

Water - MDPI
Supporting Information for manuscript

**Arsenite to Arsenate Oxidation and Water Disinfection via Solar Heterogeneous
Photocatalysis: A Kinetic and Statistical Approach**

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S1 Ferric chloride dose determination.

Multiple linear regression has been reported as a tool to find optimal dosage for coagulant [1–3]; in the present experiment, simple linear regression analysis was used to find the optimum ferric chloride (FeCl₃) dose. 0.5 L of groundwater were spiked with a sodium arsenite (NaAsO₂; J.T. Baker, USA, CAS: 7784-46-5) solution to increase arsenite (As^{III}) concentration in 300 µg /L; groundwater already had an arsenic (As) concentration of 51.52 µg/L (46.06 µg/L of As^{III} and 5.46 µg/L of As^V). Different doses were assessed in a coagulation-flocculation experiment following a jar test protocol with rapid mixing (400 rpm) for 1 min, followed by slow mixing (20 rpm) for 10 min, and 20 min for settling [4]. After settling, As concentration in the supernatant was quantified by graphite furnace atomic absorption spectroscopy (GH-AAS). Table S1 shows the different testes dosages, as well as the As concentration in the supernatant.

Table S1. FeCl₃ dose and As concentration in the supernatant.

FeCl ₃ (mg / L)	As ^{III} (µg / L)
7.68	1.93
3.84	4.44
1.92	15.53
0.96	70.23
0.48	301.07
0.24	341.97
0	365.43

Data was fitted to exponential regression equation, as show in Equation S1

$$y = \alpha \times e^{\beta \times x} \quad (\text{S1})$$

Coefficient of determination (R^2) was 0.90; coefficients were calculated with regression analysis: $\alpha = 211.92$, and $\beta = -1.442$. To attain an As concentration lower than $10 \mu\text{g} / \text{L}$, $2.19 \text{ mg} / \text{L FeCl}_3$ is needed.

References

1. Laky, D. Predictive model for drinking water treatment technology design – the efficiency of arsenic removal by in-situ formed ferric-hydroxide. *Period. Polytech. Civ. Eng.* **2010**, *54*, 45, doi:10.3311/pp.ci.2010-1.05.
2. Tshukudu, T.; Zheng, H.; Yang, J. Optimization of Coagulation with PFS-PDADMAC Composite Coagulants Using the Response Surface Methodology Experimental Design Technique. *Water Environ. Res.* **2013**, *85*, 456–465, doi:10.2175/106143012X13560205144515.
3. Corral Bobadilla, M.; Lorza, R.; Escribano García, R.; Somovilla Gómez, F.; Vergara González, E. Coagulation: Determination of Key Operating Parameters by Multi-Response Surface Methodology Using Desirability Functions. *Water* **2019**, *11*, 398, doi:10.3390/w11020398.
4. Laky, D.; Licskó, I. Arsenic removal by ferric-chloride coagulation – effect of phosphate, bicarbonate and silicate. *Water Sci. Technol.* **2011**, *64*, 1046–1055, doi:10.2166/wst.2011.419.