


Article

Controlling Segregation Behavior of Primary Si in Hypereutectic Al-Si Alloy by Electromagnetic Stirring

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Abstract: Controlling the segregation behavior of primary Si in the solidification process of hypereutectic Al-Si alloy is crucial for enhancing the design ability of the solidification structure. To explore the separation condition and morphological evolution of primary Si in detail, a series of experiments concerning the coupling effect of a temperature field and electromagnetic stirring on the segregation behavior of primary Si were carried out. Experimental results show that the temperature field and fluid flow in the melt are two key points for controlling the segregation behavior of primary Si. The establishment of a temperature gradient in the Al-Si melt is a precondition for realizing the separation of primary Si. On the basis of the temperature gradient, the electromagnetic stirring can further strengthen the separation effect for primary Si, forming a Si-rich layer with 65~70 wt.% Si content. The formation of the Si-rich layer is a continuous growth process of primary Si by absorbing Si atoms from Al-Si melt with the help of electromagnetic stirring. The separation technology for primary Si is proposed to realize the segregation control of primary Si, which not only broadens the application of Al-Si alloys in the functionally gradient composites but also provides a low-cost supply strategy of Si raw materials for the solar photovoltaic industry.

Keywords: electromagnetic stirring; segregation behavior; solidification; hypereutectic Al-Si alloy; microstructure

1. Introduction

Hypereutectic Al-Si alloys are recognized as excellent candidates for structural application in the aircraft, automotive and electronic packaging industries, due to their excellent wear resistance, high heat resistance and low thermal expansion coefficient [1–3]. The uneven growth of the primary Si easily occurs in the casting solidification process of Al-Si alloy with increasing Si content, resulting in severe macro-segregation in large ingots. The macro-properties of the materials usually depend on the micro-structures, namely, the mechanical properties show a transition from uniformity to non-uniformity with a gradient segregation of second phase particles [4]. Therefore, improving macro-segregation of primary Si is commercially important, which plays a critical role in designing service material performance.

Numerous efforts have been made to strengthen the segregation behavior of primary Si during the solidification of Al-Si alloy by applying physical fields, such as ultrasonic field [5], super gravity field [6], electric field [7–9], static magnetic field [10], and electromagnetic stirring [11–20]. Among various

fields, electromagnetic stirring is the most efficient method used to realize the remote transmission of solute atoms [21,22] and even to control the directional growth of dendrite [23]. As early as 1991, Ren et al. [24] identified the phenomenon of a “separated eutectic” in the unidirectional solidification process of the eutectic Al-Si alloy under a rotating magnetic field (RMF). The research of Yoshikawa et al., [11–13] indicates that the bulk flow forced by an intermediate frequency magnetic field can directionally drive primary Si particles, resulting in the axial macro-segregation of primary Si during the directional solidification of hypereutectic Al-Si alloy. Ban et al. [25,26] tried to separate primary Si by using RMF at slow cooling condition and discussed the influence of the frequency of the RMF on the separation efficiency of primary Si. On the other hand, we also struggled with the fact that the electromagnetic separation of primary Si during the solidification of Al-30Si alloy has been entrenched by changing the Si content [27] and adding Sn element [28]. The morphological evolution of primary Si in the electromagnetic directional solidification of Al-30Si alloy was studied by Xue et al. [29] and Jiang et al. [30]. More specifically, they established a predominance area diagram for Si morphology based on the constitutional super-cooling theory, and indicated that the morphology can be controlled by adjusting the crystal growth rate, temperature gradient, and solute concentration. With over a century of research into macro-segregation, the separation of primary Si has been well-realized by electromagnetic stirring. However, there are many disputes about the understanding of the separation mechanism, especially regarding the issue for the separation condition and morphological evolution of primary Si, which greatly limits the implementation of electromagnetic separation technology to large commercial ingot production.

Hence, the present work aims to confirm the separation condition and morphological evolution of primary Si during the solidification of hypereutectic Al-Si alloy under electromagnetic stirring. The separation condition for primary Si was determined under the coupling action of a temperature field and RMF. Moreover, the evolution process for the Si-rich layer was revealed in the electromagnetic separation process of primary Si. On the basis of fundamental understanding of the electromagnetic separation mechanism, the electromagnetic separation technology for primary Si was further developed, and its potential perspective in future industry was proposed.

2. Experimental Procedure

2.1. The Separation Condition of Primary Si

The hypereutectic Al-30 wt.% Si alloy (in weight) was prepared by melting the metallurgical-grade Si (MG-Si, purity 99.7 wt.%) and commercial Al (purity 99.7 wt.%) in the medium frequency induction furnace (power 25 kw) with an argon atmosphere. To determine the separation condition for primary Si, two groups of experiments were carried out. The first group was conducted with a changed cooling condition by adjusting the position of the insulation materials on the outside surface of a graphite crucible to investigate the effect of the temperature field on the segregation behavior of primary Si. The pre-prepared Al-30Si melt was moved to a SiC electric furnace and held at 830 °C for 20 min to enable uniform melting. Then, the Al-30Si melt was poured into a graphite crucible (Φ 60 mm, preheated at 830 °C). The insulation materials were coated on the different positions of the graphite crucible to establish the required temperature field into the Al-30Si melt (Figure 1a). K-type thermocouples, connected to a multichannel data logging system, were inserted into the center of the melt to record the cooling curves. The second group was conducted with forced melt flow by introducing an RMF based on the above cooling condition, which mainly aims to reveal the role of electromagnetic stirring on the separation of primary Si. The Al-30Si melt was poured into a graphite crucible with the above cooling condition. The graphite crucible was placed into the RMF with a frequency of 50 Hz and a magnetic flux density of 25 mT which was induced by a three-phase-three-pole magnetic generator (Figure 1b). The magnetic field was switched on when the melt was cooled to 810 °C. The concept and logical relationship for each experimental group are given in Table 1.

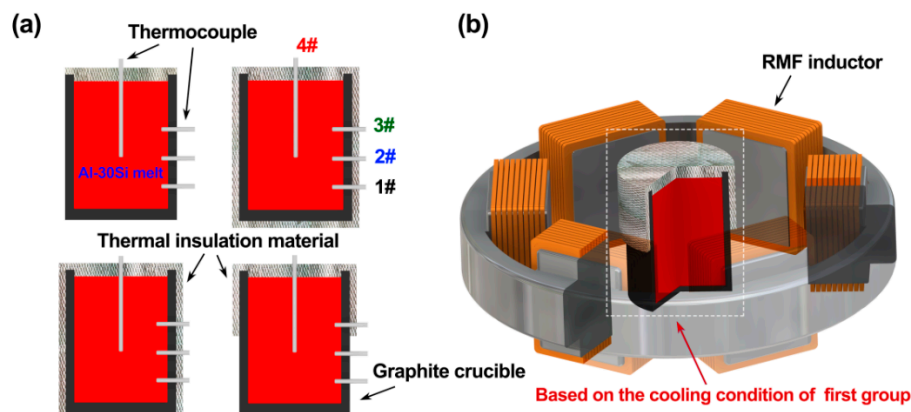


Figure 1. Schematic diagram of the experimental device for each group: (a) insulation details of the graphite crucible, (b) structural features of the rotating magnetic field (RMF).

Table 1. The design details and the logical relationship of each group.

Groups	Temperature Field		Electromagnetic Stirring	Experiment Objective
	Temperature Gradient	Cooling Rate		
First group	C _I -1	Uniform	Without RMF	The influence of the cooling rate on the segregation behavior of primary Si was investigated under a uniform temperature field.
	C _I -2			
	C _I -3	Uneven		The influence of the temperature gradient on the segregation behavior of primary Si was determined after eliminating the influence factors of the cooling rate.
	C _I -4			
Second group	C _{II} -1	Uniform	With RMF	The purpose was to investigate whether or not electromagnetic force plays a decisive role on the transport behavior of primary Si under a uniform temperature field with a different cooling rate.
	C _{II} -2			
	C _{II} -3	Uneven		The effect of melt flow forced by the RMF on the separation of primary Si was investigated on the basis of confirming the role of electromagnetic force.
	C _{II} -4			

2.2. The Separation Process of Primary Si

In order to clarify the formation process for the Si-rich layer, a series of experiments were designed, and the corresponding schematic flow is given in Figure 2. The Al-30Si alloy was melted to 830 °C in the SiC electric furnace and then cooled slowly to specific temperatures (790, 760, 730 and 700 °C) by turning off the power (Figure 2a). With decrease of temperature, the Si crystals initially precipitated from the melt to form the primary Si particles. Correspondingly, the number of Si atoms in the melt was gradually reduced. According to the Al-Si alloy phase diagram [31], the precipitated mass fractions of the primary Si were 0, 45, 25 and 5% at temperatures of 790, 760, 730 and 700 °C, respectively. In this cooling process with the furnace, the Al-30Si melt was stirred by a ceramic stick to prevent the primary Si phase from forming a mesh-shape around the inner wall of crucible. It is noteworthy that the Al-30Si melt was contained by the graphite crucible with an optimum separation condition. When the predetermined temperature was reached, the semisolid Al-30Si melt was transferred to the RMF inductor for the electromagnetic separation of primary Si (Figure 2b). The solidified ingots were cut along the axis of the cylinder to exhibit the distribution characteristics of primary Si, and the microstructures were characterized by an optical microscope. All the experiments were conducted at least three times in order to assess reproducibility.

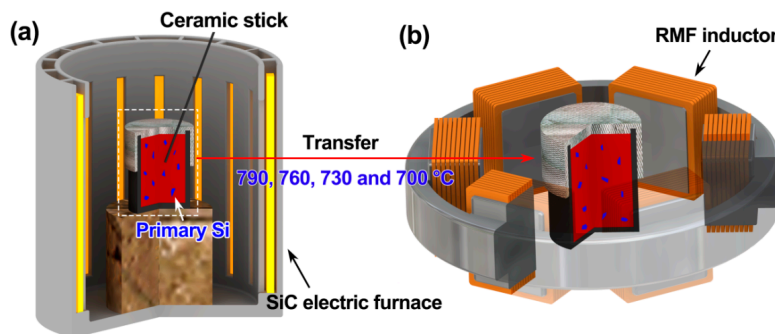


Figure 2. Experiment flow chart of the formation process of the Si-rich layer: (a) Cooling with furnace, (b) RMF inductor.

3. Results and Discussion

3.1. Electromagnetic Separation Condition of Primary Si

3.1.1. Effect of Temperature Field on the Segregation Behavior of Primary Si

The cooling curves of the Al-30Si melt with different insulation conditions were recorded by the multichannel data logging system (see Figure 3). Without the insulation layer (C_I-1), the temperature field inside the Al-30Si melt tended to be uniformly distributed, and the cooling rate was approximately $60\text{ }^{\circ}\text{C}/\text{min}$ (Figure 3a). Under the condition of complete insulation (C_I-2), the cooling rate of the Al-30Si melt was reduced to $1.5\text{ }^{\circ}\text{C}/\text{min}$, and the distribution of the temperature field was more uniform in the entire melt (Figure 3b). When the insulation materials were coated on the top and periphery of the crucible (C_I-3), the heat preferentially escaped through the bottom of the Al-30Si melt during slow cooling, forming a temperature gradient ($0.5\text{ }^{\circ}\text{C}/\text{mm}$) in the axial plane (Figure 3c). With the heat dissipation area further expanded (C_I-4), the temperature gradient in the entire Al-30Si melt became more obvious, as shown in Figure 3d. There were two kinds of orientation: one was a top-bottom temperature gradient ($1.5\text{ }^{\circ}\text{C}/\text{mm}$) in the axial direction, while the other was an inside-out temperature gradient ($0.3\text{ }^{\circ}\text{C}/\text{mm}$) in the radial direction.

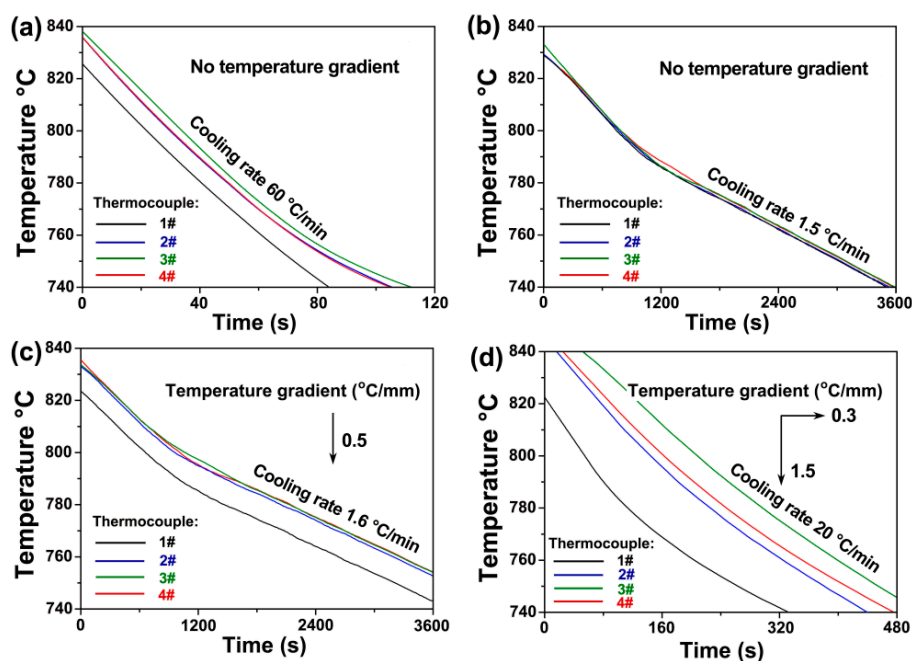


Figure 3. Cooling curves of the Al-30Si alloy with different insulation conditions: (a) C_I-1 , (b) C_I-2 , (c) C_I-3 , (d) C_I-4 .

To more directly reflect the effect of the temperature field on the segregation behavior of primary Si, the vertical-sections of Al-30Si alloy solidified with different cooling conditions were observed (see Figure 4). For the case without an insulation layer, the primary Si tended to be uniformly distributed in the entire ingot (Figure 4a). The heat loss in the Al-30Si melt became more uniform and slower because of the complete insulation, thus promoting a uniform distribution and growth of primary Si (Figure 4b). By comparing Figure 4a to Figure 4b, it was not difficult to find that the segregation behavior of primary Si was not controlled by changing the cooling rate under the condition of a uniform temperature field. This is attributed to the uniform nucleation of primary Si in the solidification process of Al-30Si alloy without temperature gradient. For an uneven temperature field, the distribution of primary Si changed significantly in the vertical-section of the ingot. The primary Si was segregated toward the bottom of the Al-30Si melt under the effect of the temperature gradient (Figure 4c,d). Therefore, it could be concluded that the establishment of the temperature gradient in the Al-30Si melt was a precondition for realizing the separation of primary Si.

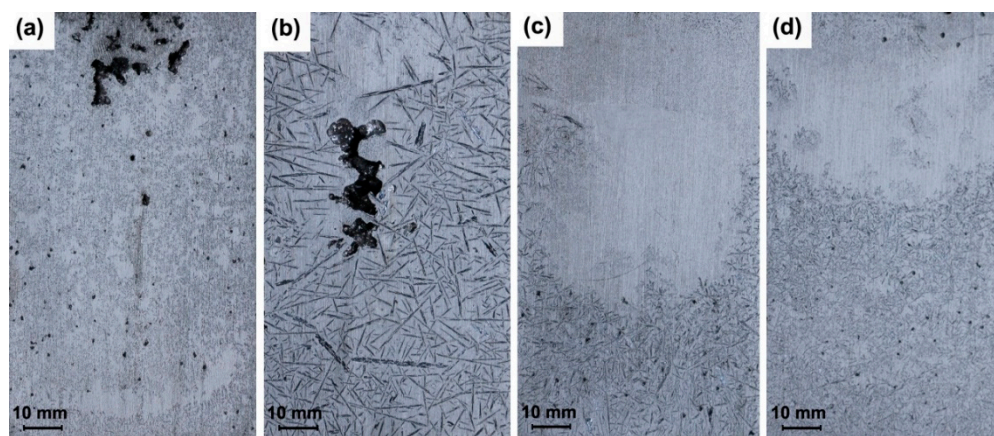


Figure 4. Vertical-sections of Al-30Si alloys with different cooling conditions: (a) C_I-1, (b) C_I-2, (c) C_I-3, (d) C_I-4.

3.1.2. Role of Electromagnetic Stirring in the Separation Process of Primary Si

On the basis of the above insulating condition, an RMF was further introduced to clarify the influence of coupling between the temperature field and the electromagnetic field on the segregation behavior of primary Si. Figure 5 shows the vertical-sections of Al-30Si alloy solidified under the coupling effect of a temperature field and electromagnetic field. Based on Figure 5a,b, during electromagnetic solidification without a temperature gradient for both rapid and slow cooling (C_{II}-1 and C_{II}-2), the primary Si was evenly distributed in the entire Al-30Si alloy. This finding indicated that electromagnetic stirring was not a decisive role for the separation of primary Si. However, under the condition of a temperature gradient (C_{II}-3 and C_{II}-4), the primary Si was separated by the electromagnetic stirring. The primary Si was transferred from the high temperature region to the low temperature region under the coupling action of the temperature gradient and the RMF, eventually forming a Si-rich layer (Figure 5c,d). In addition, the RMF could fully separate the primary Si under axial and radial temperature gradients (Figure 5d). From Figure 4c,d, it was not difficult to obtain the conclusion that the separation of primary Si could be further strengthened by electromagnetic stirring on the base of the temperature gradient.

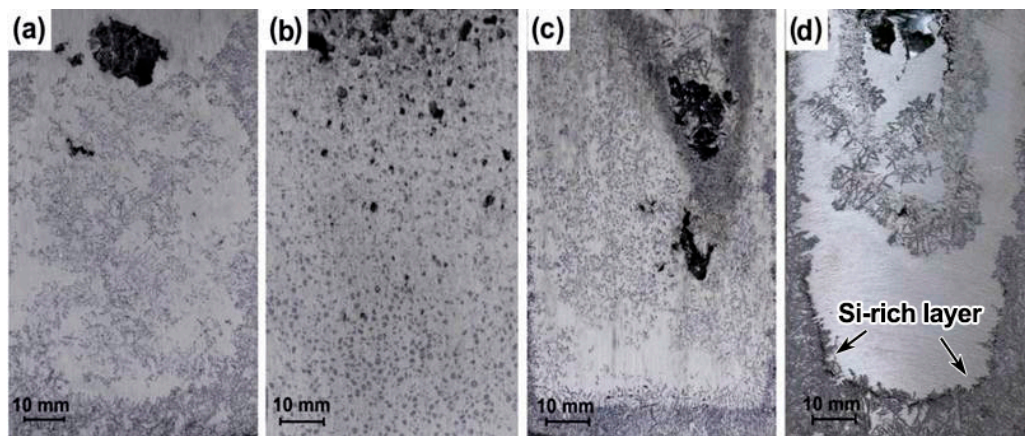


Figure 5. Vertical-sections of Al-30Si alloys solidified under coupling action of a temperature field and an electromagnetic field: (a) C_{II}-1, (b) C_{II}-2, (c) C_{II}-3, (d) C_{II}-4.

3.2. Electromagnetic Separation Process of Primary Si

3.2.1. The Transport Behavior of Primary Si under Electromagnetic Stirring

The vertical-sections of the solidified Al-30Si alloy were observed by starting the RMF at temperatures of 790, 760, 730 and 700 °C (see Figure 6). Note that the primary Si particles marked by arrow 1 were precipitated from the Al-30Si melt in furnace cooling before being placed under the RMF; the Si-rich layer marked by arrow 2 was formed after starting the RMF. The primary Si particles pre-precipitated by slow cooling in the furnace to 700 °C remained evenly distributed in the entire ingot under the RMF (see Figure 6a and illustration of Figure 6a). This finding also indicates that the electromagnetic force could not separate the primary Si phase in the form of particles from the Al-Si melt. With the rise of the cooling temperature in the furnace, the number of pre-precipitated primary Si particles decreased while the Si-rich layer gradually formed (Figure 6b,c). When the temperature reached 790 °C (liquidus temperature), the primary Si particles disappeared completely, and a layer structure with a Si-rich outer layer/Si-poor inside region is formed (Figure 6d). The Si-rich layer as the cooling temperature increased in the furnace is attributed to the fact that the content of Si atoms in the residual melt increased as the number of pre-precipitated primary Si particles decreased. Therefore, the electromagnetic separation process of primary Si is not transport in the form of primary Si particles to the periphery of the ingot by an electromagnetic force but continual growth by absorbing Si atoms from the melt under the action of electromagnetic stirring.

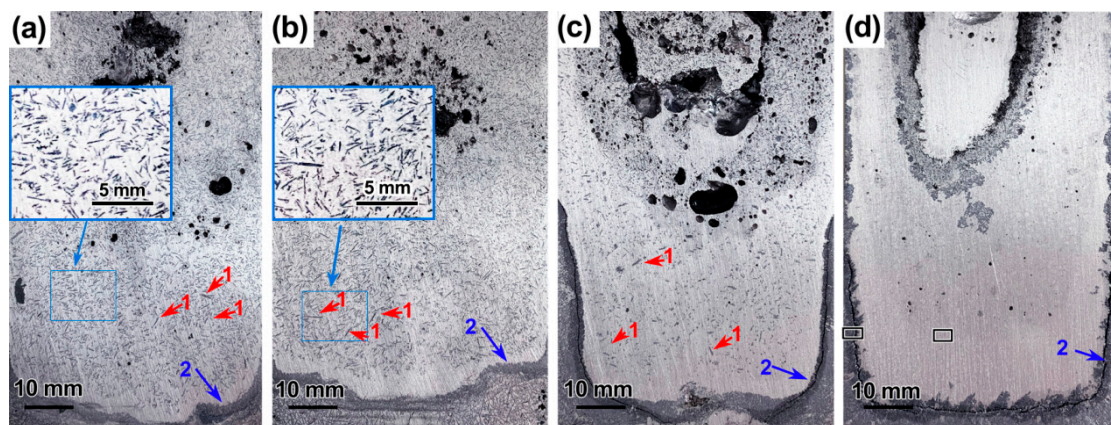


Figure 6. Vertical-sections of Al-30Si alloys solidified by starting RMF at temperatures of (a) 700 °C, (b) 730 °C, (c) 760 °C, (d) 790 °C.

To reveal the electromagnetic separation process for primary Si, the microstructures of the Si-rich layer and the Si-poor region of the Al-30Si alloy with the best separation condition were observed (marked in Figure 6d), and the results are shown in Figure 7. According to the morphological characteristics of primary Si (Figure 7a), the formation process for the Si-rich layer can be divided into three stages: segregation growth, continuous growth and merger growth. First, driven by the temperature gradient, the primary Si particles grew in parallel in close proximity to each other based on the inner wall surface of the graphite crucible (Figure 7a(I)). Then, the primary Si phases grew continuously and intertwined into a network-like structure by absorbing Si atoms from the melt. The eutectic Al-Si structure was distributed in the inter-network region of primary Si (Figure 7a(II)). As the electromagnetic stirring progressed, the primary Si phases interconnected with each other more obviously, and the volume fraction of the eutectic Al-Si structure in this area was dramatically decreased (Figure 7a(III)). Apparently, the centrifugal extrusion generated by the RMF was important for increasing the mass fraction of primary Si in the Si-rich layer, which was measured in the range of 65–70 wt.% when the magnetic intensity was maintained at 25 mT. Figure 7b reveals that the Si-poor region of the ingot was mainly composed of the eutectic Al-Si structure, and no primary Si could be found in this area. This finding indicated that the electromagnetic separation limit for primary Si was reached when the content of Si atoms in the Al-Si melt was reduced to the eutectic composition.

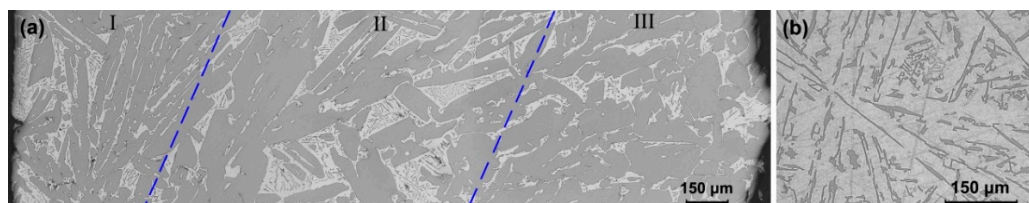


Figure 7. Microstructures of (a) the Si-rich layer and (b) the Si-poor region of the Al-30Si alloy under the best separation condition.

3.2.2. Electromagnetic Separation Mechanism of Primary Si

According to the above analysis, the electromagnetic separation of primary Si involves a complex coupling growth process based on the temperature field, flow field, and solute distribution. Figure 8 shows a schematic diagram of the electromagnetic segregation process for primary Si under the coupling effect of a temperature gradient and electromagnetic stirring. When the RMF is turned on, the liquid metal is driven by virtue of the azimuthal Lorentz force induced, which leads to the formation of a swirling flow in the azimuthal direction. Then a secondary flow in the meridional plane appears, resulting from the imbalance between centrifugal force and radial pressure gradient (Figure 8a). Although the secondary flow condition is relatively weak, comprising only approximately 30% of the primary flow condition [32], it plays an important role in improving the transport of the solute atoms in the axial direction of the Al-Si melt. With cooling proceeding, the heat preferentially escapes through the bottom of the crucible, and thereby, the temperature gradient in the Al-30Si melt is formed. The establishment of this temperature gradient provides a priority nucleation zone for separating primary Si. The Si crystals are pre-nucleated near the bottom of the melt because the temperature there is lower (Figure 8b). Then, the secondary flow promotes continuously the growth of the pre-nucleated Si crystals by absorbing Si atoms from the bulk Al-Si melt, finally resulting in the macro-segregation of primary Si (Figure 8c). When the content of Si atoms in the melt is reduced to the eutectic composition, the separation process reaches the limitation to form a Si-rich layer (Figure 8d). As the solidification progresses, the additional pressure on the inner wall caused by the swirling flow compresses the Si-rich layer and further crowds out the Al-rich melt from the inter-network region of primary Si, thus increasing the density of the primary Si within the Si-rich layer.

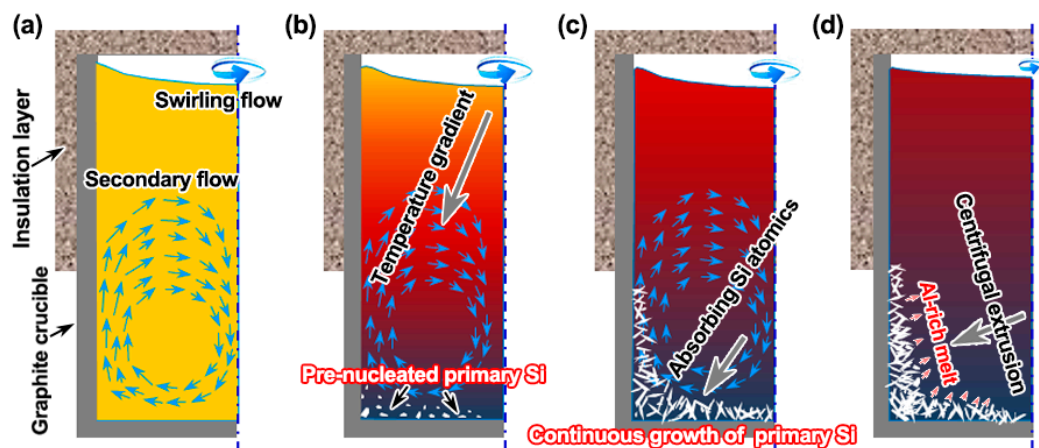


Figure 8. Schematic diagram of the electromagnetic segregation process of primary Si: (a) characteristics of flow pattern, (b) nucleation stage of Si crystals, (c) continuous growth stage of primary Si, (d) merger formation stage of Si-rich layer.

3.3. Application Exploration of Electromagnetic Separation of Primary Si

3.3.1. The Preparation of In-Situ Particle Reinforced Al-Base Gradient Composites

From the perspective of the structural design of composite materials [33], if the primary Si that serves as a hard phase can be directionally separated to form a gradient structure with a Si-rich/Si-poor layer, different sides of the materials can present different functions. On the basis of a full understanding of the electromagnetic separation mechanism, the hypereutectic Al-18Si in-situ graded gear reinforced with primary Si particles was fabricated successfully by controlling the coupling between the temperature field and the electromagnetic field (Figure 9a). An analysis of the microstructures revealed that the Si-rich outer layer was formed with a high mass fraction of primary Si; the Si-poor inside region was mainly composed of the Al-Si eutectic structure (Figure 9b). The properties of the Si-rich layer and Si-poor region were characterized (as marked by the positions 1~6 in Figure 9a), and the results are shown in Figure 9c. It was clear that the distribution of the hardness presented a step-like feature between the Si-rich outer layer and the Si-poor inside region. The hardness of the Si-rich layer was approximately 200 Hv higher than that of the Si-poor region. The primary Si-rich outer layer, which has a higher hardness, as the tooth of the gear, can effectively enhance the wear resistance. Meanwhile, the eutectic Si-poor inside region can improve the impact resistance of the gear due to its good toughness. It is expected that this hypereutectic Al-Si composite material with a Si-rich layer/Si-poor region can be considered as a kind of designable graded gear, which has great potential for practical application in astronautics and aeronautics.

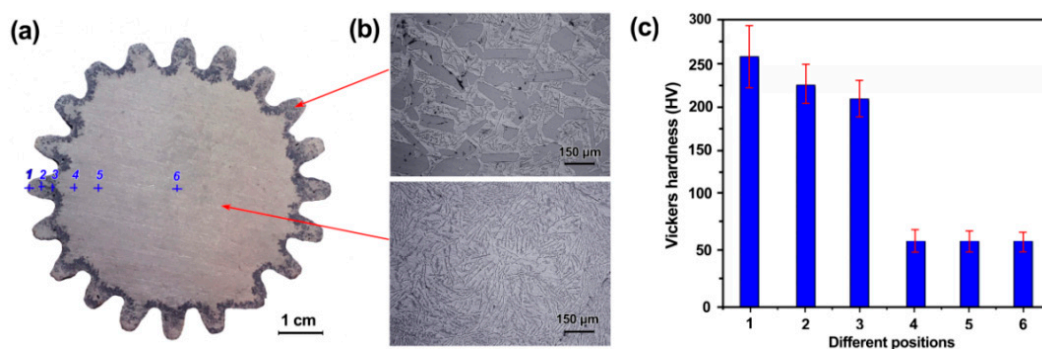


Figure 9. (a) Cross-section images of hypereutectic Al-18Si in-situ graded gear, (b) microstructures of the Si-poor region and the Si-rich layer, (c) Vickers hardness values for different positions.

3.3.2. The Purification of Metallurgical Grade Si

For upgrading MG-Si to solar-grade Si (SOG-Si), the solidification purification with the hypereutectic Al-Si alloy as a novel metallurgical process shows potential in the manufacture of low-cost and environmentally friendly silicon solar cells. In the solidification process of hypereutectic Al-Si alloys, the purification of Si crystals can be achieved by redistributing the impurity elements at the interfacial front of the primary Si/Al-Si melt. However, the primary Si is uniformly distributed in the entire ingot because the primary Si and the Al-Si melt have a similar density, which leads to the result that it is hard to collect the high-purity Si. Therefore, separating primary Si is the bottleneck restricting industrial applications.

To solve the above problem, we have developed an electromagnetic continuous separation technology of primary Si to realize the efficient collection of the high-purity Si [34]. The continuous growth of Si crystals was controlled by the RMF during semi-continuous casting of the hypereutectic Al-30Si alloy to achieve the efficient separation of primary Si (Figure 10a). The Si-rich layer was peeled from the periphery of the ingot, followed by acid leaching to collect the primary Si (Figure 10b). By applying the mass production advantage of the continuous separation technique, the primary Si was purified via multiple solidification purifying steps. The results of the sample for the purity test showed that the content of all impurity elements, except for Al, in the primary Si could be reduced to a solar-grade level by refining just three times (Figure 10c). A poly-crystalline Si ingot was prepared by smelting the primary Si crystals, which satisfied the purity requirement (Figure 10d). Table 2 gives the summary of the impurity removal effect by the traditional metallurgical method and continuous separation technique of primary Si. It can be clearly detected that the traditional metallurgical method needs to run through the coupling of three refining processes at five-step high temperatures (over 1500 °C) to gradually remove the metallic impurities, B, and P in the raw material MG-Si. Compared to the traditional metallurgical method, the continuous separation technique for primary Si was obviously superior in terms of cost and convenience, as it only needs to meet the requirements of SOG-Si by three times solidification at low temperatures (under 950 °C). Therefore, the continuous separation technique for primary Si is a possible energy-saving way to provide low-cost SOG-Si for the solar photovoltaic industry.

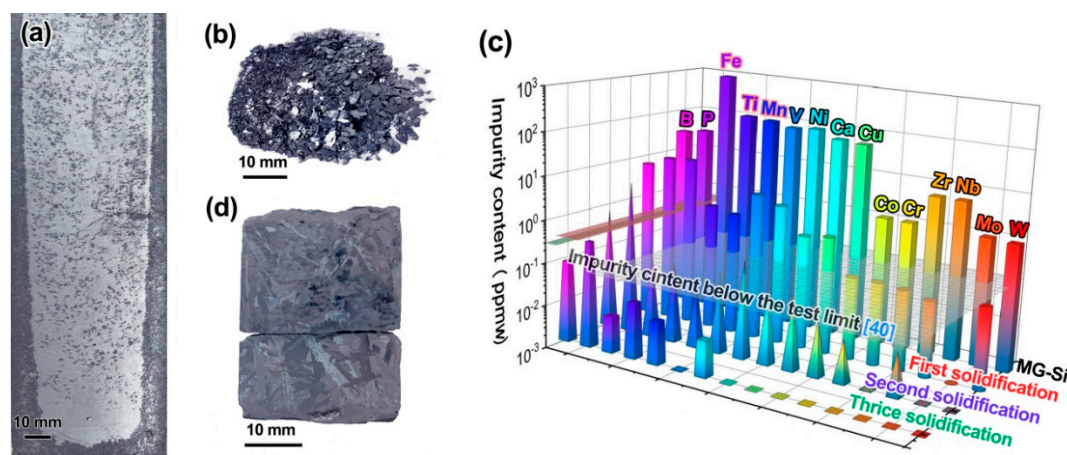


Figure 10. (a) Vertical section of Al-30Si alloy prepared by the continuous separation technique, (b) image of the collected primary Si particles, (c) impurity contents in the primary Si after each solidification purifying, (d) poly-crystalline Si ingot.

Table 2. The summary of the impurity removal effect by the traditional metallurgical method and continuous separation technique of primary Si.

	Purification Method	Purification Process	Objective/ppmw [35]	Impurity Contents in Si after Each Refining/ppmw			Rf.
				Once	Twice	Thrice	
Traditional metallurgical process	First step: Slag refining to remove B	Na ₂ O-SiO ₂ , temperature: 1700 °C, 30 min	<0.3	24 → 0.8	0.8 → 0.4	0.4 → 0.1	[36]
		CaO-SiO ₂ -LiF, temperature: 1550 °C, 240 min		22 → 3.3			[37]
		CaO-SiO ₂ -Li ₂ O, temperature: 1550 °C, 240 min		24 → 3.6			
		CaF ₂ -Al ₂ O ₃ -CaO-SiO ₂ , temperature: 1800 °C, 240 min		25 → 5.1	5.1 → 2.6		[38]
	Second step: Vacuum plasma refining to remove P	Power: 200 kW	<0.5	25 → <0.1			[39]
		Vacuum degree: 10 ⁻² ~10 ⁻³ Pa, Power: 21 kW, 30 min		15 → <0.1			[40]
		Vacuum degree: 5 × 10 ⁻² Pa, Power: 30 kW, 30 min		33 → <0.1			
	Third step: Directional solidification to remove the metallic	Temperature: 1414 °C, Solidification rate: 0.6 mm/min	<0.1	Fe 2800 → 0.29 Ti 140 → <0.1			[41]
		Power: 600 kW, Solidification rate: 0.6 mm/min Power: 800 kW, Solidification rate: 0.18 mm/min		Fe 1000 → <10 Ti 200 → <10	Fe < 10 → <0.1 Ti < 10 → <0.1		[39]
In this work	Continuous separation technique of primary Si	Casting temperature: 950 °C Magnetic flux density: 35 mT Electromagnetic frequency: 50 Hz Casting speed: 50 mm/min	<0.3 <0.5 <0.1	B 21.2 → 4.3 P 38.5 → 11.2 Fe 987 → <10.6 Ti 110 → <1.3	4.3 → 0.8 11.2 → 3.8 10.6 → <0.1 1.3 → <0.1	0.8 → <0.1 3.8 → 0.3	

4. Conclusions

In the present work, the separation condition and morphological evolution for primary Si in the solidification of hypereutectic Al-Si alloy was investigated under electromagnetic stirring. The main results and conclusions can be summarized as follows:

1. The temperature field and fluid flow in the melt are two key points for controlling the segregation behavior of primary Si. The establishment of a temperature gradient in the Al-Si melt was determined to be a precondition for realizing the separation of primary Si. Electromagnetic stirring can further strengthen the separation effect of primary Si on the basis of the temperature gradient.
2. The formation of a Si-rich layer is based on the continuous growth of primary Si via the absorption of Si atoms from the Al-Si melt with the help of secondary flow. The Al-rich melt can be squeezed out in the Si-rich layer under the centrifugal effect of the primary flow, resulting in an increasing mass fraction of primary Si up to 65~70 wt.% under a magnetic intensity of 25 mT.
3. Based on an understanding of the separation mechanism, the segregation control of primary Si can be achieved successfully by coupling the temperature gradient and electromagnetic stirring. The separation technology for primary Si reported in this study not only presents a new design concept for hypereutectic Al-Si in-situ graded gears for the fields of astronautics and aeronautics, but also proposes a new energy-saving strategy to provide low-cost SOG-Si for the solar photovoltaic industry.

Author Contributions: Conceptualization, Q.Z. and J.J.; methodology, Q.Z., H.T. and C.S.; software, Q.Z., H.T. and C.S.; validation, Q.Z. and N.H.; investigation, Q.Z. and Z.Z.; resources, Q.Z. and N.H.; writing—original draft preparation, Q.Z.; writing—review and editing, Q.Z., X.A. and N.H.; funding acquisition, Q.Z. All authors have read and agreed to the published version of the manuscript.

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