

Article

Incorporating Rainfall-Runoff Events into Nitrate-Nitrogen and Phosphorus Load Assessments for Small Tile-Drained Catchments

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Abstract: Rainfall-runoff events significantly influence water runoff and the loss of pollutants from tile-drained agricultural land. We monitored ten small (4 to 38 ha) tile-drained catchments in Czechia for three to five years (2012 to 2016). The discharge was measured continuously; a regular 14-day scheme of water quality monitoring was accompanied with event sampling provided by automatic samplers in 20 to 120 min intervals. A new semi-automated algorithm was developed for the identification of runoff events (RE) based on discharge and water temperature changes. We then quantified the share of RE on the total runoff and the N and P losses, and we compared six methods for nutrient load estimation on an annual and monthly basis. The results showed considerable differences among the monitored sites, seasons, and applied methods. The share of RE on N loads was on average 5% to 30% of the total annual load, whereas for P (dissolved and total), the share of RE was on average 10% to 80% on the total annual load. The most precise method for nutrient load estimation included the RE. The methods based on point monitoring of the discharge and water quality underestimated the loads of N by 10% to 20% and of P by 30% to 80%. The acquired findings are crucial for the improvement of nutrient load assessment in tile-drained catchments, as well as for the design of various mitigation measures on tile-drained agricultural land.

Keywords: runoff events; tile drainage; load assessment methods; nitrate; phosphorus

1. Introduction

There is great concern among hydrologists, watershed managers, and as policy makers about how different rainfall-runoff events influence hydrology as well as the loss of pollutants from tile-drained agricultural land [1,2]. Intensively managed tile-drained landscapes have been found to have a considerable potential for N and P losses, with regard to different soil conditions and cropping systems, especially during periods with elevated flows [3–9]. Nutrient concentrations in drainage waters may change rapidly within a rainfall-runoff event due to variable pre-event and event soil/catchment moisture conditions, related soil biogeochemical processes [10–13], precipitation characteristics, and water flow paths into drainage and with different origin and residence times [14–17].

Tile-drained fields and catchments of various scales have been subject to many studies trying to quantify how different sampling strategies, monitoring schemes, and load calculation methods influence the assessment of runoff and nutrient fluxes from tile drains, from one season to longer periods. While there is in-depth research for individual fields or paired catchments [8,14,18–21], not many mid-term studies have been conducted to compare nutrient losses and load assessment

methods for tile-drained fields or small catchments with different agricultural management and runoff characteristics, especially in central European conditions. In the Czech Republic, around 30% of the agricultural land is tile-drained, and in some regions land drainage exists on every field [22,23].

The basic classification of load estimation methods is usually in four categories: averaging methods, ratio estimators, period-weighted, and regression methods. For nitrate-N load estimation, two methods have been recommended by numerous authors: (1) linear interpolation, a period weighted method, and (2) flow-weighted mean concentration, an averaging method [18,24,25]. Previous research has shown that the uncertainty due to infrequent sampling and nutrient load estimation approaches for drainage systems or small streams is often much greater than the uncertainty brought about by other steps in the sample collection process [25–27]. In general, the uncertainties in annual or monthly nutrient load estimates are reported to be influenced both by the sampling interval and the load assessment methods and tend to increase with an increasing sampling interval for the majority of load estimation algorithms [24,25,28]. Ratio methods are often reported as being unsatisfactory compared with the two aforementioned simple methods. Regression based algorithms are also found to poorly characterize load variation (especially for nitrates) in drainage or small watercourses [27,29] despite the implementation of error correction techniques [20,30].

To our knowledge, only a few studies have been published to compare monitoring approaches and nutrient load assessment methods for tile-drained fields or small catchments [6,25,27,31]. These studies often conclude that the most dominant factors influencing nutrient fluxes are precipitation characteristics and catchment hydrological connectivity. This pertains, compared to nitrogen, to a greater extent to phosphorus, as high P concentrations in water from land drainage are associated predominantly with elevated flows, both from ploughland and grassland [4,5,32–34]. Load assessment approaches without continuous discharge measurements and event sampling tend to underestimate P loads especially [33,35]. However, little is still known about how and to what extent various nutrient load assessment approaches, including those used in operational activities (e.g., of River Basin Authorities) may differ for small, tile-drained catchments, situated in sloping conditions. Further, there is an obvious research gap in the knowledge of the hydrological behaviour of small, tile-drained catchments with different soil and land-use characteristics, especially during various rainfall-runoff events captured by different monitoring strategies [1,36].

The necessity of the accurate assessment of nutrient loads from tile-drained fields or small catchments is invoked by watershed management and agricultural policy aims oriented towards diminishing nutrient and pesticides losses from drained land [2,36,37]. Therefore, it is crucial to develop an approach to identify the processes responsible for the input of pollutants from land to water via tile drainage. To reveal the rapid discharge/concentration changes, describe the related processes, and estimate the true pollutant loads, a proper monitoring programme and appropriate methods for the evaluation of matter fluxes are necessary to support [6,18,38] the design of field to catchment scale mitigation measures for tile drainage or on drained land, as well as when estimating their effects [2,9,22,38–40].

The aim of this study was to quantify the proportion of N and P losses in drainage waters from runoff events, assess the real N and P losses, and to compare six different methods for N and P load estimation at ten very small tile-drained catchments with different drainage and agricultural management characteristics in Czechia on a monthly and annual basis in three to five hydrological years between 2012 and 2016.

2. Materials and Methods

2.1. Experimental Sites

The research was conducted in the Bohemo-Moravian Highlands, Czech Republic. The catchment areas were 4 to 38 ha, and the sites were monitored for three to five hydrological years. These sites represent the prevailing soil types and agricultural management practices across the Czech Highland

region. At all the sites, tile drainage is located on slopes of 3° to 6° . The substrate of the sites is crystalline rocks, i.e., various forms of paragneiss, ortogneiss, or granite. Soils at the sites are heterogenous; in discharge areas (mid to low parts of slopes), there are usually stagnic cambisols, haplic stagnosol, haplic gleysols, and sporadically histosols (sandy clay loam/loam) [41]. In the recharge areas (upper slope parts, close to catchment boundaries), there are haplic and shallow haplic cambisols and cambic hyperskeletal leptosol (loamy sand/sandy loam) [41]. Artificial drainage is placed 0.9 to 1.1 m below the soil surface, drain spacing is between 10 to 18 m, and, since the drainage is built on slopes, the hydrologically contributing area (subcatchment) for a drainage group is far larger than the drained field itself [15,17,42,43]. The average annual precipitation at the sites ranged between 550 and 750 mm. On ploughland, cereals, oil seed rape, maize, and, to a lesser extent, potatoes were the typical planted crops. Ploughland catchments were fertilized on average by 120 to 180 kg N·ha⁻¹·y⁻¹ and by 20 to 30 kg P·ha⁻¹·y⁻¹. The sites PD1 and PD2, where maize was grown, were fertilized by 250 to 300 kg N·ha⁻¹·y⁻¹. The basic characteristics of the sites are given in Table 1, and the locations of the sites are depicted in Figure 1.

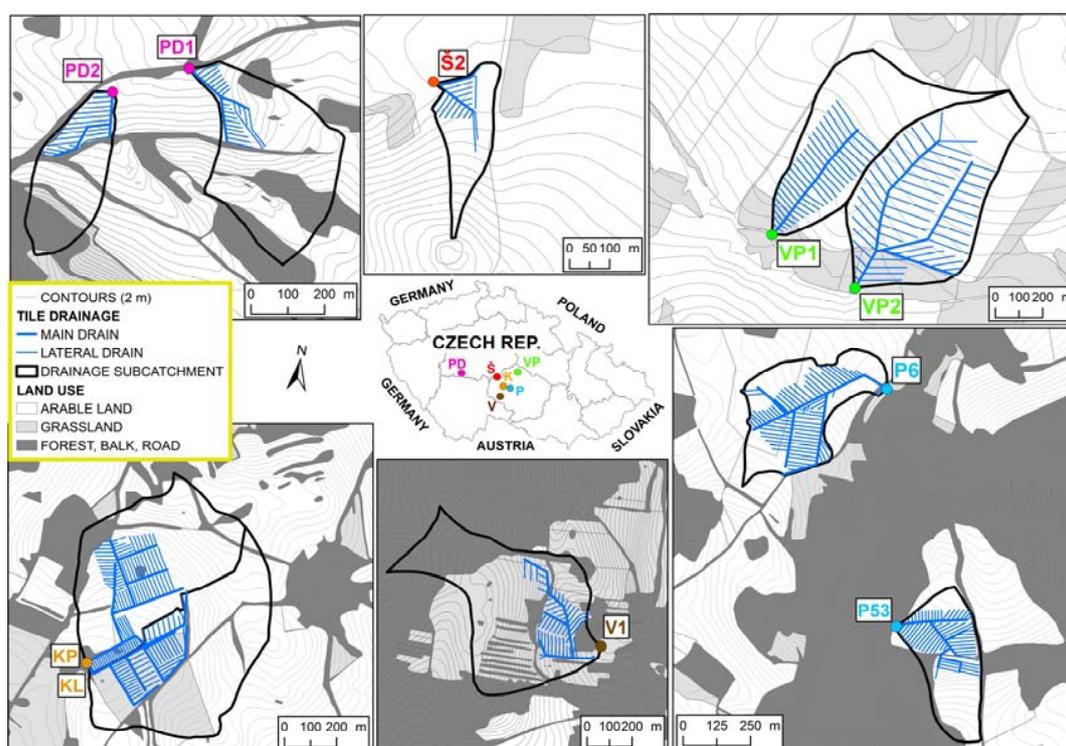


Figure 1. Characteristics and location of the monitored sites in the Czech Republic.

Table 1. Basic characteristics of the monitored sites.

Site	Mean Catchment Altitude (m a.s.l.)	Drained Area (ha)	Catchment Area (ha)	Primary Land Use	Avg. Discharge (l/s)	Specific Discharge (l/s/ha)	Fertilization/Management	Evaluated Period (HR)
KL	550	6.51	29.6	grassland	0.219	0.007	Digestate	2012–2016
KP	550	9.51	28.3	arable land	1.265	0.044	Mineral + manure	2012–2016
P53	565	5.46	14.86	arable land	0.045	0.003	Mineral	2012–2016
P6	510	9.85	15.73	arable land	0.559	0.036	Mineral	2012–2016
PD1	395	1.92	13.42	arable land	0.307	0.023	Digestate	2014–2016
PD2	395	2.31	6.98	arable land	0.244	0.035	Mineral	2014–2016
Š2	515	1.21	3.82	arable land	0.256	0.067	Mineral	2012–2016
V1	655	5.85	37.9	pasture	0.993	0.026	Cattle grazing	2012–2014
VP1	495	8.68	19.95	arable land	0.57	0.028	Fugate + mineral	2014–2016
VP2	495	21.32	28.25	arable land	0.705	0.025	Fugate + mineral	2014–2016

HR—hydrological year. Specific discharge calculated using the catchment area.

2.2. Monitoring the Setup and Analyses of Samples

The drainage discharges were measured continuously at the sites of all drained catchments (manholes or drainage outlets) using ultrasound water level sensors and calibrated weirs (see example in Figure 2). Further, drainage water temperatures were monitored continuously and used as a proxy for the detection and selection of unsampled discharge events; the details are given below. At each site, a weather station measured precipitation and selected meteorological parameters. The withdrawal of water samples differed according to the discharge situation. During periods of prevailing baseflow and slow interflow, the samples were collected manually in a regular two-week step (grab sampling). During runoff events (RE), samples were taken by automatic samplers (ISCO, Morava) in time steps varying from 20 min (summer events) to 2 h (winter events). Sampling was activated by an increase of drainage discharge. The particular discharge level that triggered automatic sampling was set according to the precipitation forecast and with regard to previously measured discharges. On average six (4 to 8) samples were taken during a single sampled RE. Immediately after withdrawal, the samples were transported to an accredited laboratory, where they were analyzed for N-NO₃, P-PO₄, and total phosphorus (P_{tot}) by an automated SKALAR device using Flow Injection and Continuous Flow Analyses (spectrophotometry).



Figure 2. An example of sampling site equipment. (a): site Š2; (b): site VP2.

For the identification of the REs, a new semi-automated algorithm was developed, taking into account previously published approaches [29,44]. A RE was considered as an episodic drainage runoff, elevated by rainfall or snowmelt. The algorithm for the detection of an RE was based on a 10-min discharge and water temperature data record. The algorithm identified a RE, based on the following criteria: drainage discharge for at least 3 h exceeding 1.5 times the mean daily discharge of the previous day. The beginning of a RE took place when the drainage discharge rose by 10% or more within 2 h. This eliminated short-term discharge changes during very low flow conditions or due to weir clogs. The end of a RE was set when the drainage water temperature became stable for >2 h so no event water appeared in the drainage discharge [17]. Runoff events with several flow peaks were considered as one RE if the time between the consecutive flow peaks was less than 24 h. The procedure for the identification of REs was applied to all REs, no matter whether they were sampled or not. An example of the use of the aforementioned method is shown in Figure 3.

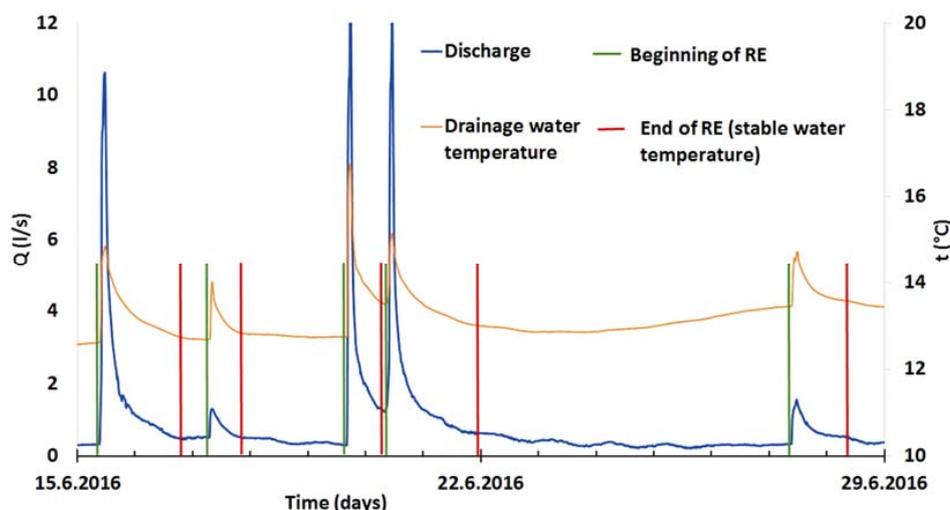


Figure 3. Using the semi-automated algorithm for the identification of REs; an example from the VP2 site.

2.3. Description of Applied Load Assessment Methods

For the load assessment of N-NO₃, P-PO₄, and P_{tot}, six different methods (M1 to M6) using annual (a) and/or monthly (m) time scales were employed and compared. M1 to M3 are commonly used techniques when 14 to 30 day grab sampling schemes are followed. The descriptions and equations of these methods are given in Table 2. Nutrient loads were further converted to year- and area-specific losses, dividing the load by the drainage subcatchment area. For load assessments in the unsampled RE (M6), flow-weighted concentration values (*C_{fw}*) from a particular season (veg; April to September/non-veg; October to March/snow melt) were used to calculate the loads during these events. The calculation of the *C_{fw}* was as follows:

$$C_{fw} = \frac{\sum(C_i \times Q_i)}{\sum Q_i} \tag{1}$$

where *C_{fw}* is the flow-weighted concentration, *C_i* is the concentration value during an *i* withdrawal, and *Q_i* is the discharge during *i* withdrawal. *C_{fw}* was further employed for the basic description of the hydrochemical behaviour of the individually monitored sites (Table 3). The nutrient loads according to M6 were considered the ‘true load’.

Table 2. The load assessment methods employed and compared in this study.

Method	Description	Equation
M1	Load (<i>a</i>) = Mean year discharge × mean annual concentration (both from 14 day sampling values)	$L = K(Q_a C_a)$
M2	Load (<i>a</i>) = Cumulative annual runoff volume (from 10 min data) × flow-weighted concentration (from 14 day sampling values)	$L = K(V_a C_{fw})$
M3	Load (<i>a,m</i>) = Actual discharge (from sampled days only) × concentration (from 14 day sampling values). For the unsampled days, a load of the previous/next sampling day is set.	$L = K(\sum_{i=1}^n Q_i C_i)$
M4	Load (<i>a,m</i>) = Mean daily discharge (from 10 min data in all days) × concentration (from 14 day sampling values). For the unsampled days, a concentration of the previous/next sampling day is set.	$L = K(\sum_{i=1}^n Q_d C_i)$
M5	Load (<i>a,m</i>) = Mean daily discharge (from 10 min data in all days) × concentration (from 14 day sampling values). For the unsampled days, a linear interpolation of the concentration is used from the consecutive sampled days	$L = K(\sum_{j=1}^n Q_d C_j^{int})$
M6	Load (<i>a,m</i>) = M5 + loads during runoff events. This method was the only one to include runoff events, both sampled and unsampled (modelled).	$L = K(\sum_{j=1}^n Q_d C_j^{int}) + K(\sum_{e=1}^m Q_e C_e)$

K is the units and time conversion constant; *Q_a* is the mean annual discharge; *C_a* is the mean annual concentration; *V_a* is the cumulative annual runoff volume; *C_{fw}* is the flow-weighted concentration; *Q_i* is the actual discharge in time of sampling; *C_i* is the concentration from grab sampling; *Q_d* is the mean daily discharge; *V_d* is the cumulative daily runoff volume (from 10 min data); *C_{jint}* is the linear interpolation of concentration values between the consecutive grab samples; *Q_e* is the actual discharge during an event; *C_e* is the actual concentration during an event, whether measured or modeled; *C_{fw}* is flow-weighted concentration; and *n* is the number of days.

Table 3. The share of runoff events in the total annual drainage runoff and in N-NO₃, P-PO₄, and P_{tot} total annual loads and the share of runoff events on average within one HR for the monitored hydrological years at all the sites.

Site	KL	KP	P53	P6	PD1	PD2	Š2	V1	VP1	VP2	
Evaluated Period (HR)	12–16	12–16	12–16	12–16	14–16	14–16	12–16	12–14	14–16	14–16	
Total	Number of RE (monitored)	71 (29)	65 (25)	53 (22)	78 (21)	21 (8)	36 (16)	39 (14)	56 (21)	37 (17)	56 (26)
	Duration of RE days (%)	133 (7.3)	177 (9.7)	168 (9.2)	226 (12.4)	46 (4.2)	62 (5.7)	51 (2.8)	125 (11.4)	61 (5.6)	110 (10.0)
	Share of total runoff (%)	24.8	27.6	62.8	34	16.1	21.7	14.8	28.2	19.6	28.1
	Share of total load N-NO ₃ (%)	12.3	21.1	57.7	34.2	24.4	37.5	10.1	22.1	17.0	18.5
	Share of total load P-PO ₄ (%)	37.8	38.3	83.6	61.4	31.7	53.5	19.3	43.1	47.6	47.8
	Share of total load P _{tot} (%)	36.6	40.5	74.4	73.2	53.9	52.1	20.3	39.5	46	50.7
Average per 1 HR	Number of RE (monitored)	14 (6)	13 (5)	11 (4)	16 (4)	7 (3)	12 (5)	10 (4)	19 (7)	12 (6)	18 (9)
	Duration of RE (days) %	26.6 (7.3)	35.3 (9.7)	33.6 (9.2)	45.1 (12.4)	15.4 (4.2)	20.7 (5.7)	17.9 (4.9)	41.6 (11.4)	20.2 (37.8)	36.5 (10.0)
	Share of annual runoff (%)	21.3	25.3	48.8	28.8	13.5	20.6	11.5	27.4	19.2	29.1
	Share of annual load N-NO ₃ (%)	10.8	22	50.9	30.8	20.8	35.4	8.6	22.8	16.9	19.5
	Share of annual load P-PO ₄ (%)	32.3	37.1	73.3	58.8	24.4	49.9	16.5	43	36.7	43.8
	Share of annual load P _{tot} (%)	30.9	36	62.8	49.7	36.1	48.6	17.1	37.7	37.2	46.7

HR means hydrological year.

2.4. Statistical Analyses and Comparison of Load Assessment Methods

Basic statistics on drainage discharges as well as on N-NO₃, P-PO₄, and P_{tot} concentration values were applied across all the sites, separately for regular and for event sampling schemes. Using both the monitored data and the semi-automated algorithm, the share of REs in the total drainage runoff was quantified. Further, the proportions of REs in the N-NO₃, P-PO₄, and P_{tot} loads were calculated on an annual and a monthly basis. The comparison of the differences in the load assessment methods both for the annual (M1 to M5) and monthly (M3 to M5) loads was related to the true load method (M6). For the statistical significance of the differences among the methods on an annual basis, one-way ANOVA with a significance level of $\alpha = 0.05$ was applied. Assumptions of the normal distribution of the data and the homogeneity of variances were checked, and, when they were not assumed to be satisfied, rank (N-NO₃ and P_{tot}) or square root transformations (P-PO₄) were carried out. For a comparison of the differences between the selected load assessment methods (M3 to M6) on a monthly basis, root mean square error (RMSE) was used. RMSE expresses the cumulative degree of the relative error of a particular method, related to M6, when both accuracy and precision are taken into account [45]. Accuracy (E) was calculated as a ratio of M6 to M1 to M5 (Equation (8)), and precision was expressed by the standard deviation s of E. The RMSE was then calculated according to Equation (9).

$$E_{M3,M4,M5} = \frac{M6}{M3, M4, M5} \quad (2)$$

$$RMSE = \sqrt{\bar{E}^2 + s^2} \quad (3)$$

3. Results

3.1. Dynamics of N and P Concentrations

The concentration values of N-NO₃, P-PO₄, and P_{tot} in drainage waters differed profoundly across the sites, between hydrological years, and within regular sampling (RS) and event sampling (ES) schemes. In RSs, N-NO₃ concentrations were 1.0 to 91.5 mg/L (median 19.4 mg/L), P-PO₄ ranged between 0.001 and 0.424 mg/L (median 0.020 mg/L), and concentrations of P_{tot} were 0.001 to 0.747 mg/L (median 0.046 mg/L). In the ES, N-NO₃ concentrations were 0.452 to 144.9 mg/L (median 14.9 mg/L), P-PO₄ ranged between 0.001 to 2.174 mg/L (median 0.043 mg/L), and P_{tot} was between 0.001 to 3.231 mg/L (median 0.120 mg/L).

The concentrations of nutrients adjusted to hydrology (*C_{fw}*) were usually lower for N-NO₃ in REs compared to RSs, whereas for both P-PO₄ and P_{tot}, the opposite was true. This means that during an RE, a dilution of N-NO₃ in drainage waters usually prevailed, whilst for both P-PO₄ and P_{tot}, the concentrations usually rose with elevated discharge (Figure 4a–c). The only exceptions were sites PD1 and PD2, with *C_{fw}* N-NO₃ being higher in REs than in RSs. No statistically significant correlation between drainage discharge and any of the substances was discovered during baseflow conditions. During an RE, positive correlations between discharge and both P forms were found, although with a broad range of slopes and shapes of the regression curves (data not shown).

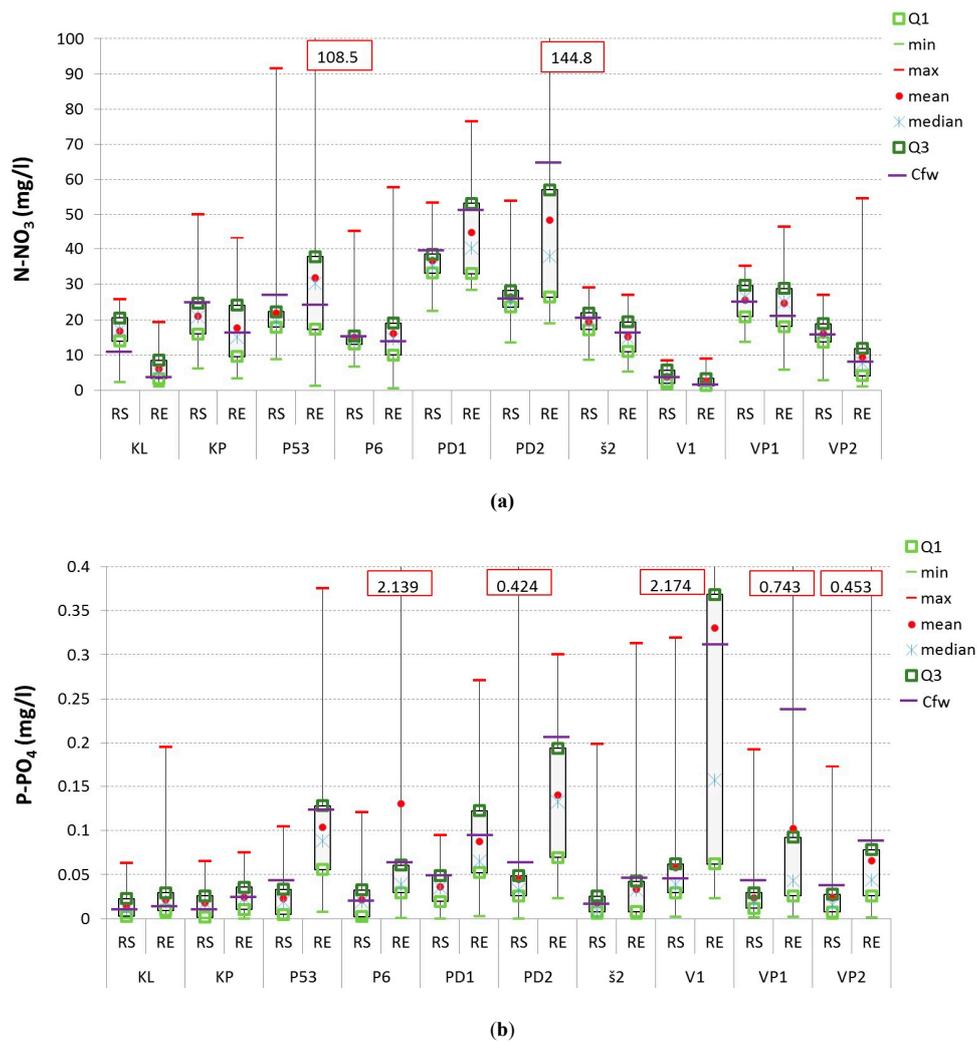


Figure 4. Cont.

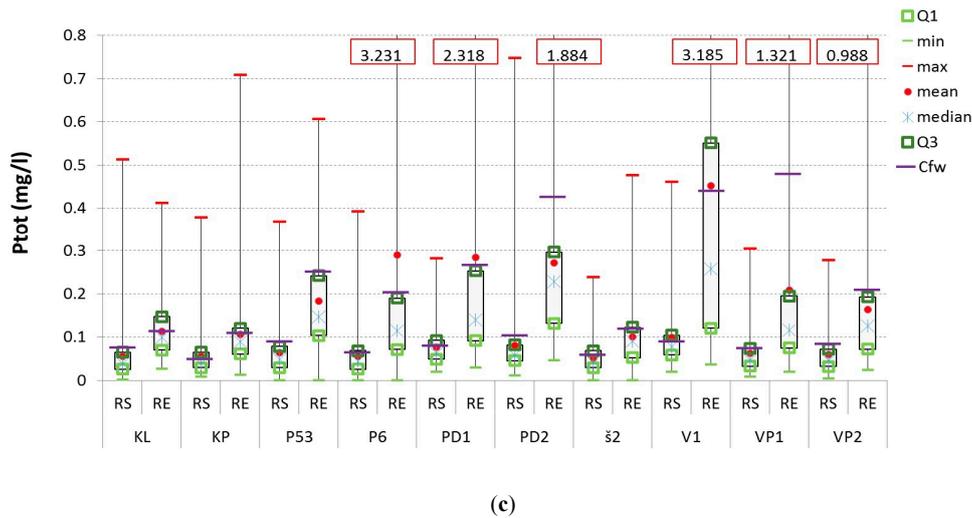


Figure 4. (a) Basic statistics of N-NO₃ concentrations in drainage waters across all the monitored sites, for regular (RS) and event (RE) sampling schemes. *Cfw* is flow-weighted concentration; (b) Basic statistics of P-PO₄ concentrations in drainage waters across all the monitored sites, for regular (RS) and event (RE) sampling schemes. *Cfw* is flow-weighted concentration; (c) Basic statistics of P_{tot} concentrations in drainage waters across all the monitored sites, for regular (RS) and event (RE) sampling schemes. *Cfw* is flow-weighted concentration.

3.2. Runoff Events and Their Proportion in the Total Runoff, N and P Loads

The average number of REs per hydrological year, across all the sites during the whole monitored period, was 13 (2 to 25), and these lasted on average for 30 (5.3 to 81.3) days within a hydrological year; see Table 3. The portion of REs sampled in one season varied from 30% to 45% of the total number of REs (Table 3). The within-period differences among the number and magnitudes of REs were induced most probably by different precipitation amounts and their variable time-distribution across the evaluated period (hydrological years). The lowest number of REs was monitored in the very dry year 2015 (an RE lasted on average 14 days, with an average 12% share on the total runoff), whereas in the wet year 2013, an RE lasted on average 48.5 days, with the mean share on the total runoff being 38.5%. The proportion of REs in the annual total runoff and in the N-NO₃, P-PO₄, and P_{tot} loads across all the monitored sites and periods was on average 24.5% (1.8–91.1%), 23.8% (1.7–85.5%), 41.6% (2.1–98.1%), and 40.3% (1.4–96.5%), respectively; see Table 3 and Figure 5 for details.

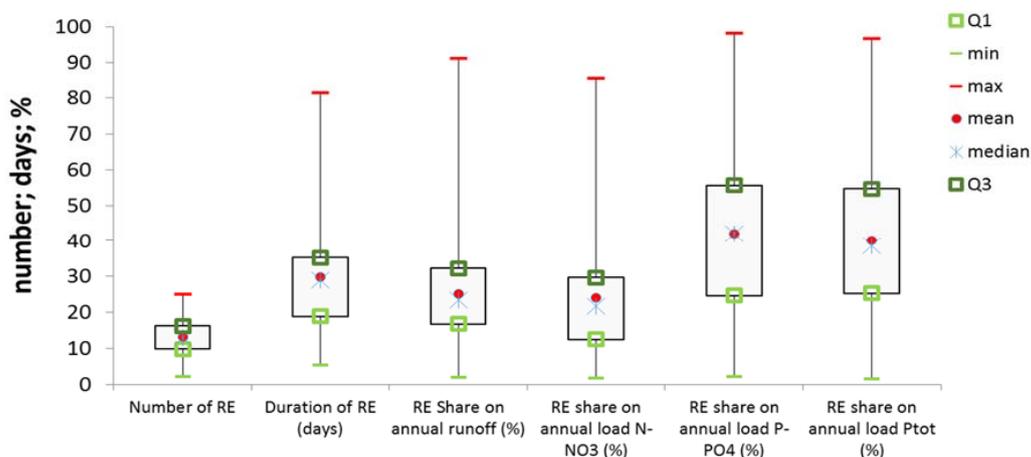


Figure 5. Basic statistics of the share of runoff events (RE) in the annual runoff and nutrient loads (data from all monitored sites and periods).

3.3. Comparison of Load Assessment Methods Annual Load Schemes

The annual true loads (M6) for N-NO₃, P-PO₄, and P_{tot} across all the monitored sites and periods were on average 19.01 kg·ha⁻¹·y⁻¹ (0.39–60.50), 32.09 g·ha⁻¹·y⁻¹ (0.64–131.85), and 99.28 g·ha⁻¹·y⁻¹ (3.83–337.65), respectively. The lowest N-NO₃ loads were measured at the grassland sites (KL, V1) and at the ploughed P53 site, which exhibits an obvious episodic runoff pattern. The N-NO₃ annual load from ploughed sites was on average around 30 kg·ha⁻¹·y⁻¹. The P-PO₄ and P_{tot} loads were comparable at the ploughed and grazed catchment (V1). The lowest P-PO₄ and P_{tot} loads were measured at sites KL and P53, the catchments with the smallest total runoff.

The nutrient load assessment algorithms differed according to the employed method of discharge monitoring and, to a lesser extent, the method of nutrient concentration monitoring (calculation), with the exception of monitoring during the REs (M6). Nutrient loads, calculated by M1 to M5, in relation to M6, along with the loads in REs, are depicted on Figure 6a,b, and the basic statistics on M1 to M5 accuracy related to the true load (M6) on an annual basis for all the substances, sites, and monitored periods are shown in Table 4. For annual N-NO₃ loads, M1 was the least accurate method, when accounting for the average 3.2% underestimation (−27.5 to 64.5%) of the M6 load. The M1 algorithm was also the least accurate for annual phosphorus loads; for P-PO₄, it underestimated M6 loads by 27.9% on average (−93.3% to 47.5%), and, for P_{tot}, it underestimated M6 loads by 28.2% on average (−78.2% to 4.2%). None of the variables (nutrient loads according to M1 to M6 across all the sites and monitored periods) was affected significantly by the methods (ANOVA; $p > 0.05$).

3.4. Monthly Load Schemes

The monthly nutrient true loads (M6) for N-NO₃, P-PO₄, and P_{tot} across all the monitored sites and periods were on average 1.52 kg·ha⁻¹·month⁻¹ (0.01–16.41), 2.81 g·ha⁻¹·month⁻¹ (0.003–48.85), and 6.87 g·ha⁻¹·month⁻¹ (0.004–139.32), respectively. The accuracy and the RMSE of M3 to M5 (M1 and M2 only on annual basis) as related to the true loads (M6) are given in Tables 5 and 6, and the accuracy for all the sites over the monitored period is displayed in Figure 7a,b. In the monthly load schemes, the results showed that the algorithm that did not use a continuous record of discharge (M3) under- or overestimated nutrient loads the most. For N-NO₃, the average underestimation by M3 on a monthly basis was 10.5%, whereas for P-PO₄ and P_{tot} it was 176% and 59%, respectively. The extensive underestimation of monthly P-PO₄ loads was due to the fact that, at some sites (P53, V1, VP1), the P-PO₄ loss occurred solely during REs. As seen in Tables 5 and 6, M4 and M5 gave comparable results; i.e., for N-NO₃ loads, the underestimation was on average only around 3%, for P-PO₄ loads it was on average around 100% and for P_{tot} it was 35% to 40%.

Table 4. Accuracy statistics (%) of the M1 to M5 algorithms related to the true load (M6) on an annual basis for all the substances, sites, and monitored periods.

	N-NO ₃				P-PO ₄				P _{tot}			
	min	max	mean	median	min	max	mean	median	min	max	mean	median
M1	−27.5	64.5	−3.2	−6.9	−93.3	47.5	−27.9	−27.8	−78.2	4.2	−28.2	−23.6
M2	−24.8	46.1	3.2	0.3	−92.0	16.1	−20.5	−15.0	−79.9	17.8	−17.8	−11.9
M3	−48.7	74.1	1.3	−2.8	−79.5	89.4	−18.8	−22.2	−80.9	34.1	−18.2	−12.7
M4	−38.4	39.8	1.4	2.3	−74.6	10.6	−22.5	−17.8	−80.1	18.5	−21.7	−16.9
M5	−37.3	41.7	1.4	2.1	−74.7	6.0	−24.6	−18.7	−79.7	20.5	−21.9	−14.5

Table 5. Average monthly accuracy (%) of the M3 to M5 algorithms related to the true load (M6) for all the substances, sites, and monitored periods.

Site	M3			M4			M5		
	N-NO ₃	P-PO ₄	P _{tot}	N-NO ₃	P-PO ₄	P _{tot}	N-NO ₃	P-PO ₄	P _{tot}
KL	0.38	−33.39	−20.93	3.97	−31.35	−16.17	4.03	−27.33	−12.22
KP	1.91	−37.20	−12.48	2.17	−39.78	−12.66	2.48	−37.35	−12.63
P53	−12.35	−962.19	−88.09	−8.58	−445.31	−51.30	−21.91	−473.09	−59.06
P6	−2.80	−145.51	−96.26	−2.42	−140.96	−88.37	−0.65	−126.26	−75.83
PD1	−11.28	−16.86	−103.62	−1.19	−3.55	−30.85	−1.42	−6.22	−29.87
PD2	−38.87	0.29	8.41	−14.62	−33.72	−37.27	−14.42	−35.68	−37.38
Š2	−16.39	−88.88	−41.40	−5.39	−29.36	−31.66	−0.36	−21.95	−13.80
V1	−6.60	−211.20	−92.73	−0.60	−155.40	−63.18	−0.20	−141.39	−41.51
VP1	−10.67	−207.78	−88.58	−1.83	−144.03	−52.79	−1.43	−128.40	−32.07
VP2	−7.72	−60.50	−53.11	−0.88	−36.21	−30.14	3.22	−39.77	−29.97
average	−10.44	−176.32	−58.88	−2.94	−105.97	−41.44	−3.07	−103.74	−34.43

Table 6. Average monthly RMSE (%) of the M3 to M5 algorithms related to the true load (M6) for all the substances, sites, and monitored periods.

Site	M3			M4			M5		
	N-NO ₃	P-PO ₄	P _{tot}	N-NO ₃	P-PO ₄	P _{tot}	N-NO ₃	P-PO ₄	P _{tot}
KL	23.58	90.87	61.16	9.98	81.77	37.59	8.90	77.27	26.96
KP	21.90	97.37	43.44	9.08	92.38	28.94	8.49	85.34	28.47
P53	61.15	4126.42	278.01	63.97	1596.52	123.47	175.61	1841.11	177.04
P6	24.43	382.84	288.40	13.28	343.94	259.29	10.92	329.51	224.72
PD1	60.91	91.76	579.89	8.96	25.68	155.82	7.29	16.13	148.69
PD2	140.71	50.32	43.11	35.40	84.58	86.69	34.43	77.05	85.87
Š2	59.11	276.52	124.46	49.25	91.19	89.28	15.62	53.71	36.59
V1	35.33	826.37	250.02	14.25	631.76	142.17	10.92	565.58	76.86
VP1	29.96	827.53	255.65	6.56	631.46	144.63	4.81	565.06	79.65
VP2	29.33	125.70	129.90	19.15	74.43	75.60	17.24	76.72	62.68
mean	48.64	689.57	205.40	22.99	365.37	114.35	29.42	368.75	94.75

4. Discussion

4.1. Dynamics of N and P Concentrations

In general, the grassed catchments (KL, V1) had lower N-NO₃ concentration values than the ploughed catchments, both during RSs and ESs due to the well-known mitigation effect of grassland on nitrate leaching [12,15,42]. For both P forms monitored in drainage waters, no such differences were found. During the REs, a dilution of N-NO₃ in drainage waters usually prevailed, whilst for both P-PO₄ and P_{tot}, the concentrations usually rose with elevated discharge, which is in accordance with many monitoring campaigns in tile-drained catchments [5,12,18,25,31]. The only exceptions were sites PD1 and PD2, with *C_{fw}* N-NO₃ higher in ESs than in RSs. This was most probably due to the over-fertilization of these catchments either by mineral nitrogen or digestate, as documented by other studies [13,44].

4.2. Runoff Events and Their Proportion on Total Runoff, N and P Loads

The within-site differences between the number and magnitudes of REs and their share of total runoff and between the N-NO₃, P-PO₄, and P_{tot} loads were brought about most probably by the distinct hydrological connectivity and runoff formation pattern in particular drainage—catchment systems [7,21,34,46]. This connectivity is affected by the position of a drainage system in a particular part of a slope (higher, lower) and by local soil variability [42,43,47–49]. This can lead to different proportions of runoff components in drainage runoff, e.g., sites lying in higher positions on slopes

(typically P53) have lower proportions of baseflow and higher numbers of REs. Similar (very variable) proportions of event water (12% to 50%) for similar amounts of precipitation (20 to 30 mm) are reported by other studies [21,50–52]. This variability in REs is more probably caused by diverse hydrological conditions in the catchments preceding the rain, namely, soil moisture, the groundwater level in summer, and snow cover for winter events, than by the intensity of rainfall [51], although some other studies reported contrarily [21,53].

In general, the relatively small share of REs for N-NO₃ loads is explained as a dilution of nitrate-rich drainage water by rain water during the majority of the REs, both on grassed as well as on ploughed sites, as discovered also by other studies [4,17,44]. The highest share of REs in N-NO₃ loads was measured in the N-overfertilized catchments (PD1, PD2; RE share up to 61%) and at site P53 (RE share on average 51%), which had a profound episodic runoff pattern (some months were almost without regular flow). The low share of REs for N-NO₃ loads was exhibited on grassed site KL (on average 10.8%) and on ploughed site Š2 (on average 8.6%), which corresponded to a high baseflow. For both P forms, higher proportions of REs for P loads were found. The higher share of RE on P loads compared to N loads was caused by the well documented different patterns of N and P leaching from soil into drainage waters [10,34], when P concentrations substantially rose with the elevated discharge across all the sites. This manifested the most at the sites with a substantial share of REs in the runoff (P53 site). However, a detailed analysis of these effects was not an aim of this study.

4.3. Comparison of Load Assessment Methods

The lowest P-PO₄ and P_{tot} loads were measured at the sites with the smallest total runoff (KL, P53). This means that, for both the P-PO₄ and P_{tot} loads, the runoff pattern seems to play in general a more dominant role than land use within the monitored catchments, as discovered also by other studies in similar and different climate and cropping systems [5,9,12,19]. The differences in total runoff in sites with similar geographical conditions were caused most probably by the different areas of their recharge zones [43]. The changeable runoff pattern probably also explains the fact that the ANOVA found the differences among the methods to be insignificant (N-NO₃: F-ratio 0.08, P-value 0.9958, P-PO₄: F-ratio 0.98, P-value 0.4286, P_{tot}: F-ratio 1.77, P-value 0.1196). The results showed supposedly small differences between the methods on the annual basis. M2 appeared to be quite a reasonable algorithm for the assessment of N-NO₃ loads, when only grab sampling (without continuous monitoring of discharge) was employed. However, it still gave large underestimations, especially for both phosphorus compounds, as the grab sampling rarely captured different REs with different P concentration values, as documented by [31–34].

For monthly nutrient loads, the M5 algorithm, with continuous flow measurements and using linear interpolations of the concentrations from the consecutively sampled days, resulted in a quite acceptable degree of accuracy for monthly N load estimation, with an exception for one overfertilized site (PD2) and site P53, which had a dominant episodic runoff pattern, where the average underestimation of N loads was 14.5% and 21.9%, respectively. M5, however, for both P compounds, gave unsatisfactory estimates of the monthly loads since the temporal changes of P concentrations were not covered by the regular sampling, as discovered in other studies when a weekly time step of sampling was employed [18,33,34].

The results have highlighted the importance of runoff events (not only erosion-generating) in delivering phosphorus by tile drainage, sometimes in large amounts. Given that the average duration of an RE within a hydrological year was 30 (5.3 to 81.3) days across all the sites and seasons, the loss of phosphorus by subsurface runoff should be given considerable attention in central European tile-drained catchments, as recommended by many other studies in tile-drained landscapes of diverse natural and agricultural characteristics [5,6,8,10,34,35]. Since the algorithms that do not use a continuous record of flow rates (M1 to M3) has considerable poorer performance, yielding biased and imprecise results, the use of continuous flow measurement is necessary to capture

discharge dynamics and to calculate the real nutrient fluxes from small tile-drained catchments with reasonable certainty [25,27,33].

The *RMSE* expressed the cumulative information on the degree and variation of the relative error of a particular method, relative to M6, when both accuracy and precision were taken into account. It clearly showed that, for monthly N load estimation, M3 had an average *RMSE* approximately two-fold greater than those of M4 and M5 (48.6%, 23%, 29.4%, respectively). For P, roughly the same ratio was discovered, although in terms of percent values in the hundreds (Table 6). As for the accuracy, for the *RMSE*, the largest degrees and variations of errors were found for the sites with significant episodic runoff patterns, especially for P-PO₄ loss.

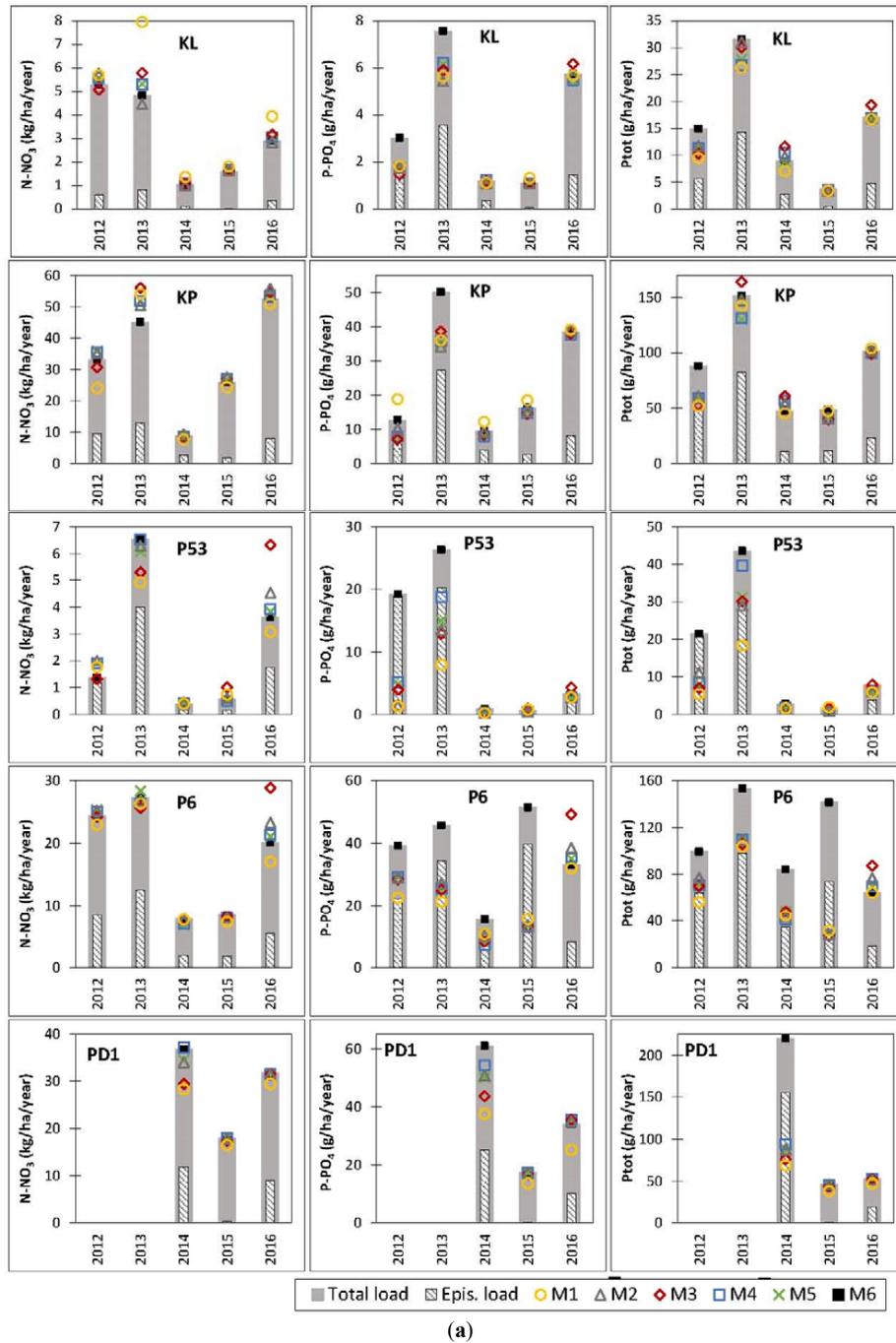


Figure 6. Cont.

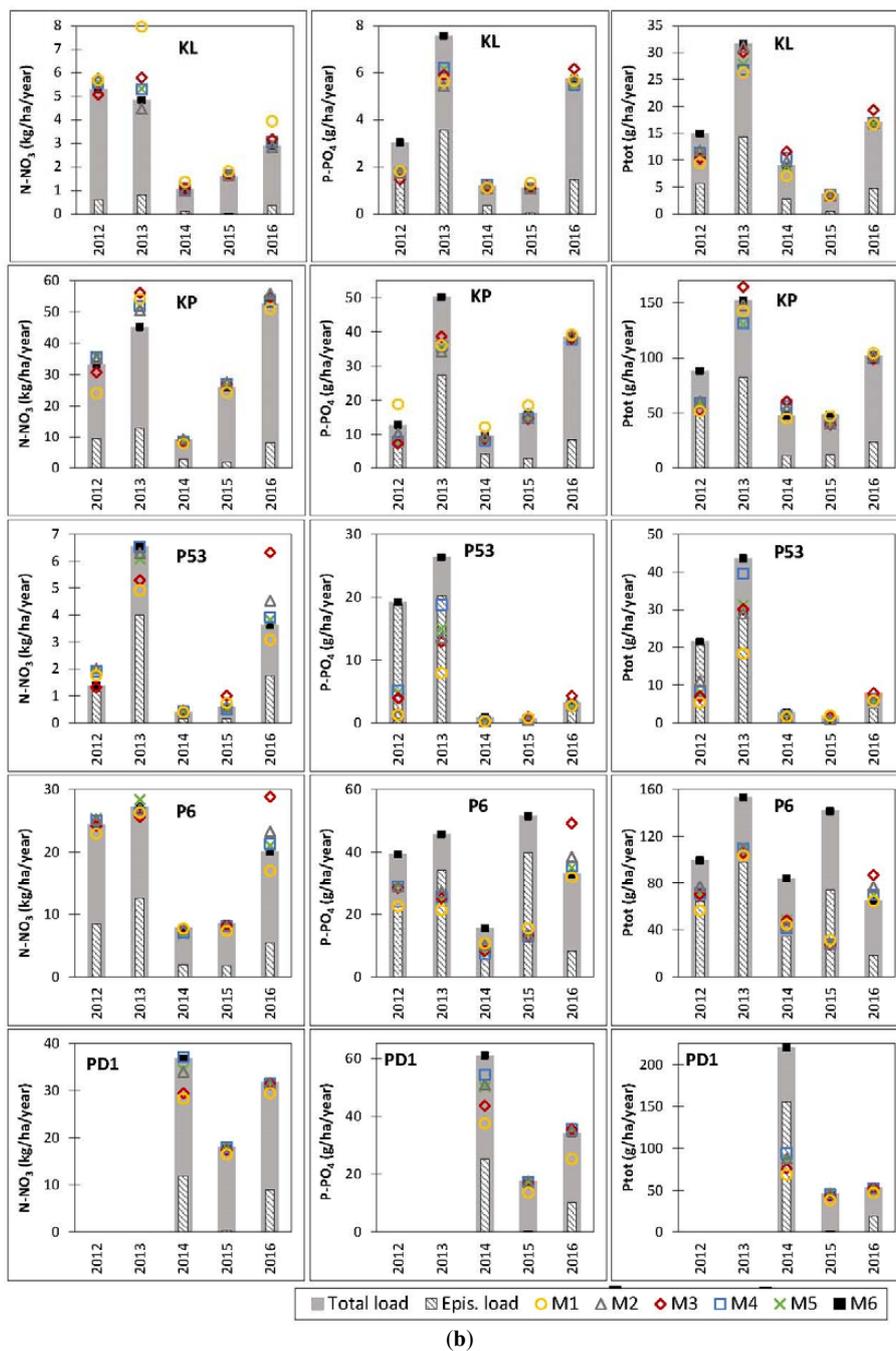
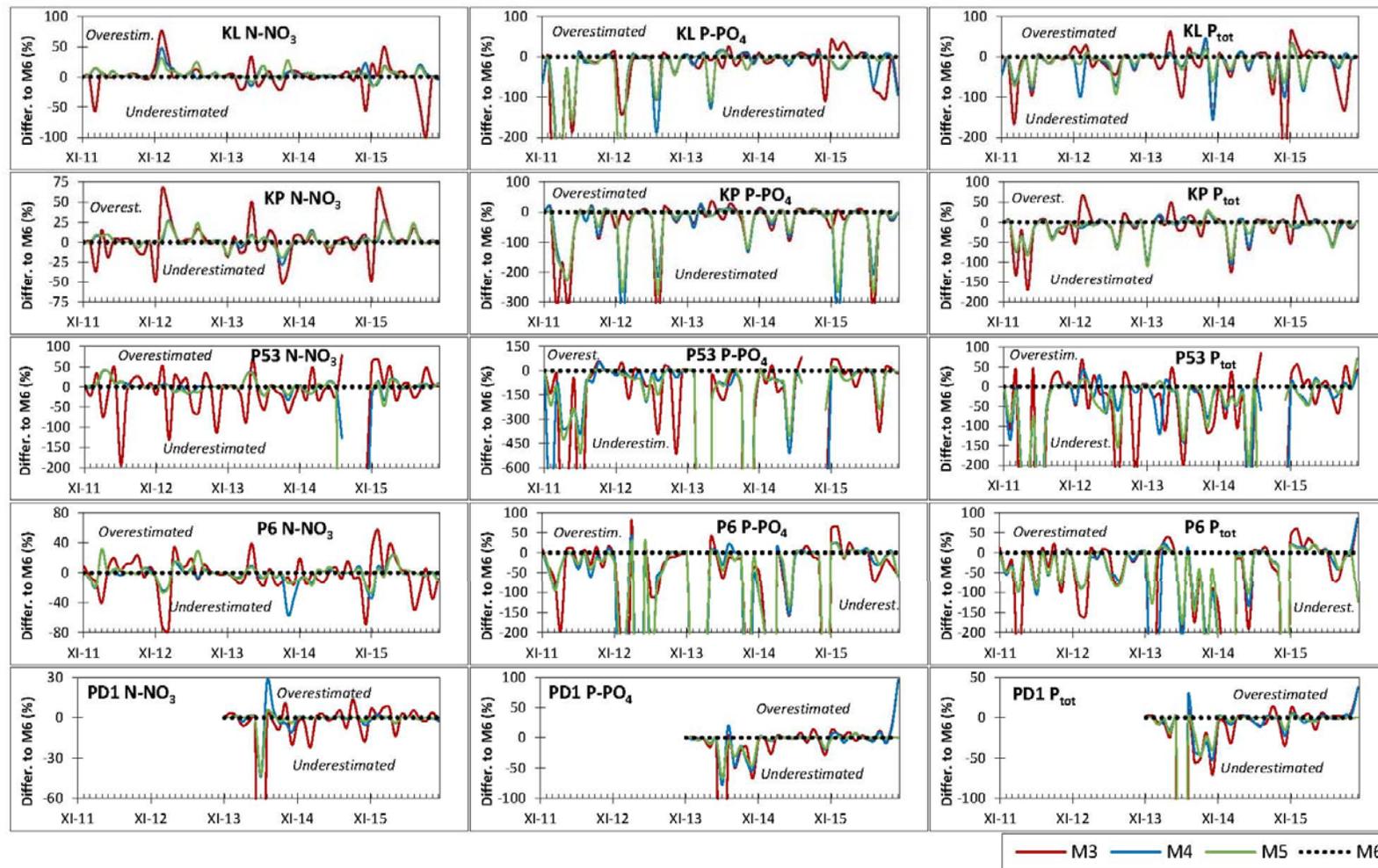
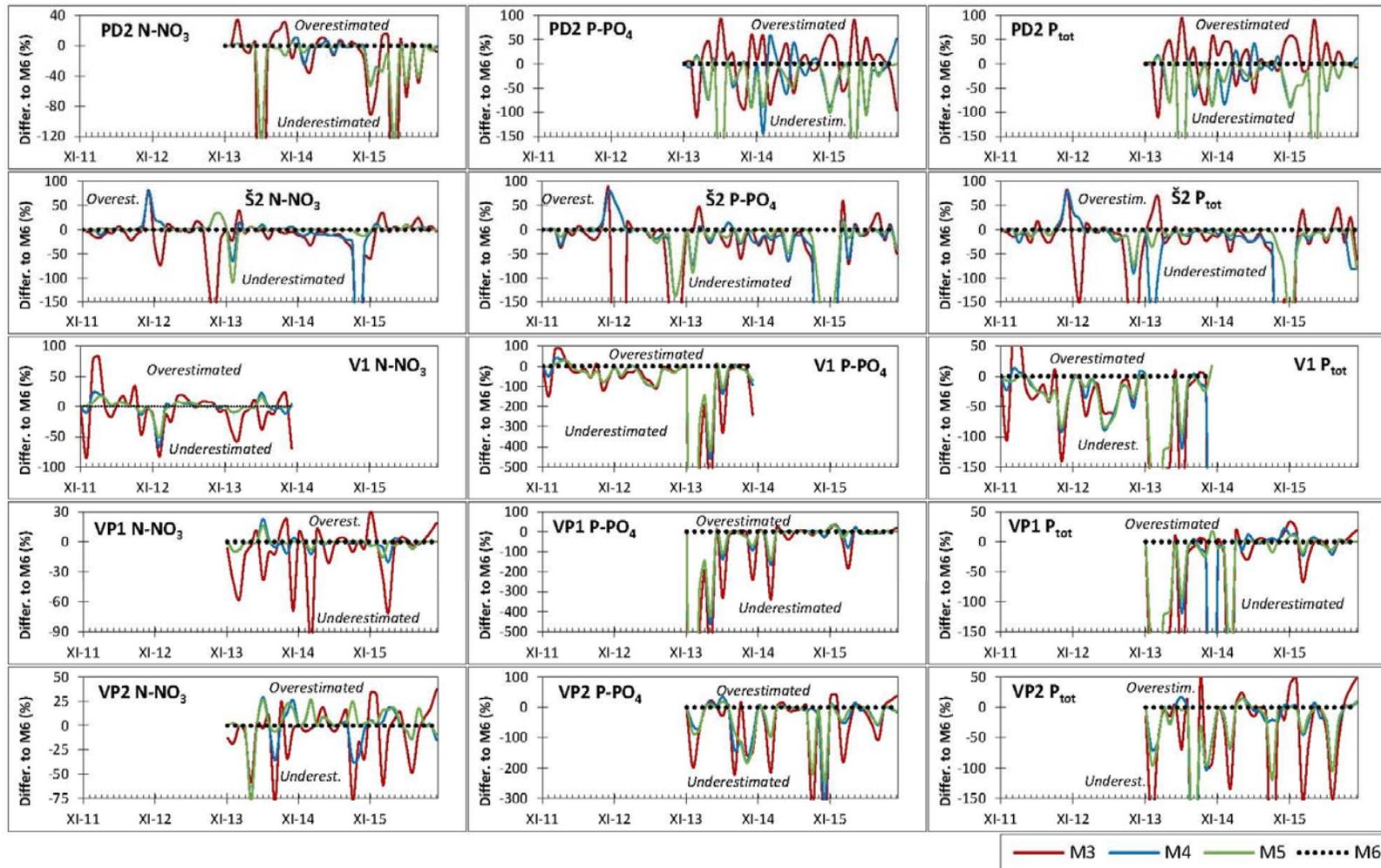


Figure 6. (a) Annual nutrient loads calculated by M1 to M6 and the proportion of runoff events in the total load for all substances at sites KL, KP, P53, P6, and PD1 and for all monitored periods. (b) Annual nutrient loads calculated by M1 to M6 and the proportion of runoff events in the total load for all substances at sites PD2, Š2, V1, VP1, and VP2 and for all monitored periods.



(a)

Figure 7. Cont.



(b)

Figure 7. (a) Monthly values of accuracy (%) of M3 to M5 related to M6 for all substances at sites KL, KP, P53, P6, and PD1 and for all monitored periods. (b) Monthly values of accuracy (%) of M3 to M5 related to M6 for all substances at sites PD2, Š2, V1, VP1, and VP2 and for all monitored periods.

5. Conclusions

This study compared six methods for nitrogen and phosphorus load calculation in ten small tile-drained sloped catchments in both annual and monthly time steps based on data from three to five hydrological years. Further, for the monitored sites and periods, the share of runoff events in the total runoff of N-NO₃, P-PO₄, and P_{tot} was quantified. A novel semi-automated algorithm for the identification and selection of runoff events from continuous flow using drainage water temperature was proposed and applied for load calculation in the unsampled events. The share of runoff events in N loads was on average 5% to 30% of the total annual load, whereas for P (dissolved and total), the share of runoff events was on average 10% to 80% of the total annual load. The most precise methods for nutrient load estimation were those with the use of continuous measurement of the discharge (M4, M5). However, without sampling the runoff events, these methods showed considerable uncertainties, especially for phosphorus load estimation. The methods based on point monitoring discharge and water quality (M1 to M3), commonly employed in practice when balancing non-point pollution sources in small tile-drained agricultural catchments, underestimated the annual loads of N by 10% to 20% and of P by 30% to 80%. For the monthly loads, this study demonstrated that methods without continuous flow measurements and with infrequent sampling tended to underestimate N and especially P loads by percentage values in the tens to the hundreds. The variability in loads between the years and sites was caused most probably by the dissimilar runoff patterns between particular sites and between particular years, which is not captured by grab sampling and regular monitoring at fixed intervals.

Based on the acquired results, we recommend continuous flow and water temperature monitoring, as well as event-based sampling programmes, to be employed on tile drainage outlets, drainage mahnoles, or ditches. Although such very small catchments as observed in the present study could hardly be the subject of routine (nation-wide or large catchment) monitoring programmes, we emphasize the need to pay increased attention to the hydrochemical role of tile drainage since these systems strongly impact water quality and quantity in agriculturally exploited headwater catchments. This work also provided regionally representative N and P loads, which we consider to be of great value when balancing the non-point pollution sources of small water courses and designing appropriate mitigation measures for tile-drained land. Future work could focus on the linkages between catchment characteristics, nutrient load dynamics, and load calculation uncertainties provided by different methods in different seasons. Further, a more detailed hydrological description of the sites such as runoff flashiness, baseflow index, antecedent moisture conditions, or water catchment residence time will be employed in a follow-up study in order to better explain the magnitude of uncertainty and the dynamics of various algorithms across different catchments [27,34,46,47].

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