



Article Electromagnetic Flow of SWCNT/MWCNT Suspensions in Two Immiscible Water- and Engine-Oil-Based Newtonian Fluids through Porous Media

Ahmad Zeeshan ¹, Nasir Shehzad ¹, Muhammad Atif ¹, Rahmat Ellahi ^{1,2,*} and Sadiq M. Sait ³

- ¹ Department of Mathematics & Statistics, Faculty of Basic and Applied Sciences, International Islamic University, Islamabad 44000, Pakistan; ahmad.zeeshan@iiu.edu.pk (A.Z.); nasir.shehzad.vt@iiu.edu.pk (N.S.); muhammad.msma636@iiu.edu.pk (M.A.)
- ² Fulbright Fellow Department of Mechanical Engineering, University of California Riverside, Riverside, CA 92521, USA
- ³ Center for Communications and IT Research, Research Institute, King Fahd University of Petroleum & Minerals, Dhahran 31261, Saudi Arabia; sadiq@kfupm.edu.sa
- * Correspondence: rellahi@alumni.ucr.edu or rahmatellahi@yahoo.com

Abstract: This article deals with steady-state laminar, electrically conducting immiscible fluids. The Newtonian fluid considered passes between two parallel vertical plates in a porous medium. The channel consists of two regions, one of them filled with engine-oil-based carbon nanotubes (CNTs) and the second region filled with water through a porous medium. The assumptions for the channel walls are electrically non-conducting and are at two different temperatures. Mathematical formulation is formed using rules for the conservation of mass, momentum and energy in both regions. Continuous conditions are used for velocity, temperature and also for shear pressure at the crossing area. The governing equations are first transformed in a non-dimensional form by using appropriate transformations, and then the subsequent differential equations are solved using a topological approach by means of the homotopy analysis method. It is found that the impact of the actual boundaries utilized in the issue is directed, and the outcomes are introduced graphically and discussed. It is noted that the engine-oil SWCNTs experience a significant increase in temperature profiles as compared to the engine-oil MWCNTs, while the movement of fluid slowdown in the nanofluid region due to the concentration of nanoparticles and the thickness of the thermal boundary layer increases by increasing the volume fraction of the carbon nanotubes.

Keywords: porous medium; Newtonian fluids; carbon nanotubes (CNTs); magnetohydrodynamics; homotopy analysis method

1. Introduction

The study of porous medium transport phenomena has been given valuable attention due to its prominence in industrial and engineering applications. Its applications contain drying technology, thermal insulation, catalytic reactions, crowded bed heat exchangers, geothermal systems, petroleum industries and electronics cooling [1]. The porous medium is used also in biomedical applications, such as drug conveyance, porous frames for tissue engineering, transportation in biological tissues and tissue replacement production. Initially, the Darcy law that addresses the exact connection of the Darcian velocity and the pressure drop through the porous media is utilized by Vafai and Tein [2,3]. They present a comprehensive study of the Brinkman–Forchheimer prolonged Darcy model. The study of fluid flows and heat production of two electrically non-conducting fluids in upward infinitely long plates in the nonexistence of porous media and by applying a magnetic field is concluded by Chamkha [4]. Khaled and Vafai [5] investigated diverse biomedical zones which use porous media models in the blood flows in tumors, diffusion process in brain



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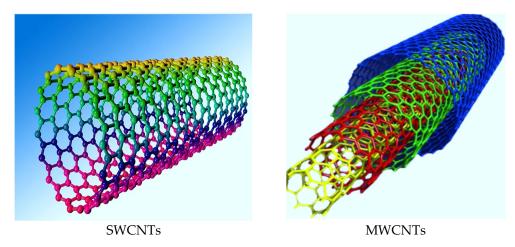
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Copyright: © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). tissues and bio-heat transmission in tissues. Natural convection in non-Darcy porous media flow is noted in a heated surface by Plumb and Huenefeld [6]. Nakayama et al. [7] found out the exact and approximate solutions of the forced convection flow through parallel porous plates.

Nanofluids set up by blending nanoparticles (10–50 nm) to base fluid [8] were recently used in energy and biomedical applications (nano-drug delivery and cancer therapeutics) [9]. Nanofluids are used to significantly increase heat transfer properties in industries' cooling applications, nuclear reactors and electronics. In 1991, Lijima and Lchihashi [10] discovered carbon nanotubes (CNTs). CNTs are hexagonally formed arrangements of carbon particles that have been transformed into tubes. CNTs with an undetermined carbon-wall structure and diameter less than 100 nm were discovered by Radushkevich and Lukyanavich [11]. The thermal conductivity of CNTs is high with exceptional corrosion resistance and exceptional mechanical strength. The novel properties of CNTs make them valuable in applications such as nanotube radars, nanotube transistors, microwave amplifiers, solar cells and handheld X-rays. CNTs are divided into two categories explicitly, as is shown in Figure 1, the single-wall carbon nanotubes (SWCNTs) and multi-wall carbon nanotubes (MWCNTs). Chio et al. [12] analyzed an uncharacteristic thermal conductivity boost in the CNTs. Homogenous CNT composites for electrical application are studied by Ramasubramaniam et al. [13]. Ellahi et al. [14] studied the natural convective boundary layer flow of nanofluids with SWCNTs and MWCNTs. Magnetohydrodynamics nanofluid hydrothermal behavior in a cubic cavity heated from below is presented by Sheikholeslami and Ellahi [15]. Haq et al. [16] studied the MHD pulsatile flow of engine-oil-based CNTs between two concentric cylinders. Ding et al. [17] inspected the heat transmission analysis of aqueous suspensions for CNTs. The investigation of SWCNTs and MWCNTs with kerosene oil and water as base fluids and the thermos-physical properties of CNTs in terms of the solid volume fraction used through empirical correlation is reported by Tiwari et al. [18]. Nadeem et al. [19] investigated the convective heat transfers in MHD slip flow over a stretching surface in the presence of CNTs; they found that the heat transfer rate and skin fraction for engine-oil-based CNTs are higher than water-based CNTs. Nasiri et al. [20] have shown that the CNTs' structure and stability are strongly dependent on the functionalization and preparation method of the nano-suspension. In conjugate heat transference in a quadrilateral porous cavity heated diagonally and loaded up with nanofluids contemplated by Chamkha and Ismael [21], the problem was interrogated numerically by using the Over Successive Relaxation (OSR) finite-difference method. Carbon nanotubes with water-based nanofluid were observed in vertical truncated cones under the consideration of the first and second levels of truncation by Ellahi et al. [22]. Authors claimed that heat transfer in cones rapidly improved as the concentration of nanoparticles, half-cone angle and wavelength ratio enhanced gradually. Heat production or immersion results depending on temperature are assumed and reported by Vajravelu and Hadjinicolaou [23], Chamkha [24], Sparrow and Cess [25], Vajravelu and Nayfeh [26] and Ellahi et al. [27]. Enhanced thermal conductivity in multi-walled carbon nanotubes (MWCNTs) with two different base fluids, ethylene glycol and engine-oil nanofluids is observed by Liu et al. [28] under the influence of nanoparticle concentration. They noted that the thermal conductivity of the engine oil MWCNT nanofluid improved up to 30% with a 2% nanoparticle concentration, as compared to the thermal conductivity of ethylene glycol MWCNT nanofluid at 12.4% with a 1% nanoparticle concentration. Carbon nanotubes (SWCNTs or MWCNTs) are used as particle material due to their high thermal conductivity properties.





The motivation of the above literature and the current innovative study is to report on the study of fluid flow between a vertical channel of two different fluids—water- and engine-oil-based CNTs through a porous medium. The governing equations are coupled and highly nonlinear due to convection and body forces. The system of equations is solved analytically by using mathematical software. The following sections represent the origination of the problem, solving the problem, the consequences and discussion, then finally, concluding remarks of significant outcomes.

2. Mathematical Formulation

The incompressible steady-state laminar movement of two immiscible fluids in between two parallel plates of infinite length extended in x and z directions packed with engine-oil carbon nanotube nanofluid and water is the matter of interest here.

The system took in a porous medium with temperatures T_{w1} of the right plate and temperatures T_{w2} of the left plate. The region $0 \le y \le h_1$ is contained with engine-oil-based carbon nanotubes (fluid-1), and region $-h_2 \le y \le 0$ is filled with water (fluid-2). Additionally, the mediums of both regions are supposed to be porous. The uniform magnetic field is applied normally to the direction of flow. The coordinate system and above assumptions are shown in Figure 2. Mathematical equations of problem in component form can be written as [4]:

$$\mu_{1nf} \frac{d^2 u_1}{dy_1^2} + \rho_{1nf} g \beta_{1nf} (T_1 - T_0) = \frac{\partial p}{\partial x} + \sigma_{1nf} B_0^2 u_1 + \frac{\mu_{1nf} u_1}{K} + \rho_{1nf} C_F u_1^2 \tag{1}$$

$$k_{1nf}\frac{d^2T_1}{dy_1^2} + Q_1(T_1 - T_0) = 0$$
⁽²⁾

$$\mu_{2f}\frac{d^2u_2}{dy_2^2} + \rho_{2f}g\beta_{2f}(T_2 - T_0) = \frac{\partial p}{\partial x} + \sigma_{2f}B_o^2u_2 + \frac{\mu_{2f}u_2}{K} + \rho_{2f}C_Fu_2^2$$
(3)

$$k_{2f}\frac{d^2T_2}{dy_2^2} + Q_2(T_2 - T_0) = 0$$
⁽⁴⁾

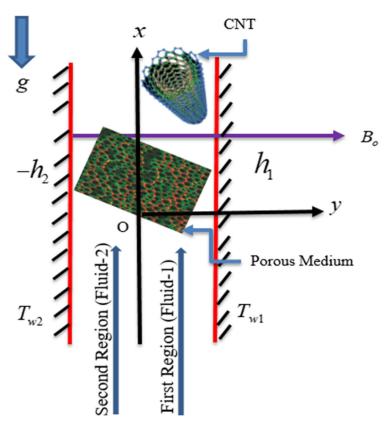


Figure 2. Geometrical representation of the problem.

The conditions at boundary and interface for this study can be expressed as

$$u_{1}(h_{1}) = 0, T_{1}(h_{1}) = T_{w1}, u_{1}(0) = u_{2}(0), \ \mu_{1nf} \frac{du_{1}}{dy_{1}}(0) = \mu_{2f} \frac{du_{2}}{dy_{2}}(0), \ T_{1}(0) = T_{2}(0), \ k_{1nf} \frac{dT_{1}}{dy_{1}}(0) = k_{2f} \frac{dT_{2}}{dy_{2}}(0), u_{2}(-h_{2}) = 0, \ T_{2}(-h_{2}) = T_{w2},$$

$$(5)$$

where the *x* axis is along flow direction and y_i (i = 1, 2) is perpendicular to both fluids. u_1 , u_2 , T_1 and T_2 are velocities and temperatures of fluid-1 and fluid-2, respectively. The fluid is flowing due to the mixed convection in the system and this convection inserts a force on flow in a downward direction along the cold surface and upward direction along the hot surface. Equation (5) shows that both plates are at rest with different temperatures at the walls. Velocity and temperature at the interface for the two fluids are indistinguishable. Heat flux at the interface is continuous and we assume that the fluids in both the regions share a common pressure gradient. To convert the above Equations (1)–(5) to their dimensionless forms with the assumption T_0 treated as T_{w2} , the following transformations are taken:

$$\zeta_i = \frac{y_i}{h_i}, \ F_i = \frac{u_i}{\overline{u}_1}, \ \theta_i = \frac{T_i - T_o}{T_{w1} - T_{w2}}, \ P = \frac{\partial p / \partial x}{\mu_{1f} \overline{u}_1 / h_1^2} \right\} \text{ where } i = 1, 2.$$
(6)

The dimensionless forms of above equations are:

$$\frac{d^2 F_1}{d\zeta_1^2} - \frac{A_4}{A_3} M^2 F_1 - DF_1 - \frac{A_1}{A_3} IF_1^2 - \frac{1}{A_3} P + \frac{A_1 A_2}{A_3} \frac{Gr}{Re} \theta_1 = 0,$$
(7)

$$\frac{d^2\theta_1}{d\zeta_1^2} + \frac{\phi_1}{A_5}\theta_1 = 0,$$
(8)

$$\frac{d^2F_2}{d\zeta_2^2} - Smh^2 M^2 F_2 - h^2 DF_2 - Ih^2 mn F_2^2 - mh^2 P + \beta mnh^2 \frac{Gr}{Re} \theta_2 = 0,$$
(9)

$$\frac{d^2\theta_2}{d\zeta_2^2} + \phi_2\theta_2 = 0.$$
 (10)

Associated boundary conditions are:

$$F_{1}(1) = 0, \ \theta_{1}(1) = 1,$$

$$F_{1}(0) = F_{2}(0), A_{3} \frac{dF_{1}(0)}{d\zeta_{1}} = \frac{1}{mh} \frac{dF_{2}(0)}{d\zeta_{2}}, \theta_{1}(0) = \theta_{2}(0), A_{5} \frac{d\theta_{1}(0)}{d\zeta_{1}} = \frac{1}{hk} \frac{d\theta_{2}(0)}{d\zeta_{2}},$$

$$F_{2}(-1) = 0, \ \theta_{2}(-1) = 0$$
(11)

where

$$Gr = \frac{\rho_{1f}g\beta_{1f}h^{3}(T_{w1}-T_{w2})}{\mu_{1f}}, \text{Re} = \frac{\overline{u}_{1}h_{1}}{\mu_{1f}/\rho_{1f}}, M^{2} = \frac{\sigma_{1f}B_{0}^{2}h_{1}^{2}}{\mu_{1f}}, \phi_{1} = \frac{Q_{1}h_{1}^{2}}{k_{1f}}, S = \frac{\sigma_{2f}}{\sigma_{1f}}, \\ m = \frac{\mu_{1f}}{\mu_{2f}}, h = \frac{h_{2}}{h_{1}}, n = \frac{\rho_{2f}}{\rho_{1f}}, \beta = \frac{\beta_{2f}}{\beta_{1f}}, \phi_{2} = \frac{Q_{2}h_{2}^{2}}{k_{2f}}, k = \frac{k_{1f}}{k_{2f}}, D = \frac{h_{1}^{2}}{K}, I = \frac{C_{F}\overline{u}_{1}h_{1}^{2}}{\mu_{1f}/\rho_{1f}} \\ A_{1} = \frac{\rho_{1nf}}{\rho_{1f}}, A_{2} = \frac{\beta_{1nf}}{\beta_{1f}}, A_{3} = \frac{\mu_{1nf}}{\mu_{1f}}, A_{4} = \frac{\sigma_{1nf}}{\sigma_{1f}}, A_{5} = \frac{k_{1nf}}{k_{1f}}. \end{cases}$$
(12)

The physical properties of base fluids and nanotubes are described in Table 1.

Thermo-Physical Properties	Base Fluid		Carbon Nanotubes	
	Water	Engine Oil	SWCNTs	MWCNTs
Density ρ (kg/m ³)	997	884	2600	1600
Thermal conductivity <i>k</i> (w/mK)	0.613	0.145	6600	3000
Electrical conductivity σ (S/m)	5×10^{-6}	2×10^{-6}	10 ⁶	10 ⁶
Thermal expansion coefficient β (K ⁻¹)	$51 imes 10^{-6}$	$70 imes 10^{-5}$	$2 imes 10^{-5}$	$2 imes 10^{-5}$

The expression of density, dynamics viscosity, electrical conductivity, thermal conductivity and thermal expansion coefficient [29–31] of CNT are, respectively, described as:

$$\rho_{1nf} = (1-\phi)\rho_{1f} + \phi\rho_p \tag{13}$$

$$\mu_{1nf} = \mu_{1f} (1 - \phi)^{-2.5} \tag{14}$$

$$\sigma_{1nf} = \sigma_{1f} \left[1 + \frac{3\left(\frac{\sigma_p}{\sigma_{1f}} - 1\right)\phi}{\frac{\sigma_p}{\sigma_{1f}} + 2 - \left(\frac{\sigma_p}{\sigma_{1f}} - 1\right)\phi} \right]$$
(15)

$$k_{1nf} = k_{1f} \left[\frac{k_p + 2k_{1f} - 2\phi \left(k_{1f} - k_p \right)}{k_p + 2k_{1f} + 2\phi \left(k_{1f} - k_p \right)} \right]$$
(16)

$$\beta_{1nf} = \beta_{1f} \left[\frac{(1-\phi)\rho_{1f} + \phi\left(\frac{\beta_p}{\beta_{1f}}\right)\rho_p}{\rho_{1f}} \right],\tag{17}$$

where ϕ is the volume fraction of nanoparticles in percentage.

3. Solution to the Problem

Equations (7)–(10) are all nonlinear coupled due to the interface conditions and buoyancy effects.

To get an analytic solution, a homotopic technique [32] is utilized. Initial approximations $F_{10}(\zeta_1)$, $F_{20}(\zeta_2)$, $\theta_{10}(\zeta_1)$, $\theta_{20}(\zeta_2)$ and linear operators \pounds_{F_1} , \pounds_{F_2} , \pounds_{θ_1} , \pounds_{θ_2} for velocities and temperatures are:

$$F_{10}(\zeta_1) = 1 - \zeta_1^2, F_{20}(\zeta_2) = \zeta_2^3 + 1 \theta_{10}(\zeta_1) = \zeta_1^2, \theta_{20}(\zeta_2) = \zeta_2^3 + \zeta_2^2$$
(18)

$$\mathcal{L}_{F_1} = \frac{d^2 F_1}{d\zeta_1^2}, \ \mathcal{L}_{F_2} = \frac{d^2 F_2}{d\zeta_2^2}, \ \mathcal{L}_{\theta_1} = \frac{d^2 \theta_1}{d\zeta_1^2}, \ \mathcal{L}_{\theta_2} = \frac{d^2 \theta_2}{d\zeta_2^2}.$$
(19)

With convergence control auxiliary parameters \hbar_{F_1} , \hbar_{F_2} , \hbar_{θ_1} , \hbar_{θ_2} and nonlinear operators N_{F_1} , N_{F_2} , N_{θ_1} , N_{θ_2} with embedding parameter $r \in [0, 1]$, the homotopy of the zeroth-order problem is written as:

$$\begin{array}{c} (1-r)\mathcal{L}_{F_{1}}[F_{1}(\zeta_{1},r)-F_{10}(\zeta_{1})] = r\hbar_{F_{1}}N_{F_{1}}[F_{1}(\zeta_{1},r),\,\theta_{1}(\zeta_{1},r)],\\ (1-r)\mathcal{L}_{F_{2}}[F_{2}(\zeta_{2},r)-F_{20}(\zeta_{2})] = r\hbar_{F_{2}}N_{F_{2}}[F_{2}(\zeta_{2},r),\,\theta_{2}(\zeta_{2},r)],\\ (1-r)\mathcal{L}_{\theta_{1}}[\theta_{1}(\zeta_{1},r)-\theta_{10}(\zeta_{1})] = r\hbar_{\theta_{1}}N_{\theta_{1}}[F_{1}(\zeta_{1},r),\,\theta_{1}(\zeta_{1},r)],\\ (1-r)\mathcal{L}_{\theta_{2}}[\theta_{2}(\zeta_{2},r)-\theta_{20}(\zeta_{2})] = r\hbar_{\theta_{2}}N_{\theta_{2}}[F_{2}(\zeta_{2},r),\,\theta_{2}(\zeta_{2},r)]. \end{array}$$

$$N_{F_{1}}[F_{1}(\zeta_{1}, r), \theta_{1}(\zeta_{1}, r)] = -\frac{1}{A_{3}}P + \frac{\partial^{2}F_{1}(\zeta_{1}, r)}{\partial\zeta_{1}^{2}} - \frac{A_{4}}{A_{3}}M^{2}F_{1}(\zeta_{1}, r) - \frac{A_{1}}{A_{3}}IF_{1}^{2}(\zeta_{1}, r) - DF_{1}(\zeta_{1}, r) + \frac{A_{1}A_{2}}{A_{3}}\frac{Gr}{Re}\theta_{1}(\zeta_{1}, r), N_{F_{2}}[F_{2}(\zeta_{2}, r), \theta_{2}(\zeta_{2}, r)] = -mh^{2}P + \frac{\partial^{2}F_{2}(\zeta_{2}, r)}{\partial\zeta_{2}^{2}} - Smh^{2}M^{2}F_{2}(\zeta_{2}, r) - Ih^{2}mnF_{2}^{2}(\zeta_{2}, r) + \betamnh^{2}\frac{Gr}{Re}\theta_{2}(\zeta_{2}, r), N_{\theta_{1}}[F_{1}(\zeta_{1}, r), \theta_{1}(\zeta_{1}, r)] = \frac{\partial^{2}\theta_{1}(\zeta_{1}, r)}{\partial\zeta_{1}^{2}} + \frac{\phi_{1}}{A_{5}}\theta_{1}(\zeta_{1}, r), N_{\theta_{2}}[F_{2}(\zeta_{2}, r), \theta_{2}(\zeta_{2}, r)] = \frac{\partial^{2}\theta_{2}(\zeta_{2}, r)}{\partial\zeta_{2}^{2}} + \phi_{2}\theta_{2}(\zeta_{2}, r).$$

$$(21)$$

For
$$r = 0$$
 $r = 1$
 $F_1(\zeta_1, r) : F_{10}(\zeta_1) F_1(\zeta_1)$
 $F_2(\zeta_2, r) : F_{20}(\zeta_2) F_2(\zeta_2)$
 $\theta_1(\zeta_1, r) : \theta_{10}(\zeta_1) \theta_1(\zeta_1)$
 $\theta_2(\zeta_2, r) : \theta_{20}(\zeta_2) \theta_2(\zeta_2)$

$$(22)$$

The solution for velocity and temperature up to the *l*-th-order approximation can be expressed as:

$$F_{1}(\zeta_{1}) = F_{10}(\zeta_{1}) + \sum_{k=1}^{l} F_{1k}(\zeta_{1}),$$

$$F_{2}(\zeta_{2}) = F_{20}(\zeta_{2}) + \sum_{k=1}^{l} F_{2k}(\zeta_{2}),$$

$$\theta_{1}(\zeta_{1}) = \theta_{10}(\zeta_{1}) + \sum_{k=1}^{l} \theta_{1k}(\zeta_{1}),$$

$$\theta_{2}(\zeta_{2}) = \theta_{20}(\zeta_{2}) + \sum_{k=1}^{l} \theta_{2k}(\zeta_{2}).$$
(23)

Up to the third-order iteration, analytic expressions of temperature of both fluids are found by solving Equations (8) and (10), and then their solution is substituted in Equations (7) and (9) to the obtained velocities of both fluids.

$$\theta_{1}(\zeta) = \begin{bmatrix} e^{\frac{-\iota(-1+\zeta)\sqrt{\phi_{1}}}{\sqrt{A_{5}}}} \begin{pmatrix} \sqrt{A_{5}} \left(1+e^{\frac{2\iota\zeta\sqrt{\phi_{1}}}{\sqrt{A_{5}}}}\right) \left(-1+e^{2\iota\sqrt{\phi_{2}}}\right)hk\sqrt{\phi_{1}}\\ +\left(-1+e^{\frac{2\iota\zeta\sqrt{\phi_{1}}}{\sqrt{A_{5}}}}\right) \left(1+e^{2\iota\sqrt{\phi_{2}}}\right)\sqrt{\phi_{2}} \end{pmatrix} \\ \hline \sqrt{A_{5}} \left(1+e^{\frac{2\iota\sqrt{\phi_{1}}}{\sqrt{A_{5}}}}\right) \left(-1+e^{2\iota\sqrt{\phi_{2}}}\right)hk\sqrt{\phi_{1}}\\ +\left(-1+e^{\frac{2\iota\sqrt{\phi_{1}}}{\sqrt{A_{5}}}}\right) \left(1+e^{2\iota\sqrt{\phi_{2}}}\right)\sqrt{\phi_{2}} \end{bmatrix}, \quad (24)$$

$$\theta_{2}(\zeta) = \begin{bmatrix} \frac{\sqrt{A_{5}} h k \sqrt{\phi_{1}} \sin((1+\zeta)\sqrt{\phi_{2}})}{\sqrt{\phi_{2}} \cos(\sqrt{\phi_{2}}) \sin\left(\frac{\sqrt{\phi_{1}}}{\sqrt{A_{5}}}\right)} \\ +\sqrt{A_{5}} h k \sqrt{\phi_{1}} \cos\left(\frac{\sqrt{\phi_{1}}}{\sqrt{A_{5}}}\right) \sin(\sqrt{\phi_{2}}) \end{bmatrix},$$
(25)

$$F_1(\zeta) = -\frac{P}{M^2 A_4} - \frac{H_1}{H_2} - \frac{H_3}{H_4} + 2\frac{H_5}{H_6}$$
(26)

$$F_{2}(\zeta) = -\frac{P}{M^{2} S} - \frac{\Omega_{1}}{\Omega_{2}} - \frac{\Omega_{3}}{\Omega_{4}} + 2\frac{\Omega_{5}}{\Omega_{6}},$$
(27)

where

$$H_{1} = -2A_{1} A_{2} A_{5}^{3/2} e^{i\frac{\sqrt{\phi_{1}}}{\sqrt{A_{5}}}} \left(-1 + e^{2i\sqrt{\phi_{2}}}\right) Gr h k \sqrt{\phi_{1}} \left(\cos\left(\frac{\zeta\sqrt{\phi_{1}}}{\sqrt{A_{5}}}\right) - \cosh\left(\frac{M\zeta\sqrt{A_{4}}}{\sqrt{A_{3}}}\right)\right),$$
(28)

$$H_{2} = Re \left(A_{4} A_{5} M^{2} + A_{3} \phi_{1} \right) \left(\begin{array}{c} \left(1 + e^{\frac{2\iota\sqrt{\phi_{1}}}{\sqrt{A_{5}}}} \right) \left(-1 + e^{2\iota\sqrt{\phi_{2}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\iota\sqrt{\phi_{1}}}{\sqrt{A_{5}}}} \right) \left(1 + e^{2\iota\sqrt{\phi_{2}}} \right) \sqrt{\phi_{2}} \end{array} \right), \quad (29)$$

$$H_{3} = -4\iota A_{1} A_{2} \sqrt{A_{5}} e^{\iota \left(\frac{\sqrt{\phi_{1}}}{\sqrt{A_{5}}} + \sqrt{\phi_{2}}\right)} Gr \sqrt{\phi_{2}} \cos \sqrt{\phi_{2}} \left(\begin{array}{c} \sqrt{A_{4} A_{5}} M \sin\left(\frac{\zeta \sqrt{\phi_{1}}}{\sqrt{A_{5}}}\right) \\ -\sqrt{A_{3} \phi_{1}} \sinh\left(\frac{\sqrt{A_{4} M}}{\sqrt{A_{3}}}\right) \end{array}\right)$$
(30)

$$H_{4} = M \operatorname{Re} \sqrt{A_{4}} \left(A_{4} A_{5} M^{2} + A_{3} \phi_{1} \right) \left(\begin{array}{c} \sqrt{A_{5}} \left(1 + e^{\frac{2i\sqrt{\phi_{1}}}{\sqrt{A_{5}}}} \right) \left(-1 + e^{2i\sqrt{\phi_{2}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2i\sqrt{\phi_{1}}}{\sqrt{A_{5}}}} \right) \left(1 + e^{2i\sqrt{\phi_{2}}} \right) \sqrt{\phi_{2}} \end{array} \right),$$
(31)

$$H_{5} = e^{-\frac{\sqrt{A_{5}}M_{5}}{\sqrt{A_{5}}}} \left[\begin{array}{c} -A_{4}^{2} A_{5}^{3/2} \left(\frac{1 + e^{\frac{\sqrt{A_{5}}M}{\sqrt{A_{5}}}} + e^{2M(\sqrt{A_{5}}^{4} + h\sqrt{m \, 5}M)}}{-2e^{2\sqrt{A_{5}}M} + h\sqrt{m \, 5}M} \right) \times \\ -2e^{2h\sqrt{m \, 5}M} + e^{\frac{\sqrt{A_{5}}M}{\sqrt{A_{5}}}} + \frac{2\sqrt{A_{5}}}{\sqrt{A_{5}}}} \\ + \dots + A_{3} e^{2i\sqrt{\Phi_{5}}} \left(\frac{1 + e^{\frac{2\sqrt{A_{5}}M}{\sqrt{A_{5}}}}}{-e^{2h\sqrt{m \, 5}M} \left(-1 + e^{\frac{\sqrt{A_{5}}M}{\sqrt{A_{5}}}} \right)^{2}} \right) \right) \right) P \operatorname{Re} S \phi_{1} \phi_{2}^{3/2}} \right], \quad (32)$$

$$H_{6} = 2A_{4} M^{2} Re \left(\begin{array}{c} \sqrt{A_{3} A_{4}} \left(1 + e^{\frac{2\sqrt{A_{5}}M}{\sqrt{A_{3}}}} \right)^{2} \right) \right) P \operatorname{Re} S \phi_{1} \phi_{2}^{3/2}} \\ + \left(-1 + e^{\frac{2\sqrt{A_{5}}M}{\sqrt{A_{5}}}} \right) \left(-1 + e^{2h\sqrt{m \, 5}} M \right) \sqrt{m}} \\ + \left(-1 + e^{\frac{2\sqrt{A_{5}}M}{\sqrt{A_{5}}}} \right) \left(-1 + e^{2h\sqrt{m \, 5}} M \right) \sqrt{S}} \right) \\ \sqrt{S} (A_{4} A_{5} M^{2} + A_{3} \phi_{1}) \left(\begin{array}{c} \sqrt{A_{5}} \left(1 + e^{\frac{2\sqrt{A_{5}}M}{\sqrt{A_{5}}}} \right) \left(-1 + e^{2i\sqrt{\Phi_{5}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\sqrt{A_{5}}M}{\sqrt{A_{5}}}} \right) \left(-1 + e^{2i\sqrt{\Phi_{5}}} \right) \sqrt{\phi_{2}} \right) \\ (h^{2} m M^{2} S + \phi_{2}), \\ \Omega_{1} = -2 \sqrt{A_{5}} e^{i\frac{\sqrt{\Phi_{1}}}{\sqrt{A_{5}}}} \left(-1 + e^{2i\sqrt{\Phi_{5}}} \right) \left(-1 + e^{2i\sqrt{\Phi_{5}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\sqrt{\Phi_{5}}}{\sqrt{A_{5}}}} \right) \left(-1 + e^{2i\sqrt{\Phi_{5}}} \right) \left(h^{2} m M^{2} S + \phi_{2} \right), \\ \Omega_{2} = Re \left(\begin{array}{c} \sqrt{A_{5}} \left(1 + e^{\frac{2\sqrt{\Phi_{5}}}{\sqrt{A_{5}}}} \right) \left(-1 + e^{2i\sqrt{\Phi_{5}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\sqrt{\Phi_{5}}}{\sqrt{A_{5}}}} \right) \left(1 + e^{2i\sqrt{\Phi_{5}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\sqrt{\Phi_{5}}}{\sqrt{A_{5}}}} \right) \left(1 + e^{2i\sqrt{\Phi_{5}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\sqrt{\Phi_{5}}}{\sqrt{A_{5}}}} \right) \left(1 + e^{2i\sqrt{\Phi_{5}}} \right) h k\sqrt{\phi_{1}} \\ \Omega_{2} = Re \left(\begin{array}{c} \sqrt{A_{5}} \left(1 + e^{\frac{2\sqrt{\Phi_{5}}}{\sqrt{A_{5}}}} \right) \left(-1 + e^{2i\sqrt{\Phi_{5}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\sqrt{\Phi_{5}}}{\sqrt{A_{5}}}} \right) \left(1 + e^{2i\sqrt{\Phi_{5}}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\sqrt{\Phi_{5}}}{\sqrt{A_{5}}}} \right) \left(1 + e^{2i\sqrt{\Phi_{5}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\sqrt{\Phi_{5}}}{\sqrt{A_{5}}} \right) \left(1 + e^{2i\sqrt{\Phi_{5}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\sqrt{\Phi_{5}}}{\sqrt{A_{5}}}} \right) \left(1 + e^{2i\sqrt{\Phi_{5}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\sqrt{\Phi_{5}}}{\sqrt{A_{5}}}} \right) \left(1 + e^{2i\sqrt{\Phi_{5}}}} \right) h k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\sqrt{\Phi_{5}}}{\sqrt{A$$

$$\Omega_{3} = -4\iota \sqrt{A_{5}}e^{\iota(\sqrt{A_{5}} + \sqrt{\phi_{2}})}Grh^{2}k\sqrt{m\phi_{1}}n\beta\cos\sqrt{\phi_{2}}$$

$$\left(h\sqrt{mS}M\sin(\zeta\sqrt{\phi_{2}}) - \sqrt{\phi_{2}}\sinh\left(\sqrt{mS}M\zeta\right)\right),$$
(36)

$$\Omega_{4} = M \operatorname{Re} \sqrt{S} \left(\begin{array}{c} \sqrt{A_{5}} \left(1 + e^{\frac{2\iota\sqrt{\phi_{1}}}{\sqrt{A_{5}}}} \right) \left(-1 + e^{2\iota\sqrt{\phi_{2}}} \right) h \, k\sqrt{\phi_{1}} \\ + \left(-1 + e^{\frac{2\iota\sqrt{\phi_{1}}}{\sqrt{A_{5}}}} \right) \left(1 + e^{2\iota\sqrt{\phi_{2}}} \right) \sqrt{\phi_{2}} \end{array} \right) \left(h^{2} \, m \, M^{2} \, S + \phi_{2} \right), \quad (37)$$

$$\Omega_{5} = e^{-h \sqrt{m \, S} \, M} \left(1 + e^{2h \sqrt{m \, S} \, M \, \zeta} \right) \left(\begin{array}{c} -\sqrt{A_{3}} \, A_{4}^{2} \, A_{5}^{3/2} \left(\begin{array}{c} -1 - e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{3}}}} + e^{2M(\sqrt{A_{3}}^{4} + h\sqrt{m \, S})} \\ + e^{2h\sqrt{m \, S} \, M} - e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{5}}}} + \frac{2\sqrt{\Phi_{1}}}{\sqrt{A_{5}}} \\ e^{2h\sqrt{m \, S} \, M} - e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{5}}}} \\ + e^{2h\sqrt{m \, S} \, M} + \frac{2\sqrt{\Phi_{1}}}{\sqrt{A_{5}}} \\ + e^{2h\sqrt{M \, S} \, M} + \frac{2\sqrt{\Phi_{1}}}{\sqrt{A_{5}}} + 2h\sqrt{m \, S} \, M \\ - e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{5}}}} + \frac{2\sqrt{A_{4}}M}{\sqrt{A_{5}}} + 2h\sqrt{m \, S} \, M \\ - e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{5}}}} + e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{5}}}} + 2h\sqrt{m \, S} \, M \\ + A_{3}^{3/2} \, e^{2t\sqrt{\Phi_{2}}} \left(-1 - e^{\frac{2\sqrt{\Phi_{1}}}{\sqrt{A_{5}}}} \left(-1 + e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{3}}}} \right)^{2} \times \right) \right) \\ + A_{3}^{3/2} \, e^{2t\sqrt{\Phi_{2}}} \left(-1 - e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{5}}}} \left(-1 + e^{2\sqrt{A_{5}}} \right)^{2} \times \right) \\ \sqrt{m} \, P \, Re \, S \, \phi_{1} \, \phi_{2}^{3/2} \right) \\ \\ \Omega_{6} = 2\sqrt{A_{4}m} \, M^{2} \, Re \left(\frac{\sqrt{A_{3} \, A_{4}} \left(1 + e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{3}}}} \right) \left(-1 + e^{2h\sqrt{m \, S} \, M} \right) \sqrt{m}} \\ + \left(-1 + e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{3}}}} \right) \left(1 + e^{2h\sqrt{m \, S} \, M} \right) \sqrt{S}} \right) \\ \\ S \left(A_{4} \, A_{5} \, M^{2} + A_{3} \, \phi_{1} \right) \left(\frac{\sqrt{A_{5}} \left(1 + e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{3}}}} \right) \left(1 + e^{2h\sqrt{m \, S} \, M} \right) \sqrt{S}} \\ + \left(-1 + e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{5}}}} \right) \left(1 + e^{2t\sqrt{\Phi_{2}}} \right) h \, k\sqrt{\phi_{1}}} \\ + \left(-1 + e^{\frac{2\sqrt{A_{4}}M}{\sqrt{A_{5}}}} \right) \left(1 + e^{2t\sqrt{\Phi_{2}}} \right) \sqrt{\phi_{2}} \right) \times \\ \left(h^{2} m \, M^{2} \, S \, + \phi_{2} \right).$$

4. Results and Discussion

The above investigation of the fluid flow of CNTs through porous media is solved analytically. The results of velocity and temperature in Figures 3–14 are presented graphically for fluid-1 (engine-oil-based CNTs nanofluid) and fluid-2 (water) with the various values of different parameters, such as the Hartman number M, Grashof number Gr, Electrical conductivities ratio S, dynamic viscosities ratio m, region heights ratio h, thermal conductivities ratio k and heat generation/absorption ω . Additionally, the comparison between the single-wall (SWCNTs) and multiple-wall carbon nanotubes (MWCNTs) is displayed in each figure. The said figures for the velocity and temperature distribution are formed against the different values of each parameter by keeping the rest of them taken as D = 2.0, M = 1.5, $Gr = 1.0, h = 0.5, I = 2.0, k = 1.0, m = 1/3, n = 1.0, P = 1.0, Re = 1.0, S = 0.5, \beta = 1.0, r = 1.0,$ $\phi_1 = 1.0$ and $\phi_2 = 1.0$. Figures 3 and 4 show the velocity profile for both fluids (water- and engine-oil-based CNT nanofluid) against different values of M and S, respectively. The inverse relation is noted between velocity and the Hartman number in Figure 3 because the magnetic field provides the Lorentz force which resists the fluid flow in the channel. In the nanofluid region, the velocity of engine-oil MWCNTs reduces as compared to the velocity of engine-oil SWCNTs, as the Hartman number is going to be large. In Figure 4, flow movement is inversely affected for positive values of S in both fluids, while it has substantial electrical conductivity but is more affected in the presence of the magnetic field. The impact of *Gr* and *m* on the velocity profile are reported in Figures 5 and 6, respectively. The fluid is flowing only due to the pressure gradient when Gr = 0, and for the case of Gr > 0 buoyancy effects complicate the governing problem because the velocity and energy equations are converted in coupled form. Physically, the presence of the thermal buoyancy

currents induces more flow in the channel which is taking place through the application of a pressure gradient. So, in both nanofluid and without nanofluid regions, the flow of fluid increases as the values of the Grashof number gradually increases, as shown in Figure 5. Similar increasing results are noted from Figure 6 for *m* in the water region and nanofluid region. The velocity of engine-oil SWCNTs boosts up rapidly as compared to the velocity of engine-oil MWCNTs for increasing values of the viscosity ratio. In Figure 7, the influence of the inverse Darcy number D on velocity is explained. In the said figure, as estimated with the increase of the inverse Darcy number, the velocity decreases because a higher inverse Darcy number leads to a lower permeability of the medium, and with lower permeability, the nanofluid cannot move easily in between the walls. The performance of the inertia coefficient of the porous medium or non-Darcy (Forchheimer) number I on velocity is shown in Figure 8. It is detected that larger values of inertia coefficient of porous medium lead to a weaker momentum boundary layer thickness and stronger thermal boundary layer. The impact of the height ratio *h* is portrayed for both nanofluids and without nanofluid in Figures 9 and 10 for the flow and heat profile, respectively. Almost symmetrical results are noted in both figures for increasing values of the height ratio regarding the interface $\zeta = 0$ in the vertical channel. Velocity and temperature in nanofluid regions accelerated quickly for values of *h* in engine-oil SWCNTs compared to engine-oil MWCNTs. The influence of thermal conductivity ratio k for the velocity and temperature distribution of fluid-1 and fluid-2 in the system has been exhibited in Figures 11 and 12. This indicates that the increasing values of k cause an enlargement in the value of velocity and temperature for greater values k. Velocity in Figure 9 for engine-oil SWCNTs and engine-oil MWCNTs gives the maximum amplitude at the center of the nanofluid region and decreases at the vicinity of the right wall for the value of k. The temperature profile in Figure 12 is almost linear for small values of k and becomes non-linear for large values of k. Figures 13 and 14 identify the outcome of heat source/sink $\phi_1 = \phi_2 = \omega$ for fluid flow and energy analysis, respectively. In the case of $\omega = 0$ mean, there is no heat source/sink or heat generation/absorption for energy transform phenomena. It is noticed that the thermal boundary layer generates energy when $\omega > 0$, and in response, the temperature field boosts up in both nanofluid and without nanofluid. However, for the case of $\omega < 0$, boundary energy is absorbed; therefore, the resulting temperature drops and falls down quickly for decreasing values of ω .

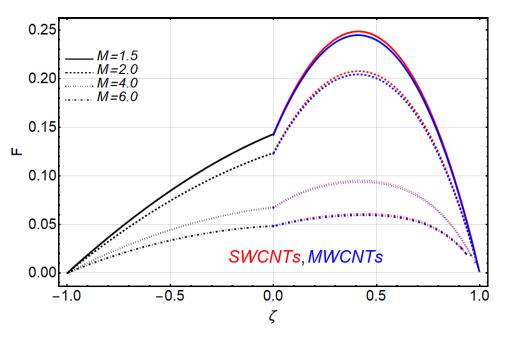


Figure 3. The result of *M* on velocity.

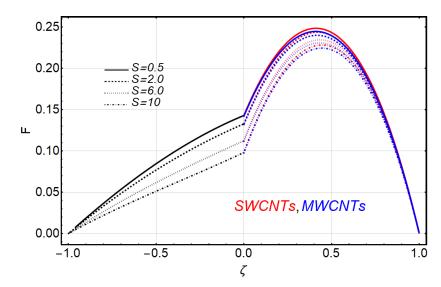


Figure 4. The result of *S* on velocity.

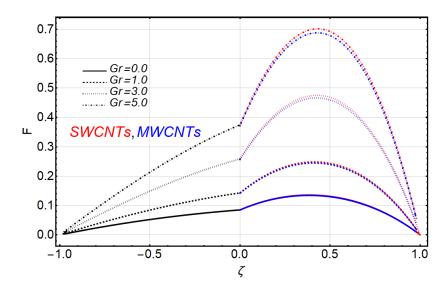


Figure 5. The result of *Gr* on velocity.

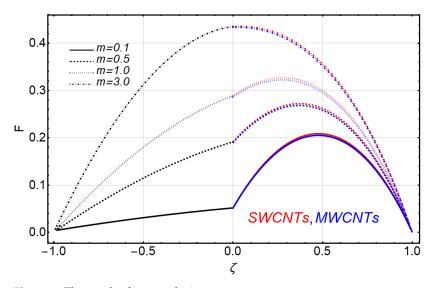


Figure 6. The result of *m* on velocity.

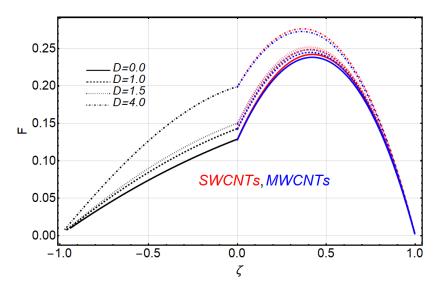


Figure 7. The result of *D* on velocity.

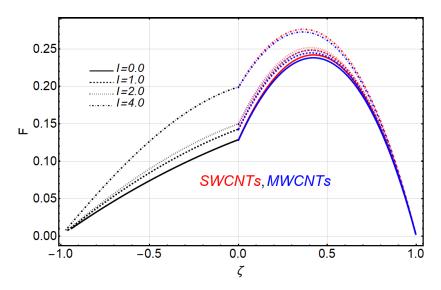


Figure 8. The result of *I* on velocity.

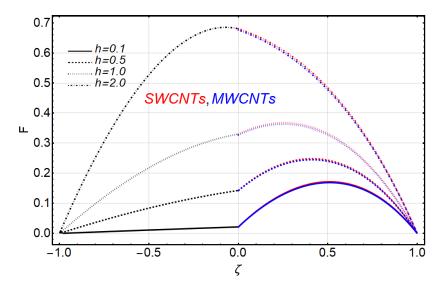


Figure 9. The result of *h* on velocity.

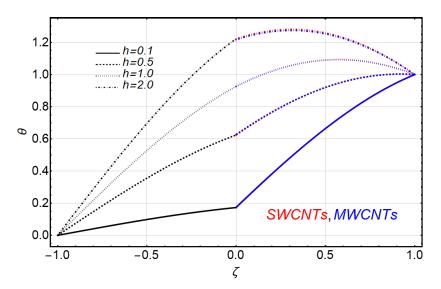


Figure 10. The result of *h* on temperature.

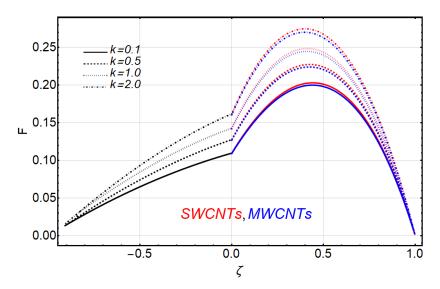


Figure 11. The result of *k* on velocity.

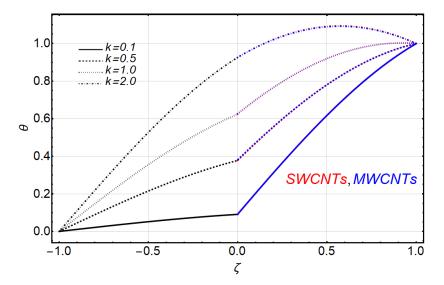


Figure 12. The result of *k* on temperature.

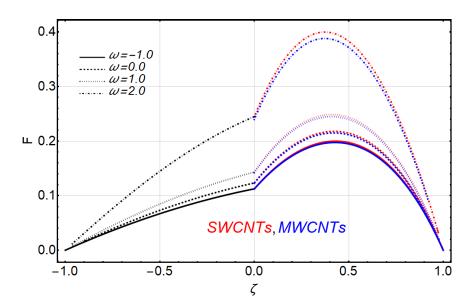


Figure 13. The result of ω on velocity.

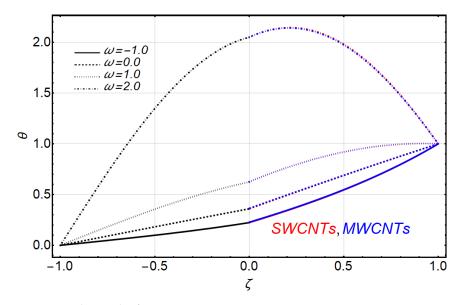


Figure 14. The result of ω on temperature.

The influence of the nanoparticle volumetric fraction ϕ is depicted for both nanofluids and without nanofluid in Figures 15 and 16 for the velocity and temperature distributions, respectively. In both figures near the interface of the second without-nanofluid region due to the interface conditions, a slight change occurs in velocity and temperature. It is noted that the nanoparticles disturbed fluid-2 due to their physical properties. In Figure 15, the velocity field gets affected by the nanoparticle's volume fraction, and the momentum boundary layer of nanofluid slows down as the concentration of particles increases. It is also noted that the velocity in engine-oil SWCNTs is higher than that of engine-oil MWCNTs. Moreover, the temperature of nanofluid in first region is enhanced as the concentration of nanoparticles increases. The thermal boundary layer thickness of engine-oil SWCNTs as compared to engine-oil MWCNTs enhanced gradually as the nanoparticle concentration increased, as shown in Figure 16.

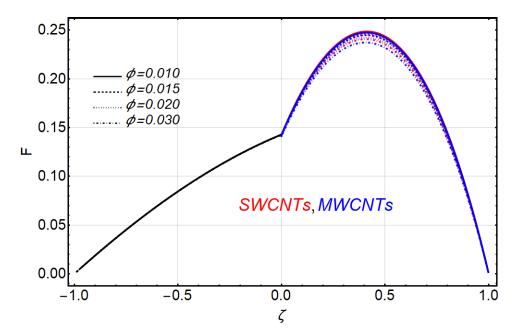


Figure 15. Results of ϕ on velocity.

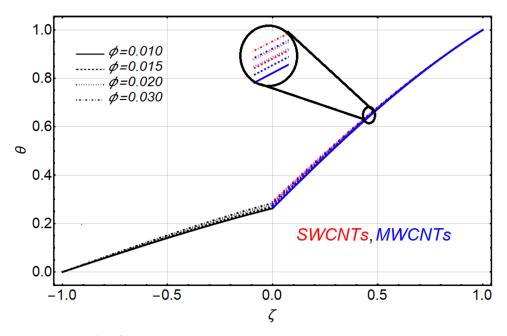


Figure 16. Results of ϕ on temperature.

5. Conclusions

This study investigates the two different fluids' flow through two parallel stationary plates and through a porous medium, with the first region containing engine-oil carbon nanotubes and the second region containing pure water fluid. Velocity and temperature are supposed to be same at the interface of both fluids. The outcomes are based on the main parts of the carbon nanotubes' base fluids, which are nanofluid engine-oil SWCNTs and engine-oil MWCNTs.

- The velocity behavior is almost the same in both nanofluid and without-nanofluid regions.
- The velocity of fluid decreased with increasing values of nanoparticle volume fraction; the Hartman number and ratio of electrical conductivities in engine-oil SWCNTs were more than with engine-oil MWCNTs.

- The velocity of the fluid increased with increasing values of the Grashof number, ratio of heights, ratio of thermal conductivities, ratio of dynamics viscosities and heat generation/absorption, similar to previous work.
- Temperature fields preserved the same impressions in both fluids.
- The temperature fields of fluids were improved with the increasing values of nanoparticle volume fraction, heat generation/absorption coefficient, ratio of heights and ratio of thermal conductivities.
- The concentration of nanoparticles directly affects velocity and temperature in a manner of decreasing and increasing behavior, respectively, due to their boundary layers.

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Nomenclature

- *A*₁ Ratio of densities between nanofluid and base fluid of 1st region.
- *A*₂ Ratio of thermal expansion coefficient between nanofluid and base fluid of 1st region.
- *A*₃ Ratio of viscosities between nanofluid and base fluid of 1st region.
- *A*₄ Ratio of electrical conductivities between nanofluid and base fluid of 1st region.
- *A*₅ Ratio of thermal conductivities between nanofluid and base fluid of 1st region.
- B_0 Magnetic field strength.
- *C_F* Inertia coefficient for the porous media.
- *D* Inverse of Darcy number.
- *F* Dimensionless velocity of fluid.
- *g* Gravitational acceleration.
- *Gr* Grashof number.
- *h* Height ratio of 1st region and 2nd region.
- *I* Dimensionless inertia coefficient of the porous medium.
- *k* Thermal conductivities ratio of 1st region fluid and 2nd region fluid.
- *K* Porous media permeability.
- *M* Hartman number.
- *m* Ratio of dynamics viscosities of 1st region fluid and 2nd region fluid.
- *n* Ratio of densities of 1st region fluid and 2nd region fluid.
- *p* Pressure gradient.
- *P* Dimensionless pressure gradient.
- *Q* Heat generation or absorption coefficient.
- Re Reynolds number.
- *S* Ratio Electrical conductivities of 1st region fluid and 2nd region fluid.
- *T* Temperature of fluid.
- *u* Velocity of fluid.
- \overline{u} Average velocity.

Greek Symbol

β

- Ratio of thermal expansion coefficient of 1st region fluid and 2nd region fluid.
- ζ Dimensionless normal distance.
- μ Viscosity of fluid.
- ρ Density of fluid.
- σ Electrical conductivity of fluid.
- θ Dimensionless temperature.
- ϕ Dimensionless coefficient heat generation or absorption.

Subscripts

- 1 1st region
- 2 2nd region
- f Fluid
- nf Nanofluid
- *p* Particle
- w Wall

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