



Article

GLOF Risk Assessment Model in the Himalayas: A Case Study of a Hydropower Project in the Upper Arun River

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Abstract: A glacial lake outburst flood (GLOF) is a phenomenon that is widely known by researchers because such an event can wreak havoc on the natural environment as well as on manmade infrastructure. Therefore, a GLOF risk assessment is necessary, especially within river basins with hydropower plants, and may lead to a tremendous amount of socioeconomic loss if not done. However, due to the subjective and objective limitations of the available GLOF risk assessment methods, we have proposed a new and easily applied method with a wider application and without the need for adaptation changes in accordance with the subject area, which also allows for the repeated use of this model. In this study, we focused our efforts on the Upper Arun Hydroelectric Project (UAHEP) in the Arun River Basin, and we (1) identified 49 glacial lakes with areas greater than 0.1 km²; (2) geographically represented and analyzed these 49 glacial lakes for the period of 1990–2018; (3) analyzed the correlation between the temperature and precipitation trends and the occurrence of recorded GLOF events in the region; (4) proposed a new method based on the documented affected lengths and volumes derived from historical GLOF events to identify 4 potentially critical lakes; and (5) evaluated the discharge profiles using widely used empirical methods and further discussed the physical properties, triggering factors, and outburst probability of the critical lakes. To achieve these objectives, a series of intensive and integrated desk studies, data collections, and GLOF simulations and analyses were performed.

Keywords: GLOF; glacial lakes; trends in discharge; Himalaya; risk assessment

1. Introduction

The Himalayas are an abundant resource of water but also have a relatively poor socioeconomic status; thus, this region has been greatly utilized for hydropower projects to help alleviate power loss and poverty. Since 1935, 62 glacial lake outburst flood (GLOF) events initiated from 56 glacial lakes in the Himalayas have been recorded, of which 8 occurred in Nepal [1], and the frequency has reached 1 event every 3–10 years [2–4]. This area has experienced many GLOFs in the past, of which the Cirenmaco GLOF (11 July 1981) located in the Sun Koshi River Basin in China [1,4–7], the Jinco GLOF (27 August 1982) at the headwaters of the Yairuzangbo River of the Pumqu Basin in China [4], the Dig Tsho (4 August 1985) [4,8,9] and Tam Pokhari (Sabai-Tsho) GLOFs (3 September 1998) [4,10–13] in the

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Dudh Basin in Nepal, and the Jialongco GLOF (23 May and 29 June 2002) in the Poiqu Basin in China [14] are good examples of the destructive consequences of GLOF disasters in the Central Himalayas, resulting in the destruction of some of the major hydropower projects, further causing socioeconomic decline [4]. Therefore, before any hydroelectric plant is built in this GLOF-hazard-prone region, a GLOF risk analysis is of crucial importance [15]. As mentioned above, documented GLOF events (such as Lake Cirenmaco and Dig Tsho) in the Central Himalayas destroyed downstream hydropower stations, roads, and bridges; killed hundreds of people; and caused millions of dollars in economic losses [16]. Such GLOFs are hazardous to resident safety, properties, infrastructure (e.g., hydropower, mining, roads, and bridges), agriculture husbandry, pasturelands, forests, tourism, and socioeconomic systems in downstream regions because of their potential to cause catastrophic breaching [4,10,17].

Nepal is endowed with vast water resources, with about 6000 rivers and rivulets contributing to an annual average runoff of 225 billion m3. The total drainage of these watercourses amounts to an area of 194,171 km², 76% of which falls within Nepal. It is noteworthy that as many as 33 of the larger rivers have drainage areas exceeding 1000 km2. The perennial nature of the rivers and the topography of the country, with steep gradients, provide excellent conditions for hydropower development, the theoretical potential of which has been estimated at 83,000 MW. In reality, however, only 1000 MW (including isolated micro and small hydropower plants)—less than 1.0% of the total potential—has been exploited so far, resulting in only 58% of the total population having access to electricity supply. The present capacity and energy generation is far less than the current electricity demand for both base and peak load and, hence, the country is forced to have load shedding during the dry season. As the electricity demand is projected to grow by 10% per year, the situation will worsen in the years to come if more sources of generation are not added to the system as soon as possible. In this context, the Nepal Electricity Authority (NEA), an undertaking of the Government of Nepal which is responsible for the generation, transmission, and distribution of electricity, has decided to initiate a detailed engineering study on hydropower projects that could be implemented at the earliest possible date. The Upper Arun Hydroelectric Project (UAHEP) is one such attractive project in the Eastern Development Region, which has very high head and firm river flow. The cabinet has also decided to implement the project through the NEA under the ownership of the Government of Nepal. In connection with this, NEA has also envisaged the development of the IkhuwaKhola Hydropower Project (IKHEP) under the umbrella of UAHEP to harness the hydropower potential of the country and to satisfy the increasing domestic power demand.

Several methods for assessing the risk of glacial lakes to outburst floods can be found in the literature [16,18–21]. These methods differentiate themselves according to the type of method structure, quantity and range of assessed characteristics, required input data, and percentage of subjectivity in assessment processes [22]. Some of them are regionally focused, and some are adjustable. The demands on input data and the rate of subjectivity of assessment procedures are generally considered as the fundamental obstructions to their repeated use. In [22], the suitability of these methods for use within the Cordillera Blanca was examined. It was shown that none of the applied methods met all of the specified criteria; therefore, a new method is desirable. Once critical lakes are identified, flood modeling and delimitation of endangered areas are the next steps in the risk management procedure [23,24].

The reasons for the presented study are as follows: First, the existing methods are not wholly suitable for use from the perspective of the assessed characteristics and the consideration of regional specificity (especially, the share and representation of various triggers of GLOFs and climate settings [22,25]). Second, the assessment procedures in the majority of these methods are at least partly subjective (based on an expert assessment without giving any thresholds when a clear instructive guide is missing); thus, different observers may reach different results even when the same input data are used. Repeated use is thus considerably limited, and this is considered the fundamental drawback of the present methods as well as a research deficit.

Due to the abovementioned reasons, the main objective of this work is to provide a comprehensive and easily repeatable methodological concept for the assessment of the risk of glacial lake hazards within the Arun River Basin, as verified using the data of glacial lakes and GLOFs recorded in this

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region. The impacts of glacial lake outburst floods cannot ever be completely eliminated; nevertheless, reliable assessment to identify critical glacial lakes is a necessary step in understanding the effects of flood hazards and, consequently, risk management and mitigation. Therefore, this assessment is of great importance.

1.1 Study Area

The UAHEP draws water discharged from the Arun River. It is located in the Sankhusabha District of the Koshi Zone in the Eastern Development Region of Nepal. The proposed dam site is located in a narrow gorge about 350 m upstream of the confluence with ChepuwaKhola in Chepuwa Village. The powerhouse lies in Hatiya Village, near the confluence of the Arun River with LeksuwaKhola. The project area is situated within longitudes 87°20′00″ to 87°30′00″E and latitudes 27°38′24″ to 27°48′09″N, as presented in Figure 1. The project area is located approximately 700 km east of Kathmandu and approximately 300 km north of Biratnagar. Fifty-two hydropower project sites have been identified within the Koshi Basin alone, and the proposed UAHEP is among the highest priorities of projects fed by mountain glaciers, which is why a GLOF risk assessment is one of the most important parts of this project.

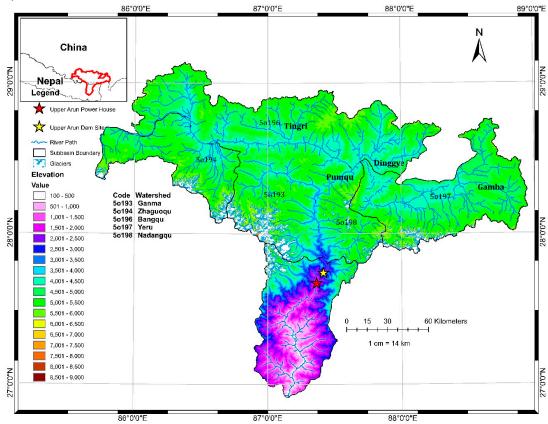


Figure 1. The study area.

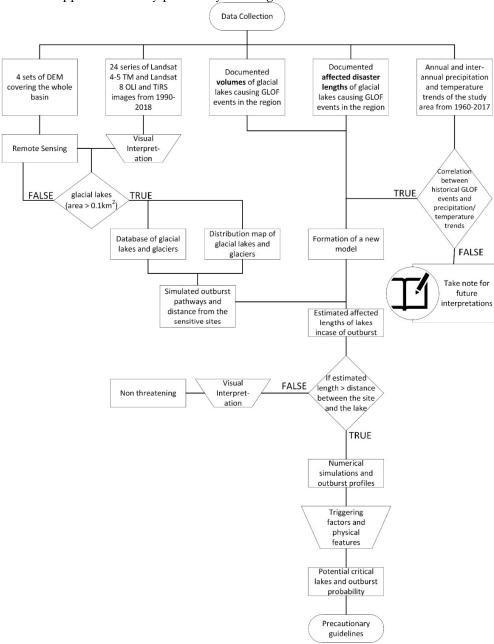
In 1985, the project site for UAHEP was recognized during the Master Plan Study of the Koshi River (Water Resources Development, JICA). In the summer of 1986, NEA conducted a reconnaissance study. In 1991, the Joint Venture of Morrison Knudsen Corporation, Lahmeyer International, Tokyo Electric Power Services Co., and NEPECON carried out a feasibility study of this project on behalf of NEA. NEA has given priority to the development of this project to augment the energy generation capability of the integrated Nepal Power System due to its relatively low cost of generation and availability of abundant firm energy. The feasibility study carried out in 1991 chose an installed capacity

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of 335 MW for the peaking run-of-river-type UAHEP. The design discharge of the project was 78.8 m³/sec, and it was expected to generate firm energy of 2050 GWh per year. In 2008, NEA obtained a license from the Government of Nepal to develop the UAHEP. The updated estimated cost was US\$446 million (335 MW/2050 GWh).

2. Materials and Methods

A detailed systematic methodological pathway is presented in Figure 2. This mainly included collected data in the form of satellite images, details of the historical GLOF events in the form of recorded volumes of the lakes and their corresponding affected lengths in the event of an outburst, and climatic data of the region, which were then analyzed through geographical information systems and statistical and analytical techniques. This methodology resulted in a new GLOF risk assessment model which was then applied to identify potentially critical glacial lakes.



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Figure 2. Methodology.

2.1. Data Collection

The data collection included four sets of digital elevation models (DEMs) covering the whole basin and satellite images, namely, 24 series of Landsat 4–5 Thematic Mapper (TM) [26], Landsat 8 Operational Land Imager (OLI), and Thermal Infrared Sensor (TIRS) from 1990 to 2018 US Geological Survey images, with four images for each year mosaicked to cover the whole basin for the years 1990, 1995, 2000, 2005, 2011, and 2018, resulting in a total of 24 satellite images. Data related to daily, monthly, and annual average temperatures, as well as precipitation for the years 1960–2017, were collected from the China Meteorological Data Service Center (CMDC). We also formed a database of documented volumes and affected disaster lengths of historical GLOF events in the region.

2.2. Remote Sensing

An advanced automated adaptive lake mapping method was adopted to interpret remote sensing images based on relevant maps to discover the distribution and annual and interannual changes of glaciers and glacial lakes in the basin. Geometric parameters of glacial lakes as well as their physical properties and river course characteristics were obtained through field investigation. These data were used to establish glacial lake databases and plot the distribution maps of glaciers and glacial lakes in the research area.

The lakes at risk are situated in remote and inaccessible areas. Remote sensing provides a feasible method to monitor glacial lakes [17]. An advanced adaptive lake mapping method was used to interpret remote sensing images (e.g., TM, Landsat 8, and other high-resolution images) based on relevant maps so as to determine the distribution, morphological characteristics, and annual and interannual changes of glaciers in the basin. Geometric parameters of glacial lakes, the physical properties of moraines, the depth of the lake, parameters of feeding glaciers, and river course characteristics were determined through field investigation and remote sensing analysis, as demonstrated in Figure 3.

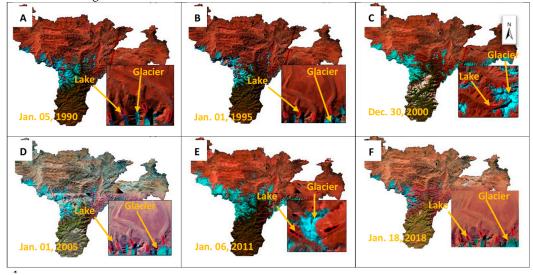


Figure 3. Remote sensing using satellite images to identify glaciers and glacial lakes for the years (**A**) 1990, (**B**) 1995, (**C**) 2000, (**D**) 2005, (**E**) 2011, and (**F**) 2018.

In total, we acquired 24 series of Landsat 8 OLI/TIRS images with no or less than 20% cloud cover for the periods of November–January in the years 1990, 1995, 2000, 2005, 2011, and 2017. The images used in this study were level 1 Geospatial Tagged Image File Format (GeoTIFF) data products, which

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were preliminarily calibrated. DEM data with a resolution of 90 m from the Shuttle Radar Topography Mission (SRTM) were used to obtain topographic information.

In this study, panchromatic images (band 8) from Landsat 8 OLI were registered with digital topographic maps using Earth Resource Data Analysis System (ERDAS) Imagine software. The registration accuracy was within 15 m (one pixel) in most areas. Furthermore, the images of other bands were resized to 15 m and were registered using the reference information from the panchromatic band.

The manual identification of individual glaciers was coupled and supplemented with the Global Land Ice Measurements from Space (GLIMS) database [10,27,28], so that the results could be merged and double-checked [28] to create an updated database. Since an individual dataset from GLIMS, ICIMOD, or CAS was not sufficient, we applied a combination of the three in addition to visual interpretation. A manual interpretation method was used to outline the glaciers and glacial lakes based on false color composite (FCC) images (6, 5, and 3 bands). DEM data were used to determine the dividing line of conjunct glaciers. The accuracy of manual interpretation has been demonstrated as optimal for identifying glaciers and glacial lakes because it allows for the consideration of both spectral characteristics and information regarding texture, patterns, shapes, and shadows. Finally, the spatial attributes of glaciers and glacial lakes were calculated using the topological analysis function of ArcInfo software based on the DEM data, and the volumes of glacial lakes were calculated based on their areas.

2.3. Formation of the Model

The main objective of this research is to determine the potential critical glacial lakes that could endanger the Hydroelectric Project. According to the results of remote sensing, there are 49 lakes with areas larger than $0.1 \, \mathrm{km^2}$. In this study, we selected the affected length to determine the potential critical glacial lakes. Firstly, we collected the affected lengths of historical GLOFs that had occurred in the Himalayan region. Secondly, an empirical equation was presented based on the collected data. Thirdly, the presented equation was used to predict the affected lengths of the 49 lakes. The lakes were determined as critical glacial lakes when the predicted affected length was longer than the distance between the lake and the dam (powerhouse) site.

3. Results

3.1. The New Model

Data including lake volumes and affected lengths from 11 historical GLOFs in the Himalayan region were collected. The detailed data are listed in Table 1.

Table 1. Volume and affected length of historical glacial lake outburst floods (GLOFs) that occurred in Nepal and Tibet (China).

No.	Name	Date	Volume V (× 106 m³)	Affected Length L (km)	Reference
1	Cirenmacuo	11 July 1981	18.9	53	[29]
2	Jialongco	23 May 2002	3.9	46	[29]
3	Taaco	28 August 1935	6.3	30	[29]
4	Qiongbixiamacuo	10 July 1940	12.4	44	[29]
5	Sangwang Lake	16 July 1954	300	200	[29]
6	Longdacuo	25 August 1964	10.8	28	[29]
7	Gelhaipuco	21 September 1964	23.4	43	[29]
8	Ayaco	18 August 1970	90	42	[29]
9	Dig Tsho	4 August 1985	8	42	[30]

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10	Tam Pokhari	3 September 1988	17.7	66	[31–33]
11	Luggye Tsho	7 October 1994	48	84	[8]

As shown in Figure 4, the affected length increases with the increase in lake volume. The fitting equation can be described as

$$L = 0.52V + 36.13 \tag{1}$$

where L is the affected length in km, and V is the lake volume in 106 m³.

Additionally, the upper limit line can be described as

$$L = 0.52V + 59.21$$
 (2)

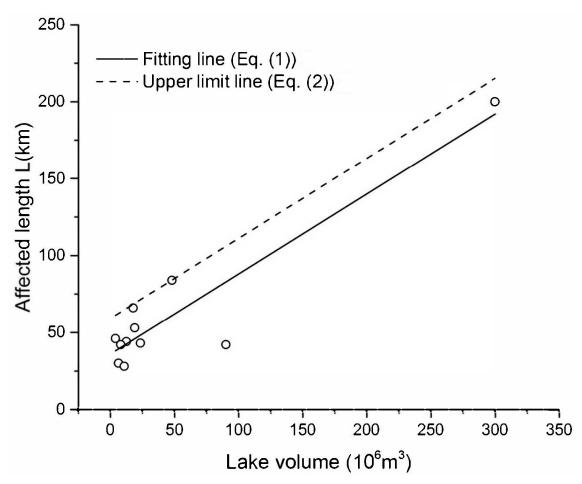


Figure 4. Lake volume versus affected length of historical GLOFs.

3.2. Determination of the Critical Lakes

After the formulation of the model, glacial lake databases were established, and the distributions of glaciers and glacial lakes in the research area were mapped. Furthermore, by carefully examining the elevations and flow paths, the expected outburst paths to the dam site were simulated (Appendix A, Figure A2) and individual distances between glacial lakes and the dam site were calculated in kilometers, as illustrated in Table 2. Table 2 summarizes the glacier inventories in the Arun River Basin for the years 1990–2017, including glacial lake locations with respect to longitudes and latitudes in decimal degrees followed by glacial lake areas in square kilometers.

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The sum of the lake area for the 49 lakes increased from 23.65 to 28.76 km². The ratio of the sum of the lake area in 2017 was 1.22 times that in 1990 because of the gradual increase in feeding from the mother glaciers and increased precipitation in the region.

In this study, the ratio of a lake area in 2017 to that in 1990 is defined as R. As shown in Appendix A, Figure A1, there are 20 lakes with R-values larger than 1. This indicates that the lake areas of the 20 lakes increased from 1990 to 2017. The maximum R is 25.23. There are 25 lakes with R-values remaining unchanged. There are four lakes with R-values less than 1. This indicates that the lake areas of these four lakes decreased from 1990 to 2017. The minimum R is 0.92.

Equation (2) was adopted to predict the affected length. The detailed data of lake volume, affected length (L_c), and distance between the lake and the Upper Arun dam site (L_d) are listed in Table 2. As shown in Table 2, the ratios of L_c to L_d of nos. 13, 20, 33, 35, 36, and 42 are larger than 1.0; this indicates that the possible GLOFs of these six lakes may endanger the dam.

The detailed data of lake volume, affected length (L_c), and distance between the lake and the Upper Arun powerhouse (L_p) are listed in Table 2. As shown in Table 2, the ratios of L_c to L_p of nos. 11, 35, 36, and 49 are larger than 1.0; this indicates that the possible GLOFs of these four lakes may endanger the Upper Arun powerhouse.

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Table 2. Annual variation in area, volume, calculated affected length (L_c), and distance between the lake and the dam site (L_d) and the Upper Arun powerhouse (L_p) for the 49 glacial lakes with areas > 0.1 km2 in the Arun River Basin for the period 1990–2017.

No.		ion	Lake Area (km²)						Volume				
110.	Longitude ()	Latitude ()	1990	1995	2000	2005	2011	2017	(10 ⁶ m ³)	L _d (km)	Lc (km)	L _p (km)	Lc/Lp
1	86.305	28.374	3.641	3.727	3.727	3.692	3.762	3.867	212.685	232.190	169.810	248.370	0.680
2	86.379	28.392	0.327	0.410	0.613	0.750	0.903	1.093	60.115	227.220	90.470	243.400	0.370
3	86.415	28.393	0.177	0.177	0.188	0.188	0.181	0.181	9.955	226.140	64.390	242.320	0.270
4	86.494	28.349	0.294	0.294	0.294	0.294	0.294	0.294	16.170	222.570	67.620	238.750	0.280
5	86.582	28.199	1.330	1.330	1.330	1.330	1.287	1.274	70.070	183.600	95.650	199.780	0.480
6	86.629	28.207	0.268	0.268	0.268	0.268	0.268	0.268	14.740	185.890	66.870	202.070	0.330
7	86.863	28.111	0.015	0.098	0.098	0.098	0.312	0.388	21.340	154.050	70.310	170.230	0.410
8	87.028	28.008	0.103	0.103	0.103	0.103	0.103	0.103	5.665	68.360	62.160	84.540	0.740
9	87.047	28.068	0.543	0.574	0.574	0.630	0.707	0.745	40.975	86.570	80.520	102.750	0.780
10	87.051	28.206	0.626	0.626	0.573	0.573	0.573	0.573	31.515	89.910	75.600	106.090	0.710
11	87.082	27.844	0.294	0.294	0.294	0.325	0.340	0.345	18.975	39.570	69.080	39.570	1.750
12	87.082	28.130	0.177	0.177	0.177	0.177	0.177	0.177	9.735	85.520	64.270	101.700	0.630
13	87.101	28.208	0.937	0.937	0.937	0.937	0.937	0.937	51.535	84.230	86.010	100.410	0.860
14	87.105	28.143	0.146	0.146	0.146	0.146	0.146	0.146	8.030	82.330	63.390	98.510	0.640
15	87.112	28.143	0.217	0.217	0.217	0.217	0.217	0.217	11.935	81.610	65.420	97.790	0.670
16	87.134	28.069	0.201	0.201	0.201	0.201	0.201	0.201	11.055	78.140	64.960	94.320	0.690
17	87.428	28.138	0.211	0.211	0.211	0.211	0.211	0.211	11.605	65.420	65.240	81.600	0.800
18	87.443	28.161	0.222	0.222	0.243	0.214	0.239	0.224	12.320	73.010	65.620	89.190	0.740
19	87.468	28.149	0.255	0.255	0.255	0.255	0.255	0.255	14.025	76.260	66.500	92.440	0.720
20	87.472	28.213	1.025	1.025	1.137	1.319	1.319	1.319	72.545	83.280	96.930	99.460	0.970
21	87.480	28.173	0.208	0.208	0.208	0.208	0.208	0.208	11.440	77.290	65.160	93.470	0.700
22	87.502	28.237	0.166	0.166	0.166	0.166	0.166	0.166	9.130	87.290	63.960	103.470	0.620
23	87.563	28.179	0.691	0.803	0.840	0.885	0.989	1.013	55.715	94.610	88.180	110.790	0.800
24	87.578	28.228	0.190	0.190	0.190	0.190	0.190	0.190	10.450	106.750	64.640	122.930	0.530
25	87.578	28.164	0.171	0.180	0.180	0.180	0.180	0.180	9.900	76.350	64.360	92.530	0.700
26	87.584	28.107	0.117	0.117	0.117	0.117	0.117	0.117	6.435	71.840	62.560	88.020	0.710

0.17	07 507	00.117	0.105	0.105	0.105	0.105	0.105	0.105	- 	70 100	(0.010	00.270	0.700
27	87.587	28.116	0.105	0.105	0.105	0.105	0.105	0.105	5.775	72.190	62.210	88.370	0.700
28	87.591	28.230	0.719	0.786	0.786	0.768	0.786	0.745	40.975	107.770	80.520	123.950	0.650
29	87.599	28.131	0.122	0.122	0.122	0.122	0.122	0.122	6.710	80.030	62.700	96.210	0.650
30	87.612	28.155	0.127	0.127	0.127	0.127	0.127	0.127	6.985	80.230	62.840	96.410	0.650
31	87.615	28.118	0.241	0.241	0.241	0.241	0.241	0.241	13.255	77.860	66.100	94.040	0.700
32	87.623	28.168	0.200	0.200	0.200	0.200	0.200	0.200	11.000	84.210	64.930	100.390	0.650
33	87.637	28.093	0.377	0.377	0.525	0.564	0.588	0.588	32.340	72.820	76.030	89.000	0.850
34	87.641	28.195	0.497	0.497	0.497	0.497	0.497	0.497	27.335	94.830	73.420	111.010	0.660
35	87.655	28.114	1.289	1.268	1.268	1.268	1.268	1.268	69.740	73.330	95.470	89.510	1.070
36	87.772	27.926	0.636	0.767	0.767	0.794	0.857	0.857	47.135	60.830	83.720	77.010	1.090
37	87.815	27.964	0.175	0.230	0.230	0.342	0.342	0.342	18.810	71.180	68.990	87.360	0.790
38	87.908	27.952	0.663	0.663	0.663	0.632	0.632	0.632	34.760	82.190	77.290	98.370	0.790
39	87.931	27.950	0.597	0.597	0.679	0.745	0.745	0.745	40.975	83.730	80.520	99.910	0.810
40	88.003	27.930	0.853	0.890	0.930	0.930	0.930	0.930	51.150	97.710	85.810	113.890	0.750
41	88.066	27.934	0.728	0.728	0.728	0.728	0.705	0.728	40.040	102.920	80.030	119.100	0.670
42	88.076	27.946	0.593	0.748	0.865	1.108	1.292	1.516	83.380	101.380	102.570	117.560	0.870
43	88.242	28.005	0.264	0.292	0.311	0.323	0.328	0.336	18.480	171.200	68.820	187.380	0.370
44	88.259	28.009	0.351	0.389	0.434	0.514	0.491	0.514	28.270	170.540	73.910	186.720	0.400
45	88.288	28.018	0.390	0.390	0.390	0.390	0.390	0.390	21.450	172.140	70.360	188.320	0.370
46	88.320	28.006	0.331	0.331	0.331	0.331	0.331	0.331	18.205	174.880	68.680	191.060	0.360
47	88.355	28.023	0.479	0.479	0.479	0.479	0.479	0.479	26.345	182.100	72.910	198.280	0.370
48	88.427	28.054	0.857	0.857	0.857	0.857	0.857	0.857	47.135	184.160	83.720	200.340	0.420
49	87.091	27.798	0.504	0.649	0.904	1.003	1.230	1.480	81.400	34.050	101.540	34.050	2.980

Note: Lake nos. 1–10 and 12–48 are located upstream of the dam site; lake nos. 11 and 49 are located downstream of the dam site.

As shown in Table 2, six glacial lakes were identified as potentially critical glacial lakes (nos. 13, 20, 33, 35, 36, and 42) for the Upper Arun dam. We selected three potential critical glacial lakes (nos. 20, 35, and 36). For these three lakes, the values of L_c/L_d are larger than 1.15. These three lakes are the most critical for the Upper Arun dam. The detailed distribution of these three potential critical glacial lakes is shown in Figure 5.

As shown in Table 2, four glacial lakes were identified as potentially critical glacial lakes (nos. 11, 35, 36, and 49) for the Upper Arun powerhouse. We selected glacial lake no. 49 as the most critical lake because the value of L_c/L_p is much larger than those of the other three glacial lakes (nos. 11, 35, and 36) (Table 2).

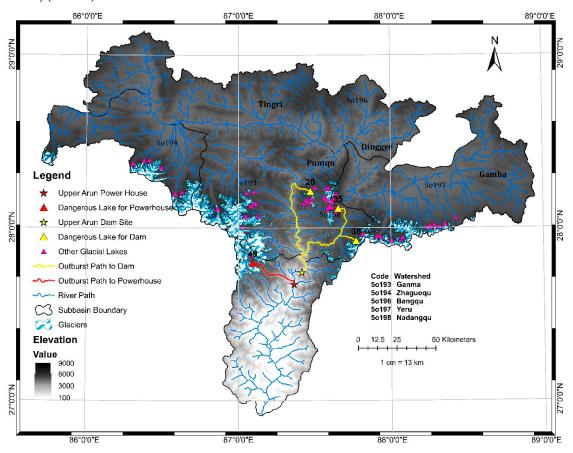


Figure 5. Locations of glaciers, glacial lakes with areas greater than 0.1 km², and potentially critical glacial lakes (nos. 20, 35, 36, and 49) and their outburst paths.

3.3. Discharge Profiles and Outburst Probability of the Critical Lakes

Table 3. Empirical formulas for calculating the peak discharge at the glacial lake dam site.

Formula	Source	Note					
$Q_m = 0.0048 V_w^{0.896}$	[34]	Q_m is the peak discharge at the dam site, and V_w is the					
$Q_{\rm m} = 0.72 V_{w}^{0.53}$	[35]	volume of water.					
$Q_{\rm m} = 0.045 V_{w}^{0.66}$	[36]						
$Q_{\rm m} = 0.00077 V_w^{1.017}$	[37]						

The peak discharge at a cross section was calculated using an empirical formula [38]:

$$Q_{xm} = \frac{V_w Q_m}{V_w + \frac{Q_m L}{v_w K}} \tag{3}$$

where V_w is the volume of water (m³); Q_m is the peak discharge at the dam site (m³/s); Q_{xm} is the peak discharge at a cross section (m³/s); L is the distance from the dam (m), and v_w K is an empirical coefficient equal to 3.13 for rivers on plains, 7.15 for mountain rivers, and 4.76 for rivers flowing through terrain with intermediate relief. The calculated results using empirical formulas listed in Table 3 are shown in Figure 6.

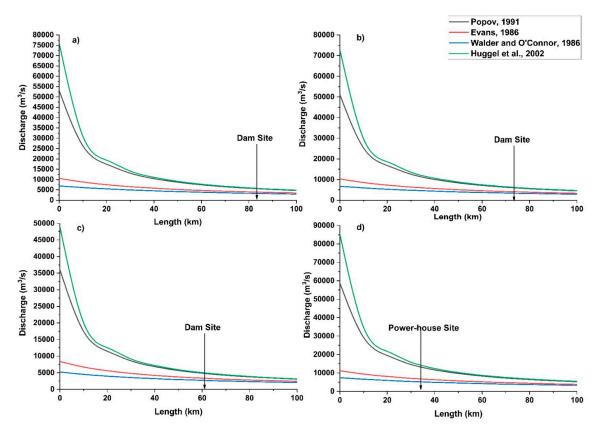


Figure 6. Discharge profiles of lake nos. 20, 35, 36, and 39 in (a)–(d), respectively, from the outburst site to the downstream.

GLOFs caused by the collapse and erosion of moraine dams seldom result in the drainage of 100% of the total lake volume. GLOFs caused by avalanche push (seiche) waves also do not normally mobilize 100% of the lake volume. However, it is difficult to predict how much volume will be mobilized; therefore, it is necessary to identify and discuss different scenarios, which include 100%, 75%, and 50% drainage of the lake volume to minimize the maximum and minimum potential risks (Figure 7, Table 4).

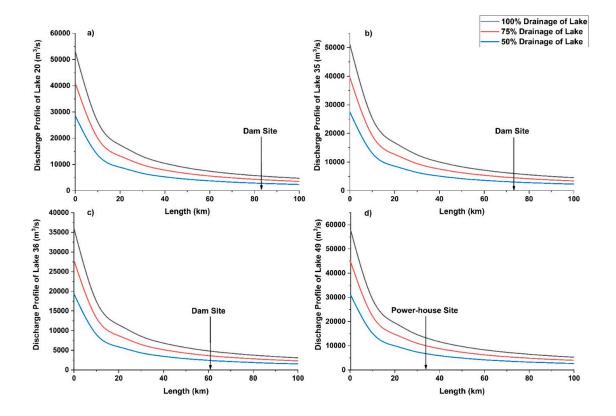


Figure 7. Discharge profiles of lake nos. 20, 35, 36, and 39 with 100%, 75%, and 50% drainage in (a)–(d), respectively, from the outburst site to the downstream region.

Glacial Lake	Discharge at Site if Drainage =			Dam Type	Potential for Lake Impacts	Dam Geometry	Freeboard	Outburst Probability
No.	100%	75%	50%					
20	4632	3542	2422	Landslide dam	Debris flow	Stable	Medium freeboard	Medium
35	4929	3772	2583	No dam	Debris flow	-	Low freeboard	Medium
36	3951	3025	2073	Moraine dam	Ice avalanches/rock fall	Unstable	Low freeboard	High
49	9866*	7586*	5238*	Moraine dam	Ice avalanches/rock fall	Unstable	Low freeboard	High

Table 4. Maximum discharge and physical features of the critical lakes.

As shown in Appendix A, Figure A4, among the identified potential glacial lakes, lake no. 35 seems the most stable considering the change in the area over the past 28 years, while lake no. 49 seems to be the most unstable in this regard. Physical features of the critical dams are recorded in Table 4 above and are visually interpreted in Appendix A, Figure A3.

Furthermore, previous studies have shown that moraine-dammed lakes have higher probabilities of outburst than those of landslide-dammed or erosion lakes [24]. Lake no. 39 (moraine lake, glacier at the end) and no. 49 (moraine lake, glacier tongue deep into the lake) are identified as being moraine dammed and possessing unstable geometry due to the rapid change in their glacial

^{*} Discharge of lake no. 49 is at the powerhouse site, as it is located downstream of the dam site.

lake area over recent decades. Along with the potential impacts of ice avalanches and rock fall because they are closer to the mother glacier, this makes their outburst probabilities higher compared with the other two lakes. Additionally, the volume of lake no. 49 is the largest among the four critical lakes, and the higher the volume of a moraine-dammed lake, the higher the possibility of outburst [24]. By contrast, lake no. 20 is a landslide-blocking lake, and glacial lake no. 35 is a glacial erosion lake, both of which are not easy to break; thus, it can be concluded that lake nos. 36 and 49 should be considered as having high outburst probabilities (Table 4).

4. Discussion

4.1. Climatic Correlation with GLOFs

Data regarding the monthly annual average rainfall for the period of 1960–2017 are represented in Figure 8b, which clearly suggests that the monsoon season starts in May and ends in October, reaching the peak monthly average value of over 100 mm in August. Moreover, the rest of the year is dry. There is a rise in monthly annual average temperature from April to July, reaching a peak of about 12 °C in June, and then a steady decrease until November. Following a steep fall from October until January, the lowest average value of –7.5 °C is in January.

The seasonal distribution of the precipitation in the project area within Nepal is dominated by a rainy season from May through September, when the monsoons bring 90% of the annual precipitation, and a dry season from November through April. Due to the high elevation and low temperatures in most parts of the Arun River Basin, a certain portion of the precipitation is in the form of snow. No snowfall records are available for the Nepalese portion. Based on records available for the Tibetan region, annual snowfall generally increases with the increment in elevation. At an elevation of 4000 m, about 15%–22% of the annual precipitation falls as snow, and 30%–40% at 4500 m elevation. Snowfall is generally recorded from November through March.

There seems to be an increasing trend in the monsoon season (i.e., from May until October), with the peak seasonal annual rainfall of about 80 mm in the years 1970–1975. However, the opposite can be seen in the dry season (i.e., from November to April), with a minimum of no rainfall and a maximum of just below 4 mm.

In Figure 8c, an overall temperature increase is observed with some minor variations over the past 47 years, with the lowest temperature of -9 °C in the seasonal annual average from November to April, and a maximum in the range of 8–10 °C. The trend line also suggests an increase in the future. In general, Dingri County exhibits a cold climate, though it is expected to take a similar course as the regional temperature rises.

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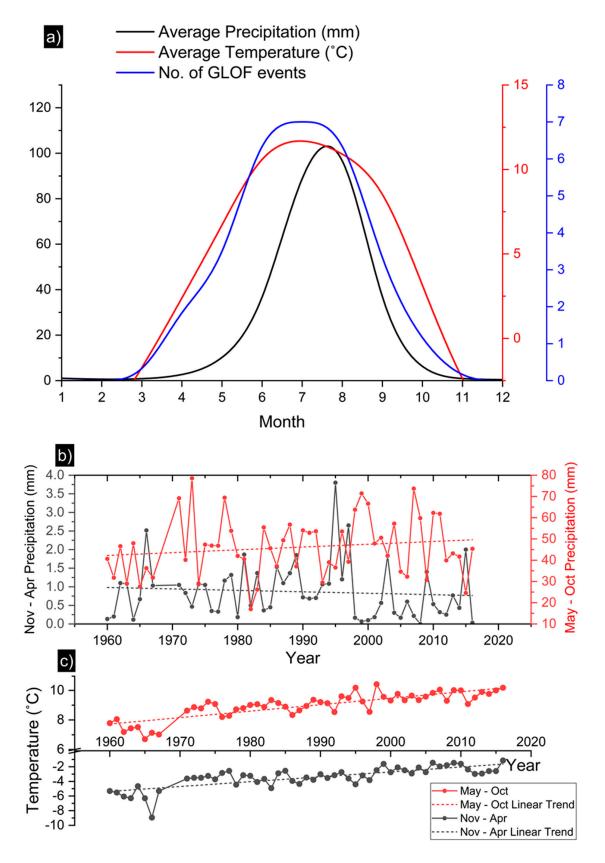


Figure 8. (a) Correlation among precipitation, temperature, and GLOF events during 1935–2017. (b) Seasonal annual average variation in precipitation during 1960–2017. (c) Seasonal annual average variation in temperature during 1960–2017.

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As shown in Figure 8a, there seems to be an apparent relationship between the increases in temperature and precipitation and the resulting increase in the frequency of glacial lake outbursts. Statistics based on the 27 well-recorded GLOF events show that all of them occurred between May and October (Figure 8a), with the majority (18) occurring between June and August. Summarized as an annual cycle, a GLOF can start as early as the beginning of May, for example, the Jialongco event on 23 May 2002, while the latest GLOF may happen in early October, such as the Luggye Tsho event on 7 October 1994. These statistics imply that GLOFs rarely occur during the frozen period from November to March. Rapid warming and precipitation during the ablation season cause ice avalanches and generate massive glacier melt water [5, 12], both of which are prone to triggering a GLOF as a result of dam failure. It can be said that in future years, the scale of GLOF events may increase as the annual temperature and precipitation also increase; however, the influence of climate change on the frequency of GLOFs is very complex. A recent study [39] showed that the average annual frequency of GLOFs had no credible posterior trend, despite reported increases in glacial lake areas in most of the Kush–Karakoram–Himalaya–Nyainqentanglha area. Therefore, the relationship between climatic features and the frequency of GLOF events is still unclear.

4.2. Justification for the Assumed Depth of the Lakes

The distances between glacial lakes and the dam (powerhouse) site were obtained from DEMs. It is difficult to obtain the average depth of glacial lakes. A previous study showed that the maximum depth of glacial lakes in the Himalayan region was 55 m. In this study, it was assumed that the depth of the 49 lakes is 55 m [40]. Figure 9 shows the relation between the average depth of lakes and the moraine lake area in the Himalayas. The average depth of lakes and the moraine lake area were obtained through field investigation. However, it is appropriate for us to assume that the average depth is 55 m for lakes with areas larger than 0.80 km². We conducted numerical simulations for four lakes (nos. 20, 35, 36, and 49). The areas of the four lakes each exceed 0.80 km².

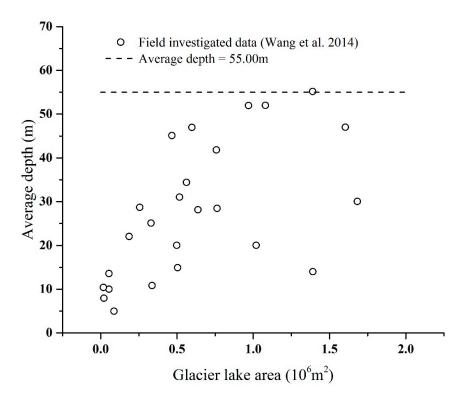


Figure 9. Relationship between moraine lake area and average depth.

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4.3. Analysis, Limitations, and Recommendations in Relation to the Model

The model is based on the influenced lengths of 11 historical GLOF events, and the reason for choosing the upper limit line (Equation (2)) is that it covers more data than the best-fit line. The findings of our study identify lake nos. 20, 35, 36, and 49 as the most critical due to their location, volume, physical features, and distance from both the Upper Arun dam and powerhouse. In other words, the values of Le/Ld or Le/Lp are large enough to pose serious risks as compared to all the other glacial lakes. Although lake no. 11 is in close proximity to lake no. 49, its lesser volume and more stable dam geometry (and thus, lower potential discharge) make it nonthreatening in the case of an outburst. This model is not only limited to the Himalayas but can also be applied to other mountainous regions. The results of this study investigating and analyzing the influence of GLOFs on the Upper Arun Hydroelectric Project and IkhuwaKhola Hydropower Project were peer-reviewed and accepted by a joint venture (CSPDR-SINOTECH JV) led by the Changjiang Institute of Survey, Planning, Design, and Research (CSPDR) with the NEA for the project entitled "Detailed Engineering Design and Preparation of Bidding Documents for Construction of Upper Arun Hydroelectric Project and IkhuwaKhola Hydropower Project".

The number of historical GLOF events used to devise the model is limited, while a larger dataset could strengthen the numerical relationship between the volume and the affected length of a GLOF. The reason for the restricted set of data used to derivate the model is that the influenced lengths of most past GLOFs were not recorded. Moreover, a quasi-process such as an earthquake can trigger a GLOF hazard, regardless of the volume and distance of the glacial lake from the site of the assessed project. Another factor that needs to be addressed is the fact that a chain outburst of glacial lakes can happen, but prediction of such an event requires further study.

The field visit by our research team in April 2018 (Appendix A, Figure A5, A6, A7 and A8) concluded that the topography and characteristics of the river channel are fairly consistent over the studied site [41]. Thus, these two factors were eliminated in the proposed model to minimize the uncertainties in the results. Although it would be very challenging, in future studies, characteristics of the river channel and an integrated model may be proposed incorporating more factors. It may also be possible to explore the possible destruction-triggering mechanism for each glacial lake in addition to the four critical lakes analyzed in Section 3.3. However, it would be very difficult to discuss the failure of a glacial lake dam under different triggering factors. It is important to address the factors that affect GLOF fluctuation, such as the outburst dynamic process and the scale. Nevertheless, to accomplish this task, the most basic step is to collect samples—which is not easy, as the terrain and environment at the glacial lakes' sites make it impossible to physically travel there—and to test the particle size and mechanical parameters of the samples.

5. Conclusions

Extensive remote sensing identified 49 lakes with areas larger than 0.1 km², namely, lake nos. 1–10 and 12–48, which are located upstream of the dam site, and lake nos. 11 and 49, which are located downstream of the dam site. The correlation between climatic features and the occurrence of GLOF events needs further investigation to conclude if there is a significant relationship or not, but it can be said that the scale of GLOF events may increase over the coming years as the trends of temperature and precipitation in the region are predicted to increase in the future.

In this study, a new but effective method was used to select the affected disaster lengths to determine the potentially critical glacial lakes. First, the affected disaster lengths of historical GLOFs that occurred in the Himalayan region were collected. Second, an empirical equation was determined based on the collected data. Third, the determined equation was used to predict the affected lengths of those 49 lakes. The lakes were considered as potentially critical glacial lakes when the predicted affected length was larger than the distance between the lake and the dam (powerhouse) site.

The reason for selecting four potentially critical glacial lakes (nos. 20, 35, 36, and 49) to conduct further investigation is that the values of L_c/L_d or L_c/L_p for these four lakes are larger compared with those of the other lakes. In other words, these four glacial lakes are potentially more critical. Further analysis to characterize the probability of an outburst was done based on the physical features and

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triggering factors of the lakes. In the case of an outburst event at lake no. 49, which is located downstream of the dam, flow-diverging engineering could be considered for preventing powerhouse destruction.

Author Contributions: Conceptualization, R.M.A.W. and N.C.; methodology, R.M.A.W., T.W., S.R.A., and N.C.; software, R.M.A.W.; validation, S.A. and S.R.A.; formal analysis, R.M.A.W., T.W., and N.C.; investigation, R.M.A.W., T.W., and N.C.; resources, N.C.; data curation, R.M.A.W., S.A., and M.R.; writing—original draft preparation, R.M.A.W., T.W., and N.C.; writing—review and editing, R.M.A.W., S.A., and S.R.A.; visualization, R.M.A.W., N.C., and T.W.; supervision, N.C.; project administration, N.C.; funding acquisition, N.C.

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Conflicts of Interest: The authors declare no conflict of interest.

Appendix A

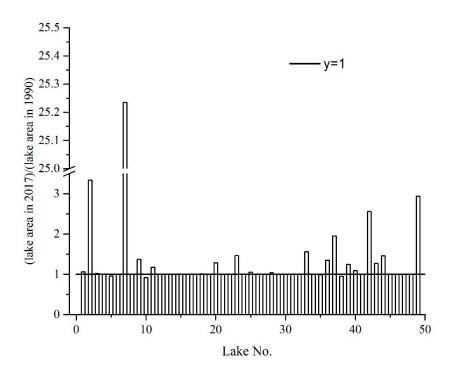


Figure A1. The ratio of lake area in 2017 to that in 1990 for each lake.

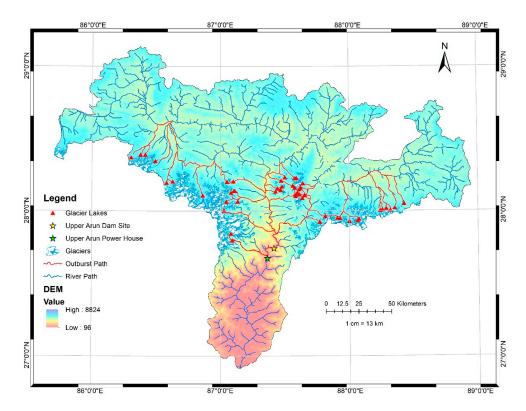


Figure A2. Simulated outburst paths.

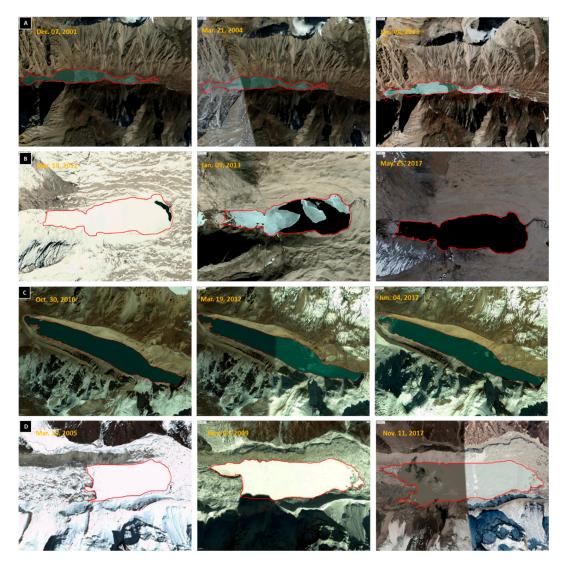


Figure A3. Glacial lake change in area profile during the period 2005–2017, where **(a)**, **(b)**, **(c)**, and **(d)** represent lake nos. 20, 35, 36, and 49, respectively (Source: Google Earth).

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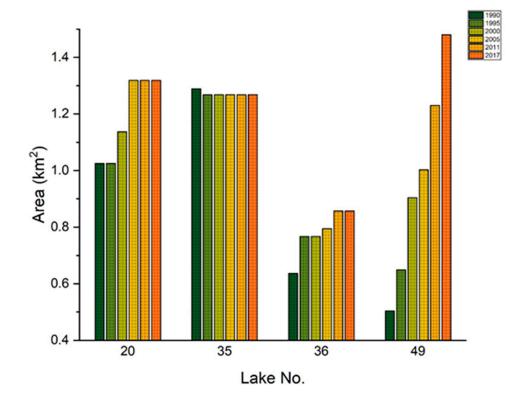


Figure A4. Critical change in area profile of glacial lakes during the period 1990–2018.





From Kathmandu to Tumlingtar by Flight From Tumlingtar to Barun khola by pick-up truck

Figure A5. Field investigation route from Kathmandu to Barun Khola.

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BARUN KHOLA TO LOWER DAMSITE





From Barun khola to lower dam site on foot

Figure A6. Field investigation route from Barun Khola to lower dam site.



FIELD INVESTIGATION IN ARUN, NEPAL 04.2018

Interview with local people especially elderly locals about historical GLOFs and soci-economic status

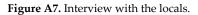






Name: Lak Bahadur Village: Barun Shaban Age: 55+





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FIELD INVESTIGATION IN ARUN, NEPAL 04.2018

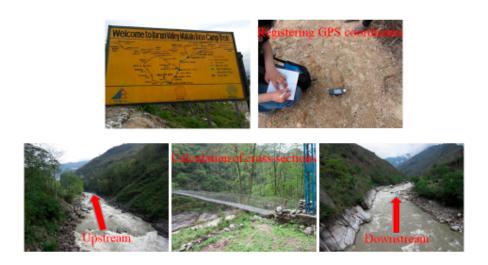


Figure A8. Field activities at the lower dam site.

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