



Article Slow Invariant Manifold of Laser with Feedback

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Abstract: Previous studies have demonstrated, experimentally and theoretically, the *existence* of *slow–fast* evolutions, i.e., slow chaotic spiking sequences in the dynamics of a semiconductor laser with AC-coupled optoelectronic feedback. In this work, the so-called *Flow Curvature Method* was used, which provides the *slow invariant manifold* analytical equation of such a laser model and also highlights its symmetries if any exist. This equation and its graphical representation in the phase space enable, on the one hand, discriminating the slow evolution of the trajectory curves from the fast one and, on the other hand, improving our understanding of this *slow–fast* regime.

Keywords: slow-fast dynamical systems; singularly perturbed systems; Flow Curvature Method



Citation: Ginoux, J.-M.; Meucci, R. Slow Invariant Manifold of Laser with Feedback. *Symmetry* **2021**, *13*, 1898. https://doi.org/10.3390/ sym13101898

Academic Editors: Marzena Ciszak, Francesco Marino and Boris Malomed

Received: 30 July 2021 Accepted: 26 September 2021 Published: 8 October 2021

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1. Introduction

More than ten years ago, Al-Naimee et al. [1] studied "the occurrence of chaotic spiking in a semiconductor laser with ac-coupled nonlinear optoelectronic feedback. The solitary laser dynamics is ruled by two coupled variables (intensity and population inversion) evolving with two very different characteristic timescales. The introduction of a third degree of freedom (and a third timescale) describing the ac-feedback loop, leads to a three-dimensional slow–fast system displaying a transition from a stable steady state to periodic spiking sequences as the dc-pumping current is varied (...) The timescale of these dynamics, much slower with respect to typical semiconductor laser timescales (few *n*s), is fully determined by the highpass filter in the feedback loop." Then, they provided a minimal physical model qualitatively reproducing the experimental results. Since this model involves two time scales, it can be considered a *slow–fast dynamical system* or a *singularly perturbed system*.

At the end of the nineteenth century, Henri Poincaré originally developed, in his *New Methods of Celestial Mechanics* [2], *singular perturbation methods*. During the thirties and in the following decades, Andronov & Chaikin [3], Levinson [4] and Tikhonov [5] generalized Poincaré's ideas and stated that *slow–fast dynamical systems*, also called *singularly perturbed systems*, possess *invariant manifolds* on which trajectories evolve slowly, and toward which nearby orbits contract exponentially in time (either forward or backward) in the normal directions. Then, from the beginning of the sixties, the seminal works of Wasow [6], Cole [7], O'Malley [8,9] and Fenichel [10–13], to name but a few, gave rise to the so-called *Geometric Singular Perturbation Theory*. Fenichel [10–13] established the *local invariance* of *slow invariant manifolds* that possess both expanding and contracting directions and which were labeled *slow invariant manifolds*. Let us note that the theory of *invariant manifolds* for an ordinary differential equation was independently developed by Hirsch et al. [14]. Since the beginning of the eighties, two kinds of approaches have been developed: *singular perturbation-based methods* and *curvature-based methods*. The former include the *Geometric*

Singular Perturbation Theory (GSPT), the Successive Approximations Method (SAM) [15,16] and the Zero-Derivative Principle (ZDP) [17,18], and the latter, the Intrinsic Low-Dimensional Manifold (ILDM) [19], the Inflection Line Method (ILM) [20] and the Tangent Linear System Approximation (TLSA) [21]. In 2005, a new approach of *n*-dimensional singularly perturbed dynamical systems or slow–fast dynamical systems based on the location of the points where the curvature of trajectory curves vanishes, called the Flow Curvature Method, was developed by Ginoux et al. [22–24] and then by Ginoux [25–27]. In a recent publication, Ginoux [28] proved, on the one hand, the identity between all the methods belonging to the same category (i.e., belonging to singular perturbation-based methods or to curvature-based methods) and, on the other hand, that between both categories. Moreover, he also established, on the one hand, that his Flow Curvature Method encompasses the three other methods (IDLM, TLSA, and ILM) and, on the other hand, the identity between his Flow Curvature Method and Geometric Singular Perturbation Method.

Thus, the aim of this work was to provide the *slow invariant manifold* analytical equation of the semiconductor laser model with AC-coupled optoelectronic feedback introduced by Al-Naimee et al. [1]. Let us observe that, since this three-dimensional model has two small multiplicative parameters in the right hand side of its velocity vector field, it has two *fast* variables and one *slow*. Thus, as highlighted by Ginoux and Rossetto [22], in this specific case, one of the hypotheses of Tihonov's theorem [5] is not checked since the *fast* dynamics of the *singular approximation*, i.e., the zero-order approximation of the *slow invariant manifold*, have a periodic solution. As a consequence, *Geometric Singular Perturbation Theory* fails to provide its analytical equation. To overcome such difficulty, we used, in this work, the so-called *Flow Curvature Method*. This paper is organized as follows: in Section 2, the laser model and its parameters are presented. In Section 3, the main features of the *Flow Curvature Method* are recalled and the *slow invariant manifold* of the laser model is provided as well as its graphical representation in the phase space. In the last section, the results are discussed, and perspectives on this work are given.

2. Slow–Fast Dynamical System

Following the work of Al-Naimee et al. [1], we will use the dynamical system:

$$\frac{dx}{dt} = x(y-1),$$

$$\frac{dy}{dt} = \nu(\delta_0 - y + f(x,z) - xy),$$

$$\frac{dz}{dt} = -\varepsilon(x+z),$$
(1)

where

$$f(x,z) = \alpha \frac{x+z}{1+s(x+z)}$$
(2)

and the parameters s = 11, $\alpha = 1$, $\nu = 10^{-3}$, and $\varepsilon = 2 \times 10^{-5}$ as well as the *bifurcation parameter* $\delta_0 = 1.017$ are exactly the same as in [1]. Due to the presence of the two small parameters ν and ε , the dynamical system (1) is considered *slow–fast*. However, let us observe that $\varepsilon = \kappa \nu$ where $\kappa = 2 \times 10^{-2}$. Thus, by posing $\tau = \nu t$, system (1) reads:

$$\frac{dx}{d\tau} = x' = \frac{x}{\nu}(y-1),$$

$$\frac{dy}{d\tau} = y' = \delta_0 - y + f(x,z) - xy,$$

$$\frac{dz}{d\tau} = z' = -\kappa(x+z),$$
(3)

Thus, $x' = O(\nu^{-1}) \gg 1$ since $\nu \ll 1$, y' = O(1) and $z' = O(\kappa) \ll 1$ since $\kappa \ll 1$. It follows that *x* is a (very) *fast* variable and *y* is a *fast* variable, while *z* is a *slow* variable.

3. Stability Analysis

3.1. Fixed Points, Jacobian Matrix and Eigenvalues

Fixed points are determined while using the classical nullclines method. System (1) has two fixed points: $I_1(0, \delta, 0)$ and $I_2(\delta - 1, 1, 1 - \delta)$.

The Jacobian matrix of system (1) reads:

$$J = \begin{pmatrix} y-1 & x & 0\\ \nu\left(\frac{\partial f}{\partial x} - y\right) & -\nu(1+x) & \nu\frac{\partial f}{\partial z}\\ -\varepsilon & 0 & -\varepsilon \end{pmatrix}$$
(4)

Let us observe that for both the fixed points I_1 and I_2 :

$$\frac{\partial f}{\partial x} = \frac{\alpha}{\left[1 + s(x+z)\right]^2} = \frac{\partial f}{\partial z} = \alpha = 1,$$
(5)

since nullcline $\dot{z} = -\varepsilon(x + z) = 0$ and the parameter $\alpha = 1$.

By replacing the coordinate of the fixed point I_1 in the Jacobian matrix (4), the Cayley– Hamilton eigenpolynomial can be easily factorized and reads:

$$[\lambda - (\delta - 1)](\lambda + \nu)(\lambda + \varepsilon) = 0$$
(6)

Thus, there are three real eigenvalues:

$$\lambda_1 = \delta - 1 \quad ; \quad \lambda_2 = -\nu \quad ; \quad \lambda_3 = -\varepsilon. \tag{7}$$

Thus, the fixed point I_1 is a *saddle-node* provided that $\delta > 1$.

Then, upon replacing the coordinate of the fixed point I_2 in the Jacobian matrix (4), the Cayley–Hamilton eigenpolynomial reads:

$$\lambda^3 - (\nu\delta + \varepsilon)\lambda^2 + \nu\delta\varepsilon\lambda - (1 - \delta)\nu\varepsilon = 0 \tag{8}$$

Numerically solving this third-degree eigenpolynomial (8) leads to:

$$\lambda_1 = -0.00124128; \quad \lambda_{2,3} = 0.000102141 \pm 0.000513301i.$$
 (9)

Thus, the fixed point I_2 is a saddle-focus.

By using *perturbation methods* [29], the real root λ_1 of the eigenpolynomial (8) may be approximated by:

$$\lambda_1 = -\nu\delta + O(\varepsilon),\tag{10}$$

where $O(\varepsilon) = -k\varepsilon$ with $k \gg \varepsilon$. Moreover, the trace of the Jacobian matrix (4), evaluated at the fixed point I_2 , provides:

$$Tr(J) = \lambda_1 + \lambda_2 + \lambda_3 = -\nu\delta - \varepsilon.$$
(11)

Since $\lambda_{2,3} = \sigma \pm i\omega$ is a complex conjugate, this trace reads:

$$Tr(J) = \lambda_1 + 2\sigma = -\nu\delta - \varepsilon.$$
(12)

Thus, by replacing, in the previous Equation (12), λ_1 with the expression (10), we obtain:

$$2\sigma = (k-1)\varepsilon > 0. \tag{13}$$

It follows that the real part of the eigenvalues $\lambda_{2,3}$ is necessarily positive and, thus, the fixed point I_2 is a *saddle-focus*.

3.2. Bifurcation Diagram

Following the work of Al-Naimee et al. [1], we used δ as a bifurcation parameter and computed the bifurcation diagram, which is presented in Figure 1. Such a diagram, which is exactly the same as that produced in [1], provides information that can be used to have a better understanding of the phase space orbits plotted in Figure 2.

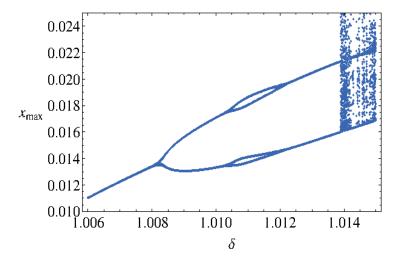


Figure 1. Bifurcation diagram x_{max} as function of δ .

From Figure 1, we observe that, for $\delta \in [1.006, 1.0082]$, the attractor is a *limit cycle* of period one (see Figure 2a). For $\delta \in [1.0082, 1.0105]$ and $\delta \in [1.0117, 1.0137]$, the period of the *limit cycle* becomes of period two (see Figure 2b). For $\delta \in [1.0105, 1.0117]$, the *limit cycle* is of period four (see Figure 2c). When $\delta > 1.037$, the attractor becomes chaotic (see Figure 2d). To confirm these results, Lyapunov characteristic exponents were computed in each case.

3.3. Numerical Computation of the Lyapunov Characteristic Exponents

The numerical computation of the Lyapunov characteristic exponents (LCEs) of the system (1) was performed in each case with the algorithm developed by Sandri [30] for Mathematica[®] and the Lyapunov Exponents Toolbox (LET) developed by Siu for MatLab[®] and involving the two algorithms proposed by Wolf et al. [31] and Eckmann and Ruelle [32] (see https://fr.mathworks.com/matlabcentral/fileexchange/233-let 15 September 2021). The results obtained by both algorithms are consistent. The LCE values were computed within each considered interval $\delta \in [1.006, 1.02]$. As an example, for $\delta = 1.007, 1.010, 1.011$ and 1.017, both algorithms provided, respectively, the following LCEs: (0, -0.15, -0.82), (0, -0.17, -0.81), (0, -0.16, -0.80) and (0.025, 0, -1.06). Then, the classification of (autonomous) continuous-time attractors of the dynamical system (6) on the basis of their Lyapunov spectrum, together with their Hausdorff dimension, is presented in Table 1 according to the work of Klein and Baier [33].

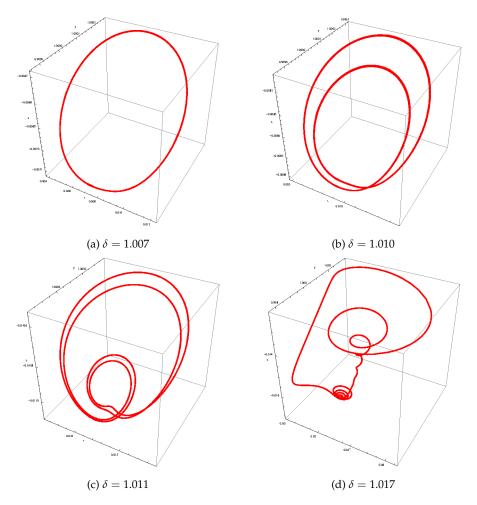


Figure 2. Phase portraits of system (1) in the phase space for various values δ .

Table 1. Lyapunov characteristic exponents of dynamical system (6) for various values of δ .

δ	LCE Spectrum	Dynamics of the Attractor	Hausdorff Dimension
$\delta \in [1.0060, 1.0082]$	(0, -, -)	Limit cycle of period 1	D = 1
$\delta \in [1.0082, 1.0105]$	(0, -, -)	Limit cycle of period 2	D = 1
$\delta \in [1.0105, 1.0117]$	(0, -, -)	Limit cycle of period 4	D = 1
$\delta \in [1.0117, 1.0137]$	(0, -, -)	Limit cycle of period 2	D = 1
$\delta \in [1.0137, 1.02]$	(+, 0, -)	2-Chaos	D = 2.02

4. Slow Invariant Manifold

In recent publications, a new approach to *n*-dimensional *singularly perturbed systems* of ordinary differential equations, called the *Flow Curvature Method*, has been developed by Ginoux et al. [22–27,34–37]. It consists of considering the *trajectory curves* integral of such systems as curves in Euclidean *n*-space. Based on the use of local metric properties of *curvatures* inherent to *Differential Geometry*, this method, which does not require the use of asymptotic expansions, states that the location of the points where the local *curvature* of the *trajectory curves* of such systems is null defines an (n - 1)-dimensional *manifold* associated with this system and called the *flow curvature manifold*. The invariance of this manifold is then stated according to a theorem introduced by Gaston Darboux [38] in 1878. Moreover, as stated in Ginoux [25], if the *slow–fast dynamical system* has a *symmetry* such as (-x, -y, z), its *flow curvature manifold* has the same, i.e., $\phi(-x, -y, z) = \phi(x, y, z)$. Thus, as previously stated (see Section 2), the system (1) is a three-dimensional *singularly perturbed dynamical system* with *two* fast variables. However, in such a specific case, one of the hypotheses of Tikhonov's theorem [5] is not checked since the *fast dynamics* of

the *singular approximation* have a periodic solution. Nevertheless, while using the *Flow Curvature Method*, an approximation up to order three in $v\varepsilon^2$ and $v^2\varepsilon$ of the *slow invariant manifold* equation of the system (1) can been computed for various values of the *bifurcation parameter* δ .

According to the *Flow Curvature Method*, the following proposition holds for any *n*-dimensional *singularly perturbed dynamical system* comprising small multiplicative parameters in its velocity vector field:

Proposition 1. The location of the points where the $(n-1)^{th}$ curvature of the flow, i.e., the curvature of the trajectory curve \vec{X} integral of any *n*-dimensional singularly perturbed dynamical systems vanishes, providing a *p*-order approximation of its slow manifold, the equation of which reads

$$\phi(\vec{X}) = \vec{X} \cdot (\vec{X} \wedge \vec{X} \wedge \dots \wedge \vec{X}) = \det(\vec{X}, \vec{X}, \vec{X}, \dots, \vec{X}) = 0,$$
(14)

(*n*)

where \vec{X} represents the time derivatives up to order n of the velocity vector field.

For a proof of this proposition and that of the invariance of the *slow manifold* (14), see Ginoux [22–28,34]. Let us observe that the *p*-order approximation depends on the number of small multiplicative parameters in the velocity vector field. In the particular case of system (1), it can be easily stated that, since the plane x = 0 is *invariant* with respect to the flow and due to the presence of two small multiplicative parameters, i.e., v and ε , the *slow invariant manifold* Equation (14) can be simply and directly expressed by:

$$p(\vec{X}) = (\vec{X} \wedge \vec{X}) \cdot \vec{i} = 0, \tag{15}$$

where \vec{i} is the unit vector along the *x*-axis. Thus, by using the *Flow Curvature Method* and Equation (15), the *slow invariant manifold* equation of system (1) reads:

$$\begin{split} \phi(x, y, z, \nu, \varepsilon) &= x(1-y)(\delta + \delta s^2 x^2 + s^2 x^2 yz - s^2 x^2 y + 2s^2 xyz^2 - 2s^2 xyz + 2\delta s^2 xz \\ &+ s^2 yz^3 - s^2 yz^2 + \delta s^2 z^2 + sx^2 + 2\delta sx + 2sxyz - 2sxy + 2sxz + 2syz^2 - 2syz \\ &+ sz^2 + 2\delta sz + yz - y) - \varepsilon(x+z)(-\delta + s^2 x^3 y - \delta s^2 x^2 + 2s^2 x^2 yz + s^2 x^2 y \\ &+ s^2 xyz^2 + 2s^2 xyz - 2\delta s^2 xz + s^2 yz^2 - \delta s^2 z^2 + 2sx^2 y - sx^2 - 2\delta sx + 2sxyz \\ &+ 2sxy - 2sxz + 2syz - sz^2 - 2\delta sz + xy + y) + \nu(x+1)(x+z)(sx+sz+1) \\ &\times (-\delta + sx^2 y - \delta sx + sxyz + sxy + syz - \delta sz + xy - x + y - z). \end{split}$$
(16)

The *slow invariant manifold* equations (16) of the system (1) have been plotted in the figures below (see Figure 3) for various values of the *bifurcation parameter* δ = 1.007, 1.010, 1.011 and 1.017.

We observe that, for $\delta = 1.007$, the *trajectory curve* integral of system (1) is a periodic *stable limit cycle* that lies partly on the left side and right side of the *slow invariant manifold*; see Figure 3a. For a *bifurcation parameter* δ equal to 1.010 and 1.011 (see Figure 3b,c), the same evolution appears. Let us observe that the kind of funnel in Figure 3a,c corresponds to the attractive eigendirection of the fixed point I_2 . When $\delta = 1.017$, the attractor becomes chaotic and the *trajectory curve* evolves slowly from the bottom to the top on nearly all the left part of the *slow invariant manifold*. Then, it jumps on the upper right part of *slow invariant manifold* and starts spiraling around the attractive eigendirection corresponding to the negative real eigenvalues $\lambda_1 \approx -v\delta$ of fixed point I_2 ; see Equations (9) and (10). When the *trajectory curve* reaches the lower right part of the *slow invariant manifold*, it jumps on its left part. Let us observe that, during its descent, it lies in the vicinity of the *slow invariant manifold*.

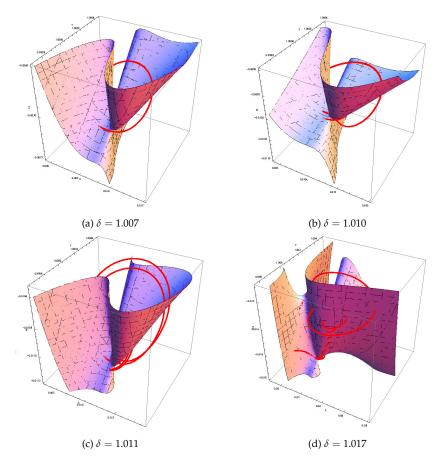


Figure 3. Slow invariant manifolds of system (1) in the phase space for various values of δ .

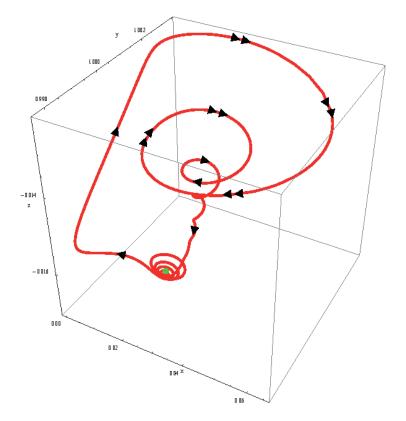


Figure 4. Evolution of the *trajectory curve* integral of system (1) for $\delta = 1.017$.

5. Discussion

In this work, by using the so-called *Flow Curvature Method*, we provide the *slow invariant manifold* analytical equation of a laser model. This equation and its graphical representation in the phase space enable, on the one hand, discriminating the *slow* evolution of the trajectory curves from the *fast* one and, on the other hand, improving our understanding of this *slow–fast* regime. Thus, the repelling and attracting branches of the *slow invariant manifold* have been specified. We also highlighted that the deformation of the surface representing, in the phase space (x, y, z), the slow invariant analytical manifold according to the bifurcation parameter δ is rather weak (see Figure 3). This confirms an assumption made by Al-Naimee et al. [1] according to which:

"Therefore, it is expected that they should not imply strong modifications of the slow-manifold shape which, as discussed above, is responsible for the observed dynamics."

Finally, our mathematical analysis also enabled confirming another assumption made by Al-Naimee et al. [1], according to which "since (x_1, y_1, z_1) is located precisely on the slow manifold, the exact homoclinic connection does not occur".

Author Contributions: Conceptualization, J.-M.G. and R.M. Both authors have equally contributed. All authors have read and agreed to the published version of the manuscript.

Funding: This research received no external funding.

Conflicts of Interest: The authors declare no conflict of interest.

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