



Article Enhanced Dispersion Monitoring Structures Based on Modified Successive Sampling: Application to Fertilizer Production Process

Mehvish Hyder¹, Syed Muhammad Muslim Raza^{1,2}, Tahir Mahmood^{3,4,*} and Nasir Abbas⁵

- ¹ Department of Economics and Statistics, Dr Hasan Murad School of Management (HSM), University of Management and Technology, Lahore 54770, Pakistan; f2018204002@umt.edu.pk (M.H.); razamuslim4@gmail.com (S.M.M.R.)
- ² Department of Statistics, Virtual University of Pakistan, Lahore 54000, Pakistan
- ³ Industrial and Systems Engineering Department, King Fahd University of Petroleum and Minerals, Dhahran 31261, Saudi Arabia
- ⁴ Centre for Smart Mobility and Logistics, King Fahd University of Petroleum and Minerals, Dhahran 31261, Saudi Arabia
- ⁵ Department of Mathematics, King Fahd University of Petroleum and Minerals, Dhahran 31261, Saudi Arabia; nasirabbas@kfupm.edu.sa
- * Correspondence: tahir.mahmood@kfupm.edu.sa

Abstract: In this era of Industry 4.0, efficient and affordable monitoring solutions are needed for the surveillance of manufacturing/service operations. In general, memory-type control charts outperform memoryless control charts when it comes to determining the changes in location and dispersion parameters of symmetrically distributed processes. Before monitoring the process location, it is essential to monitor the process dispersion, since the latter presumes that the process variance remains stable. In practice, the modified successive sampling (*MSS*) mechanism is preferred over simple random sampling for its cost-effectiveness and efficiency. This study was designed in order to propose moving average and double moving average control charts based on the *MSS* mechanism for monitoring the dispersion parameter. The performance of the proposed charts is evaluated using run-length measures, and a comparison is made with an existing control chart based on *MSS* and repetitive sampling. Furthermore, the application of the designed moving and double moving average charts is demonstrated using a case study related to fertilizer production. It is observed that the proposed double moving average control chart performs better than the other control charts designed under the *MSS* and repetitive sampling schemes.

Keywords: process dispersion; ARL; MA; DMA; control charts; MSS; statistical process control

1. Introduction

In statistical process control (SPC), a control chart is the most important and frequently used tool to monitor process parameters (such as location and/or dispersion). Quality practitioners mostly prefer using control charts to identify sustainable variations in the process parameters. In a process, the main application of control charts is the visual detection of unusual variations for which educative action is needed to move the process back into the in-control (IC) state [1]. Shewhart [2] invented the first control chart, named the Shewhart chart, which was designed based on a current sample. Therefore, Shewhart-type (memoryless) control charts are more efficient for detecting large shifts in the process and are less efficient for detecting shifts of small magnitude. On the other hand, memory-type control charts, such as cumulative sum (CUSUM) by Page [3], exponentially weighted moving average (EWMA) by Roberts [4], moving average (MA) by Wong et al. [5] and double moving average (DMA) by [6], perform more efficiently for the timely detection of



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Copyright: © 2023 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). small shifts in the process. The reason for this is that their structures are based on current as well as past observations of the process [7].

Many quality practitioners have studied MA and DMA control charts in detail. MA and combined MA-Shewhart design procedures were designed by Wong et al. [5]. To monitor both process parameters (mean and variance), Khoo and Yap [8] designed an MA chart for the joint monitoring of both upwards and downwards shift. For the monitoring of process variability, Adeoti et al. [9] designed a double moving average-S chart that detects small to moderate shifts. Khoo and Wong [10] presented a double exponentially weighted moving average (DEWMA) chart to monitor the location parameter of a process. For monitoring defective products, Areepong [11] explicated formulas for the average run length (ARL) of an MA chart, and Phant et al. [12] gave an expression for the ARL of a DMA chart under the integer-valued autoregression of order one (INAR(1)) processes. Adeoti et al. [9] and Alevizakos et al. [6] studied a double moving average (DMA) chart to enhance the detection ability of a moving average (MA) chart under normal distribution and assuming a simple random sampling (SRS) mechanism.

In the literature, many studies have presented more accurate and efficient estimators, some of which use sampling schemes other than SRS. Their findings reveal that such sampling mechanisms are more reliable, time- and cost-effective as compared to SRS. Salazar and Sinha [13] designed memoryless control charts using ranked set sampling (RSS). Al-Nasser and Al-Rawwash [14] developed Shewhart control charts based on a robust RSS mechanism. Abujiya et al. [15] suggested an EWMA structure based on median RSS, while Munir and Haq [16] presented a CUSUM structure using an ordered and double ordered RSS scheme. For location monitoring, Nawaz et al. [17], Nawaz and Han [18] and Hussain et al. [19] studied different median- and mean-based Shewhart, CUSUM, EWMA and homogeneously weighted moving average (HWMA) charts under ranked set sampling (RSS) and neoteric ranked set sampling (NRSS) schemes. Reynolds Jr and Lou [20] evaluated a GLR control chart for the monitoring of process mean. The generalized control chart is based on the likelihood ratio of normal distribution under SRS. The average time to signal measure is used to evaluate the performance of the proposed charts. A comparison with the Shewhart, CUSUM and the combined Shewhart-CUSUM charts is provided. Furthermore, Sheriff et al. [21] performed a comparative study on PCA-based GLR control charts for process monitoring. Their method is based on the likelihood ratio of principal component analysis for high-dimensional data. The proposed chart is used to monitor location and/or dispersion shifts. Riaz et al. [22] designed a new HWMA control chart for the monitoring of the dispersion parameter using wind farm data. Anwar et al. [23] and Anwar et al. [24] proposed mixed memory-type control charts for the simultaneous monitoring of more than one parameters using auxiliary information. A double generally weighted moving average (GWMA) control chart for monitoring dispersion parameters was designed by Alevizakos et al. [25]. Akhtar et al. [26] evaluated the EWMA control chart by using log-normal distributions with estimated parameters to monitor process variability. A GWMA maximum chart for joint monitoring was designed by Chatterjee et al. [27]. Similarly, Chatterjee et al. [28] introduced an efficient control charting structure named double GWMA (DGWMA) for the monitoring of location and dispersion parameters. Khan et al. [29] developed a hybrid EWMA control chart based on a ranked set sampling scheme under a Bayesian approach using hard-bake process data. For the monitoring of variability in a process, an exponentially weighted moving average control chart based on generalized fast initial response was designed by Ajibade et al. [30]. Recently, a new weighted adaptive CUSUM chart using a bivariate normal process to monitor generalized variance was proposed by Haq and Abbasi [31].

All these aforementioned studies under the Shewhart setup and their analyses are conducted under the assumption that all n sample observations are available and no information from the previous sample(s) is used for making decisions. The CUSUM and EWMA structures overcome this issue partially by defining the plotting statistics as functions of current and previous samples. There are many practical situations in which

it is desirable to conduct control charting analysis with a sample size n but only n - c observations are available at each time point, where c is a positive integer. For such situations, a cost-effective and time-saving sampling procedure named modified successive sampling (*MSS*) was first introduced by Yaqub et al. [32]. Yaqub et al. [32] and Abbas et al. [33] proposed Shewhart charts based on MSSS schemes for the detection of location and dispersion parameters, respectively. The modified form of the successive sampling scheme is more effective than other existing sampling techniques and is specially designed to monitor process parameters (location or dispersion). For the real-time surveillance of the location parameter, memory-type control charts based on *MSS* were designed by Hyder et al. [34].

The situation of a reduced sample size can also occur in the case of dispersion monitoring. To the best of our knowledge, there are no studies in the literature that provide a solution for such situations under memory-type structures. Filling this research gap, the current study is focused on designing efficient memory-type control charts ($MA-S^2_{MSS(S)}$, $DMA-S^2_{MSS(S)}$) based on the *MSS* scheme for the monitoring of symmetrical process variability. The performance of the designed control charts is compared with the existing Shewhart chart for process dispersion monitoring under various *MSS* schemes.

The rest of this article is organized as follows. In Section 2, a summary of *MSS* schemes is given, along with the construction of the designed charts based on these schemes. Section 3 presents the performance of proposed charts, which is evaluated through simulations. A comparative analysis is presented in Section 4, Section 5 illustrates the implementation of the designed charts using real-life data and the concluding remarks of the article and future recommendations are given in Section 6.

2. Methodology

This section briefly defines the structure and several schemes of *MSS*. Additionally, for the efficient monitoring framework of the scale parameter, we construct $MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ charts based on *MSS* in this section.

2.1. Modified Successive Sampling

The timely inspection of defective items may improve the cost-efficiency of any industrial process. To improve cost-efficiency, Jessen [35] developed the successive sampling technique for various inventory problems. However, in most surveys, SRS is suggested for a single occasion. However, an item's quality is regularly examined in industrial practices. Therefore, to obtain reliable estimates, successive sampling plays an important role in such repeated assessments. The structure of successive sampling is that the initial sample is selected on the 1st occasion and the next sample (having some sample points from the previous sample) is drawn on the 2nd occasion, and so on. This sampling procedure will be carried out until desired sample size is achieved. Patterson [36], Rao and Graham [37], Choudhary et al. [38], Yaqub et al. [32], Abbas et al. [33] and Hyder et al. [34] described some modifications of successive sampling.

Abbas et al. [33] discussed the structure of modified successive sampling (*MSS*) for memoryless control charts. The procedure of *MSS* is outlined as follows:

- 1. Firstly, select a sample $(y_{1,1}, y_{1,2}, ..., y_{1,n})$ of size '*n*' from a symmetric distribution by using simple random sampling (SRS).
- 2. New observations (n c) are drawn by using SRS for the 2nd sample $(y_{2,1}, y_{2,2}, ..., y_{2,n-c})$ and the rest of the 'c' observations are some selected quantiles of the previous sample as $[(y_{2,1}, y_{2,2}, ..., y_{2,n-c}), (y_{2,n-c+1}, y_{2,n-c+2}, ..., y_{2,n})]$, where $y_{2,n-c+1} = f_1(y_{1,1}, y_{1,2}, ..., y_{1,n}), y_{2,n-c+2} = f_2(y_{1,1}, y_{1,2}, ..., y_{1,n})$ and so on, up to $y_{2,n} = f_c(y_{1,1}, y_{1,2}, ..., y_{1,n})$.
- 3. Using the SRS scheme again, take (n c) new observations as the 3rd sample and the leftover 'c' observations are selected by using some quantile points of the 2nd sample. Similarly, this procedure will continue for the complete production process run.

The *MSS* is symbolized as $MSS_{n,c,f1,f2,...,fc.}$, where '*n*' and '*c*' denote the size of the sample and the number of values chosen the preceding sample and f_p is a function of the preceding sample $\forall p = 1, 2, ..., c$, respectively. For the monitoring of the dispersion parameter, following Abbas et al. [33], we have considered ten different *MSS* schemes, as given below:

- (a) For c = 2, the (n 2) new observations are selected by using the SRS scheme, and the other two observations are specific quantile points (Q_1, Q_2) of the previous sample. Notationally, this is defined as $MSS_{n,2,Q_1,Q_2}$. In this study, different choices of quantile pairs such as $(Q_{0.25}, Q_{0.75}), (Q_{0.30}, Q_{0.70}), (Q_{0.35}, Q_{0.65}), (Q_{0.40}, Q_{0.60})$ and $(Q_{0.45}, Q_{0.55})$ are used. By using these quantile pairs, the various $MSS_{(S)}$ schemes are considered, which are described below:
 - i. $MSS_{n,2,Q_{0.25},Q_{0.75}}$ is the first $MSS_{(1)}$ scheme, where S = 1.
 - ii. $MSS_{n,2,Q_{0.30},Q_{0.70}}$ is the second $MSS_{(2)}$ scheme, where S = 2.
 - iii. $MSS_{n,2,Q_{0.35},Q_{0.65}}$ is the third $MSS_{(3)}$ scheme, where S = 3.
 - iv. $MSS_{n,2,Q_{0.40},Q_{0.60}}$ is the fourth $MSS_{(4)}$ scheme, where S = 4.
 - v. $MSS_{n,2,Q_{0.45},Q_{0.55}}$ is the fifth $MSS_{(5)}$ scheme, where S = 5.
- (b) When c = 3, (n 3) new observations are drawn by using the SRS scheme, and the remaining three observations are specific quantiles points (Q_1, Q_2, Q_3) of the previous sample. Symbolically, This is defined as $MSS_{n,3,Q_1,Q_2,Q_3}$. In this study, different choices of quantile points such as $(Q_{0.25}, Q_{0.50}, Q_{0.75}), (Q_{0.30}, Q_{0.50}, Q_{0.70}), (Q_{0.35}, Q_{0.50}, Q_{0.65}), (Q_{0.40}, Q_{0.50}, Q_{0.60})$ and $(Q_{0.45}, Q_{0.50}, Q_{0.55})$ are used. By using these quantile pairs, the other $MSS_{(S)}$ schemes are described as follows:
 - i. $MSS_{n,3,Q_{0.25},Q_{0.50},Q_{0.75}}$ is the sixth $MSS_{(6)}$ scheme, where S = 6.
 - ii. $MSS_{n,3,Q_{0.30},Q_{0.50},Q_{0.70}}$ is the seventh $MSS_{(7)}$ scheme, where S = 7.
 - iii. $MSS_{n,3,Q_{0.35},Q_{0.50},Q_{0.65}}$ is the eighth $MSS_{(8)}$ scheme, where S = 8.
 - iv. $MSS_{n,3,Q_{0.40},Q_{0.50},Q_{0.60}}$ is the ninth $MSS_{(9)}$ scheme, where S = 9.
 - v. $MSS_{n,3,Q_{0.45},Q_{0.50},Q_{0.55}}$ is the tenth $MSS_{(10)}$ scheme, where S = 10.

It should be noted that the subscript (S) in $MSS_{(S)}$ describes the different pairing schemes of modified successive sampling (MSS).

2.2. Existing Shewhart- $S^2_{MSS(S)}$ Control Chart

For the detection of large shifts in the dispersion parameter, Abbas et al. [33] introduced a *Shewhart-S*² chart based on modified successive sampling. The plotting statistic of the *Shewhart-S*²_{MSS(S)} control chart is as follows:

$$S_i^2 = \frac{\sum_{j=1}^n (X_{ij} - X)^2}{n - 1} \tag{1}$$

The lower and upper control limits of the *Shewhart-S*²_{MSS(S)} chart are defined as follows:

$$LCL_{MSS} = S_{s^2} - L_{MSS}MSE_{S^2}$$
⁽²⁾

$$UCL_{MSS} = \bar{S}_{s^2} + L_{MSS}MSE_{S^2}$$
(3)

where S_{s^2} is the mean of S^2 , MSE_{S^2} is the mean square error of S^2 and L_{MSS} is the charting coefficient of the existing Shewhart chart based on MSS.

2.3. Proposed $MA-S^2_{MSS(S)}$ Control Chart

Initially, the moving average (*MA*) control chart structure was proposed by Wong et al. [5]. For the monitoring of the dispersion parameter, the statistic of the designed chart ($MA-S^2_{MSS(S)}$) under different *MSS* schemes is described as follows:

$$MA_{i(S)} = \begin{cases} \frac{\sum_{j=1}^{i} S_{j(S)}^{2}}{i}, & \text{for } i < w, \\ \frac{\sum_{j=i-w+1}^{i} S_{j(S)}^{2}}{w}, & \text{for } i \ge w. \end{cases}$$
(4)

where $S_{j(S)}^2$ indicates the variance of the j^{th} sample with the specific *MSS* schemes shown by the subscript (*S*), *i* is the sampling time and *w* denotes the span of the moving average. The mean of the $MA_{i(S)}$ statistic is $E(MA_{(S)}) = \overline{S}_{s^2}$, and the variance of $MA_{i(S)}$ is given as

$$Var(MA_{(S)}) = \begin{cases} \frac{MSE_{S^2}}{ni}, & \text{for } i < w, \\ \frac{MSE_{S^2}}{nw}, & \text{for } i \ge w \end{cases}$$
(5)

The control limits of the MA- $S^2_{MSS(S)}$ chart are calculated as follows:

$$LCL_{MA(S)} = 0 \tag{6}$$

$$UCL_{MA(S)} = \overline{S}_{s^2} + L_{MSS(S)} \sqrt{Var(MA_{(S)})}$$
(7)

where $L_{MSS(S)}$ is a control charting coefficient observed against the specified values of ARL_0 and sample size (*n*). If MA- $S^2_{MSS(S)}$ statistic is plotted outside the control limits $(LCL_{MSS(S)}/UCL_{MSS(S)})$, then the process is declared to be out of control (OOC).

2.4. Proposed DMA- $S^2_{MSS(S)}$ Control Chart

Alevizakos et al. [6] proposed a memory-type double moving average (*DMA*) control chart for efficient monitoring. The statistic of $DMA-S^2_{MSS(S)}$ under *MSS* schemes is defined as follows:

$$DMA_{i(S)} = \begin{cases} \frac{\sum_{j=1}^{i} MA_{j(S)}}{i}, \text{ for } i < w, \\ \frac{\sum_{j=i-w+1}^{i} MA_{j(S)}}{w}, \text{ for } i \ge w. \end{cases}$$

$$(8)$$

The expected value of the $DMA_{(S)}$ statistic is obtained as

$$E\left(DMA_{(S)}\right) = \bar{S}_{s^2} \tag{9}$$

and the variance of the $DMA_{(S)}$ statistic is evaluated as follows:

for i < w,

$$Var(DMA_{(S)}) = \frac{\sum_{j=1}^{i} a_j^2 MSE_{S^2}}{ni^2},$$
 (10)

for $w \leq i < 2w - 1$,

$$Var\left(DMA_{(S)}\right) = \left(\frac{MSE_{S^2}}{nw^2}\right) \left[\sum_{j_1=i-w+1}^{w-1} \frac{1}{j_1} + \sum_{i-w+1 \le j_{11} < j_{12} \le w-1} \frac{2}{j_{12}} + \sum_{j_1=i-w+1}^{w-1} \sum_{j_2=w}^{i} \frac{2(j_1-j_2+w)}{j_1w} + \frac{i-w+1}{w} + \sum_{w \le j_{21} < j_{22} \le i} \frac{2(j_{21}-j_{22}+w)}{w^2}\right].$$
(11)

and for $i \geq 2w - 1$,

$$Var(DMA_{(S)}) = \frac{MSE_{S^2}}{nw^2} \left[1 + \sum_{i-w+1 \le j_1 < j_2 \le i} \frac{2(j_1 - j_2 + w)}{w^2} \right].$$
 (12)

The mean and variances of the *DMA* statistic are derived by Alevizakos et al. [6]. The control limits of the DMA- $S^2_{MSS(S)}$ control chart are defined as follows:

$$LCL_{DMA(S)} = 0 \tag{13}$$

$$UCL_{DMA(S)} = \overline{S}_{s^2} + K_{MSS(S)} \sqrt{Var(DMA_{(S)})}$$
(14)

The charting constant is denoted as $K_{MSS(S)}$. If the statistic $DMA_{i(S)}$ lies between these (lower and upper) control limits, the process is called IC; otherwise, it is OOC.

3. Performance Evaluations of Designed Charts

In this section, performance evaluations and comparative analysis of the designed charts with the existing Shewhart control charts proposed by Abbas et al. [33] have been conducted. All the comparisons are carried out under the assumption of known parameters. However, the effect of parameter estimation on some moving average control charts is studied in detail by Jones et al. [39] and Noorossana et al. [40]. The performance of the designed $MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ charts are evaluated by using run length (RL) metrics. The RL metrics include various performance measuring criteria such as average RL (ARL), standard deviation RL (SDRL) and median RL (MDRL). The average RL (ARL) is the average of the number of plotting statistics before detecting an OOC signal [41,42]. ARL_0 is defined as the ARL of the IC process, while ARL_1 is the ARL of an OOC process. In practice, the control limits of their corresponding charts are set against the pre-specified value of ARL_0 , and then the performance is evaluated based on the ARL_1 values [43,44]. It should be noted here that there are several short production runs with low-volume manufacturing environments where the quality of characteristics is monitored [45]. The shifts in such processes, if any, occur at or close to the start. The current study is targeted towards such processes where early change point detection is desired for shifts that occur close to the beginning of the process. Accordingly, the algorithm of zero-state ARL computation is used where the possible change point is at i = 1.

Assuming normal distribution (symmetrical distribution) with $\mu = 0, \sigma = 1$, the average run length of an IC process is pre-fixed at 370, i.e., $ARL_0 = 370$, the moving span is set at w = 2 and $\delta = 1$ (this means that the process variability has no shift). For a fixed $ARL_0 = 370$, the values of charting coefficients ($L_{MSS(S)}$ and $K_{MSS(S)}$) of the designed $MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ charts, \overline{S}_{s^2} and MSE_{s^2} under different schemes of MSS are presented in Table 1 for the sample size choices n = 5 and 7.

Table 1. Control charting coefficients	$L_{MSS(S)}$ and $K_{MSS(S)}$	for the proposed c	control charts under
different schemes of MSS ($w = 2$).			

		n	=5		<i>n</i> =7								
Scheme	\overline{S}_{S^2}	MSE_{S^2}	L _{MSS(S)}	K _{MSS(S)}	\bar{s}_{s^2}	MSE_{S^2}	L _{MSS(S)}	K _{MSS(S)}					
MSS ₍₁₎	1.08	0.37	10.18	17.14	0.97	0.26	10.72	17.74					
$MSS_{(2)}$	0.86	0.34	9.39	15.64	0.86	0.26	9.994	16.48					
$MSS_{(3)}$	0.73	0.38	8.37	13.84	0.8	0.28	9.36	15.35					
$MSS_{(4)}$	0.67	0.40	7.76	12.8	0.76	0.29	8.95	14.58					
$MSS_{(5)}$	0.64	0.42	7.49	12.3	0.74	0.30	8.78	14.27					
$MSS_{(6)}$	0.76	0.3	9.6	16.1	0.78	0.25	9.8	16.32					
$MSS_{(7)}$	0.55	0.40	7.12	11.85	0.68	0.29	8.5	14.04					
MSS ₍₈₎	0.46	0.48	6.08	10.03	0.63	0.32	7.81	12.8					
$MSS_{(9)}$	0.43	0.51	5.75	9.53	0.60	0.34	7.5	12.23					
MSS(10)	0.41	0.52	5.57	9.17	0.59	0.35	7.38	12.02					

The control chart with the fewest values of ARL_1 is said to be more efficient and have higher detection ability than the others. For this instance, the complete profiles of RL with different shifts (δ) in process variability, sample sizes (n) and moving span (w) are presented under various *MSS* schemes in Tables 2 and 3.

				Shewhar	$t-S^2_{MSS(S)}$					MA-S	2 MSS(S)			$DMA-S^2_{MSS(S)}$						
Schemes	δ		<i>n</i> =5			<i>n</i> =7			<i>n</i> =5			<i>n</i> =7			<i>n</i> =5			<i>n</i> =7		
		ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	
	1	369.56	309.5	369.08	369.21	308.1	371.56	371.03	254.00	375.92	369.91	260.00	368.71	370.61	261.00	367.68	369.37	251.00	363.10	
	1.1	193.53	162	194.28	177.70	149	177.88	181.63	126.00	180.77	165.03	113.00	165.99	180.83	129.00	184.70	156.43	108.00	156.00	
	1.2	113.28	94.5	113.41	97.62	82	97.61	102.83	72.00	102.67	85.11	59.00	85.59	102.64	73.00	98.51	83.57	58.00	82.99	
	1.3	72.18	60.5	72.09	59.70	50	60.09	65.18	44.00	62.99	49.36	34.00	49.42	64.29	46.00	64.25	47.61	34.00	45.74	
	1.4	49.45	41.5	49.48	39.16	32.5	39.31	44.30	30.00	42.58	31.72	22.00	29.82	43.79	31.00	44.25	31.67	22.00	31.76	
$MSS_{(1)}$	1.5	35.53	29.5	35.46	27.24	23	27.26	31.87	23.00	30.27	22.35	16.00	20.70	31.83	22.00	31.50	22.27	15.00	22.18	
	1.6	26.97	22.5	26.90	20.18	17	20.37	24.27	17.00	22.70	16.58	12.00	14.84	24.09	17.00	23.82	16.38	11.00	16.44	
	1.7	21.23	17.5	21.13	15.36	12.5	15.33	18.73	14.00	17.74	12.88	9.00	11.46	18.20	13.00	18.10	12.54	9.00	12.25	
	1.8	17.04	14.5	16.96	12.23	10	12.15	15.38	11.00	13.95	10.58	8.00	9.13	15.25	11.00	14.78	10.18	7.00	9.93	
	1.9	14.09	11.5	14.00	9.94	8.5	9.81	13.39	10.00	11.94	8.95	7.00	7.54	12.83	9.00	12.16	8.09	6.00	7.83	
	2	11.88	9.5	11.78	8.32	6.5	8.22	11.15	8.00	9.96	7.55	6.00	6.13	10.84	8.00	10.20	7.10	5.00	6.79	
	1	370.31	310	371.98	370.72	310.1	375.07	369.67	249.00	368.53	369.49	252.00	369.52	369.95	250.00	373.62	369.56	253.00	357.75	
	1.1	200.19	167	202.15	183.68	153.5	185.50	181.62	124.00	185.11	161.31	111.00	163.25	180.49	127.00	186.63	160.13	113.00	159.44	
	1.2	119.88	99.5	121.58	102.47	86	103.13	102.96	71.00	104.10	85.62	59.00	86.67	101.68	72.00	103.17	84.08	59.00	84.42	
	1.3	77.33	64.5	78.68	62.62	52	63.46	66.06	45.00	67.80	49.21	34.00	49.95	64.60	45.00	63.28	48.95	35.00	47.53	
	1.4	53.30	44	54.19	41.59	34.5	42.56	44.46	31.00	43.19	32.37	23.00	31.23	44.38	30.00	46.02	31.60	22.00	31.74	
$MSS_{(2)}$	1.5	38.63	32	39.71	29.24	24.5	29.94	32.26	23.00	31.26	22.38	16.00	21.27	31.76	22.00	32.73	22.12	15.00	22.46	
	1.6	29.29	24.5	30.11	21.33	18	21.85	24.60	18.00	23.25	16.70	12.00	15.49	23.95	17.00	24.32	16.13	11.00	16.35	
	1.7	22.69	19	23.32	16.33	13.5	16.61	19.64	14.00	18.83	12.85	9.00	11.50	18.27	13.00	18.75	12.44	9.00	12.73	
	1.8	18.49	15.5	19.18	12.93	10.5	13.27	15.53	11.00	14.27	10.53	8.00	9.26	15.16	10.00	15.78	9.66	7.00	9.74	
	1.9	15.15	12.5	15.69	10.51	9	10.77	13.14	9.00	12.18	8.88	6.00	7.70	12.55	8.00	12.94	8.06	5.00	8.22	
	2	12.70	10.5	13.19	8.65	7	8.82	11.32	8.00	10.23	7.54	5.00	6.28	10.47	7.00	10.66	6.55	4.00	6.56	
	1	370.12	313.5	375.77	369.67	306.5	367.15	370.35	250.50	375.53	369.46	256.00	372.18	370.45	261.00	372.14	369.14	260.00	367.74	
	1.1	206.36	172.5	208.55	184.49	154	185.84	186.20	128.00	189.26	163.16	113.00	167.37	184.92	134.00	193.63	160.93	112.00	157.70	
	1.2	124.14	103.5	126.43	103.32	86	105.21	105.86	73.00	108.69	85.53	59.00	87.62	103.29	77.00	108.00	83.53	58.00	82.80	
	1.3	81.44	68	83.01	63.94	53	65.25	66.60	44.00	70.46	49.61	33.00	51.83	65.23	48.00	70.38	49.32	35.00	47.16	
	1.4	56.46	47	58.17	42.17	35	43.11	44.64	30.00	46.71	32.43	23.00	30.68	43.51	33.00	46.87	31.81	22.00	32.94	
$MSS_{(3)}$	1.5	41.10	34.5	42.65	29.71	25	30.59	33.15	23.00	32.21	22.66	16.00	21.75	32.08	21.00	34.05	21.93	15.00	23.10	
	1.6	31.10	26	32.49	22.06	18.5	22.76	25.62	18.00	25.12	16.64	12.00	15.30	23.93	16.00	25.34	16.07	11.00	16.91	
	1.7	24.32	20	25.58	16.70	13.5	17.38	19.83	14.00	19.00	13.15	9.00	11.84	18.70	12.00	19.91	12.31	8.00	13.00	
	1.8	19.49	16	20.61	13.20	10.5	13.84	16.11	11.00	15.28	10.49	7.00	9.38	15.14	10.00	16.26	9.65	6.00	10.09	
	1.9	16.00	13.5	16.99	10.63	9	11.12	13.35	9.00	12.44	8.90	6.00	7.72	12.40	8.00	13.48	7.84	5.00	8.28	
	2	13.40	11	14.31	8.89	7	9.28	11.59	8.00	10.72	7.48	5.00	6.30	10.12	6.00	10.88	6.60	4.00	6.91	

Table 2. Run length profile of the proposed charts under *MSS* at pre-specified $ARL_0 = 370$, w = 2 and c = 2.

Table 2. Cont.

				Shewhar	$t-S^2_{MSS(S)}$				MA-S ² _{MSS(S)}						DMA-S ² _{MSS(S)}							
Schemes	δ	<i>n</i> =5				<i>n</i> =7			<i>n</i> =5			<i>n</i> =7			<i>n</i> =5			<i>n</i> =7				
		ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL			
	1	370.03	313.5	379.63	370.33	313.5	378.75	369.81	252.50	371.42	369.00	256.00	369.53	370.51	254.00	376.92	370.17	257.00	374.43			
	1.1	207.91	173.5	211.00	189.03	157.5	191.70	185.47	126.00	192.29	163.40	111.00	170.20	185.00	131.00	191.72	162.91	114.50	165.71			
	1.2	127.41	106.5	129.93	107.02	89	108.71	105.98	72.00	109.41	86.78	60.00	86.12	105.25	77.00	110.24	86.10	59.00	89.59			
	1.3	84.13	70	86.42	66.26	55	67.76	66.83	45.00	70.29	51.16	36.00	49.78	65.35	49.00	69.44	49.78	33.00	52.16			
	1.4	58.41	48.5	60.58	44.02	36.5	45.16	45.14	33.00	45.75	33.18	24.00	31.32	44.46	30.00	47.31	31.71	21.00	33.36			
$MSS_{(4)}$	1.5	42.51	35.5	44.10	30.86	25.5	31.93	34.47	24.00	33.89	22.97	16.00	22.01	31.94	21.00	34.68	22.19	15.00	23.34			
	1.6	32.41	26.5	34.13	22.66	19	23.57	26.15	18.00	25.75	16.89	12.00	15.81	23.72	16.00	25.68	16.07	11.00	16.88			
	1.7	25.32	21	26.93	17.35	14	18.33	20.49	14.00	19.97	13.01	9.00	11.90	18.59	12.00	20.30	12.21	8.00	13.18			
	1.8	20.21	16.5	21.49	13.68	11	14.42	16.48	12.00	15.65	10.79	8.00	9.86	14.92	10.00	16.31	9.65	6.00	10.29			
	1.9	16.72	14	17.94	11.10	9.5	11.72	13.76	10.00	13.08	9.01	6.00	8.01	12.26	8.00	13.69	7.85	5.00	8.36			
	2	14.02	11.5	15.26	9.09	7.5	9.62	11.62	8.00	11.10	7.54	5.00	6.39	10.21	6.00	11.23	6.44	4.00	6.84			
	1	370.87	311.5	373.74	370.04	316	377.20	369.75	250.00	378.34	371.98	258.00	375.82	369.95	252.00	367.78	369.82	261.00	358.28			
	1.1	208.89	174.5	211.68	188.64	157.5	190.19	187.49	129.00	192.44	167.65	115.00	172.97	186.50	129.00	188.01	161.28	111.00	162.45			
	1.2	128.23	107	131.36	107.90	90	109.52	106.97	73.00	111.64	86.99	59.00	91.39	105.16	75.00	108.44	85.08	60.00	82.69			
	1.3	85.32	71	88.56	66.78	55.5	68.19	67.23	45.00	71.09	50.54	35.00	48.99	66.90	48.00	67.66	50.12	34.00	51.97			
	1.4	59.26	49	61.36	44.49	37	46.04	45.19	30.00	48.68	32.98	23.00	32.17	44.21	34.00	47.13	32.16	22.00	33.95			
$MSS_{(5)}$	1.5	43.07	35.5	45.14	31.10	26	32.17	32.15	21.00	35.36	21.91	16.00	21.82	31.59	24.00	34.09	21.64	15.00	23.81			
	1.6	32.60	27	34.48	23.10	19	24.01	25.99	18.00	25.76	16.76	12.00	15.52	24.01	16.00	26.75	16.12	11.00	17.26			
	1.7	25.61	21	27.48	17.55	14.5	18.42	20.53	14.00	19.85	13.25	9.00	12.26	18.60	12.00	20.60	12.39	8.00	13.36			
	1.8	20.54	16.5	22.18	13.87	11	14.59	16.64	12.00	15.96	10.67	8.00	9.68	14.99	9.00	16.92	9.63	6.00	10.59			
	1.9	16.79	13.5	18.27	11.22	9.5	11.90	13.81	10.00	13.34	8.91	6.00	7.96	12.27	8.00	13.72	7.95	5.00	8.55			
	2	14.06	11.5	15.44	9.22	7.5	9.81	11.43	8.00	10.75	7.59	5.00	6.57	9.95	6.00	11.23	6.45	4.00	6.80			

				Shewhar	$t-S^2_{MSS(S)}$					MA-S	2 MSS(S)			$DMA-S^2_{MSS(S)}$						
Schemes	δ		<i>n</i> =5			<i>n</i> =7			<i>n</i> =5			<i>n</i> =7			<i>n</i> =5			<i>n</i> =7		
		ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	
	1	370.83	311	379.94	370.13	313	377.80	370.40	257.00	371.47	369.86	250.00	370.83	370.31	254.00	375.76	370.99	256.00	368.59	
	1.1	208.43	173	213.70	187.60	156	191.13	195.24	134.00	201.60	167.49	115.00	171.74	194.09	133.00	194.52	165.25	124.00	176.65	
	1.2	126.35	105	130.14	106.39	89	108.87	116.99	79.00	123.07	88.44	66.00	91.71	115.63	80.00	115.91	90.60	61.00	93.61	
	1.3	82.62	68.5	85.98	65.75	54.5	68.32	74.97	50.00	78.58	55.56	38.00	55.71	74.67	51.00	77.00	55.05	37.00	57.81	
	1.4	58.02	47.5	61.31	43.29	36	45.25	50.99	34.00	54.33	35.96	25.00	35.37	50.68	36.00	52.94	35.75	24.00	38.52	
$MSS_{(6)}$	1.5	42.32	35	45.48	30.70	25	32.42	37.22	25.00	39.90	25.21	17.00	24.76	37.09	26.00	37.35	24.18	16.00	25.77	
	1.6	31.92	26	34.57	22.47	18.5	23.80	28.77	19.00	29.37	18.82	13.00	18.38	27.72	20.00	28.62	17.92	12.00	19.15	
	1.7	25.01	20	27.42	17.15	14	18.35	23.06	16.00	23.26	15.05	11.00	14.37	21.65	14.00	23.88	13.39	9.00	14.45	
	1.8	20.22	16.5	22.22	13.51	11	14.64	18.50	12.00	18.86	11.70	8.00	11.15	17.29	11.00	19.08	10.78	7.00	11.59	
	1.9	16.63	13.5	18.44	10.92	8.5	11.96	15.26	10.00	15.80	9.77	7.00	8.88	14.62	9.00	16.32	8.56	5.00	9.37	
	2	13.88	11	15.63	9.09	7.5	9.88	13.09	9.00	13.18	8.19	6.00	7.41	12.29	8.00	13.81	7.19	4.00	7.65	
	1	369.52	307	376.50	370.10	313	379.64	370.76	256.00	388.48	369.39	248.00	372.77	370.38	255.00	373.82	369.72	264.00	371.97	
	1.1	211.02	175.5	219.56	190.71	158	195.74	198.16	135.00	211.65	168.35	111.00	172.04	197.03	135.00	203.24	167.05	121.00	166.65	
	1.2	131.91	109	139.26	108.75	90	112.75	115.59	77.00	126.94	92.59	60.00	94.35	114.09	81.00	126.98	91.57	64.00	91.41	
	1.3	87.46	71.5	93.80	68.32	56.5	71.99	74.23	47.00	83.80	57.30	36.00	57.04	73.85	52.00	78.44	55.97	39.00	56.26	
	1.4	61.64	50	66.89	45.49	37.5	48.13	49.71	31.00	56.71	37.96	22.00	37.64	48.37	36.00	56.04	35.60	24.00	35.41	
$MSS_{(7)}$	1.5	45.13	36.5	50.20	32.17	26.5	34.72	36.58	22.00	42.17	27.32	14.00	26.18	35.98	25.00	39.90	25.11	17.00	25.47	
	1.6	34.21	27.5	38.58	23.62	19	25.91	27.74	19.00	30.29	18.81	13.00	18.78	27.24	17.00	31.56	17.06	11.00	19.33	
	1.7	26.68	21	30.66	17.98	14.5	19.77	22.53	14.00	24.42	14.34	10.00	14.14	20.63	12.00	24.96	13.13	8.00	14.82	
	1.8	21.61	17	25.21	14.12	11	15.83	18.94	12.00	20.21	11.53	8.00	11.20	16.42	9.00	20.10	10.09	6.00	11.45	
	1.9	17.65	13.5	20.85	11.36	9	12.81	15.40	10.00	16.45	9.55	6.00	9.05	13.72	7.00	17.05	8.30	5.00	9.44	
	2	14.78	11.5	17.64	9.40	7	10.69	13.11	8.00	14.14	8.03	5.00	7.60	11.30	6.00	14.25	6.83	4.00	7.94	
	1	370.11	311.5	385.43	369.13	306.5	372.65	369.21	251.00	383.21	369.71	248.00	381.95	370.38	260.00	376.17	370.92	255.00	378.80	
	1.1	217.49	180.5	228.07	190.47	158	195.58	197.04	130.00	216.21	168.85	112.00	179.77	196.47	136.00	207.60	167.63	121.00	175.42	
	1.2	135.84	111.5	145.65	110.47	92	114.50	116.06	75.00	131.40	89.47	59.00	95.15	115.87	81.00	125.95	88.79	65.00	92.54	
	1.3	91.23	74	99.84	69.39	57	73.47	73.84	46.00	84.78	54.44	36.00	59.81	72.27	52.00	82.88	53.10	38.00	57.29	
	1.4	64.46	52	71.81	46.38	38.5	49.53	48.80	29.00	58.16	34.79	22.00	39.39	47.11	35.00	58.31	33.72	25.00	37.26	
$MSS_{(8)}$	1.5	47.28	37.5	53.58	32.68	27	35.63	36.23	21.00	43.98	23.42	14.00	26.69	35.54	25.00	42.80	22.60	17.00	26.13	
	1.6	35.71	28	41.39	24.33	19.5	26.87	26.55	15.00	32.32	17.91	13.00	18.98	25.73	19.00	32.82	17.21	10.00	19.93	
	1.7	28.14	22	33.37	18.45	14.5	20.73	20.58	11.00	25.72	14.62	10.00	14.48	20.51	15.00	26.23	12.93	8.00	14.93	
	1.8	22.69	17.5	27.22	14.44	11.5	16.40	17.89	12.00	20.89	11.69	8.00	11.62	16.15	8.00	21.03	10.15	6.00	11.98	
	1.9	18.46	14	22.64	11.61	9	13.32	12.91	6.00	17.23	9.45	6.00	9.19	11.64	9.00	17.33	8.03	4.00	9.68	
	2	15.32	11.5	19.01	9.58	7.5	11.14	11.12	5.00	14.65	8.10	5.00	7.57	10.00	8.00	14.52	6.64	4.00	7.90	

Table 3. Run length profile of the proposed charts under *MSS* at pre-specified $ARL_0 = 370$, w = 2 and c = 3.

Table 3. Cont.

				Shewhar	$t-S^2_{MSS(S)}$				MA-S ² _{MSS(S)}						$DMA-S^2_{MSS(S)}$							
Schemes	δ	<i>n</i> =5				<i>n</i> =7			<i>n</i> =5			<i>n</i> =7			<i>n</i> =5			<i>n</i> =7				
		ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL	ARL	MDRL	SDRL			
	1	370.46	313.5	388.17	369.15	306.5	375.18	370.32	250.00	392.33	369.71	250.00	376.49	369.39	253.00	377.28	370.61	252.00	374.99			
	1.1	219.78	180.5	232.80	193.73	160.625	198.72	198.35	130.00	221.03	168.32	113.00	178.71	197.35	130.00	210.57	168.15	120.00	177.68			
	1.2	138.21	113	149.28	112.05	92.5	116.81	118.23	75.00	135.93	89.98	60.00	96.09	116.89	77.00	127.20	88.04	64.00	95.91			
	1.3	92.89	75.5	101.98	70.82	58.5	74.91	74.37	44.00	87.75	55.03	36.00	61.22	73.13	43.00	82.29	54.16	39.00	57.19			
	1.4	65.66	52.5	73.55	47.19	38.5	50.86	49.84	29.00	60.16	34.99	22.00	40.03	48.52	28.00	60.24	33.96	25.00	38.15			
$MSS_{(9)}$	1.5	48.34	38.5	55.43	33.43	27.5	36.61	36.27	21.00	44.38	23.43	14.00	26.82	35.58	20.00	44.02	22.63	17.00	25.64			
	1.6	36.65	29	43.04	24.51	19.5	27.41	26.46	14.00	33.09	17.45	10.00	20.35	25.79	13.00	33.65	16.28	13.00	19.19			
	1.7	28.73	22	34.63	18.72	15	21.27	20.29	10.00	26.12	12.87	7.00	15.18	19.27	10.00	26.72	11.00	10.00	14.87			
	1.8	22.88	17.5	28.14	14.62	11.5	16.80	14.42	9.00	21.63	10.13	6.00	12.11	13.97	8.00	20.85	9.02	8.00	11.85			
	1.9	18.65	14.5	23.12	11.83	9.5	13.71	12.14	6.00	17.92	7.97	4.00	9.74	12.01	6.00	17.53	6.60	6.00	9.53			
	2	15.66	11.5	19.72	9.68	7.5	11.36	9.63	5.00	15.22	6.53	3.00	7.79	8.86	5.00	14.97	5.13	5.00	7.94			
	1	370.20	306.5	386.05	369.79	309	376.85	369.95	246.00	400.58	370.58	251.00	384.72	369.99	248.00	381.01	370.15	251.00	364.44			
	1.1	215.30	177.5	229.16	193.10	161	197.78	195.87	126.00	220.30	167.96	114.00	179.01	194.50	137.00	211.75	164.12	123.00	177.52			
	1.2	136.48	111.5	148.08	113.43	94	118.53	116.60	72.00	137.39	90.63	61.00	96.49	114.89	83.00	127.09	88.81	65.00	94.08			
	1.3	91.67	74	102.09	71.11	59	75.48	73.65	43.00	88.02	56.02	37.00	62.19	72.63	52.00	87.23	55.02	39.00	58.06			
	1.4	65.05	52	73.81	47.94	39	51.99	48.60	28.00	60.00	34.77	22.00	40.15	46.19	35.00	61.22	33.61	26.00	38.40			
MSS ₍₁₀₎	1.5	47.89	38	55.95	33.56	27.5	36.85	35.92	19.00	45.04	23.85	14.00	27.63	34.59	25.00	44.02	22.57	18.00	26.62			
	1.6	36.22	28.5	43.49	24.99	20	27.98	25.94	13.00	33.26	17.45	10.00	20.20	24.81	19.00	34.02	17.36	13.00	19.51			
	1.7	28.32	21.5	34.58	18.88	15	21.49	20.42	14.00	25.55	13.98	10.00	15.17	20.17	10.00	26.75	13.08	8.00	15.47			
	1.8	22.61	17	28.12	14.85	11.5	17.18	16.31	12.00	21.53	10.08	8.00	12.04	15.81	7.00	21.43	10.21	6.00	12.36			
	1.9	18.39	13.5	23.37	11.85	9	13.94	12.57	9.00	17.74	7.80	7.00	9.68	12.48	5.00	17.41	7.97	4.00	9.67			
	2	15.15	11	19.54	9.73	7.5	11.51	11.15	8.00	14.88	6.26	5.00	8.15	10.67	4.00	14.70	6.65	3.00	8.05			

Algorithm for Control Charting Constants

In this section, under various MSS schemes, the following basic procedure has been carried out to find the suitable values of the charting coefficients $(L_{MSS(S)} \text{ and } K_{MSS(S)})$ of the designed $MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ charts, respectively.

Step 1: The first step of this procedure is to select the values of the parameters

 $(S_{s^2}, MSE_{S^2}, w, n)$ for the designed chart with pre-fixed $ARL_0 = 370$. This article also considers the various choices of the above-mentioned design parameters (i) sample size (n = 5 and 7) and (ii) moving average span (w = 2, 3, 5, 10 and 15) for both the proposed $MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ charts.

Step 2: A normally distributed random sample of size *n* (symmetrical sample) is generated using $\mu = 0, \sigma = \delta \times 1$, and the remaining samples with size *n* will be generated through the MSS technique. It should be noted that δ refers to the size of the shift; hence, to calculate *ARL*₀, it is considered to be equal to 1; otherwise, for the *ARL*₁ study, it is set to be more than 1.

Step 3: The variance given in Equation (1) is computed for each sample, which is further used to compute the $MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ plotting statistics using Equations (4) and (8).

Step 4: The arbitrary values of the charting coefficients $(L_{MSS(S)} \text{ and } K_{MSS(S)})$ of the designed $MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ charts are set, and the control limits of the designed charts are computed.

Step 5: The proposed charts' statistics are plotted against their control limits to obtain a single RL value by the number of samples. Afterwards, the process is declared to be OOC.

The R language software is used to run steps 1–5 100,000 times and obtain the ARL_0 value. If the obtained ARL_0 is not equal to the pre-specified value of 370, then the $L_{MSS(S)}$ and $K_{MSS(S)}$ values are adjusted and this procedure is repeated to find the desired value of ARL_0 . Once the proper choice of $L_{MSS(S)}$ and $K_{MSS(S)}$ are obtained, then the shifts in variance and obtained ARL_1 values are added.

4. Comparative Analysis

In practice, if the variation in the quality characteristics is reduced, this leads to an efficient production process. However, if the variation in the quality characteristics increases, the production process deteriorates. Hence, most quality experts are interested in diagnosing the effect of process deterioration. Therefore, this study is also designed to evaluate the performance of the designed charts ($MA-S_{MSS(S)}^2$) and $DMA-S_{MSS(S)}^2$) by using incremental shifts ($\delta = 1, 1.1, 1.2, 1.3, 1.4, 1.5, 1.6, 1.7, 1.8, 1.9, 2$) in the dispersion parameter. The shift is defined as $\delta = \sigma_1/\sigma_0$ for the dispersion parameter, where σ_0 and σ_1 are the standard deviation of IC and OOC processes, respectively. Under different MSS schemes, a comparative analysis has been made between these designed charts along with the existing *Shewhart-S*²_{MSS(S)} chart (cf. Tables 2 and 3). The *ARL*₁, *MDRL*₁ and *SDRL*₁ are used as performance measures to examine the performances of the above-mentioned control charts.

Under different sampling schemes of *MSS* at constant c = 2, the results of the *Shewhart*- $S^2_{MSS(S)'}MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ charts are shown in Table 2. The primary findings are listed below:

It is observed that the $DMA-S^2_{MSS(S)}$ chart outperformed the $Shewhart-S^2_{MSS(S)}$ and $MA-S^2_{MSS(S)}$ charts on the same amount of shift in the dispersion parameter. For example, when n = 5, a 30% increase in the change in the dispersion parameter reduces the ARL_1 values of the $Shewhart-S^2_{MSS(1)}$, $MA-S^2_{MSS(1)}$ and $DMA-S^2_{MSS(1)}$ charts to 72.18, 65.18 and 64.29, respectively. However, when n = 7 and $\delta = 1.5$, the ARL_1 values 31.10, 21.91 and 21.64 are reported for the $Shewhart-S^2_{MSS(5)}$, $MA-S^2_{MSS(5)}$ and $DMA-S^2_{MSS(5)}$ charts, respectively.

The findings also reveal that increasing the sample size leads to better performance of the charts. For example, the $DMA-S^2_{MSS(S)}$ chart outperformed the others; therefore, at $\delta = 1.4$, the ARL_1 value of the $DMA-S^2_{MSS(2)}$ chart is reported as 44.36 when n = 5, while for the same settings with n = 7, it is reported as 31.60.

The findings of the *Shewhart-S*²_{MSS(S)}, $MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ charts under the *MSS* scheme with c = 3 are shown in Table 3. The primary findings are listed below:

- It is noted that the $DMA-S^2_{MSS(S)}$ chart outperformed the $Shewhart-S^2_{MSS(S)}$ and $MA-S^2_{MSS(S)}$ charts at a fixed amount of shift in the dispersion parameter. For example, when n = 5, a 60% increase in the dispersion parameter reduces the ARL_1 values of the $Shewhart-S^2_{MSS(7)}$, $MA-S^2_{MSS(7)}$ and $DMA-S^2_{MSS(7)}$ charts to 34.21, 22.74 and 17.00, respectively. However, when n = 7 and $\delta = 1.7$, the ARL_1 values 28.73, 20.29 and 10.00 are reported for the $Shewhart-S^2_{MSS(9)}$, $MA-S^2_{MSS(9)}$, $MA-S^2_{MSS(9)}$ and $DMA-S^2_{MSS(9)}$ charts, respectively.
- Moreover, the results also show that the charts' performance improved as the sample size increased. For example, the $DMA-S^2_{MSS(S)}$ chart outperformed the others; therefore, at $\delta = 1.2$, the ARL_1 value of the $DMA-S^2_{MSS(8)}$ chart is reported as 115.87 when n = 5, while for the same settings with n = 7, it is reported as 88.79.

Overall, from Tables 2 and 3, it is also revealed that based on different *MSS* schemes, the $DMA-S^2_{MSS(S)}$ chart performed better than the *Shewhart-S*²_{MSS(S)} and $MA-S^2_{MSS(S)}$ charts with respect to ARL_1 at a pre-fixed $ARL_0 = 370$.

Furthermore, to check the effect of moving average span on the detection ability of the designed $MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ charts, sensitivity analysis was performed based on various choices of moving average span (w = 2, 3, 5, 10 and 15). The results of the sensitivity analysis for the $MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ charts with c = 2 and 3 are presented in Figures 1–4. At the pre-specified $ARL_0 = 370$, it is noted that the performance ability of the $MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ charts increased with the increase in the moving average span. For example, it can be easily observed in Figures 1–4 that at w = 15, both the designed charts have the lowest curves of ARL_1 for all the above-mentioned MSS schemes as compared to all the choices of w for c = 2 and 3.

Furthermore, a comparative study of the best proposed $MA-S^2_{MSS(1)}$ and $DMA-S^2_{MSS(1)}$ charts with the existing S^2 chart was designed based on the repetitive sampling $\left(S^2_{repetitive}\right)$ proposed by Aslam et al. [46]. For the pre-fixed $ARL_0 = 370$ and c = 2, the run length curves of the $MA-S^2_{MSS(1)}$, $DMA-S^2_{MSS(1)}$ and $S^2_{repetitive}$ are plotted in Figure 5. It is observed that for small amounts of shift (i.e., 1.1 to 1.5), the $MA-S^2_{MSS(1)}$ and $DMA-S^2_{MSS(1)}$ charts have comparatively better detection ability, while for large shifts (i.e., more than 1.5), the $S^2_{repetitive}$ chart showed relatively lower ARL values. The dominance of the $S^2_{repetitive}$ chart in the presence of large shifts is natural because of the Shewhart structure.



Figure 1. The effect of moving average span parameter (*w*) on the performance of the $MA-S^2_{MSS(S)}$ control chart under MSS schemes for constant c = 2; (**a**) $MSS_{(1)}$, (**b**) $MSS_{(2)}$, (**c**) $MSS_{(3)}$, (**d**) $MSS_{(4)}$, (**e**) $MSS_{(5)}$.



Figure 2. The effect of moving average span parameter (*w*) on the performance of the MA- $S^2_{MSS(S)}$ control chart under MSS schemes for constant c = 3; (**a**) $MSS_{(6)}$, (**b**) $MSS_{(7)}$, (**c**) $MSS_{(8)}$, (**d**) $MSS_{(9)}$, (**e**) $MSS_{(10)}$.



Figure 3. The effect of moving average span parameter (*w*) on the performance of the $DMA-S^2_{MSS(S)}$ control chart under MSS schemes for constant c = 2; (**a**) $MSS_{(1)}$, (**b**) $MSS_{(2)}$, (**c**) $MSS_{(3)}$, (**d**) $MSS_{(4)}$, (**e**) $MSS_{(5)}$.



Figure 4. The influence of moving average span parameter (*w*) on the performance of the *DMA*- $S^2_{MSS(S)}$ control chart under *MSS* schemes for constant c = 3; (**a**) $MSS_{(6)}$, (**b**) $MSS_{(7)}$, (**c**) $MSS_{(8)}$, (**d**) $MSS_{(9)}$, (**e**) $MSS_{(10)}$.



Figure 5. At a fixed constant c = 2, a comparison of the best proposed $MA-S^2_{MSS(1)}$ and $DMA-S^2_{MSS(1)}$ charts with the S^2 chart based on repetitive sampling $\left(S^2_{repetitive}\right)$.

5. Case Study

This section contains real-life applications of the designed control charts to monitor process dispersion in a ZA fertilizer production-based dataset. Mashuri et al. [47] also used this dataset to illustrate the better performance of proposed multivariate control charts in terms of monitoring the process variability. ZA fertilizer is frequently used to increase the concentration of sulfur and nitrogen in soil. It is also called ammonium sulfate fertilizer. The production process of ZA fertilizer is based on six stages (cf. Figure 6): carbonation, reaction and gas scrub, filtration, neutralization, evaporation and crystal, and drying and cooling stages. Air and carbon dioxide are emitted in this production process.



Figure 6. Stages of ZA fertilizer production process.

In this case study, the concentration of $CO_2(g/L)$ is the variable of interest in the fertilizer production process. This variable has 526 values consisting of the concentration of $CO_2(g/L)$ in the body and in the glassy coating on ceramics called glaze. These observations related to the body are considered in-control (239 values) data, while observations related to glaze are considered out-of-control (287 values) data. To assess the normality of both datasets, probability plots were prepared, which are shown in Figure 7. It should be noted that the in-control data are normally distributed, with a mean of 0.3975 and 0.2115 standard deviation. However, the out-of-control data are not normally distributed; their mean is 0.5459 with 0.424 standard deviation. By adopting the mechanism of MSS, 174 samples of size 5 were drawn from this dataset, which has two subgroups (79 in control and 95 out of control). To evaluate the performance of both the designed charts, the in-control subgroup of this dataset was utilized to calculate the proposed $MA-S^2_{MSS(1)}$ and $DMA-S^2_{MSS(1)}$ charts' control limits at the pre-defined $ARL_0 = 370$.



Figure 7. The probability plots of the concentration of $CO_2(g/L)$ with respect to body and glaze.

Figure 8 presents a graphical view of both the proposed charts. On the X-axis, the subgroups (sample numbers) are plotted, and on the y-axis, the plotting statistics of both the proposed charts are plotted against their respective control limits. The pink shaded area represents in-control points while white colored is referring to the out-of-control region. It shows that the $MA-S^2_{MSS(1)}$ control chart detects an out-of-control signal after inspecting 92 samples, while the $DMA-S^2_{MSS(1)}$ control chart detects out-of-control points after observing 90 samples. Both control charts have alternatively in-control and out-of-control points in out-of-control regions; therefore, a specific pattern can be seen in both the $MA-S^2_{MSS(1)}$ and $DMA-S^2_{MSS(1)}$ charts (cf. Figure 8). From the above simulation study, it is noted that the $DMA-S^2_{MSS(5)}$ chart has outperformed the *Shewhart-S*²_{MSS(5)} and $MA-S^2_{MSS(5)}$ charts with a fixed amount of shift in the dispersion parameter. Similarly, by implementing the real-life example, we observe that the detection ability of the $DMA-S^2_{MSS(1)}$ control chart is high, and it is more sensitive than the $MA-S^2_{MSS(1)}$ control chart for the monitoring of process variability.



Figure 8. Demonstration for (**a**) $MA-S^2_{MSS(S)}$ and (**b**) $DMA-S^2_{MSS(S)}$ control charts using ZA fertilizer production dataset.

Furthermore, the proposed charts have wide real-life applications in different major fields of life. For example, we can utilize this control charting structure in the chemical industry, medical industry, glass field, ceramic industry, engineering, fertilizer production, hard-bake process and wind farm data (cf. Riaz et al. [22], Anwar et al. [24] and Khan et al. [29]).

6. Conclusions

Usually, memory-type control charts are used to detect small to moderate shifts in the location or dispersion process parameters. The process is said to be OOC depending on the amount of shift detected in the location or dispersion parameters. Usually, it is preferable to detect a shift in the dispersion parameter of the process before the detection of a shift in the location parameter. In this study, we have designed memory-type $MA-S^2_{MSS(S)}$ and $DMA-S^2_{MSS(S)}$ control charts for the monitoring of the process dispersion parameter using a modified successive sampling technique. Additionally, a comparative analysis with the existing *Shewhart-S*²_{MSS(S)} chart has been presented using different performance measures (ARL, MDRL and SDRL). From the results, we have observed that the value of ARL_1 decreases with the increasing value of dispersion shift and sample size at a fixed value of $ARL_0 = 370$ (cf. Tables 2 and 3). Moreover, the findings lead to the conclusion that the designed $DMA-S^2_{MSS(S)}$ control chart performs better than $Shewhart-S^2_{MSS(S)}$ and $MA-S^2_{MSS(S)}$ under all the aforementioned MSS schemes. We have also noted that increasing values of the moving average span (w) show a declining trend in ARL_1 curves under all MSS schemes (cf. Figures 1–4).

Generally, the structure of mixed EWMA and CUSUM charts are more efficient compared to traditional MA, DMA, EWMA and CUSUM charts because they are more sensitive to the detection of small shifts in any process (cf. [48]). Therefore, one could extend this study by using different choices of MSS schemes and sample sizes to design a new mixed structure of the EWMA and CUSUM control charts. Moreover, the current study is designed based on the known parameter case (K-case), while the unknown parameter case (U-case) is recommended for future study. Furthermore, the MSS structure is proposed under normal distribution (symmetric distribution); however, one could propose *MSS* structure based on asymmetrical distribution and further extend the performance ability of the proposed control charts under the new MSS structure based on asymmetrical distributions.

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