

# Mechanistic Model and Optimization of the Diclofenac Degradation Kinetic for Ozonation Processes Intensification

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### S1. Six-Flux Model parameters

In Table S1 were presented the constants required to compute the LVRPA for a given point at the flotation cell based in equations (x-y). The scattering and absorption coefficients were taken for the Evonik p25.

Table S1. Constants employed to estimate the LVRPA.

Constants		Value	Units
Intensity	$I_0$	$2.06 \times 10^{-5}$	$Einstein\ s^{-1}\ m^{-2}$
Scattering coefficient	$\sigma$	5420	$m^2\ kg^{-1}$
Absorption coefficient	$\kappa$	287	$m^2\ kg^{-1}$

First, the scattering albedo  $\omega_{corr}$  was computed according to Equation (S1), then, by replacing within Equations (S2) and (S3), the corrected value for this variable was obtained (S4). Here  $p_s$ ,  $p_b$ , and  $p_f$  were the sides, backward and forward scattering probabilities.

$$\omega = \frac{\sigma}{\kappa + \sigma} \quad (S1)$$

$$a = 1 - \omega p_f - \frac{4\omega^2 p_s^2}{1 - \omega p_f - \omega p_b - 2\omega p_s} \quad (S2)$$

$$b = \omega p_b + \frac{4\omega^2 p_s^2}{1 - \omega p_f - \omega p_b - 2\omega p_s} \quad (S3)$$

$$\omega_{corr} = \frac{b}{a} \quad (S4)$$

This value was used to calculate the corrected wavelength  $\lambda_{corr}$  and the optical thickness  $\tau$  according to Equations (S5) and (S6). Then, the apparent value for the optical thickness  $\tau_{app}$  was computed from (S7). Finally, the six-flux model parameter  $\gamma$  was obtained by equation (S8).

$$\lambda_{corr} = \frac{1}{a(\sigma + \kappa)C_{mp}\sqrt{1 - \omega_{corr}^2}} \quad (S5)$$

$$\tau = (\sigma + \kappa)C_{mp}r_p \quad (S6)$$

$$\tau_{app} = a\tau\sqrt{1 - \omega_{corr}^2} \quad (S7)$$

$$\gamma = \frac{1 - \sqrt{1 - \omega_{corr}^2}}{1 + \sqrt{1 - \omega_{corr}^2}} \exp(-2\tau_{app}) \quad (S8)$$

## S2. Mass Transfer

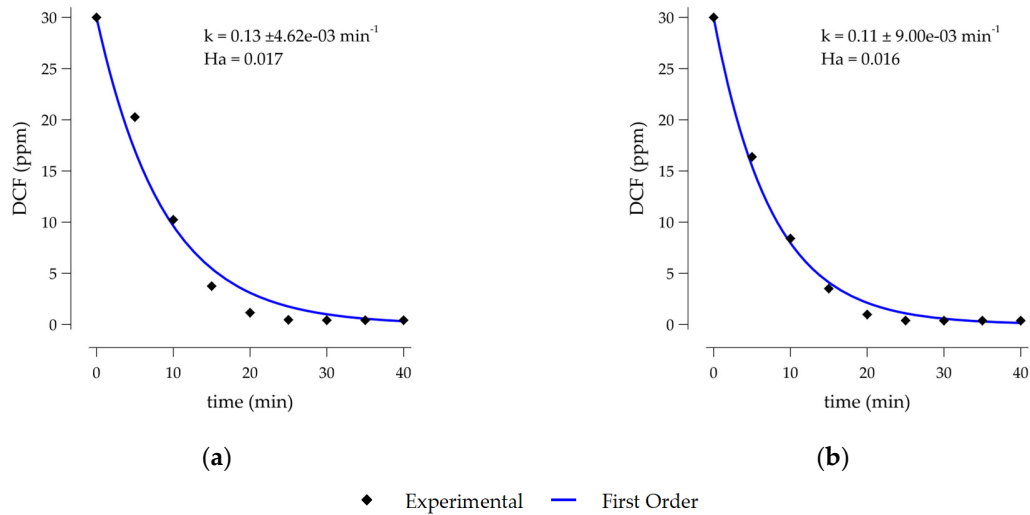
The estimated values for the mass constants at the flotation cell were summarized in Table S2.

Table S2. Mass transfer constants for the flotation cell.

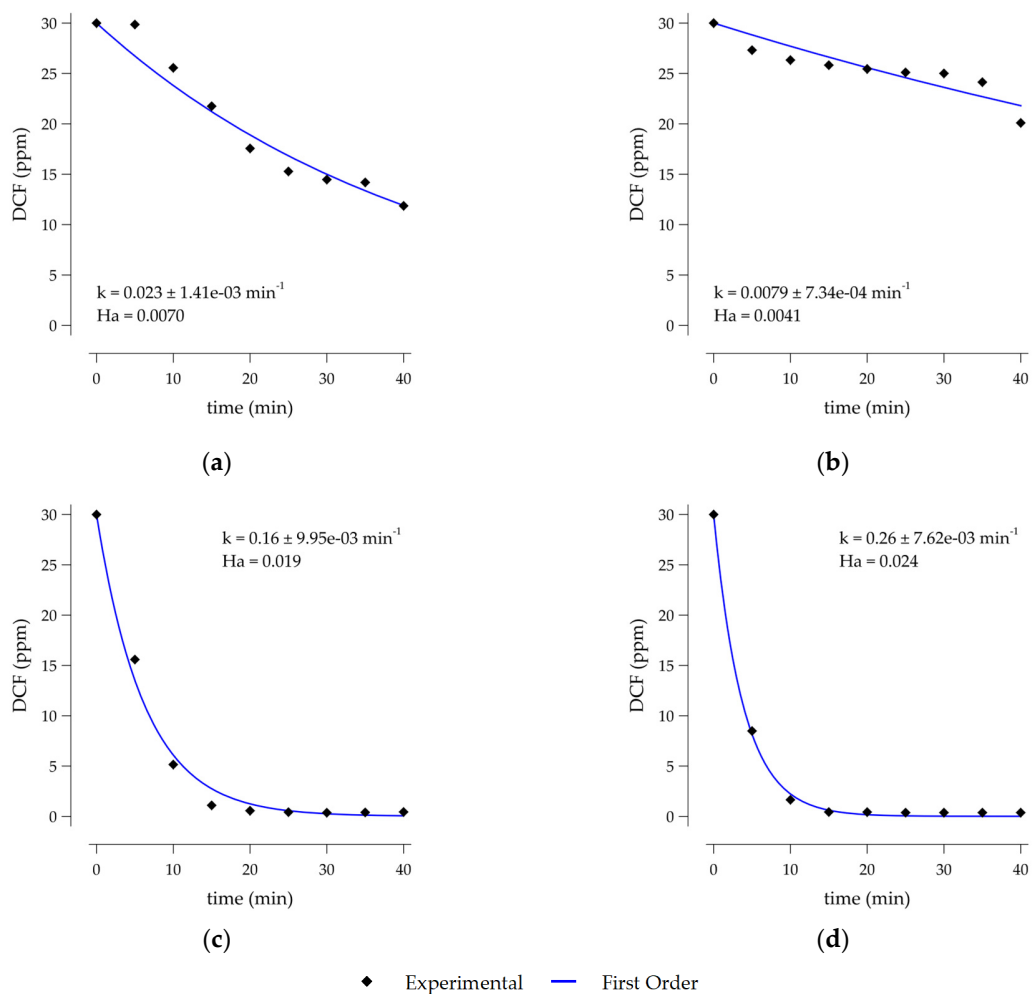
Constants	Value	Units
$k_L$	$4.56 \times 10^{-3}$	$m \min^{-1}$
$a$	220.33	$m^{-1}$
$\phi_{(g)}$	$4.13 \times 10^{-3}$	---
$d_b$	0.11	$mm$
$D_{O_3}$	$7.80 \times 10^{-8}$	$m^2 \min^{-1}$

## S3. Kinetic Regime

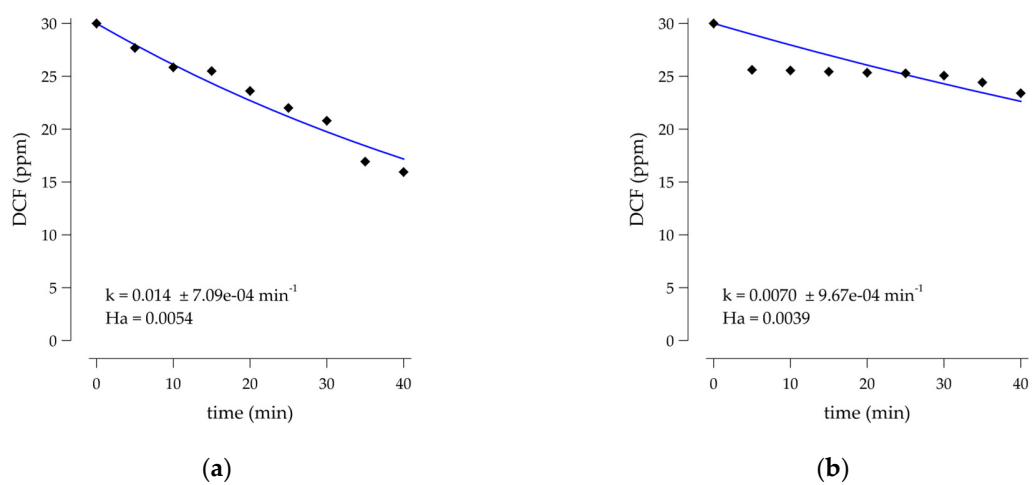
Figures S1–S3 depicted the estimated values of the Hatta number based on a first-order rate law for the ozonation, catalytic ozonation, and photocatalytic ozonation processes.

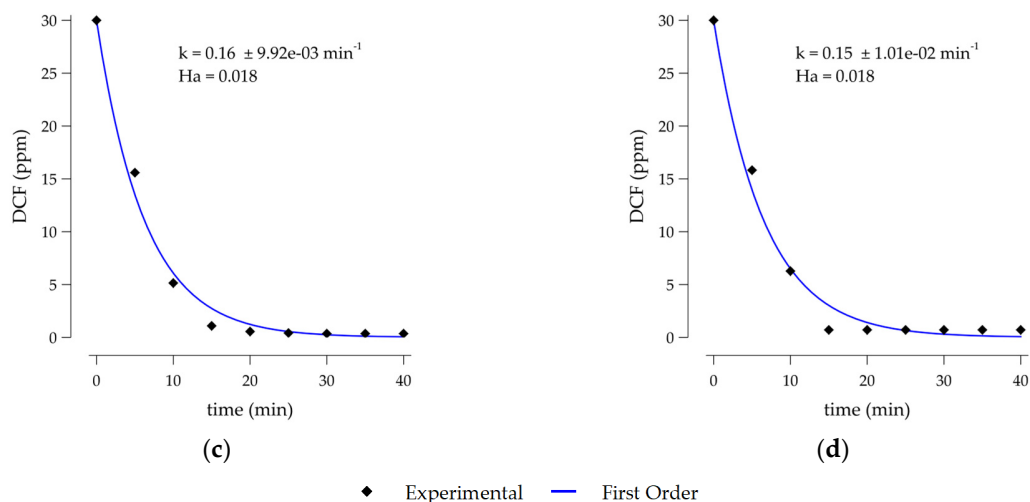


**Figure S1.** First-order rate law predictions for the diclofenac concentration in the ozonation process at (a) 2.66 and (b) 7.44 ppm in the ozone dose.



**Figure S2.** First-order rate law predictions for the diclofenac concentration in the catalytic ozonation process at (a) 2.66 & 300, (b) 2.66 & 800, (c) 7.40 & 300, (d) 7.40 & 800 ppm in the ozone dose and the catalyst load respectively.





**Figure S3.** First-order rate law predictions for the diclofenac concentration in the photocatalytic ozonation process at (a) 2.66 & 300, (b) 2.66 & 800, (c) 7.40 & 300, (d) 7.40 & 800 ppm in the ozone dose and the catalyst load respectively.

#### S4. Electrical Energy per Order

**Table S3.** Electrical energy per order (EE/O) for each process conditions.

Process	Ozone dose (ppm)	Catalyst load (ppm)	EE/O ( $\text{kWh m}^{-3}$ )
Ozonation	2.66	---	14.44
	7.40	---	17.07
Catalytic Ozonation	2.66	300	81.62
	2.66	800	237.64
	7.40	300	11.73
	7.40	800	7.22
Photocatalytic Ozonation	2.66	300	158.47
	2.66	800	316.45
	7.40	300	13.86
	7.40	800	14.79