

Development of an Aspen Plus® model for the process of hydrogen production by black liquor electrolysis

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Supplementary information

Mass balance

The mass balance provided the information needed to simulate the BL electrolysis (Table S1). The mass balance was obtained through BL electrolysis in a laboratory cell with the following conditions: $T = 25\text{ }^{\circ}\text{C}$, $N = 1$, $V_{\text{cell}} = 3.0\text{ V}$, $P = 1\text{ bar}$, and $W_{\text{stack}} = 0.915\text{ W}$. The cell worked in batch operation for 3 hours.

Table S1. Mass balance based on BL electrolysis in a laboratory cell.

| Component | | Inlet (g) | Outlet (g) |
|-----------------------|---------------------------------|-----------|------------|
| Anode: Nickel plate | | 20.650 | 20.076 |
| Cathode: Nickel plate | | 20.507 | 20.507 |
| Black liquor | H ₂ O | 264.720 | 264.454 |
| | NaOH | 3.574 | 3.574 |
| | Na ₂ S | 2.118 | 2.118 |
| | Na ₂ SO ₄ | 7.412 | 7.412 |
| | KOH | 10.920 | 10.920 |
| | K ₂ CO ₃ | 0.199 | 0.199 |
| | K ₂ SO ₄ | 0.596 | 0.596 |
| | Lignin | 4.798 | 4.598 |
| | Sugars | 2.214 | 2.214 |
| | Hydroxy-carboxylic acids | 0.417 | 0.417 |
| | Acid Low MW volatiles | 6.419 | 6.419 |
| Solid | Ni | 0 | 0.026 |
| | H ₂ | 0 | 0.030 |
| | Ni | 0 | 0.548 |
| | O | 0 | 0.172 |
| | S | 0 | 0.103 |
| Total | Lignin | 0 | 0.200 |
| | | 344.543 | 344.581 |

The following assumptions were made to obtain the mass balance: (i) the formed gas was pure hydrogen, and (ii) hydrogen came only from the water. Due to the components

simplifications described in section 2.3 of the paper, the mass balance used in Aspen Plus® is presented in Table S2.

Table S2. The mass balance used in Aspen Plus®.

| Component | Inlet (mol/h) | Outlet (mol/h) |
|---------------------------------|------------------------|------------------------|
| Ni (s) | 0.1173 | 0.1140 |
| H ₂ O | 4.902 | 4.897 |
| NaOH | 0.02978 | 0.02978 |
| Na ⁺ | 0.01810 | 0.01810 |
| S ²⁻ | 9.050×10 ⁻³ | 7.978×10 ⁻³ |
| Na ₂ SO ₄ | 0.01669 | 0.01669 |
| KOH | 0.06488 | 0.06488 |
| K ₂ CO ₃ | 4.789×10 ⁻⁴ | 4.789×10 ⁻⁴ |
| K ₂ SO ₄ | 1.139×10 ⁻³ | 1.139×10 ⁻³ |
| p-Coumaryl Alcohol | 1.838×10 ⁻³ | 1.762×10 ⁻³ |
| Glycose | 4.095×10 ⁻³ | 4.095×10 ⁻³ |
| Citric Acid | 7.235×10 ⁻⁴ | 7.235×10 ⁻³ |
| Acetic Acid | 0.03560 | 0.03560 |
| H ₂ | 0 | 1.469×10 ⁻⁴ |
| Ni ²⁺ | 0 | 3.731×10 ⁻³ |
| O ₂ | 0 | 1.865×10 ⁻³ |
| Anthracene | 0 | 7.680×10 ⁻⁵ |
| S | 0 | 1.073×10 ⁻³ |
| Total | 5.202 | 5.204 |

From this mass balance, it is possible to extract useful information, such as the stoichiometric factors (Table S3).

Table S3. Stoichiometric factors for the different compounds.

| Compounds | Stoichiometric factors |
|---------------------------------|------------------------|
| Acetic Acid | 0 |
| Citric Acid | 0 |
| p-Coumaryl Alcohol | −0.0155 |
| Anthracene | 0.0155 |
| Glycose | 0 |
| H ₂ | 1 |
| H ₂ O | −0.993 |
| K ₂ CO ₃ | 0 |
| K ₂ SO ₄ | 0 |
| KOH | 0 |
| Na ₂ SO ₄ | 0 |
| Na ⁺ | 0 |
| NaOH | 0 |
| Ni | −0.656 |
| Ni ²⁺ | 0.751 |
| O ₂ | 0.376 |
| S | 0.216 |
| S ^{2−} | −0.216 |

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Batch operation vs. continuous operation

Figures S1 and S2 compare the experimental data and the adjusted polarization curve, both for batch and continuous operation.

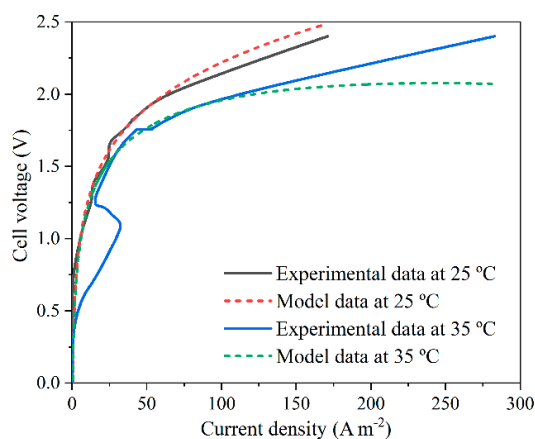


Figure S1. Comparison between experimental data and the model for batch simulation at 25 °C and 35 °C.

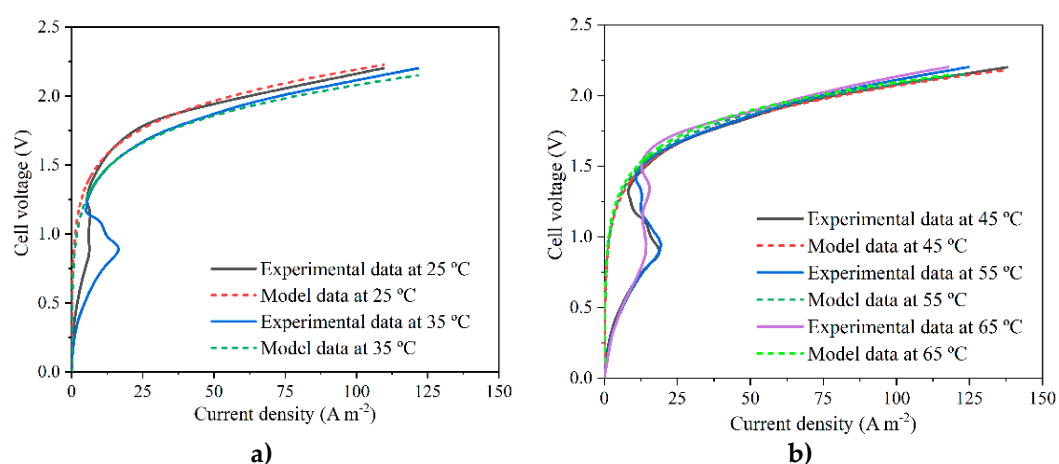


Figure S2. Comparison between experimental data and the model at different temperatures for continuous operation.

Sensitivity analysis

This section shows the electrolyzer sensitivity analysis data to understand how each variable influences the others.

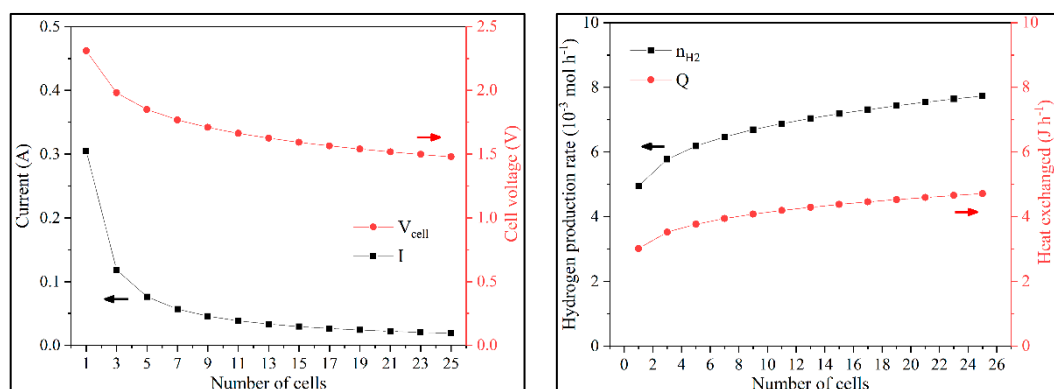


Figure S3. Variation of i , V_{cell} , n_{H_2} , and Q_{T} with N in continuous operation.

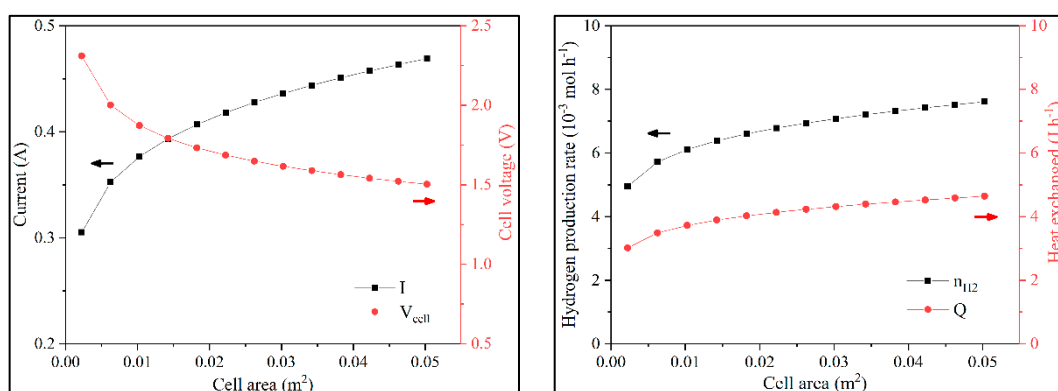


Figure S4. Variation of i , V_{cell} , n_{H_2} , and Q_{T} with A_{cell} in continuous operation.

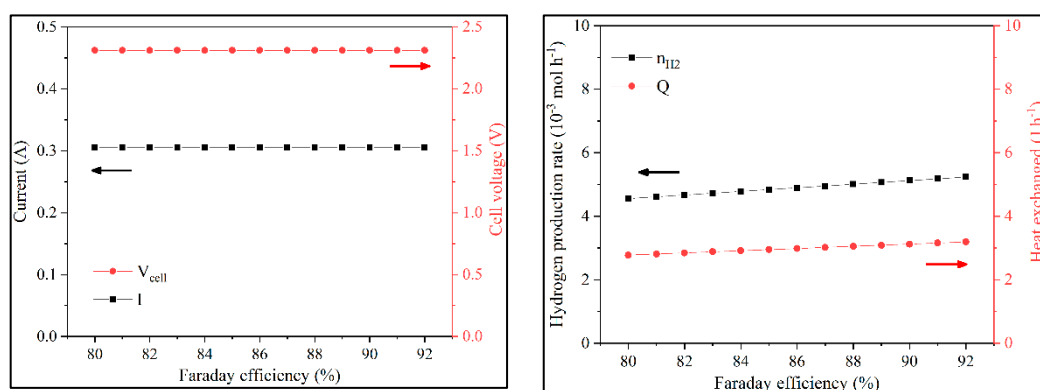


Figure S5. Variation of i , V_{cell} , n_{H_2} , and Q_T with the Faraday efficiency in continuous operation.

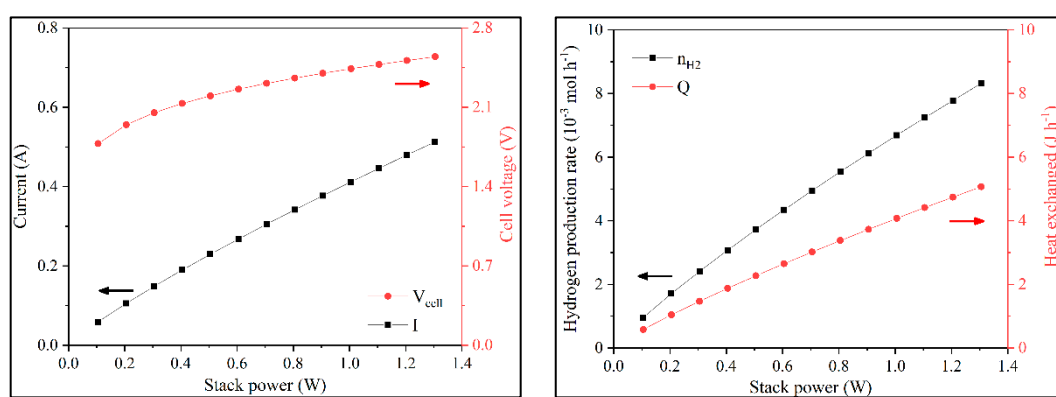


Figure S6. Variation of i , V_{cell} , n_{H_2} , and Q_T with the electric power in continuous operation.

Table S4. Sensitivity analysis for Faraday efficiency.

| Efficiency Increment (%) | Batch operation | | | | Continuous operation | | | |
|--------------------------|-----------------|------------------------------|-----------------------------|------------------|----------------------|------------------------------|-----------------------------|------------------|
| | Δi (%) | ΔV_{cell} (%) | Δn_{H_2} (%) | ΔQ_T (%) | Δi (%) | ΔV_{cell} (%) | Δn_{H_2} (%) | ΔQ_T (%) |
| -5.75 | 0 | 0 | -5.75 | -5.75 | 0 | 0 | -5.75 | -5.75 |
| -3.45 | 0 | 0 | -3.45 | -3.45 | 0 | 0 | -3.45 | -3.45 |
| 3.45 | 0 | 0 | 3.45 | 3.45 | 0 | 0 | 3.45 | 3.45 |
| 5.75 | 0 | 0 | 5.75 | 5.75 | 0 | 0 | 5.75 | 5.75 |

Table S5. Sensitivity analysis for temperature.

| T Increment (%) | Batch operation | | | | Continuous operation | | | |
|-----------------|-----------------|------------------------------|-----------------------------|------------------|----------------------|------------------------------|-----------------------------|------------------|
| | Δi (%) | ΔV_{cell} (%) | Δn_{H_2} (%) | ΔQ_T (%) | Δi (%) | ΔV_{cell} (%) | Δn_{H_2} (%) | ΔQ_T (%) |
| 16 | 1.28 | -1.26 | 1.28 | 4.27 | 2.54 | -2.48 | 2.54 | 14.54 |
| 28 | 3.99 | -3.84 | 3.99 | 12.99 | 3.78 | -3.64 | 3.78 | 24.82 |
| 32 | 6.96 | -6.51 | 6.96 | 19.00 | 4.55 | -4.35 | 4.55 | 34.66 |
| 40 | 15.98 | -13.78 | 15.98 | 34.11 | 5.08 | -4.84 | 5.08 | 81.09 |