

Article

Selection of Optimal Magnets for Traction Motors to Prevent Demagnetization

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Abstract: Currently, permanent-magnet-type traction motors drive most electric vehicles. However, the potential demagnetization of magnets in these motors limits the performance of an electric vehicle. It is well known that during severe duty, the magnets are demagnetized if they operate beyond a ‘knee point’ in the B(H) curve. We show herein that the classic knee point definition can degrade a magnet by up to 4 grades. To prevent consequent excessive loss in performance, this paper defines the knee point k as the point of intersection of the B(H) curve and a parallel line that limits the reduction in its residual flux density to 1%. We show that operating above such a knee point will not be demagnetizing the magnets. It will also prevent a magnet from degenerating to a lower grade. The flux density at such a knee point, termed *demag flux density*, characterizes the onset of demagnetization. It rightly reflects the value of a magnet, so can be used as a basis to price the magnets. Including such knee points in the purchase specifications also helps avoid the penalty of getting the performance of a low-grade magnet out of a high-grade magnet. It also facilitates an accurate demagnetization analysis of traction motors in the worst-case conditions.



Citation: Rao, D.; Bagianathan, M. Selection of Optimal Magnets for Traction Motors to Prevent Demagnetization. *Machines* **2021**, *9*, 124. <https://doi.org/10.3390/machines9060124>

Academic Editor: Antonio J. Marques Cardoso

Received: 20 May 2021
Accepted: 16 June 2021
Published: 20 June 2021

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Keywords: traction motors; electric vehicle (EV); permanent magnets; knee point; demagnetization curve; severe duty; short-circuit fault; IDF; magnetic field analysis; reversible segment; heat-resistant magnet

1. Introduction

At present, 80 to 90% of electric vehicles sold globally use permanent magnet (PM) type traction motors [1]. Rare-earth magnets are a critical but expensive component of all such applications. However, these magnets carry a demagnetization risk which can cause a permanent loss in the performance of the electric vehicle. Vehicle manufacturers recently recognized that such an irreversible demagnetization fault (IDF) is a major risk factor of PM motors [2–4]. This Achilles heel of PM motors prevents them from competing with the induction motors for applications such as pumps, fans, and compressors [5]. Therefore, engineers constantly seek approaches that minimize the demagnetization risk. This risk can occur during severe duties such as short-circuit, rapid acceleration from 0 to 60 mph, hill climbing, etc. Such worst cases or severe duties apply large demagnetizing fields on the magnets. Large fields that are beyond the capability of a magnet can cause excessive demagnetization. Thus, there is a fundamental need to define a proper metric to judge as to when an unacceptably large demagnetization occurs. In traction motors, this occurs at high temperatures, so it is sometimes called heat resistance.

The magnetic characteristics of a magnet are described by plots that show the variation of flux density B or J [tesla] with demagnetizing field H [kA/m]. They can be represented as a magnetic flux density B(H) curve or a ferric flux density J(H) curve. J is also known as polarization or intrinsic flux density. It is the magnetic flux density B less vacuum flux density $\mu_0 H$ where $\mu_0 = 4\pi \cdot 10^{-7}$ [N/A²] is the permeability of vacuum ($J \equiv B - \mu_0 H$).

Both curves have a ‘knee’ that joins a reversible line segment smoothly with an irreversible segment. On a J(H) curve, the knee will fall in the 2nd quadrant. On a B(H)

curve, for traction motors that operate at elevated temperatures, the knee will also fall in the 2nd quadrant. For others, it can fall in the 3rd quadrant, so it will require additional data. The knee signifies the transition to demagnetization.

A specific ‘knee point’ within a knee demarcates the change in the behavior of the magnet from a reversible state to an irreversibly demagnetized state. When a magnet operates above the ‘knee point’, it will return reversibly to its initial state, with no reduction in the residual flux density B_r [6–8]. However, operating below the knee point will cause it to return along a parallel path which will reduce the residual flux density to a smaller value B_r' . This reduction in residual flux density $\delta B_r = B_r - B_r'$ is known as a *demagnetization loss*, irreversible loss, or simply loss.

Such reduction in B_r requires more current to generate the same torque. This increases the copper loss, which increases the magnet temperature further, which in turn degrades the magnet more. The resulting vicious circle can cause a significant loss in the performance of the electric vehicle.

An unacceptably large demagnetization loss will push the operating point below the knee point, thereby causing an unacceptably large permanent reduction in the flux-producing capability of the magnet [8,9]. Since the flux density falls sharply as a waterfall beyond the knee, a minute increase in the demagnetizing field can drastically reduce the performance of a traction motor [9,10]. This can reduce the service life of the electric vehicle. In addition, replacing a demagnetized magnet in an electric vehicle is labor-intensive and very expensive. The resulting large downtime can even dissuade a consumer from using electric vehicles altogether.

The knee point thus plays a critical role in limiting the performance of an electric vehicle. It also characterizes IDF. Therefore, knowledge of the precise position of the knee point is critical for the selection of magnets in traction motors and to prevent IDF. The primary purpose of this paper is therefore to develop a well-defined method to locate the position of the knee point of a magnet on its $B(H)$ curve.

At present, different engineering communities seem to have different views of the location of the knee point. To distinguish them, we label them as:

- Classic knee point K ;
- Knee endpoint k' .

Classic knee point K —The magnet material engineers (who develop/test magnets) use the $J(H)$ curve to define the classic knee point K . They define K as the point on the $J(H)$ curve that permits 10% B_r demagnetization loss. (In the 1960s, up to 20% loss was considered acceptable [11,12]). Their metric for demagnetization is the respective field H_K .

Historically, in the 1980s, material engineers used such H_K to indicate magnets with fewer defects [13,14]. A $J(H)$ curve that is closest to the largest rectangle $B_r H_{cJ}$ is deemed to have the least defects (H_{cJ} = coercivity on the $J(H)$ curve). They used the ‘loop squareness’ H_K/H_{cJ} [15,16] as a metric to develop better compositions that yielded magnets with the fewest defects [17,18].

In the 1990s, they used the same H_K to define the acceptable limit on the demagnetization loss [19–21]. Initially, they presumed that the linear segment of $J(H)$ of rare-earths to be nearly horizontal. Therefore, they defined the classic knee point K as the point on the $J(H)$ curve where it intersects a horizontal line that passes through the $0.9 \cdot B_r$ point [22–24]. However, the linear segment is slightly inclined [25,26]. Therefore, later Gaster [27,28] redefined it as the point on the $J(H)$ where it intersects a parallel inclined line that passes through the $0.9 \cdot B_r$ point. Both definitions indicate that the material engineers considered the 10% reduction in B_r to be acceptable.

Material engineers widely consider that coercivity H_{cJ} is the metric for the demagnetizability of a magnet. However, in 2008, Trout [29] wrote that the ‘(classic) knee point field H_K may be a better figure of merit’ (than coercivity H_{cJ}) or better metric for the onset of demagnetization. Since then, all commercial $B(H)$ measurement systems are programmed to list this H_K [30–33]. Currently, manufacturers use this H_K in purchase specifications as a basis to negotiate the price of the magnets. However, over the past 10 years, tremendous

improvements enabled the manufacturers to make superior magnets to tighter tolerances. Modern magnets, therefore, require a better metric with a tighter tolerance than the 10% loss allowed by H_K .

Knee endpoint k' —The motor design engineers (who select and size the magnets for traction motors), on the other hand, rely on the Maxwell laws-based magnetic field software for the detailed design of traction motors [34–36]. Such software uses the $B(H)$ curve rather than the $J(H)$ curve. Therefore, these engineers rely on the $B(H)$ curve to define the knee endpoint k' . They define it as one where the knee on the $B(H)$ curve starts deviating from a straight line to a curve [37].

Their metric for demagnetization is the knee endpoint flux density $B_{k'}$. Motors subject the magnets to nonuniform fields, so the demagnetized volumes (where the flux density is less than the knee endpoint flux density $B_{k'}$) are local at the edges or center of magnets. The motor design engineers rely on $B_{k'}$ to estimate the demagnetized volume fraction V_d [38–42], which is then used to limit the loss in performance caused by the demagnetization of the magnets.

1.1. Difference between K, k'

The following examples illustrate that these prior-art knee points K, k' differ significantly.

Figure 1a displays the demagnetization curves for Arnold's N38UH grade at 180 °C [43]. It shows that the classic knee point K lies close to the irreversible segment, while the knee endpoint k' lies close to its reversible segment. Specifically, the classic knee point flux density B_K (0.25 T) is ~30% lower than the knee endpoint flux density $B_{k'}$ (0.37 T). It shows that the classic knee point field H_K (−517.2 kA/m) is numerically 9% higher than that $H_{k'}$ at the knee endpoint (−475 kA/m).

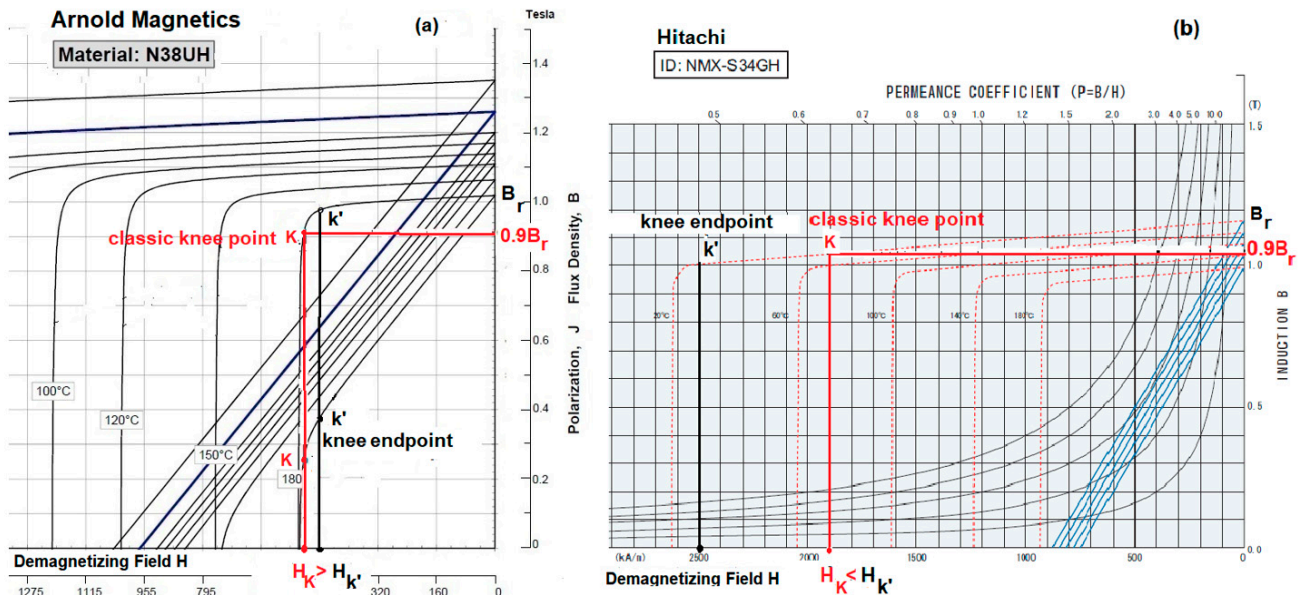


Figure 1. (a) For Arnold's N38UH, the knee flux densities $B_{k'}$, B_K differ by ~50%. (b) For Hitachi's NMX-S34GH, the knee fields $H_{k'}$, H_K differ by 30%. Therefore, the knee endpoint k' differs significantly from the classic knee point K .

As indicated earlier, at present engineers tie the price of the magnet to the field H_K at the classic knee point. The higher this H_K , the higher the price. However, Figure 1a demonstrates that, by specifying H_K as the basis to price magnets, a buyer is paying a significant, but spurious 9% higher price for a magnet.

Figure 1b displays the demagnetization curves for Hitachi's NMX-N34GH [44]. It shows that (for the 20 °C curves) the classic knee point K lies far inside the reversible

segment, while the knee endpoint k' lies close to the knee. Moreover, it shows that the classic knee point field H_K (-1900 kA/m) is 30% (numerically) smaller than the knee endpoint field $H_{k'}$ (-2500 kA/m).

Figure 2 displays Innuovo's N48UH at 180°C [45]. As shown, the manufacturer lists the classic knee point field H_K as -6.583 kOe ($= -524$ kA/m). However, its knee endpoint field $H_{k'}$ of -495.5 kA/m is 5.4% lower. This again demonstrates that using the classic knee point K to price magnets, a buyer is paying a significant, but spurious 5.4% higher cost for the magnet.

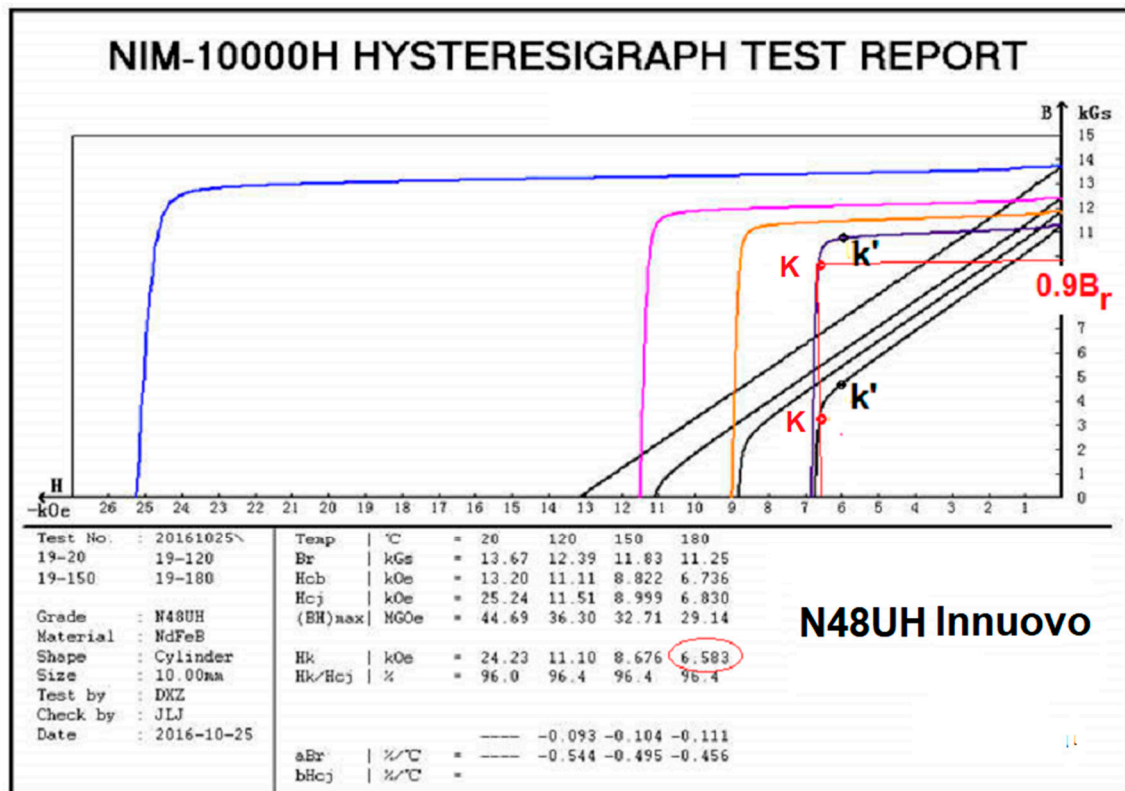


Figure 2. For Innuovo's N48UH grade, the classic knee point K lies inside the nonlinear segment. Therefore, a minute decrease in H can result in a sharp fall in the flux density.

This plot also shows that its classic knee point K lies in the irreversible waterfall segment. Therefore, even a minute reduction in H will cause the flux density to fall sharply, thereby resulting in severe demagnetization. Moreover, it shows that its 0.32 T classic knee point flux density B_K is 40% lower than the 0.45 T knee endpoint flux density $B_{k'}$.

All these examples confirm that the classic knee point K does not adequately represent the onset of demagnetization or value of a magnet. Moreover, it can be significantly different from the knee endpoint k' . So, from now onwards, we focus on the knee endpoint as it signals the onset of demagnetization better.

1.2. Manual Method to Locate k'

At present, a precise method to locate k' is not available. The motor designers locate the knee endpoint k' on a $B(H)$ curve by a manual method, i.e., visually judging where the straight-line possibly 'ends' [46–50]. However, where exactly the knee 'ends' depends on the intuitive judgment of the person who picks it. For example, in Hitachi's NMX-36EH at 180°C , Choi [39] picked 0.14 T as the knee endpoint. However, actually, it is ~ 0.2 T—a 25% error.

Figure 3 shows that, for the HPMG N42UH grade at 150°C [51], one engineer may pick point k_1' , while another may pick point k_2' . However, their flux densities are 0.21 and

0.31 T, respectively—a 50% error. These examples illustrate that the manual method of locating the knee endpoint k' is imprecise and prone to significant errors.

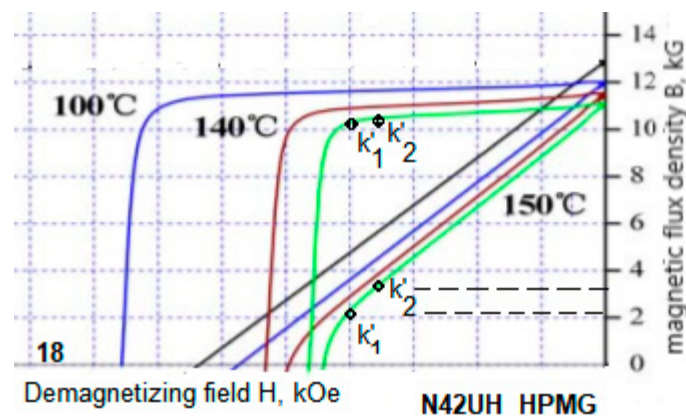


Figure 3. Manually picked knee endpoints k'_1 and k'_2 can differ by 50%.

1.3. Other Prior Methods to Locate k'

To define the starting point of demagnetization more precisely, over the past 20 years, several experts strived to devise various non-manual methods, but they fell short of expectations as discussed below.

By fitting a single model. These methods fit the entire $B(H)$ data to a simple function, such as a hyperbola [52], arctan, tanh [53–57], coth [8], exponential [56], polynomial [58], or splines [59]. Over the past century, scores of attempts have been made to model the $B(H)$ curves accurately [60]. However, most $B(H)$ models are known to suffer from significant errors [59,61,62]. In addition, Peng [10] found that the k' predicted by the tanh model differs significantly from that of tests. Moreover, fitting a single model does not locate k' anyway. Due to all these considerations, the single model methods have not gained traction.

By fitting two models. These methods split the data into several segments. It fits one segment of data to a 'straight-line model' function and another segment to a 'knee model' function. Then, it determines k' as the point of intersection of both. Several experts have employed diverse knee-models, e.g., arc of circle [61], exponential [6,7,62,63] or rational fraction [64]. However, the knee is so narrow that one usually can capture 2 to 4 data points at most [41]. Hence, fitting a knee model to so few data points can result in large errors [6,7]. For example, the Neo Grade 3512 at 160 °C, [7] showed that fitting the exponent model resulted in a 30% error. Therefore, these methods have also not gained traction.

Therefore, this prior-art review indicates so far that there has been no satisfactory method that can determine the knee endpoint precisely [65]. Thus, there is still a need to develop a method to precisely locate this critical point, called simply *knee point k* from now onwards. To achieve this, we first introduce the concept of *degeneration*.

2. Knee Point k

Degeneration is the phenomenon in which a higher grade magnet gets so demagnetized during the operation that its residual flux density degrades to that of a lower grade magnet. Once degenerated, a high-grade magnet behaves as a lower-grade magnet over its entire life. As a result, a degenerated magnet reduces the torque capacity of the motor permanently, thereby causing severe degradation of the performance of an electric vehicle forever.

Higher-grade magnets are very expensive. Their *degeneration* means that the extra dollars spent in buying the higher grade are wasted—it does not deliver the superior performance expected from the higher grade. To avoid such waste of money, one must make every effort to prevent degeneration.

To this end, we propose herein the *knee point k* as the point which prevents a magnet from *degenerating* to a lower grade. Operating above such knee point k will prevent an

expensive high-grade from delivering the performance of a lower-grade magnet. We detail below an optimal method to determine this knee point k .

2.1. Offset Method

It is well known that, for metals, the stress-strain curve comprises linear (elastic) and nonlinear (inelastic) segments. A century ago, engineers faced the challenge of defining the ‘knee point’ of metals that demarcates the inelastic segment. They resolved it by creating the *offset method*. As shown in Figure 4b, this method defines a *yield point* Y as the point of intersection of the stress-strain curve and a parallel straight-line that is offset by a small but acceptable 0.2% strain. Yield strength is the stress at such yield point Y . The stress-strain curve above Y demarcates the inelastic segment.

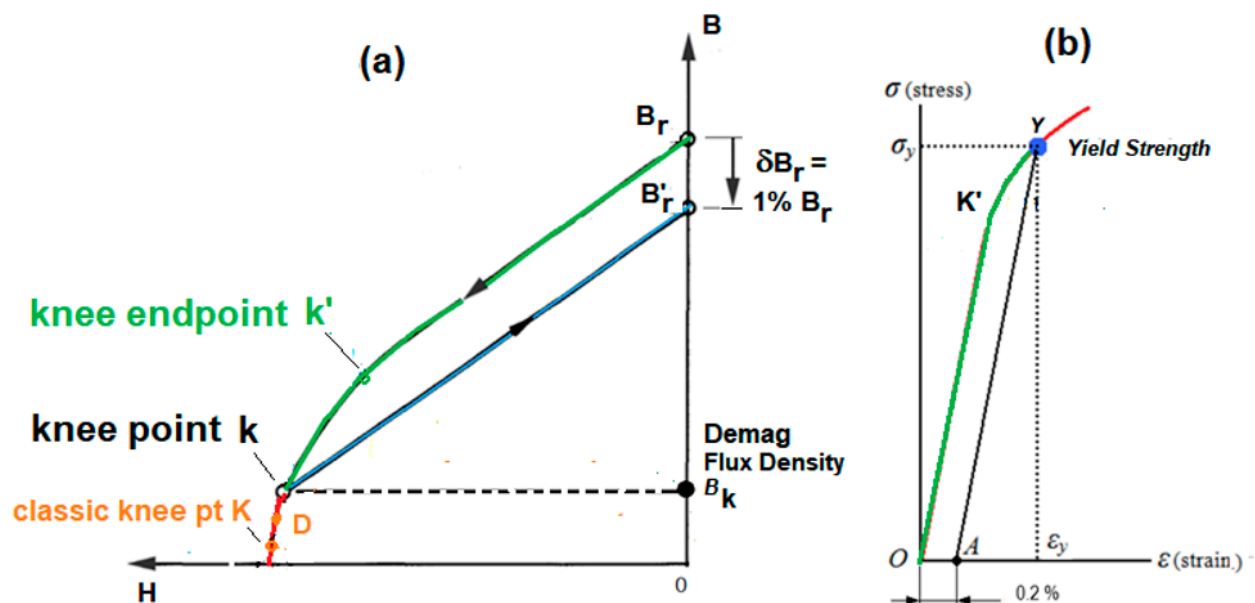


Figure 4. (a) Knee point k defined by the 1% offset method prevents the degeneration of a magnet. (b) Yield strength defined by the 0.2% offset method prevents the metal from going plastic.

In 1924, ASTM adopted this as the standard method to compute the yield strength. It codified this method in its Standard E8 [66]. Such a codified offset method is now universally used to quantify the strength of steels. Over the past 100 years, engineers relied on it to protect thousands of bridges and buildings against the inelastic behavior of steel.

Figure 4a shows that the $B(H)$ curve of magnets is strikingly similar to the stress-strain curve of metals shown in Figure 4b. The offset method—which was used for years to protect against the yielding of metals—thus can also be used to protect against the demagnetization of magnets.

We define the *knee point* k as the point of intersection of the $B(H)$ curve and a parallel straight-line that is offset by a small but acceptable demagnetization loss. To define it precisely, one has to specify as to what is an acceptable loss. As already indicated, the return path reduces the magnet’s residual flux density from B_r to a smaller B_r' . The reduction $\delta B_r = B_r - B_r'$ is called demagnetization loss. Alternately, we reformulate it as *offset* $x = \delta B_r / B_r$ (expressed as a percentage). Then, defining k amounts to specifying x .

2.2. Options for Offset x

Figure 4a displays knee point k as well as all prior-art knee points K , k' , and D (not to scale). We demonstrate herein how prior-art definitions of knee point are inadequate in protecting magnets against degeneration.

- *10% offset (K)*. This classic knee point K was proposed in the 1990s by magnet material engineers [20] as one that tolerates 10% B_r loss. However, consider the N40UH grade with B_r of 1.29 T. A 10% loss reduces it to B_r' of 1.16 T. Table 1 below shows that this is the B_r for N33UH, which is three grades below N40UH. Thus, operating at the classic knee point K degenerates a magnet forever to a lower grade, so is unacceptable.
- *5% offset (D)*. This demagnetization point D was suggested in IEC 60404-8-1 [25,67] as one that tolerates 5% B_r loss. However, consider the N50H magnet with B_r of 1.40 T. A 5% loss reduces it to B_r' of 1.33 T. Table 1 shows that this is the B_r for N42H, which is three grades below N50H. Thus, operating at the demag point D degenerates a magnet forever to a lower grade, so is unacceptable.
- *2% offset*. This does not degenerate some magnets (for example, it reduces the 1.25 T B_r of N35UH to 1.226 T. It is larger than the 1.15 T B_r for a lower grade N33UH. Therefore, it will not degenerate this magnet). However, consider N52H with B_r of 1.42 T. The 2% loss reduces it to B_r' of 1.39 T. This is B_r for N50H, which is one grade below N52H. Thus, operating at this 2% loss the knee point can degenerate some magnets forever to a lower grade, so is unacceptable.
- *0.5% offset*. This also does not degenerate a magnet, so it may seem to be acceptable. However, for N28EH with B_r of 1.05 T, it amounts to 0.005 T, which is close to the measurement noise floor. However, at present, manufacturing a grade to such tight tolerances is nearly impossible. Specifying such tight tolerance will only increase their cost. Furthermore, tests by Allcock [68] revealed that most magnets suffer from a 0.4% B_r long-term irreversible loss (LTIL). Therefore, specifying a 0.5% offset is unacceptable.

2.3. Rationale for 1% Offset

In this section, we present additional rationale to show that a 1% offset is the best option to define the knee point.

2.4. Grade Spacing

The standards subdivide the Neo magnets into about 10 grades. The B_r of the lowest/highest grade N28/N55 is 1/1.5 T. Therefore, as one changes from the lowest grade to the highest, B_r increases by 0.5 T. Since 10 grades fit into this 0.5 T span, they are spaced at about 0.05 T.

Table 1 below shows the spacing of conventional grades in greater detail. (It excludes the recent dysprosium-free ‘case hardened’ magnets which concentrate neodymium on the surface and refine the grain to reduce cost [69]). It shows that the grades in the 30–40 MGOe range are spaced at 0.05 T, while those in the 40–54 MGOe range are spaced at ~0.02 T. Thus, the smallest grade spacing is 0.02 T.

Therefore, to prevent a magnet from degenerating to a lower grade, the x% loss must be smaller than this smallest grade spacing of 0.02 T. Note that 0.02 T is 1.3% (~1%) of the largest B_r of 1.5 T. Therefore, x = 1% offset is the best option to define the knee point k that prevents degeneration of a magnet to a lower grade.

2.5. Example

Figure 5a shows the B(H) curve and the return path (blue line) of grade N50H at its *knee point k*. In it, the red dotted line refers to the B(H) curve of the next lower grade N48H. It shows that the blue line is *above* the red dotted line. This indicates that, during the return path, the N50H residual flux density reduces from B_r of 1.247 T to B_r' of 1.234 T. However, this is still greater than the 1.222 T residual flux density of the lower grade N48H. This establishes that operating a magnet up to its *knee point k* **will not degenerate** it to a lower grade.

Table 1. Conventional grades of neodymium magnets and their residual flux densities B_r .

B_r tesla	1.05	1.10	1.15	1.20	1.25	1.29	1.32	1.35	1.38	1.40	1.42	1.45	1.49	Max Temp deg C
Label	GRADES													
AH	28AH	30AH	33AH	35AH	38AH	40AH								230
EH	28EH	30EH	33EH	35EH	38EH	40EH	42EH	45EH						200
UH		30UH	33UH	35UH	38UH	40UH	42UH	45UH	48UH	50UH	52UH	54UH		180
SH		30SH	33SH	35SH	38SH	40SH	42SH	45SH	48SH	50SH	52SH			150
H		30H	33H	35H	38H	40H	42H	45H	48H	50H	52H			120
M		30M	33M	35M	38M	40M	42M	45M	48M	50M	52M			100
		N30	N33	N35	N38	N40	N42	N45	N48	N50	N52	N54	N55	80
BHmax	28	30	33	35	38	40	42	45	48	50	52	54	55	MGOe

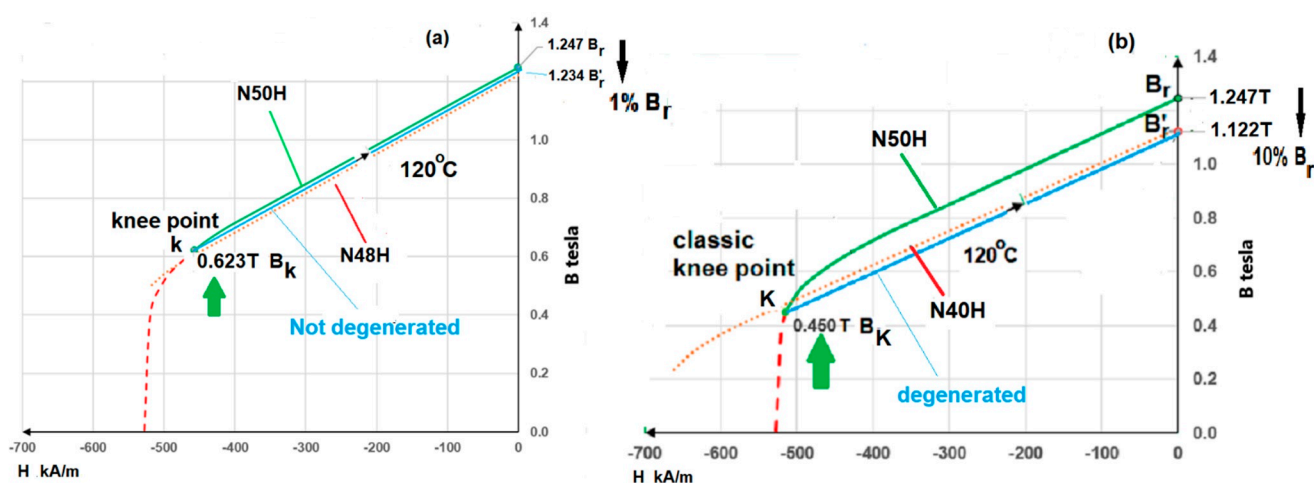
**Figure 5.** (a) The *knee point* k will not degenerate the magnet to a lower grade. (b) The *classic knee point* K will degenerate the magnet to a four grades lower magnet.

Figure 5b shows the $B(H)$ curve and the return path (blue line) of the same grade N50H, but now operating at its *classic knee point* K. In it, the red dotted line refers to the $B(H)$ curve of N40H, which is four grades lower. It shows that the return blue line is *below* the red dotted line. This indicates that, during the return path, the N50H residual flux density now reduces from B_r of 1.247 T to B_r' of 1.122 T. This is less than the 1.134 T residual flux density of N40H. This establishes that operating a magnet up to its *classic knee point* K *will degenerate* it to a lower grade.

3. Demag Flux Density

To prevent confusion, we rename the flux density B_k at the knee point k as the demagnetization flux density or simply *demag flux density* herein. B_k signals the onset of excessive demagnetization of magnets. It is similar to that of yield strength σ_y —which signals the onset of plastic or yielding of metals. Therefore, it is a key property of magnets.

Figure 6 shows a simplified representation of the demagnetization curves of a magnet (for Arnold's N52M grade) [70]. It highlights that the residual flux density B_r and the demag flux density B_k define the usable segment (green) of a magnet. It also shows that, with increasing temperature, B_k increases sharply while B_r decreases mildly. Therefore, the rate at which a magnet's usable range narrows with temperature is defined more by B_k than B_r . This confirms that B_k is a key property of the magnet. Such a clutter-free

demagnetization plot often provides a better insight as to how temperature impacts the usable range (conventional demagnetization curves cluster $B(H)$ curves with $J(H)$ curves, obscuring the usable range, see Figures 1–3).

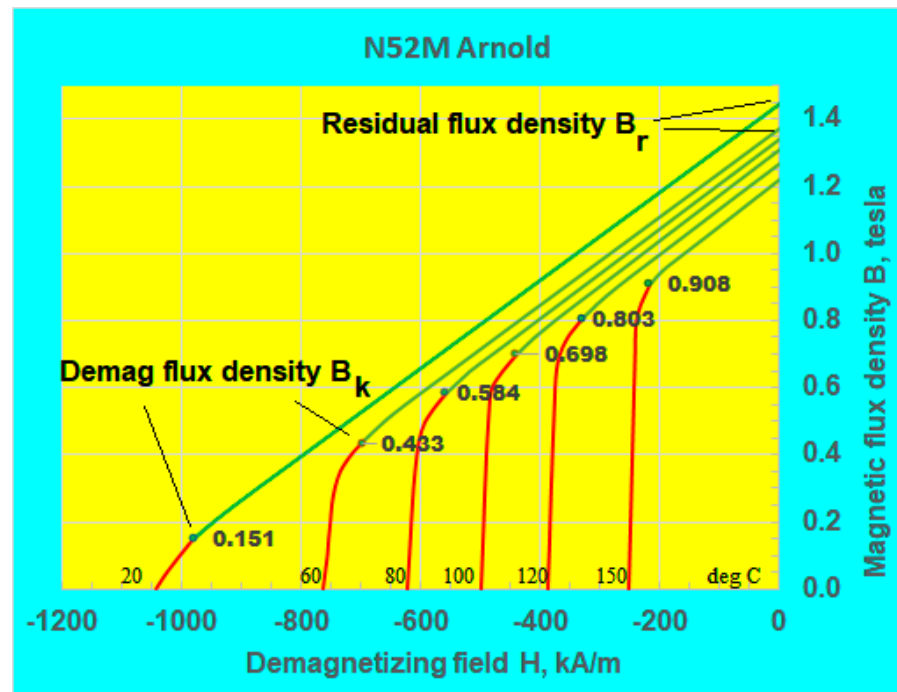


Figure 6. Simplified representation of the demagnetization curves for magnets.

At present, all manufacturers of steel list the yield strength of all metals they produce. Similarly, it is hoped that all manufacturers of magnets will list the demag flux density B_k for their magnets. Just as the ASTM E8 spec helped widespread use of ‘yield strength’ σ_y , incorporating the ‘demag flux density’ B_k into international standards will enable its widespread use.

The key properties (B_r , B_k) characterize the torque capability and heat resistance of the magnet, respectively. These metrics are valued by a motor designer. Therefore, they form the optimal cost basis for magnets.

Currently, engineers manually use the read B_k to compute the demagnetized volume fraction. However, as already shown, such manually read values can be imprecise. Instead, using the demag flux density B_k determined by the 1% offset method proposed herein will avoid such errors, resulting in more precise demagnetized volume fractions.

The demag flux density definition presented herein helps designers find an optimum tradeoff between performance degradation and the cost of the magnet. It is a better cost metric than H_k (as B changes more rapidly than H in the knee). The *eDrive systems* by Magna Motors utilize it in their design, thereby resulting in a less expensive and more reliable drive system for future transportation mass market.

Recently, a new and comprehensive magnet property database by Rao [70] listed the coordinates (H_k , B_k) of the knee point k for all magnets produced worldwide. The demag flux density B_k included therein simplifies the task of accurate estimation of demagnetized volume fractions to limit performance degradation of electric vehicles.

The demag flux density maps presented in the next section allow one to examine how B_k varies with temperature and grade. This, in turn, shortens the process of selection of an optimal magnet that meets specific severe-duty performance requirements of electric vehicles.

4. Demag Flux Density Map

A *demag flux density map* displays the demag flux density B_k of all grades and temperatures. Figure 7 shows such a map for a specific manufacturer, over 120 to 180 °C. The grade corresponding to a point can be read off from Table 1. For example, the N33M-N52M curve has 9 points ranging from N33M to N52M, the 7th point refers to N48M, and its B_k at 120 and 150 °C is 0.7 and 0.85 T. Note that some curves are non-monotonic. This may be due to irregular grade spacing, inherent measurement noise, manufacturer variations, etc., which will be investigated in the future.

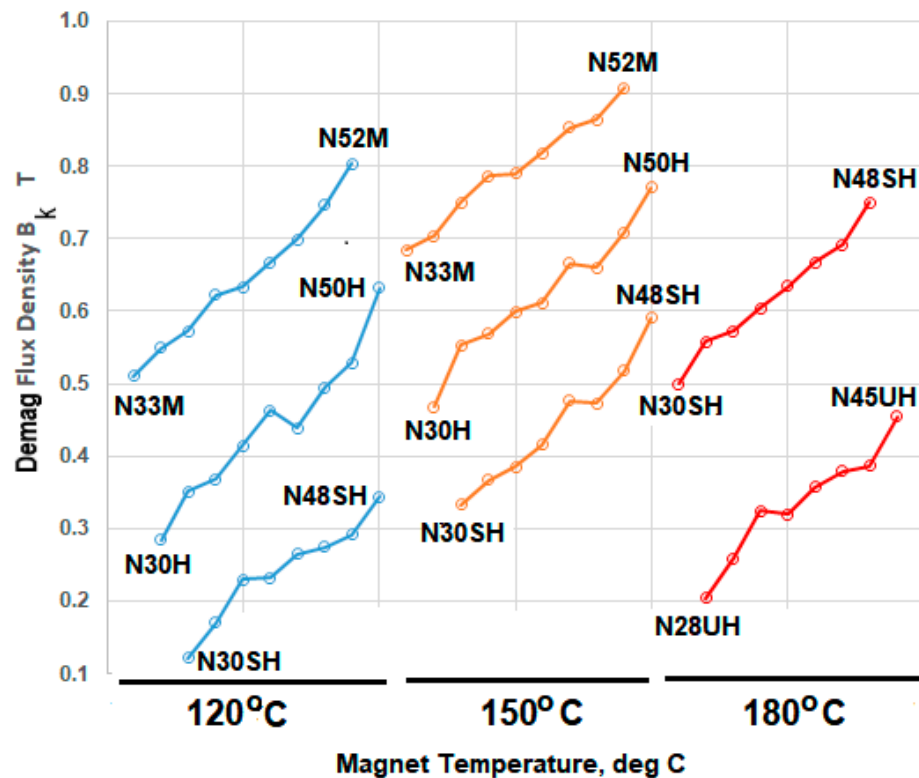


Figure 7. Demag flux density map for all grades over a typical usable temperature range.

Such a plot can be used to determine the demag flux density offered by any grade at a specific temperature of interest. For example, it shows that N30SH offers a demag flux density of 0.32 T at 150 °C. It shows that a typical 0.7 T B_k requirement is met by the N48M grade at 120 °C or the N35M grade at 150 °C.

Such a plot can also be used to reduce the cost of magnets. For example, it shows that, by reducing the magnet temperature from 180 to 150 °C, one can replace an expensive N42UH grade with a less expensive N35SH grade. Both magnets have the demag flux density B_k of 0.38 T, which indicates that both deliver the same severe-duty performance. Therefore, this plot demonstrates how cooling a magnet can save significant costs of magnets.

5. Conclusions

It is well known that, at high temperatures, rare earth magnets will be demagnetized excessively if operated below a knee point on the $B(H)$ curve. In this paper, we define the knee point k as one where the $B(H)$ curve intersects with a parallel line that is offset by 1% B_r . We showed herein that operating above such knee point k protects it from degenerating to a lower grade forever. The paper, therefore, recommends using this newly defined knee point k to prevent the degradation of magnets to a lower grade when simulating the

severe-duty short circuit performance of traction motors. Data on this knee point k are available in the comprehensive PMAG database recently developed by MagWeb.

The respective demag flux density B_k is a key property of a magnet that signals the onset of excessive demagnetization. Listing it by manufacturers or incorporating it into international standards will help engineers better protect the magnets from degrading to a lower grade during the operation. Moreover, it helps them discover the right manufacturer who offers a better grade (with an optimal demag flux density B_k) for their application and cost reference. This helps in the selection of optimal magnets for traction motors in electric vehicles.

At present, the classic knee point field H_K of a magnet (on a $J(H)$ curve where a magnet can lose 10% Br) is popularly used to negotiate the price of the magnets. This paper, however, shows that this metric can overprice a magnet. Instead, it shows that the demag flux density B_k of a magnet (at the operating temperature) is a better cost metric as it prevents a magnet from degenerating to a lower grade. Using B_k rather than H_K (to price the magnets) would be a milestone for future procurement strategies and the specification of magnets for traction motors in electric vehicles.

Author Contributions: Conceptualization, D.R.; methodology, M.B.; validation, M.B.; formal analysis, D.R.; investigation, D.R.; resources, D.R. writing—original draft preparation, D.R.; writing—review and editing, M.B.; visualization, supervision and project administration, D.R.; All authors have read and agreed to the published version of the manuscript.

Funding: This research received no external funding in conducting this research.

Institutional Review Board Statement: Not applicable.

Informed Consent Statement: Not applicable.

Data Availability Statement: Not applicable.

Conflicts of Interest: The authors declare no conflict of interest.

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