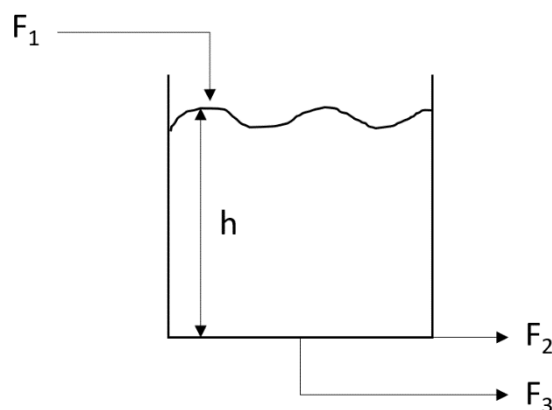


# Tank Network Model Development and Implementation

The tank network model was developed by performing a mass balance around a tank, and extending that to all the tanks in the network. The symbols used in the model development correspond to those in Figure S1.



**Figure S1.** Diagram with symbols corresponding to one-tank model development.

$$\frac{dm}{dt} = \rho(F_1 - F_2 - F_3) \quad (S1)$$

Assume the fluid is incompressible, so the density is constant.

$$\frac{dV}{dt} = F_1 - F_2 - F_3 \quad (S2)$$

$$\frac{d(Ah)}{dt} = F_1 - F_2 - F_3 \quad (S3)$$

Since the cross-sectional area  $A$  remains constant:

$$\frac{dh}{dt} = \frac{F_1 - F_2 - F_3}{A} \quad (S4)$$

Divide by the maximum height possible in the tank  $H_{max}$  to obtain the tank height as a fraction of its total:

$$\frac{d\left(\frac{h}{H_{max}}\right)}{dt} = \frac{F_1 - F_2 - F_3}{AH_{max}} \quad (S5)$$

$$\frac{dh_{frac}}{dt} = \frac{F_1 - F_2 - F_3}{V_{max}} \quad (S6)$$

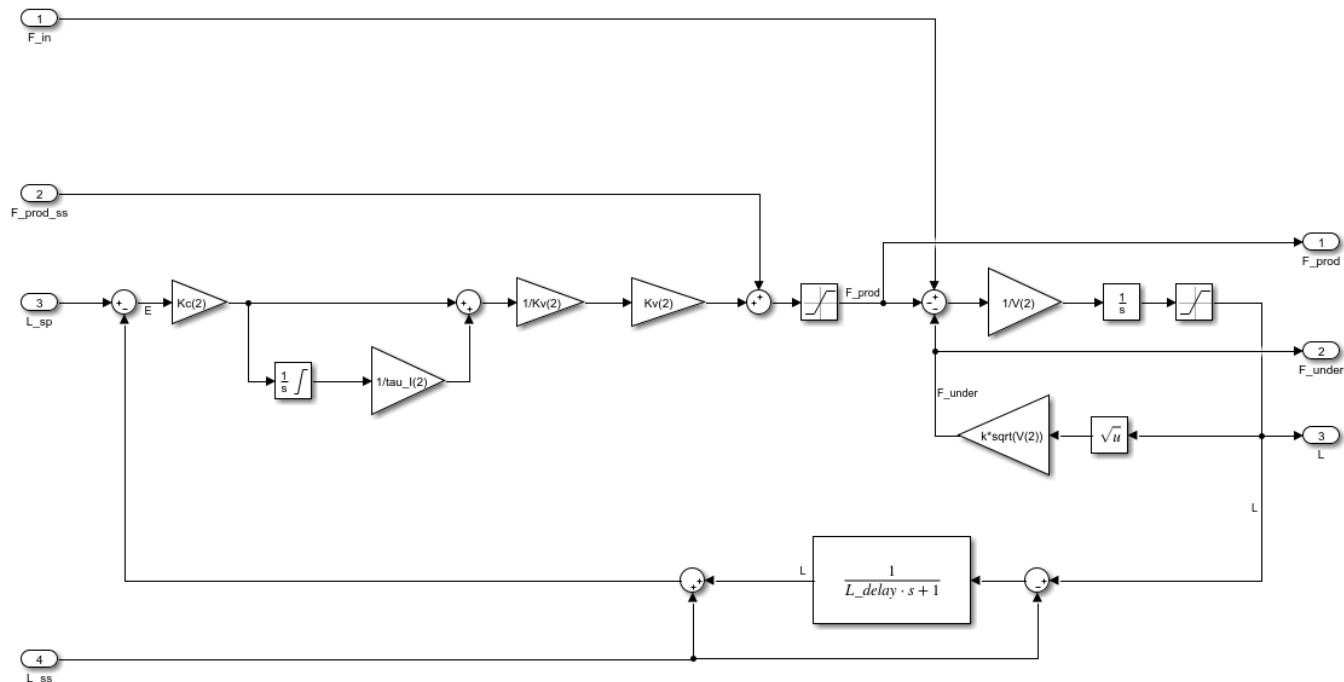
Since  $F_2$  is the MV, it is calculated using the PI controller equation in the Laplace domain.

$$F_2 = K_c \left[ 1 + \frac{1}{s\tau_I} \right] \quad (S7)$$

$F_3$  is the underflow, which is proportional to the squareroot of the tank level:

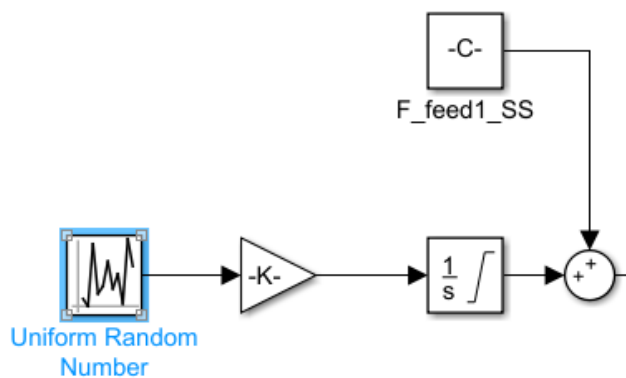
$$F_3 = k \sqrt{h_{frac}} \quad (S8)$$

Equations S6, S7, and S8 were implemented in Simulink, as shown in Figure S2, and the tanks were connected into a tank network as described in the process description in the article.



**Figure S2.** Simulink implementation of the one-tank model.

The exogenous disturbances fed to each plant section were modelled as random walks by integrating a series of random numbers multiplied by a gain, as shown in Figure S3.



**Figure S3.** Random walk implementation in Simulink.