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Assessing Impacts of Climate Change and Sea-Level Rise on Seawater Intrusion in a Coastal Aquifer

Jong Ahn Chun ¹, Changmook Lim ¹, Daeha Kim ^{1,*} and Jin Sung Kim ²

¹ APEC Climate Center, 12 Centum 7-ro, Haeundae-gu, Busan 48058, Korea; jachun@apcc21.org (J.A.C.); cmlim@apcc21.org (C.L.)

² Jeju Regional Headquarter, Seonsa-ro, Jeju-si 63318, Korea; gwater@ekr.or.kr

* Correspondence: d.kim@apcc21.org; Tel.: +82-51-745-3983

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Abstract: The objectives of this study were to assess the climate change impacts on sea-level rise (SLR) and freshwater recharge rates and to investigate these SLR and freshwater recharge rates on seawater intrusion in coastal groundwater systems through the Saturated-Unsaturated Transport (SUTRA) model. The Gunsan tide gauge station data were used to project SLR based on polynomial regressions. Freshwater recharge rates were assumed as 10% of the projected annual precipitation under climate change. The Byeonsan2 groundwater monitoring well for seawater intrusion was selected for the study. A total of 15 scenarios, including the baseline period (2005–2015), were made based on SLR projections and estimated freshwater recharge rates. The changes in salinity relative to the baseline at the monitoring well for each scenario were investigated through the SUTRA model. From the scenario of 0.57 m SLR with a freshwater recharge rate of 0.0058 kg s^{-1} , the largest salinity increase (40.3%) was simulated. We concluded that this study may provide a better understanding of the climate change impacts on seawater intrusion by considering both SLR and freshwater recharge rates.

Keywords: sea-level rise; seawater intrusion; freshwater recharge rate; SUTRA

1. Introduction

Global mean sea-level under Representative Concentration Pathway (RCP) 8.5 is projected to rise by 0.45–0.82 m from 1986–2005 to 2081–2100, while 0.32–0.70 m of the global mean sea level rise is projected by 2100 under RCP 4.5 [1]. For the Korean peninsula, sea-level rise (SLR) of 0.75 m under RCP 4.5 is estimated at the coast line in the East Sea by 2100, followed by the South Sea (0.58 m) and the West Sea 0.57 m [2]. Those under RCP 8.5 are 1.08 m for the East Sea, 0.72 m for the West Sea, and 0.70 m for the South Sea.

Several approaches have been used to assess SLR or sea-level acceleration (SLA) [3–6]. Breaker and Ruzmaikin [4] employed the ensemble empirical model decomposition (EEMD) method to estimate acceleration from 1855 to 2010 with the monthly averaged sea level data for San Francisco (CA, USA). They reported that SLA was $0.011 \pm 0.003 \text{ mm yr}^{-2}$ over the 157-year record of sea level. They also used polynomial regression for the SLA estimation and found that 0.013 mm yr^{-2} , $-0.0006 \text{ mm yr}^{-2}$, and $-0.023 \text{ mm yr}^{-2}$ for the periods 1855–2011, 1900–2011, and 1925–2011, respectively. Eazer and Corlett [5] showed that SLA for Chesapeake Bay (USA) ranged from 0.05 to 0.10 mm yr^{-2} using Empirical Mode Decomposition and Hilbert-Huang Transformation [6]. Kim and Cho [7] reported that the average SLR around the Korean peninsula over the study period was 2.57 mm yr^{-1} and the average SLA $0.075 \pm 0.026 \text{ mm yr}^{-2}$ based on EEMD. They also found that $2.603 \pm 0.0266 \text{ mm yr}^{-1}$ and $0.114 \pm 0.040 \text{ mm yr}^{-2}$ for SLR and SLA, respectively, using polynomial regressions. Yoon [8] found that SLR around the Korean peninsula was higher the global mean SLR using a regression approach from tide gauge data.

Seawater intrusion has been frequently reported around the world: USA [9–12], Europe [13], Australia [14], China [15], India [16–18], Egypt [19], Bangladesh [20], and South Korea [21,22]. There have been many studies on the assessment of the impacts of SLR on seawater intrusion using various conceptual and mathematical models. Werner and Simmons [23] used a simple conceptual approach to assess seawater intrusion in coastal unconfined aquifers by SLR. Pool and Carrera [24] proposed a double pumping barrier system with two extraction wells combined with an inland well and a seaward well. The former was for pumping freshwater and the latter for seawater. They investigated the proposed system by a three-dimensional variable density flow model and concluded that the proposed system in their study had higher efficiency than a simple negative barrier. Numerical models based on the sharp interface approach have also been implemented [25,26]. Rasmussen et al. [27] attempted to assess impacts of climate change, SLR, and drainage canals on seawater intrusion to coastal aquifers located in an island in Denmark using the modeling package MODFLOW/MT3D/SEAWAT. They found that changes in recharge largely influenced the seawater intrusion to the aquifer. Datta et al. [17] assessed pumping strategies for locally controlling seawater intrusion in a coastal aquifer in India using the FEMWATER model.

The Saturated-Unsaturated Transport (SUTRA) model [28], a variable density flow and solute transport model, is widely used for the investigation of seawater intrusion and is well documented [14]. Narayan et al. [29] employed the SUTRA model to investigate the impacts of various pumping and recharge conditions on seawater intrusion in the Burdekin Delta aquifer (Australia). They observed that pumping rates and recharge much higher influenced seawater intrusion than aquifer properties. Hussain et al. [30] assessed the impacts of pumping and recharging from a single pond system on seawater intrusion in the Wadi Ham aquifer in UAE using the SUTRA model. They showed that the artificial recharge considerably reduced salinity in the aquifer. Ghassemi et al. [31] suggested that the SUTRA model may provide better simulation results for two-dimensional problems than for three-dimensional problems. They tested the SUTRA model for seawater intrusion investigation on Nauru Island in the Pacific Ocean.

Few studies have been conducted on the impacts of changes in SLR projection based on tide gauge measurements and recharge rates estimated from projected precipitation under climate change on seawater intrusion in coastal aquifers. The objective of this study was to investigate the impacts of climate change on coastal groundwater systems through the SUTRA model. We investigated SLR from tide gauge measurements and estimated freshwater recharge rates based on RCP 4.5 and RCP 8.5.

2. Materials and Methods

2.1. Site Description and Data Collection

To monitor groundwater level, temperature, and electric conductivity (EC) at coastal areas where seawater intrusion was reported or a seawater intrusion risk was high, the Seawater Intrusion Monitoring Network (SIMN) was established and has been operated by the Korea Rural Community (KRC) since 1998 [32,33]. The SIMN consists of 154 monitoring wells and Byeonsan2, close to the Gunsan tide gauge station, selected to investigate seawater intrusion for this study (Figure 1). The groundwater monitoring well was installed in 2004 and located at 670 m from the coastal line. An EC sensor in the well was installed at 44 m below sea level. The observed data from 2005 to 2015 were used for this study. The average temperature during this period was 15.0 ± 0.3 °C and the average salinity 0.0050 ± 0.00054 kg-dissolved solids (kg-seawater)^{−1}. A Piper trilinear diagram [34] was applied for hydrogeochemical facies of the Byeonsan2 monitoring site and the results from the diagram showed that the dominant hydrogeochemical facies were classified with Na-Cl type (data not shown).

Hourly sea level measurements at the Gunsan tide gauge station (Figure 1) were collected from the Korea Hydrographic and Oceanographic Administration (KHOA, <http://www.khoa.go.kr>). The Gunsan station was installed in 1980. These sea level data from 1981 to 2015 at the station were used to project SLR under climate change for this study. For this study, freshwater recharge rates

were estimated from annual precipitation. The observed precipitation data were collected from the nearest Automated Synoptic Observing System (ASOS) station from the Byeonsan2 monitoring well, which is the Buan station operated by the Korea Meteorological Administration (KMA). Annual mean precipitation and temperature at the station are approximately 1250 mm and 12.6 °C, respectively. The predicted precipitation data under RCP 4.5 and RCP 8.5 were used to estimate the freshwater recharge rates under climate change. These climate change scenarios at 1-km resolution were collected from the Korea Global Atmosphere Watch Center (KGAWC, <http://www.climate.go.kr>). Outputs of a global climate model (HadGEM2-AO) were dynamically and statistically downscaled using a regional climate model (HadGEM3-RA) and Modified Korean-Parameter-elevation Regressions and Independent Slopes Model (MK-PRISM), respectively. More detailed information on these downscaled methods can be found in Kim et al. [35].

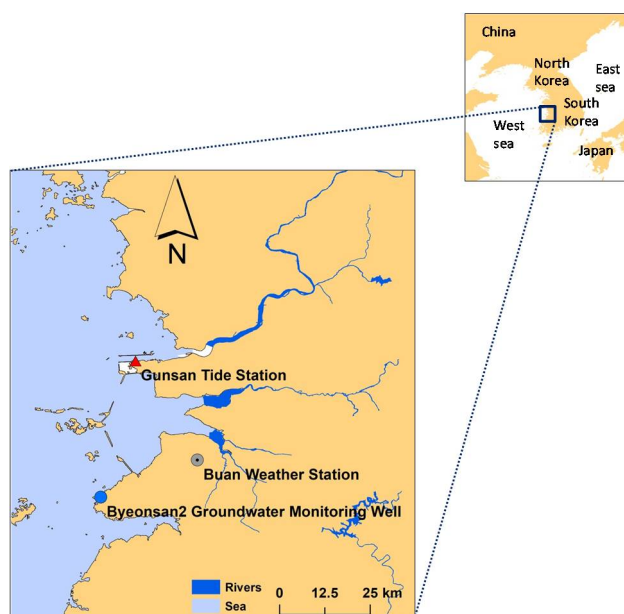


Figure 1. Location map of the Gunsan tide gauge station (35.98° N 126.56° E), the Byeonsan2 groundwater monitoring well for seawater intrusion (35.64° N 126.48° E), and the Buan weather station (35.73° N 126.72° E).

2.2. Sea-Level Rise Projection

Polynomial regressions were used to project SLR at the Gunsan tide gauge station in the 2050s (2051–2060) and 2090s (2091–2100) from the observed sea level data. Linear and quadratic regressions were used to estimate a trend and acceleration of SLR, respectively. Boon et al. [3] used this method to project the trend and acceleration of SLR of Chesapeake Bay (USA). Missing values were frequently found in the tide gauge measurements and adequately filled before further analyses. These missing values were interpolated using the Tidal Analysis Software Kit-2000 (TASK-2000) package [36], which implements tidal harmonic analysis. This package is widely used for tidal analyses and more detailed information on the package can be found in Murray [37]. For this study, the observed hourly sea level data were aggregated to daily to monthly sea level (Figure 2a,b). The seasonal cycle (i.e., repetition over time) of sea level (Figure 2c) was defined as monthly mean values during the monitored period (1981–2015). A clear seasonal component was seen as shown in Figure 2c. While the seasonal component of sea level in August was highest, the lowest seasonal component of sea level was in February. This estimated seasonal cycle was removed from the monthly sea level data (Figure 2d). Finally, polynomial regressions were performed using the monthly sea level data in which

the seasonal components were removed. These projected SLR was used for boundary conditions of the SUTRA model.

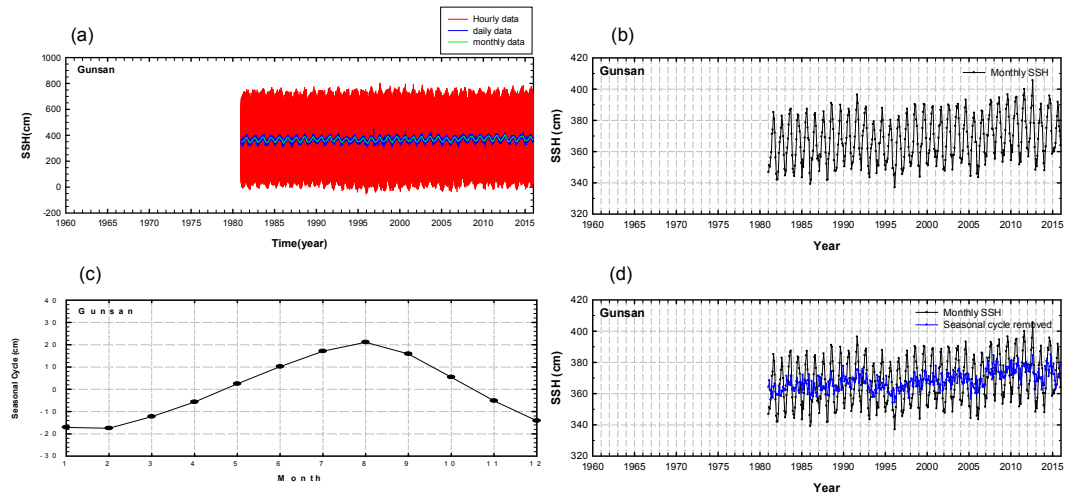


Figure 2. The observed sea level data at the Gunsan tide gauge data: (a) hourly, daily, and monthly sea level data; (b) monthly sea level data; (c) seasonal cycle of sea level; and (d) monthly sea level data with no seasonal components. SSH is the sea surface height.

2.3. Seawater Intrusion Modeling

Seawater intrusion can be defined as a variable density saturated flow and non-reactive solute transport of total dissolved solids (TDS) or chloride. Therefore, the governing equations for seawater intrusion can be expressed as the following Equations (1)–(3):

$$\rho S_{op} \frac{\partial \rho}{\partial t} + \epsilon \frac{\partial \rho}{\partial U} \frac{\partial U}{\partial t} - \nabla \cdot \left[\frac{k\rho}{\mu} \cdot (\nabla p - \rho g) \right] = Q_p \quad (1)$$

where ρ is the fluid density (ML^{-3}), S_{op} is the specific pressure storativity ($\text{ML}^{-1}\text{T}^{-2}$)⁻¹, t is the time (T), ϵ is the fractional porosity [1], U is the solute mass fraction (MM^{-1}), k is the permeability tensor (L^2), μ is the fluid viscosity ($\text{ML}^{-1}\text{T}^{-1}$), p is the fluid pressure ($\text{ML}^{-1}\text{T}^{-2}$), g is the gravity vector (MT^{-2}), and Q_p is the fluid mass source ($\text{ML}^{-3}\text{T}^{-1}$):

$$v = \frac{k\rho}{\epsilon\mu} \cdot (\nabla p - \rho g), \quad (2)$$

where v is the fluid velocity (MT^{-1}):

$$\epsilon\rho \frac{\partial U}{\partial t} + \epsilon\rho v \cdot \nabla C - \nabla \cdot [\epsilon\rho(D_m I + D) \cdot \nabla U] = Q_p(C^* - C). \quad (3)$$

where D_m is the coefficient of molecular diffusion in porous medium fluid (L^2T^{-1}), I is the identity tensor [1], D is the dispersion tensor (L^2T^{-1}), C is the concentration of solute (MM^{-1}), and C^* is the concentration of a fluid source (MM^{-1}).

The SUTRA model was used to investigate seawater intrusion in the Byeonsan2 groundwater monitoring well. A two- or three-dimensional finite-element (FEM) and finite-difference method (FDM) is employed to simulate groundwater flow and solute transport [38]. The SUTRA model can be used to investigate seawater intrusion in aquifers at near-wells through two-dimensional cross-sectional modeling. For this study, the ModelMuse software package [39] was used to generate irregular quadrilateral finite element meshes and to construct input files for the SUTRA model. The ModelMuse software package, a graphical user interface, can create input files for various the U.S. Geological Survey

(USGS) models including MODFLOW-2005 [40], MODFLOW-CFP [41], PHAST [42], and SUTRA [38]. We originally assumed that the paths of flow and solute transport in the study region coincided with streamlines. A streamline from 300 m distant to the coastline to the Byeonsan2 monitoring well was stretched and two-dimensional irregular meshes were created along the stretched streamline. Figure 3 illustrates the simulation domain describing initial and boundary conditions. A total of 4637 nodes and 4539 elements in the 2-D vertical cross-sectional domain were generated for this study (Figure 3).

A homogeneous and anisotropic porous medium was assumed for the simulation domain. Hydraulic conductivity and transmissivity of this site were $3.4 \times 10^{-4} \text{ m day}^{-1}$ and $0.67 \text{ m}^2 \text{ day}^{-1}$, respectively. Longitudinal dispersivity and transverse dispersivity were estimated through the SUTRA model by comparing the simulated salinity against the observed salinity converted from the observed EC. An observation node was inserted at the location of the EC sensor (i.e., 44 m below sea level). In this study, the observed salinity from 2005 to 2010 were selected for the calibration of the transport parameters (i.e., longitudinal dispersivity and transverse dispersivity), while those in 2011 to 2015 were selected for the validation of the SUTRA model. The performance of the SUTRA model was assessed with Mean Absolute Percentage Error (MAPE, Equation (4)). The simulation periods selected in this study were the baseline period (2005–2015), 2050s (2051–2060), and 2090s (2091–2100).

$$\text{MAPE} = \frac{100}{N} \sum_{i=1}^n \left| \frac{O_i - P_i}{O_i} \right|, \quad (4)$$

where O_i is the observed value and P_i is the simulated value.

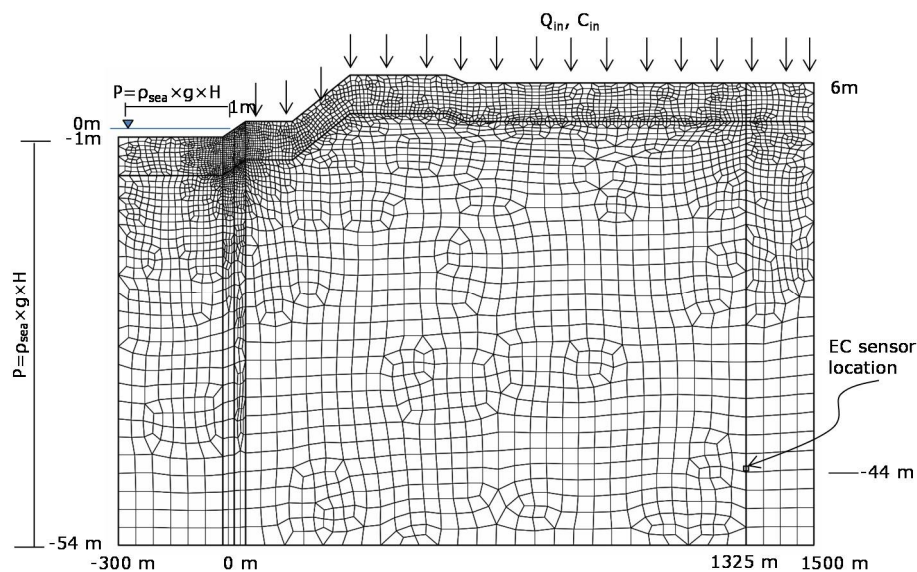


Figure 3. Initial and boundary conditions and finite-element meshes for the simulation domain. $\rho_{\text{sea}} = 1024.99 \text{ kg m}^{-3}$; H = depth (m); $g = 9.81 \text{ (m s}^{-2}\text{)}$; P = hydrostatic seawater pressure; Q_{in} = freshwater recharge rate (kg m^{-2}); $C_{\text{in}} = 0.0 \text{ (kg kg}^{-1}\text{)}$; $C_{\text{sea}} = 0.0357 \text{ (kg kg}^{-1}\text{)}$. A total of 4637 nodes and 4539 elements were generated for the simulation domain.

3. Results and Discussion

3.1. Sea-Level Rise Projection

Figure 4 displays the results of polynomial regressions. An increase of approximately 0.12 m in the sea level at the Gunsan tide gauge station was observed from 1981 to 2015. Over this period, the sea level at the station increased with a constant rate of $3.45 \pm 0.49 \text{ mm yr}^{-1}$ (p -value < 0.0001), based on the linear regression, which is assumed as a constant rate of SLR. An acceleration of 0.08 mm yr^{-2} (p -value < 0.001) was found over same period from the quadratic regression. This linear trend is in

good agreement with that by Yoon [8]. Yoon [8] reported that a constant rate of 3.4 mm yr^{-1} and 3.7 mm yr^{-1} were estimated from the Gunsan tide gauge station data for the periods 1981–2014 and 1985–2014, respectively. The constant rate ($3.45 \pm 0.49 \text{ mm yr}^{-1}$) in this study is slightly lower than that ($3.53 \pm 0.29 \text{ mm yr}^{-1}$) at the Mokpo tide gauge station by [6] and very close to that ($3.4 \pm 0.4 \text{ mm yr}^{-1}$) for the global mean sea level by [43], while the constant rate is higher than the average SLR (2.57 mm yr^{-1}) from their study. The acceleration in this study is close to the average acceleration of SLR (0.075 yr^{-2}) by [6]. They estimated the trend and acceleration of SLR at the five tide gauge stations around the Korean peninsula using the ensemble empirical mode decomposition (EEMD) approach.

The SLR by the year 2050 was projected by using these polynomial regression results. These projections were used for the initial and boundary conditions of the simulation domain to investigate the impacts of SLR on seawater intrusion in the Byeonsan2 groundwater monitoring well. By the year 2050, an increase in sea level of approximately 0.12 m was projected based on the linear regression, while sea level was projected to increase by approximately 0.32 m relative to the sea level in the year 2015 based on the quadratic regression. However, it should be noted that the acceleration was estimated using only 35 years of monitored tide gauge measurements, which might be short for the SLR projection to the year 2050.

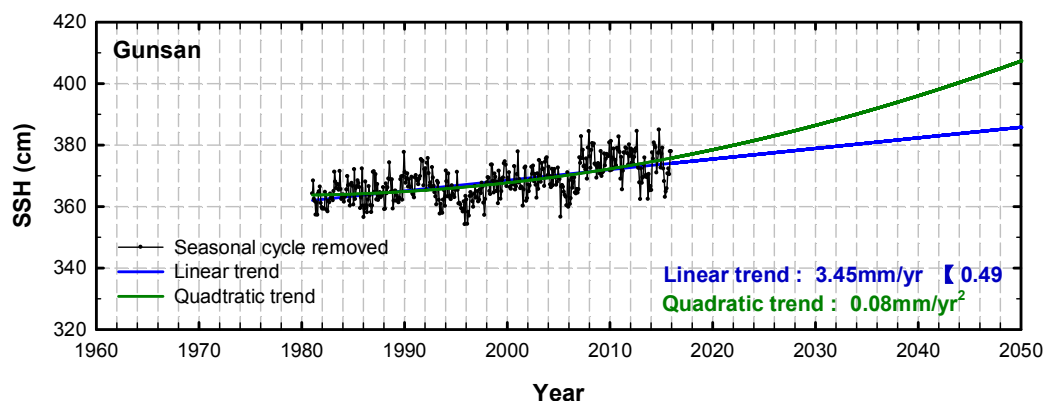


Figure 4. Sea level (black curve), fitted straight line (blue line, linear trend), and fitted quadratic line (green curve, quadratic trend) at the Gusan tide gauge station.

3.2. Seawater Intrusion Modeling

It is generally known that climate change may have impacts on SLR and precipitation which may be associated with freshwater recharge rates and that seawater intrusion is influenced by not only sea level, but also freshwater recharge rates. While a higher freshwater recharge rate could lower salinity in groundwater, a higher sea level may increase seawater intrusion. For this study, the freshwater recharge rates of the simulation domain were assumed as 10% of the annual mean precipitation for the baseline, the 2050s, and the 2090s. Chung et al. [44] reported that the freshwater recharge rate for the Korean peninsula was approximately 10% of annual precipitation. For the baseline period, 10% of annual mean precipitation from 2005 to 2015 was assumed as the freshwater recharge rate and it was $0.00603 \text{ kg s}^{-1}$. For the 2050s and 2090s, annual mean precipitations were first calculated with RCP 4.5 and 8.5 climate change scenarios from the KGAWC and these annual mean precipitations were then used for freshwater recharge rates, respectively. There were four freshwater recharge rates except for the baseline period. However, it should be noted that this simple approximation of the freshwater recharge rate from annual mean precipitation may lead to inadequate inference of seawater intrusion investigation. For example, for the water-balance method, evapotranspiration, runoff, and precipitation should be considered to estimate groundwater recharge rates [45]. A further study is suggested for the accurate estimation of freshwater recharge rates. Four SLR scenarios, including the projections from

the polynomial regressions and the projections for the West Sea under the two emission scenarios [2] were assumed for this study: 0.12 m by the year 2050 from the linear regression, 0.32 m by the year 2050 from the quadratic regression, 0.57 m under RCP 4.5 [2], and 0.72 m under RCP 8.5 [2]. A total of 15 scenarios were made considering these four freshwater recharge rates and SLR scenarios and the baseline. These scenarios in this study are summarized in Table 1. The lowest freshwater recharge rate (0.0549 kg s^{-1}) was found in the 2090s under RCP 4.5 and the highest freshwater recharge rate (0.0694 kg s^{-1}) was found in the 2090s under RCP 8.5.

Table 1. Fifteen scenarios, including the baseline with SLR and freshwater recharge rates.

| Cases | SLR (m) | Freshwater Recharge Rate (kg s^{-1}) | Descriptions |
|-----------------------|---------|-------------------------------------------------|--------------------------------------|
| Baseline | 0.0 | 0.00603 | 2005–2015 |
| RR2050RCP45 | 0.0 | 0.00627 | 2050s, RCP4.5, Precipitation (1) |
| RR2050RCP85 | 0.0 | 0.00580 | 2050s, RCP8.5, Precipitation (2) |
| RR2090RCP45 | 0.0 | 0.00549 | 2090s, RCP4.5, Precipitation (3) |
| RR2090RCP85 | 0.0 | 0.00694 | 2090s, RCP8.5, Precipitation (4) |
| 2050L | 0.12 | 0.00603 | Linear trend by 2050 (5) |
| 2050C | 0.32 | 0.00603 | Quadratic trend by 2050 (6) |
| 2090RCP45 | 0.57 | 0.00603 | SLR of the West sea under RCP4.5 (7) |
| 2090RCP85 | 0.72 | 0.00603 | SLR of the West sea under RCP8.5 (8) |
| 2050L_RR2050RCP45 | 0.12 | 0.00627 | (1) and (5) |
| 2050L_RR2050RCP85 | 0.12 | 0.00580 | (2) and (5) |
| 2050C_RR2050RCP45 | 0.32 | 0.00627 | (1) and (6) |
| 2050C_RR2050RCP85 | 0.32 | 0.00580 | (2) and (7) |
| 2090RCP45_RR2090RCP45 | 0.57 | 0.00549 | (3) and (7) |
| 2090RCP85_RR2090RCP85 | 0.72 | 0.00694 | (4) and (8) |

For the baseline simulation, sea level and Q_{in} were set to be 0.0 m and $0.00603 \text{ kg s}^{-1}$, respectively. The longitudinal dispersivity and transverse dispersivity were estimated by comparing the observed and simulated salinities from the observation node (located at 44 m below sea level), based on the assumption of anisotropic and homogeneous domains for the transport parameters. The estimates of the longitudinal dispersivity and transverse dispersivity were 10.0 m and 0.1 m, respectively. The value of MAPE of the observed and simulated salinities for the calibration period was approximately 1.6%, while the MAPE value for the validation period was about 2.4%. The ratio of longitudinal dispersivity to transverse dispersivity was 100 for this site. This ratio is in substantial agreement with that reported by Anderson [46]. Anderson [46] found that the ratio of longitudinal dispersivity to transverse dispersivity ranged from 10 to 100. Gelhar et al. [47] reported a “scale effect” that transport parameters are generally proportional to the sizes of the study regions. Therefore, a further study on a tracer test is suggested to accurately determine transport parameters, including longitudinal dispersivity and transverse dispersivity.

When sea level rises (i.e., relative sea level > 0.0 m), the coastal line will move inland and hydrostatic seawater pressure at each node will be changed in the simulation domain. For example, sea level will rise by approximately 0.57 m for the 2090RCP45 scenario (Table 1). This SLR will move the coastline approximately 17.1 m inland. Therefore, the initial and boundary conditions for the SLR scenarios (i.e., relative sea level > 0.0 m) should be adequately configured according to the new sea level. Figure 5 presents salinity changes relative to the baseline at the observation node (located at 44 m below sea level) for the 14 scenarios. Among the cases with no SLR scenario (i.e., with consideration of only the freshwater recharge rate: RR2050RCP45, RR2050RCP85, RR2090RCP45, and RR2090RCP85), the highest increase in salinity (approximately 13.3%) was simulated for RR2090RCP45, while the highest decrease in salinity was approximately 19.6% for case RR2090RCP85. Overall, the highest salinity change (approximately 40.3%) was simulated for the scenario 2090RCP45_RR2090RCP45 (i.e., SLR of 0.57m and a freshwater recharge rate of $0.00549 \text{ kg s}^{-1}$) and the results for the baseline and this scenario are displayed in Figure 6. A salinity change of only 7.7% increased with the case 2090RCP85_RR2090RCP85 (i.e., the highest SLR of 0.72 m and the highest freshwater recharge rate of $0.00694 \text{ kg s}^{-1}$). These results imply that a freshwater recharge rate of $0.00694 \text{ kg s}^{-1}$ may largely offset the impact of SLR on seawater intrusion. This finding is in good

agreement with that by Hussain et al. [30]. They found that salinity in the aquifer could be largely reduced by the artificial recharge application. These results suggest that to accurately assess the impacts of climate change on seawater intrusion in coastal groundwater systems, both SLR and freshwater recharge rates should be considered.

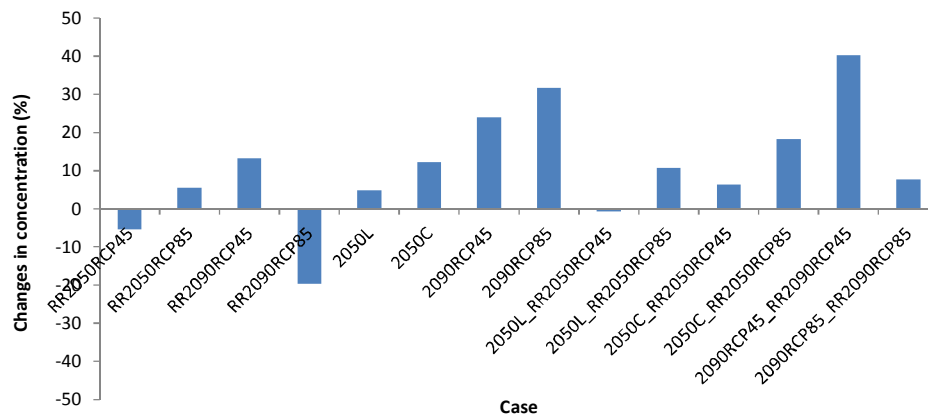


Figure 5. Salinity changes (%) relative to the baseline at the observation node for the 14 scenarios.

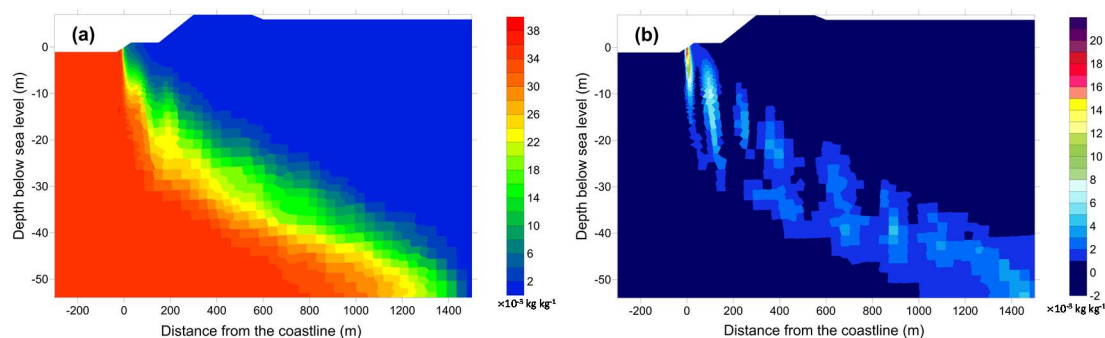


Figure 6. (a) Salinity for the baseline and (b) salinity differences between the baseline and the scenario 2090RCP45_RR2090RCP45 (0.57 m SLR with a freshwater recharge rate of 0.0058 kg s^{-1}) in $\times 10^{-3} (\text{kg-dissolved solids}) (\text{kg-seawater})^{-1}$.

4. Conclusions

We attempted to investigate the impacts of climate change and SLR on seawater intrusion in the coastal groundwater systems in South Korea through the SUTRA model. The Gunsan tide gauge station and the Byeonsan2 groundwater monitoring well for seawater intrusion were selected for this study. The longitudinal dispersivity and transverse dispersivity estimated by the SUTRA model with the baseline period (2005–2015) were 10.0 and 0.1 m, respectively. Due to the “scale effect”, a further study on a tracer test is suggested to accurately determine the transport parameters. For the 14 scenarios, the largest salinity change relative to the baseline (approximately 40.3%) was simulated with case 2090RCP45_RR2090RCP45 (i.e., 0.57 m SLR and a freshwater recharge rate of $0.00549 \text{ kg s}^{-1}$), while the change in salinity increased by only 7.7% for case 2090RCP85_RR2090RCP85, even though the highest SLR (0.72 m) was assumed for this case. These findings indicate that a freshwater recharge rate of $0.00694 \text{ kg s}^{-1}$ may largely offset the impact of SLR on seawater intrusion at the Byeonsan2 groundwater monitoring well. These findings suggest that both freshwater recharge rate and SLR should be considered for the accurate assessment of climate change impacts on seawater intrusion in coastal groundwater systems. We concluded that this study may provide a better understanding of the climate change impacts on seawater intrusion in coastal groundwater systems by considering the climate change impacts on SLR and freshwater recharge rates.

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Author Contributions: Jong Ahn Chun and Daeha Kim conceived and designed the experiments; Jong Ahn Chun simulated the SUTRA model; Jong Ahn Chun, Daeha Kim, and Changmook Lim analyzed the data; Jong Ahn Chun, Daeha Kim, and Jin Sung Kim contributed materials; and Jong Ahn Chun and Daeha Kim wrote the paper.

Conflicts of Interest: The authors declare no conflict of interest.

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