

Article Using the Periodic Dynamics of Well Water Levels to Estimate Time Series Changes in Aquifer Parameters

Peng Qiao¹, Shuangshuang Lan^{1,*}, Hongbiao Gu² and Zhengtan Mao¹

- ¹ Faculty of Architecture, Civil and Transportation Engineering, Beijing University of Technology, Beijing 100020, China; qiaopeng1997@foxmail.com (P.Q.); y1971362510@163.com (Z.M.)
- ² College of Transportation Engineering, Nanjing Tech University, Nanjing 210000, China; hongbiaosw@126.com
- * Correspondence: lanshuangs@bjut.edu.cn

Abstract: Due to the long duration and high cost of traditional pumping tests, the response of well water levels to seismic waves, earth tides, and barometric pressure provides a feasible method for determining continuous changes in aquifer hydraulic parameters. Aimed at the problem that the response phase shift of well BB water levels to tide M_2 is greater than that of tide O_1 , this paper preferentially calculated the time series changes in *S*, *B*_e, *n*, and *BK*_u based on the response mechanism of well water levels to barometric pressure and earth tides with the help of the smooth moving method. Then, by using the mixed flow model, the variation in the transmissivity and leakage coefficient over time was simultaneously obtained, and the evolution process and characteristics of aquifer parameters near well BB caused by the Wenchuan earthquake are ultimately discussed. The calculation results are basically consistent with the previous pumping test, and have been verified and compared by using other scholars' methods. This solving process avoids problems such as excessive dependence on initial values, multiple solutions, and unstable tide O_1 , which has a promoting effect on the study of the impact of seismic activity on aquifer systems.

Keywords: tidal response; hydraulic characteristics; transmissivity; leakage coefficient

1. Introduction

As the main hydrodynamic parameters of an aquifer, the transmissivity (T) and leakage coefficient (σ) represent the horizontal and vertical water exchange capacity of the aquifer, respectively, which directly determine the characteristics of groundwater movement and the law of solute transport [1]. The accurate calculation of aquifer hydraulic parameters and their continuous changes play an important role in guiding the rational development and utilization of groundwater resources, and also provide a theoretical basis for the stability analysis of underground space, the safe burial of nuclear waste, and the migration of groundwater pollutants [2].

Groundwater-level dynamics is an important observation reflecting the crustal activity, which is often affected by many factors, such as barometric pressure [3–5], earth tides [6,7], seismic wave propagation [8–10], and fault activity [11,12], so the response of well water levels to these factors provides a feasible method for determining aquifer hydraulic parameters. Cooper et al. [8] established a model for the response of well water levels to periodic loading, and proposed that the response amplitude of well water levels to pore pressure mainly depends on the dimensions of the well and the transmissivity and storage coefficient (S) of the aquifer. Hsieh et al. [7] and Rojstaczer [13] estimated the hydraulic parameters of an aquifer by using the response models of well water levels to barometric pressure and earth tides. Following Roeloffs [14], Doan and Brodsky [15] developed a tutorial to estimate the poroelastic parameters and the permeability of the reservoir by analyzing the amplitude and phase of the tidal response. Wang et al. [16,17] established a mixed flow model for the tidal response of groundwater in an aquifer; the model gave



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Copyright: © 2024 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). the expressions of the *T* and σ , and they provided an important supplement to the previous tidal analysis model. Based on the analysis of changes in groundwater responses to earth tides and barometric pressure, Wang and Manga [18] reviewed the latest research progress on the effects of earthquakes on aquifer parameters, and stressed the importance of real-time and continuous monitoring of groundwater. The above models have been widely used in the study of co-seismic well water level response mechanisms [19–21], the response of well–aquifer systems to different frequency waves [22,23], and changes in aquifer permeability caused by earthquakes [24–30]. For example, Shi et al. [20] identified five types of co-seismic groundwater level responses and two types of post-earthquake responses by recording the response of a large number of well water levels to earthquakes. Sun et al. [22] compared the sensitivity of two wells to different cyclic loads in the same area. Wang et al. [26] analyzed the causes and frequency of increases in the vertical permeability of an aquifer caused by large earthquakes.

Previous studies could only calculate the permeability (*T*) or leakage coefficient (σ) of an aquifer using the horizontal flow model or the vertical flow model separately [7,26], which cannot reflect the horizontal and vertical water exchange capacity of the aquifer simultaneously. Sun et al. [31] calculated the aquifer parameters using a graphical method, where only one set of T and σ values can be obtained at a time. Yang et al. [30,32,33] used tide M_2 and O_1 responses in a least squares inversion of the unknown parameters in the leaky aquifer model, with three inputs used to obtain three parameters (*S*, *T*, and σ) simultaneously, which reflect the water storage capacity and the horizontal and vertical water exchange capacity of the aquifer. This method is suitable for situations where the phase shift of tide O_1 is greater than that of tide M_2 . For the situation that the phase shift of tide M_2 is larger than that of tide O_1 in well BB, the time series and correct solution cannot be obtained by using Yang et al.'s method. And there will be multiple solutions in the calculation results using this method. Here, taking well BB near the Huayingshan fault as an example, this paper attempts to explore the way of obtaining the time series changes in aquifer hydraulic parameters in this case by synthesizing the barometric pressure and earth tide effect on the well water level, and discusses the accuracy, applicability, and advantages and disadvantages of the solution process, so as to achieve the purpose of explaining the changes in aquifer hydraulic characteristics caused by seismic activities.

2. Observation Background and Data

The Huayingshan fault is located in southwest China and is a type of dextral strike slip reverse fault that is about 460 km long. It is a boundary fault between the block-type fold belt in eastern Sichuan and the gentle structure of central Sichuan. Well BB is located within 10 km of the Huayingshan fault zone (Figure 1a) (Table S1), which is a typical "red bed" area in Sichuan basin; that is to say, the main exposed strata in this area are interbeds of purplish-red mudstone and gray–white arkose. The underground aquifer is mainly composed of feldspathic sandstone with a thickness of about 10~50 m. The upper and lower water-bearing sandstones are sandwiched by relatively impermeable mudstones. This type of aquifer is widespread and has numerous hydraulic connections. The confined water in this area's red bed is recharged primarily by precipitation in the outcrop area, followed by vertical infiltration of the surface water and partial leakage of adjacent aquifers. The precipitation and surface water infiltrate the aquifer through the exposed crack near the surface, and runoff or vertical leakage occurs along the river bed or along the sandstone fissure. When the aquifer is depleted, groundwater is discharged into the surface water or spring, and it can also be discharged through the adjacent aquifers.

The lithology of borehole BB is shown in Figure 1b. The depth of well BB is 105.36 m, the diameter of the 127 mm casing is lowered to 42.1 m, and the casing is sealed with cement. Purple mudstone is found at 3.54~29.90 m. The main aquifer is located at 29.90~70.24 m, and the borehole lithology is light grayish-white medium–coarse-grained thick-bedded arkose of the middle Jurassic. The level of 70.24~105.36 m is mainly purplish-red sandy mudstone with purplish-gray siltstone bands. The well water level is observed in static



water with an LN-3A digital piezometer, with a sampling interval of 1 min, an accuracy of 1 cm, and a resolution of 1 mm (Table S2).



As shown in Figure 2, the daily dynamic fluctuations in the groundwater level in well BB are stable, with a typical change amplitude of about 6 cm. And it has clear tidal variation characteristics of two peaks and two valleys, which are negatively correlated with the barometric pressure. A spectrum analysis of the groundwater level, barometric pressure, and earth tide data was performed using the calculation package Matlab[®] (Mathworks Inc., Natick, MI, USA), with spectrum analysis power plotted according to period (days/period) (Figure 3). According to the spectrum analysis results of well BB, the main tidal components of well water level are tides O₁, K₁, M₂, and S₂ (M₂ and O₁ are half-diurnal and diurnal

tides caused by the moon, respectively; K_1 is the diurnal tide caused by the sun and moon; S_2 is the half-diurnal tide caused by the sun), and is affected by both barometric pressure and earth tide. Considering that tides S_2 and K_1 are affected by barometric pressure and have small signal-to-noise ratios, tides O_1 and M_2 are mainly used in well water level tidal analysis to reduce calculation errors. Among them, the tide M_2 groundwater level data typically have a significant amplitude and a modest amount of errors.



Figure 2. (a) Groundwater level, (b) barometric pressure, and (c) theoretical tidal volumetric strain of well BB in 2016. The data of groundwater level and barometric pressure were obtained from the China Earthquake Precursor Monitoring Network; the theoretical tidal volumetric strain was obtained using the program EIS2000.



Figure 3. Results of spectrum analysis of well BB's hourly values of (**a**) groundwater level, (**b**) barometric pressure, and (**c**) earth tide in 2016.

3. Methods

To solve the unknown parameters in the mixed flow model proposed by Wang et al. [16], a tidal analysis of the well water level should be performed first. Through the tidal analysis of well BB's hourly values of the groundwater level in 2016 (Figure 4), it can be found that the M₂ phase shift (the average is 26.435°) is greater than the O₁ phase shift (the average is 14.92°), which does not match the standards of the literature [30]. And due to the unstable phase shift of tide O1, it is challenging for us to obtain time series and correct solutions using Yang et al.'s method for calculations, while tide M₂ has the advantages of having sufficient amplitude, being easily extracted, and not being affected by barometric pressure [34,35]. Therefore, here, only the response of the well water level to tide M_2 was used to estimate the T and σ of the aquifer near well BB. Based on the mixed flow model of aquifers proposed by Wang et al. [16], there are four unknowns (S, T, σ , and BK_{μ}) in the analytical expressions of the tidal factor (A') and the phase shift (η) (A' is the ratio of the measured amplitude of the tide to the theoretical amplitude of the earth tide; η represents the lag of the well water level relative to the pressure head). S and BK_u were determined beforehand based on the barometric influence and tidal effect of the well water level; then, the numerical solutions of T and σ were solved simultaneously using the least square method.



Figure 4. Phase shift of tides M_2 and O_1 obtained through tidal analysis using the Baytap08 program [36], with the time window of 30 days and the running step of 3 days.

3.1. Determination of Storage Coefficient

The specific storativity (S_s) is a parameter that describes the water release capacity of an aquifer [L⁻¹]. Assuming that the change in the aquifer porosity is equal to the change in the aquifer volume, the S_s of a confined aquifer can be expressed as [37,38]

$$S_{\rm s} = \rho_w g(\frac{1}{K} + \frac{n}{K_w}) = \frac{gn\rho_w}{K_w} = -\frac{\varepsilon_{kk}}{h} = \frac{1}{A'} \tag{1}$$

$$S = S_s \times M \tag{2}$$

where ρ_w refers to the density of water [L⁻³M], *n* refers to the porosity of the entire aquifer, *A*' is tidal factor [L], *M* refers to the aquifer thickness [L], and *K* and *K*_w refer to the bulk modulus of the aquifer and water [LM⁻¹T⁻²], respectively.

To obtain the A' in the aquifer, the tidal analysis data of the Baytap08 program were used [36]; the program uses Akaike's Bayesian information criterion. The following sections are presumptively possible for a time series [15,36,39]:

$$y_i = \sum_{m=1}^{M} \left(\alpha_m C_{mi} + \beta_m S_{mi} \right) + \sum_{k=0}^{K} b_k x_{i-k} + d_i + e_i$$
(3)

The tidal component is the first term on the right-hand side: C_{mi} and S_{mi} are theoretically computed values for the mth group of tidal elements, and α_m and β_m are the tidal response constants to be established in the statistical model. The barometric response element is established as $\sum_{k=0}^{K} b_k x_{i-k}$, where x_{i-k} is the observed barometric pressure and b_k is the response coefficient, d_i is the long-term trend, and e_i is the noise. The Akaike Bayesian information criterion is established from Equation (3), and this program features a Bayesian inversion procedure that enables the parameters α_m and β_m to be calculated and subsequently evaluated. The result of the Baytap08 analysis provides the A' and η for each tide group [40].

3.2. Determination of BK_u

 BK_u represents the elasticity of the rock (*B* is the Skempton coefficient; K_u is the undrained bulk modulus [41]), which is related to the bulk modulus of porous media (*K*), the bulk modulus of solids (K_s), the bulk modulus of fluids (K_w), and the porosity (*n*) of porous media. The calculation equations for K_u are shown in Table 1 [42–44].

In this calculation, the aquifer porosity is determined by the response of the well water level to barometric pressure [45]:

r

$$a = \frac{B_e S_s K_w}{\rho g} \tag{4}$$

where $K_w = 2.065 \times 10^3$ MPa; $\rho g = 9.8 \times 10^{-3}$ MPa/m. B_e is the barometric efficiency (dimensionless); it is a key index to directly reflect the barometric effect of the well water level. Here, in order to eliminate the influence of earth tide, the daily series values of the groundwater level and barometric pressure were selected to obtain B_e . The well water level (H(t)) is mainly composed of a trend term $(H^0(t))$, the response to barometric pressure $(B_e P(t))$, and rainfall (H'(t)):

$$H(t) = H^{0}(t) + H'(t) + B_{e}P(t)$$
(5)

The first-order difference is calculated using Equation (5) to eliminate the influence of the trend term, so that the value of B_e is calculated:

$$\Delta H(t) = \Delta H'(t) + B_e \Delta P(t) \tag{6}$$

where $\Delta H(t)$ is the change value of the well water level; $\Delta P(t)$ represents the water column height corresponding to the change values of the barometric pressure. The barometric efficiency obtained by the first-order difference method can eliminate the influence of trend change factors on the groundwater level. It is worth noting that the signs of $\Delta H(t)$ and $\Delta P(t)$ are both positive or negative at the same time, and $\Delta H(t)/\Delta P(t) < 1$; all of these can avoid the interference of rainfall ($\Delta H'(t)$) on the well water level.

Table 1. Calculation equations of *BK_u* and related physical quantities.

	Κ	α	Ν	В	K _u
Equation	$\frac{1}{K} = \frac{1-n}{K_s} + \frac{n}{K_w}$	$1 - K/K_s$	$\frac{1}{(\alpha/K_s)+n(1/K_w-1/K_s)}$	$\frac{1/K - 1/K_s}{(1/K - 1/K_s) + n(1/K_w - 1/K_s)}$	$K + \alpha^2 N$

Notes: α is Biot coefficient, *N* is Biot modulus. The aquifer lithology of well BB is grayish-white medium–coarsegrained thick-bedded arkose, and the solid skeleton bulk modulus is an empirical value, i.e., $K_S = 3.6 \times 10^4$ MPa.

3.3. Calculation Theory of Horizontal Transmissivity and Leakage Coefficient

According to the borehole structure of well BB (Figure 1b), it is considered that $3.54 \sim 29.90$ m is the aquitard, and $29.90 \sim 70.24$ m is the aquifer. It meets the requirements of the mixed flow model of Wang et al. [16]; that is, the thickness and leakage of the aquifer should not be too small. Based on the mixed flow model proposed by Wang et al., the analytical expressions of A' and η are as follows:

$$\begin{cases}
A' = abs\left(\frac{i\omega S}{(i\omega S + (K'/b'))\zeta}\right) * \frac{BK_u}{\rho g} \\
\eta = \arg\left(\frac{i\omega S}{(i\omega S + (K'/b'))\zeta}\right)
\end{cases}$$
(7)

$$\zeta = 1 + \left(\frac{r_c}{r_w}\right)^2 \frac{i\omega r_w K_0(\beta r_w)}{2T\beta K_1(\beta r_w)} \tag{8}$$

$$\beta = \left(\frac{K'}{Tb'} + \frac{i\omega S}{T}\right)^{1/2} \tag{9}$$

$$A' = A * \frac{BK_u}{\rho g} \tag{10}$$

where A' and η can be obtained through tidal analysis using the Baytap08 program [36]; A is the amplitude ratio (amplitude ratio of well water level to pressure head fluctuation); ω is the tidal wave frequency; K_n is the second kind of modified Bessel function (BesselK function) with order n and aquifer leakage coefficient $\sigma = K'/b'(K' \text{ and } b' \text{ represent the permeability coefficient and thickness of the aquitard in the vertical direction, respectively); and <math>r_w$ and r_c represent the well radius and the case radius. When S, BK_u , A', and η are known, Equation (7) can be used to simultaneously obtain T and σ .

4. Results

Considering that there were no major earthquakes in Sichuan–Chongqing area in 2016, and that the characteristics of the well water level are not interfered with by human factors, information on the well water level of well BB in 2016 was collected for research. A tidal analysis was performed on the hourly groundwater levels of well BB with a time window of 30 days and a running step of 3 days (Figure 5a,b); then, the dynamic change in *S* (Figure 5c) was obtained according to *A'* (Equations (1) and (2)). Based on the first-order difference method to solve *B_e*, the time series change in *B_e* was obtained by taking 30 days as a group and sliding for 3 days at a time (Figure 5d). And then the aquifer *n* was obtained according to the corresponding equation (Equation (4)), and finally, the *BK_u* values of the aquifer were obtained (Table 1; Figure 5e). The mean values of *S* and *BK_u* are 6.88×10^{-5} and 7.22 GPa, respectively.



Figure 5. The change characteristics of (**a**) tidal factor, (**b**) phase shift, (**c**) storage coefficient, (**d**) Barometric efficiency, and (**e**) BK_u in 2016. Here, the error bars are three times the standard deviation; the blue lines represent the mean of the data set.

According to Equation (7), when the values of *S* and BK_u are determined, Equation (7) has two equations with two unknowns (*T* and σ). Based on the least square method to solve the equations, if we input the corresponding parameters (*S*, BK_u , *A'*, and η) in the Matlab program, the time series changes in the aquifer hydraulic parameters near well BB (Figure 6) can be obtained. The mean values of *T* and σ are 3.7×10^{-6} m²/s and 1.35×10^{-8} s⁻¹, respectively. The hydraulic parameters are relatively stable as a whole because the aquifer near well BB was not disturbed significantly in 2016.



Figure 6. The changes in aquifer parameters near well BB in 2016, including (**a**) transmissivity and (**b**) leakage coefficient. The blue lines represent the mean of the data set.

5. Discussion

5.1. Verification of Results

Since there are always inconsistencies between the assumed conditions established by the theoretical equations and the actual site conditions, certain errors will inevitably occur in the process of solving. In this calculation, the variation of aquifer *n* near well BB ranges from 15.6% to 22% (Figure S1). The main lithology of well BB's aquifer is sandstone; according to Zhou et al.'s survey and laboratory test of the sandstone reservoir in the area where well BB is located [46–49], the *n* of the sandstone reservoir in this area ranges from 5% to 30%.

The previous pumping test showed that the *T* of the aquifer in the observed section of the well was $6.94 \times 10^{-6} \text{ m}^2/\text{s}$, which is close to the current calculation (Figure 6a). In order to further verify the calculation results of the aquifer parameters of well BB, the methods of Sun et al. [31] and Yang et al. [30] were cited and calculated based on the tidal analysis results. Based on the method of Sun et al. [31], the relationship between the hydraulic parameters of the aquifer (*T* and σ) and the tidal parameters (*A* and η) of well BB was calculated and is established in Figure 7. When *A* and η were 0.831 and 26.435° (point data, the mean of tidal analysis results of well BB in 2016), the variation curves of *T* and σ could be obtained and cross-solved to establish them as $3.76 \times 10^{-6} \text{ m}^2/\text{s}$ and $1.38 \times 10^{-8} \text{ s}^{-1}$. Although Yang et al.'s method [30] is challenging to obtain time series changes in parameters of the aquifer near well BB, it can be used to obtain point values to validate the results of this paper. All results of the above methods are shown in Table 2, which indicates that the calculation results of the aquifer parameters near well BB in this paper are reliable.



Figure 7. In the calculation, when $S = 6.88 \times 10^{-5}$, $r_c = 63.5$ mm, $r_w = 75$ mm, and $\tau = 12.42$ hr, the relationship between the hydraulic parameters of aquifer (*T* and σ) and the tidal parameters (*A* (**a**) and η (**b**)) of well BB are determined. The red lines represent the mean tidal parameters for well BB in 2016; the *T* and σ can be obtained when they intersect.

Method	Storage Coefficient S	Horizontal Transmissivity T (m ² /s)	Leakage Coefficient σ (s $^{-1}$)
Pumping test	-	$6.94 imes10^{-6}$	-
Yang et al.'s method cited *	$8.10 imes10^{-5}$	$3.1 imes10^{-6}$	$3.0 imes10^{-8}$
Sun et al.'s method cited	$6.88 imes10^{-5}$	$3.76 imes10^{-6}$	$1.38 imes10^{-8}$
This paper	$6.88 imes10^{-5}$	$3.7 imes 10^{-6}$	$1.35 imes10^{-8}$

Notes: * In Yang et al.'s method, the parameters of tide M_2 are $A' = 0.58 \text{ mm}/10^{-9}$ and $\eta = 26.402^{\circ}$; those of tide O_1 are $A' = 0.59 \text{ mm}/10^{-9}$ and $\eta = 23.799^{\circ}$ (point data, the mean of tidal analysis results of well BB in 2016).

The graphical method proposed by Sun et al. [31] can guarantee the accuracy of the results, but only one set of *T* and σ can be calculated and obtained at a time, making it challenging to calculate the time series changes in aquifer parameters. Yang et al.'s method [30] can simultaneously obtain the *S*, *T*, and σ of the aquifer. The outcomes of the calculations using the least square optimal fitting method, however, also depend on the initial values of the parameters to a certain extent, and there will be various solutions. Considering that when it is applied to an aquifer such as well BB (the phase shift of tide M₂ is greater than tide O₁), it is difficult to obtain a correct solution even if a reasonable initial value is set. Here, firstly, the barometric pressure and earth tide effects of the well water level were introduced to solve the *S* and *BK*_u, and then only the relatively stable tide M₂ was considered to solve Equation (7). By reducing the number of unknown parameters in the equations compared with the method of Yang et al., the dependence of the results on the initial values is greatly reduced. In addition, when substituting the calculated values of the horizontal transmissivity and leakage coefficient into Equation (7), the error of each equation was less than 1×10^{-5} .

5.2. The Effects of Earthquakes

Based on the above solving process, the effects of the Ms8.0 Wenchuan earthquake on the aquifer parameters near well BB is discussed. The values of *S* and BK_u of the aquifer before and after (4/12–6/12) the Wenchuan earthquake were firstly calculated (Figure 8a,b). The mean value of *S* caused by the earthquake increased from 6.32×10^{-5} before the

earthquake to 1.27×10^{-4} after the earthquake, and the mean value of BK_u decreased from 7.21 GPa before the earthquake to 4.36 GPa after the earthquake. The results showed that the *T* increased from 3.59×10^{-6} m²/s (mean value) to 1.03×10^{-5} m²/s (the maximum value after the earthquake) (Figure 8c), and the σ increased from 1.71×10^{-8} s⁻¹ (mean value) to 4.16×10^{-8} s⁻¹ (the maximum value after the earthquake) (Figure 8d). It can be inferred that the Wenchuan earthquake led to an increase in the aquifer's permeability. According to the changes in the co-seismic pore volumetric strain proposed by Shi et al. [50] and Lai et al. [51] during the Wenchuan earthquake, well BB was located in an expanding area and the aquifer permeability was enhanced accordingly.



Figure 8. The time series changes in (**a**) *S*, (**b**) BK_u , and hydraulic parameters ((**c**) *T* and (**d**) σ) of the aquifer before and after the Wenchuan earthquake. The green lines ($-\diamond$ -) represent the changes in hydraulic parameters after the earthquake using the mean values of *S* and BK_u one month before the earthquake as the input parameters.

Some scholars believe that even if *S* changes by one order of magnitude, the change in the value of *T* is very small [22]. If the mean values of *S* and BK_u ($S = 6.32 \times 10^{-5}$, $BK_u = 7.21$ GPa) before the earthquake were used as input parameters to solve the aquifer after the earthquake (the tidal parameters were still post-earthquake), although it did not make a big difference to the outcomes (the error of *T* is about 2.59×10^{-6} m²/s, and the error of σ is 9.05×10^{-9} s⁻¹), the variation interval of aquifer parameters (- \diamond -) will be the same as that before the earthquake. And the impact of the earthquake on the aquifer characteristics cannot be accurately reflected. Therefore, it is necessary to obtain the dynamic changes in *S* and BK_u , especially when the stratum is seriously disturbed.

6. Conclusions

Based on the response of well water levels to barometric pressure and earth tides, the aquifer parameters near well BB are estimated in this paper with the help of a mixed flow model. The evolution process and characteristics of the aquifer parameters near well BB caused by the Wenchuan earthquake are also obtained. The calculation results are unique and continuous, and have little dependence on the initial values in the least square method and do not utilize the unstable tide O_1 . The results have reference significance for the estimation of aquifer parameters near other wells. Due to the simplification and assumption of the mathematical model, there may be errors between the calculation results and the actual situation. And the process of solving aquifer parameters in this paper is a little complicated; the more accurate determination of *S* and *BK*_u values can improve the accuracy of aquifer parameter estimation.

Supplementary Materials: The following supporting information can be downloaded at https://www. mdpi.com/article/10.3390/w16081119/s1: Table S1. Longitude and latitude of well BB. Table S2. Groundwater level of well BB. Figure S1. Dynamic change in aquifer *n* near well BB in 2016.

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