Ta₂₂, Co₇₀Re₅Ta₂₅, Co₆₆Re₅Ta₂₉ and Co₆₄Re₇Ta₂₉) were located in the λ_3 single-phase region. The solubility of Re in the λ_3 phase was measured to be about 20.1 at. % while the solubility of Re in the λ_2 phase and was wrapped around the λ_2 phase. The solubility of Re in the left side to the right side of the λ_2 phase was about 16.8 at. %. The (ε Co, Re) phase extended from the Re-rich side to the Co-rich side, and the solubility of Ta in (ε Co, Re) phase was about 21.7 at. %.



Figure 5. Cont.



Figure 5. Experimentally determined isothermal section of the Co-Re-Ta system: (**a**) 1100 °C, (**b**) 1200 °C, (**c**) 1300 °C.

Figure 5b shows the isothermal section at 1200 °C. Four three-phase regions of the (α Co) + (ϵ Co, Re) + λ_3 , λ_3 + bcc-(Ta) + μ -Co₆Ta₇, λ_3 + χ -Re₇Ta₃ + bcc-(Ta), and (ϵ Co, Re) + λ_3 + χ -Re₇Ta₃ were experimentally determined. The 1200 °C isothermal section was similar to the 1100 °C isothermal section. The solubility of Re in the λ_3 phase increased a little from 20.1 at. % at 1100 °C to 21.5 at. % at 1200 °C. The solubility of Re in the λ_2 phase was about 3.5 at. %, almost the same as at 1100 °C. The μ -Co₆Ta₇ and CoTa₂ phases dissolved about 3.8 at. % and 1.4 at. % Re, respectively. The solubility of Ta in the (ϵ Co, Re) phase was about 24.1 at. %. The solubility of Co in the χ -Re₇Ta₃ + bcc-(Ta) at the 1200 °C isothermal section was larger than that of the 1100 °C isothermal section, while the (ϵ Co, Re) + λ_3 + χ -Re₇Ta₃ three-phase region was smaller.

The isothermal section at 1300 °C is shown in Figure 5c. Compared to the 1200 and 1300 °C isothermal sections, another Laves phase of λ_1 , which existed at 1293 °C~1587 °C in the Co-Ta binary system, appeared in the 1100 °C isothermal section. However, the solubility of Re was so small that it was not identified. The 1300 °C isothermal section had one more three-phase region ($\lambda_1 + \lambda_2 + \mu$ -Co₆Ta₇) than in the 1100 and 1200 °C isothermal sections. The solubility of Re in the λ_3 and λ_2 phases was about 22.3 at. %, 3.6 at. %, respectively. The solubility of Re in μ -Co₆Ta₇ was found to be about 6.1 at. %, occupying the most out of all the investigated isothermal sections. The CoTa₂ phase dissolved about 1.8 at. % Re. The solubility of Ta in the (ϵ Co, Re) phase was about 23.2 at. %. There were seven three-phase regions of (α Co) + (ϵ Co, Re) + λ_3 , λ_3 + bcc-(Ta) + μ -Co₆Ta₇, λ_3 + χ -Re₇Ta₃ + bcc-(Ta), (ϵ Co, Re) + λ_3 , λ_3 + bcc-(Ta), λ_1 + λ_2 + μ -Co₆Ta₇, λ_3 + χ -Re₇Ta₃, λ_3 + λ_2 + μ -Co₆Ta₇, λ_1 + λ_2 + μ -Co₆Ta₇, and CoTa₂ + μ -Co₆Ta₇ + bcc-(Ta) existing at 1300 °C. The former four three-phase regions were experimentally confirmed, and the last three three-phase regions were not experimentally evidenced. The three-phase equilibrium of λ_3 + bcc-(Ta) + μ -Co₆Ta₇ was smaller than those in the 1100 and 1200 °C isothermal sections.

4. Conclusions

The isothermal sections of the Co-Re-Ta ternary system at 1100, 1200, and 1300 °C were experimentally investigated. The results were as follows: (1) There were six three-phase regions at the 1100 and 1200 °C isothermal sections and seven three-phase regions at the 1300 °C isothermal section; (2) the (ϵ Co, Re) phase had a large solubility of Ta and extended from the Re-rich side to the Co-rich side; (3) the λ_3 phase, with a large solubility of Re, surrounded the λ_2 phase which dissolved a little Re; (4) the solubility of Re in the CoTa₂ phase changed little while the solubility of Re in the μ -Co₆Ta₇ phase increased with the temperature increase from 1100 to 1300 °C; (5) no ternary compound was found.

Author Contributions: Conceptualization, X.L. and C.W.; funding acquisition, X.L. and C.W.; investigation, D.W., J.Z. (Jinbin Zhang), J.H. and Y.L.; supervision, X.L. and C.W.; writing—original draft, D.W.; writing—review and editing, M.Y., J.Z. (Jiahua Zhu), L.L., Y.C. and S.Y.

Funding: This work was supported by the National Key R&D Program of China (Grant No. 2016YFB0701401) and National Natural Science Foundation of China (Grant Nos. 51831007 and 51471138).

Acknowledgments: This work was supported by the National Key R&D Program of China (Grant No. 2016YFB0701401) and National Natural Science Foundation of China (Grant Nos. 51831007 and 51471138).

Conflicts of Interest: The authors declare no conflicts of interest.

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