

Article

Water Allocation Computation Model for River and Multi-Reservoir System with Sustainability-Efficiency-Equity Criteria

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Abstract: Limitation and inequality of water in interspace and time opposite to the increased water demand indicated from the density of headwork nodes in the river system. It requires proportional-equal water allocation determined by the model. Existing models are not based on water as a public good and not using the sustainability-efficiency-equity criteria despite irrigation is the biggest use. The Water Allocation Model Equalization or in Indonesian it is called “*Model Ekualisasi Alokasi Air*” (MEQAA) is proposed. MEQAA modeling system is inspired by the shortage of irrigation water for a quite extended period of time and the complexity of the water allocation system in the Lombok river basin. MEQAA is assisted by MS Excel-VBA 2016 that can be tracked automatically on an independent river system scheme to create a network equation with mass balance principle and operation rule. This model is based on the dynamic-deterministic, so the performance test can be used with synthetic data. This experiment was compared with the output from the equalization method and the “first-come, first-served” (FCFS) method. The conclusions of this experiment are: (a) MEQAA can build a specific model according to a network-flow configuration for optimization-simulation with iteration of K-factor (release portion) and C-factor (storage portion) in order to get a maximum and equal and (b) the FCFS method can be detrimental to the river system. MEQAA is suggested as a decision support tool for water allocation planning or real-time operation.

Keywords: C-factor; iteration; K-factor; network equation; river scheme

1. Introduction

Water deficit becomes a problem in the irrigation sector in Indonesia, as it uses up more than 90% of the total water demand, and therefore it is necessary to limit water [1]. The water deficit is becoming more severe due to selfish water users, which leads to the inequality of water allocation, due to weak government control [2]. Furthermore, water allocation planning is not supported by suitable models to achieve common goals and reduce conflicts [3,4]. Water as a public good should be allocated equally, with the priority of daily necessities and agricultural irrigation [5]. However, water allocation practices have not been system-based and have not yet been emphasized to the triangle of UN Water criteria, which is simultaneous sustainability-efficiency-equity [6], for mutual benefit in the system [7].

Software packages of modeling systems such as RIBASIM (Deltares, Delft, Netherland), REALM (Victoria University of Technology, Melbourne, Australia), WEAP (Stockholm Environmental Institute, Stockholm, Sweden), MODSIM (Colorado State University, Colorado, USA), and WRAP (Texas A&M University, Texas, USA) are user-friendly tools for water allocation planning with the orientation in demand priority. The models mentioned above are decision support tools based on the deterministic

model; they are integrated with hydrological analysis and water quality. Further details about comparative studies of these models can be found in [8–11].

However, other modeling systems such as RIBASIM cannot produce an optimum volumetric release in inter-headwork nodes, and they are not appropriate with the Indonesian government regulations [12]. Moreover, considering the irrigation sector as the main support of food security and as the largest water user [1], the irrigation water allocation has to be managed with the sustainability-efficiency-equity criteria. Regarding the gap, MEQAA (*“Model Ekualisasi Alokasi Air”*) is a computation model for internode water distribution (similar users) in the river system [13,14].

MEQAA accommodates the UN Water criteria [6] with simplified elaboration, which are (a) sustainability, as the security of water, food, and environment/ecosystem with equal priority; (b) efficiency, as utilization in accordance with water demand and availability in order to maximize the release; and (c) equity, as equality of water in internode and time. To meet these criteria, MEQAA performs an equalization of water allocation portions, by integrating that as the main constraint.

From this research [8–11], all of the other models mentioned above are not integrated with sustainability, efficiency, and equity criteria as constraint and not calculated directly (requiring much input). Their model characteristics are: (a) a water allocation plan with the first-come-first-serve method; (b) a decision support system on a watershed basis, and integrated with hydrology analysis and so on, requiring much more input data than the water allocation solution itself [15,16]; (c) not being simple and requiring a professional operator and long negotiation [11]; and (d) not considering the ability among reservoirs, causing the operational problems in the future [17]. These model outputs do not fulfill the Indonesian government’s regulation that prioritizes proportional and equal water allocation, including the ecosystem needs, so they are difficult to put into practice.

The idea of MEQAA comes from the need to equate water distribution by using the K-Factor (release/demand ratio) indicator in the Lombok river basin (RB) [18]. The Lombok river basin was chosen as the modeling inspiration, because: (a) there are suppletion channels for wet-dry rivers, with weir/diversion and multi-reservoirs (with average density 1 node/4 km²) [19]; (b) the area is known as a paddy surplus zone, despite irrigation water deficit still happening in most of the watershed (demand/available ratio more than 200%) [20]; and (c) the survey result of the K-factor class in inter-irrigation areas is unequal, because the withdrawal of water has not yet been controlled/measured [12,21].

From global conditions of water balance and the uniqueness of the utility of river systems in the Lombok river basin, as well as limited preliminary MEQAA capabilities in a simple system [12], further research has the aim that MEQAA can be applied generically in a complex independent river system, with multi-reservoir and suppletion channel/double estuary. The idea of making MEQAA as a generic model was conceived because: (a) the preparation of procedures and mathematical functions do not need to be repeated in every system modeling [10] and (b) this negates human error while compiling water balance and optimizing the equation manually throughout the various systems.

Another objective, is that MEQAA is able to calculate water allocation with the indicator of release portion (K-factor) and storage portion (C-factor) based on sustainability-efficiency-equity criteria. MEQAA will equalize the supply/demand in interspace and time, including: (a) inter-user with K-Factor; (b) inter-reservoir with C-factor; and (c) between end period volume of the current operation and anticipated volume in the next period. For this solution a linear program is used, because it is widely used as an optimization of water allocation in river and reservoir systems [7,10,22,23]. The optimizations of MEQAA are solved by simulation of progressive iteration algorithm [24], for optimal/approximate output value [10]. The optimization simulations will solve linear and nonlinear aspects in multi-reservoirs, so it is suitable for water allocation solutions in a complex system [8,24–26].

This paper presents the latest MEQAA computation experiments using synthetic data based on the characteristics of the Lombok river basin. Furthermore, the outputs of two water allocation methods are compared between equalization and first-come-first-serve (FCFS). FCFS is one of the water allocation methods that have long been used and widely practiced for irrigation in Indonesia [20]. In the future,

MEQAA is expected to become the core of water allocation planning to support centralized control of real-time operation based on feedback from operators on the field.

2. Modeling Concept

2.1. Equalization of Water Allocation Portion

UN Water emphasizes the integrated water resources management (IWRM) guideline of sustainability-efficiency-equity criteria [6] that is appropriate with Indonesian regulations [5]. In water allocation practice, the triangle of these criteria can be elaborated as: (a) sustainability emphasizing equal priority between food security and environmental resilience/ecosystem; (b) efficiency emphasizing the use of sufficient water according to water requirements and water availability potential; and (c) equity emphasizing equality of water allocation portion in upstream-downstream and wet-dry rivers [12]. All three are accommodated in MEQAA.

In the context of social welfare, water allocation can be measured by equality of supply/demand proportionately [27]. The proportional approach is largely practiced on irrigation in many countries [28]; it is the provision of water according to individual needs. The definition of K-factor as the weight of the water allocation is the supply/demand ratio which can be found in [10,11,28]. K-factor indicates (a) volumetric reliability of water allocation in the system [29] and (b) schedule of water distribution in the irrigation area [30,31].

Water should be allocated equally among similar users in the system [11]. Water allocation control is the transference of surplus water to other parts of the system so there is no decrease in productivity [28]. Water distribution in the river is done to realize the allocation of water that has maximum discharge with the same K-factor. Controlling each node in the river will have an impact on the operation in the irrigation area, so the K-factor classification is required. The class of K-factor in Table 1 is based on irrigation practices in the Lombok river basin [21].

Table 1. K-factor standard for irrigation operation.

Class	Range of K-Factor (%)	Deficit	Operation Categories	Interlude of Water Distribution
K1	80–100	Zero-Very low	Continuous	-
K2	60–79	Low	Rotation 1	Short
K3	40–59	Medium	Rotation 2	Medium
K4	20–39	High	Rotation 3	Long
E	0–20	Very high	Emergency	Priority is inter-irrigation areas

If a user obtains water allotment with a similar value to a K-factor, it means that the interspace of using water can be called equal. In addition to K-factor as an indicator of water adequacy at the user level, C-factor is needed as an indicator of storage portion for water distribution in multi-reservoirs. Water cannot be claimed by one reservoir but must be distributed among reservoirs in the system. If the inter-reservoir has the same C-factor, then the interspace that serves to hold water can be called equal. Furthermore, water is not only needed for the moment, as anticipation of the future is necessary, which concerns the final volume in the reservoir being needed as inter-time inventory. This anticipated volume is the expected final volume, calculated from period to period based on the predicted hydrological conditions or approached from the planned reservoir rule curve. MEQAA will make equalization of K-factor, C-factor and K-factor, and C-factor as a guarantee of operational sustainability.

Equalization will make water allocation result in sync with triangle criteria, and the operation rule as the policy decision is that: (a) water distribution from upstream to downstream is in hydraulic-gravity; (b) if water is at a surplus (K-factor = 100%) then the reservoir is prioritized to store water so C-factor \geq 100%; (c) if water is sufficient to limit (40% < K-factor < 100%), then the release/spill flow/discharge contribution is adjusted so that K-factor and C-factor are equal or user priority are equal to reservoir storage; (d) if water is very limited (K-factor < 40%) then the outflow from the reservoir is set so that K-factor > C-factor or user priority is more than reservoir storage, with

K-factor equal and C-factor equal; and e) for the anticipated volume of operations in later periods, the outflow from the reservoir is adjusted so that the K-factor \approx C-factor or current operating priority is equal to the future period. Meanwhile, in emergency conditions due to drought (K-factor < 20%), it is recommended to implement on-off rotation internodes, in order to increase K-factor. The selection of nodes in the on-off rotation is determined based on the risk level priority in every node [28].

2.2. River System Categories

MEQAA was inspired by the water allocation system in Lombok river basin [21] (Figure 1) (3.43 million people, 197 watersheds, 4738 km², rainfall 213–3153 mm/year, evaporation 2.23–6.26 mm/day). The potential of surface water availability in the river basin is 2.978 million m³/year; the sources are mostly from Lake Segara Anak in Mount Rinjani (+3726.00 m) and the water requirement is 2809 million m³/year (96% for irrigation). Moreover, there are 186 weirs/diversions and 26 “embung” (small dam) in 40 independent rivers for 35,333 ha irrigation areas and 12 interconnection rivers with 310 weirs/diversions, 74 small reservoirs, and three reservoirs (dam) (capacity 23–26 million m³). In the interconnection system, there are two suppletion channels (high-level diversion or HLD) with a total length of 60.28 km. Both of these channels transfer water from wet waters (4–12 m³/s) in western Lombok to dry watersheds in central Lombok, east Lombok to south Lombok for 97,797 ha irrigation area. For example, most nodes are found in Dodokan River (dry river category) with 82 nodes which have 25 small reservoirs and two reservoirs.

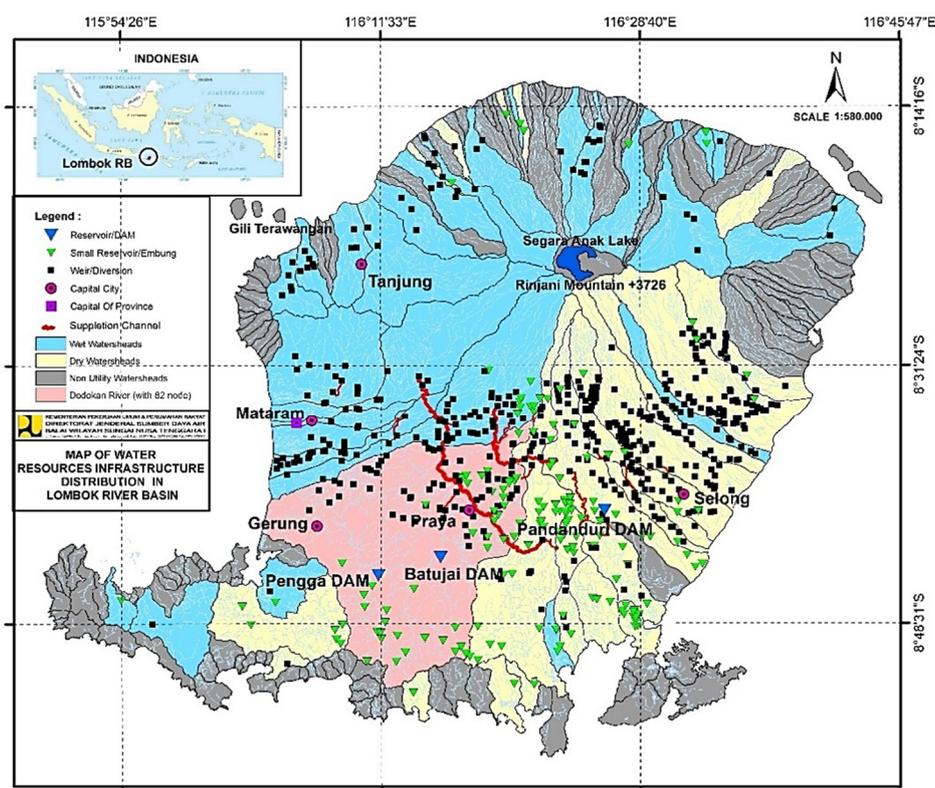


Figure 1. Lombok river basin with headwork nodes distribution.

52 watershed utilities (3486 km²) can be categorized as river system structures containing headwork nodes as in Figure 2. Each independent river can consist of one or more nodes of diversion and reservoirs. The rivers have wet and dry hydrological conditions. To make the water distribution smooth, they can be connected via suppletion channels to become interconnected, that is, interdependent between two rivers and interdependent among more than two rivers.

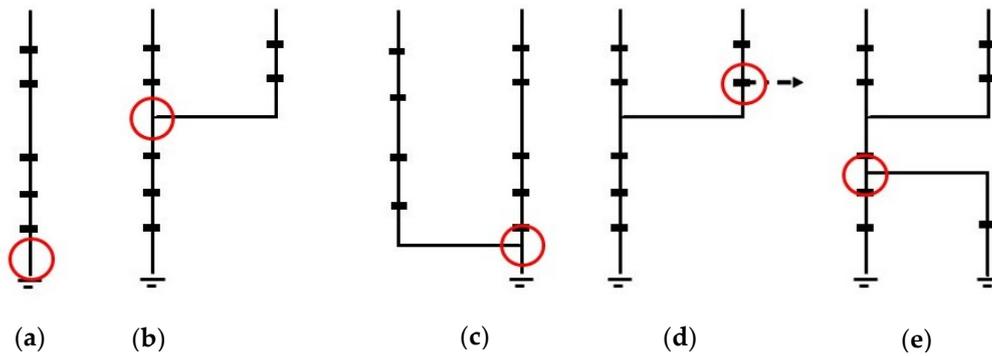


Figure 2. River system type categories in Lombok river basin. (a) Single trajectory type; (b) Connected trajectory type, tributary with one most downstream node on the main river; (c) Unconnected trajectory type, the most downstream nodes of the tributary do not connect upstream to the most downstream nodes in the main river; (d) Suppletion channel type, river with suppletion channel; (e) Double estuary type, river with double estuary. The red circle is a type of category.

2.3. Network-Flow Node

MEQAA using the principle of mass balance equation [10,22,25] is:

$$I - O = \Delta V. \tag{1}$$

Network Equation (NE) will be compiled based on Equation (1) in each node as a model object as shown below.

In Equation (1) and Figure 3 there are: (a) input (*I*) from upstream which is local inflow or spill flow; (b) input (*I*) from left/right that is local inflow spill flow/contribution from suppletion channel; (c) output (*O*) to the downstream for the next node; and (d) output (*O*) to left/right which is release/contribution to suppletion channel. The input and output deviation is notated as delta storage (ΔV) at a specific time step (Δt), are $\Delta V = 0$ (weir/diversion) and $\Delta V \neq 0$ (reservoir) [10,22]. Basically, NE contains variables in Equation (1), and it is useful for optimization-simulation of water allocation in the system.

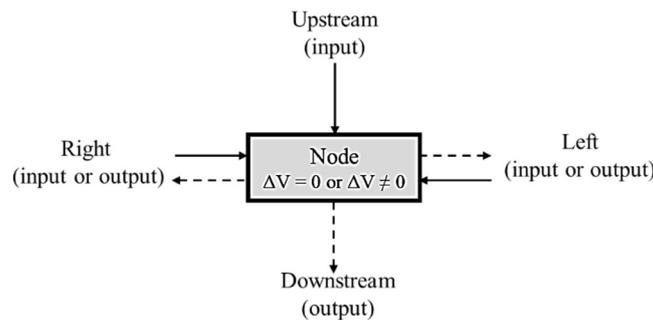


Figure 3. Input-output balance in headwork node.

NE arrangement follows the domino effect of the flow [10,32]. NE is formed by linking up the water balance equation internodes which are connected hydraulically-gravitationally through the link/reach in each river reach (RR). Each river consists of one or more river reaches, depending on the tributary. For example, in Figure 4 is a river scheme (a) as a transformation of the watershed map (b). In this scheme, there are three river reaches, one main river and two tributaries with domino effect that are: (a) at RR 100 across nodes 1-2-3-4-5; (b) at RR 200 across nodes 6-7-3-4-5; and (c) at RR 300 across nodes 8-9-5, so the system formed trajectories of 1-2, 6-7, 3-4, 8-9, and 5. Network-flow node in MEQAA preliminary [12–14] has been confirmed with the concept of upstream to downstream computational sequencing in the control points [10].

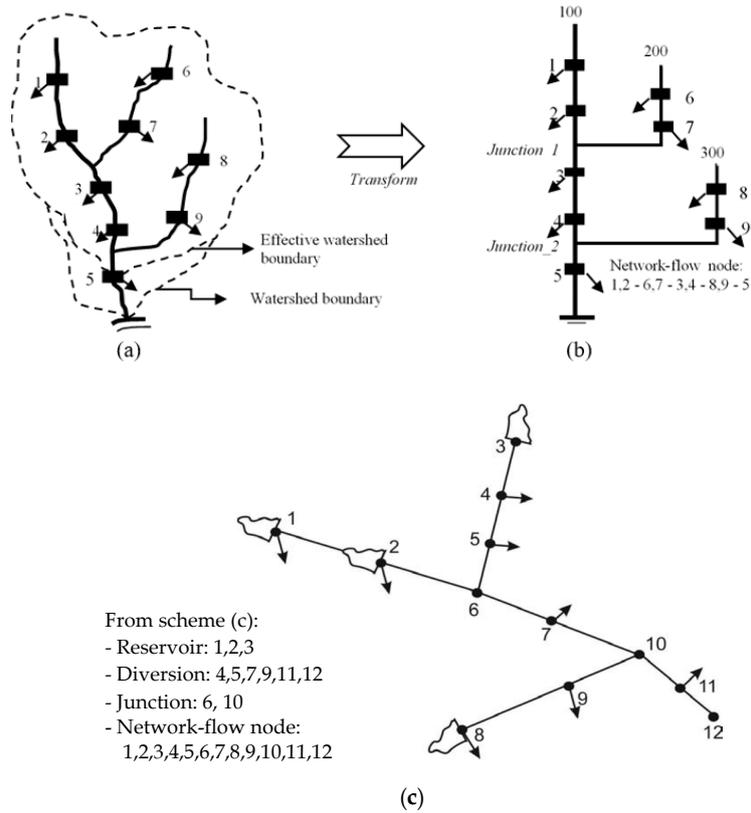


Figure 4. Transformation sketch from map to the scheme in Independent River. (a) Watershed map with headwork nodes; (b) River scheme (MEQAA version); (c) River scheme (Wurbs version).

2.4. Optimization-Simulation

Water allocation objective function in the river system which maximizes release at each node is:

$$Total\ QR = \max \sum_{i=1}^n QR_i. \tag{2}$$

For the elaboration objective function, the simple sketch (Figure 5) informs the mathematical relationship on inter headwork (HW) node through the link or reach within the river reach (RR). Each spill flow from the upstream node affects the water availability in the downstream node.

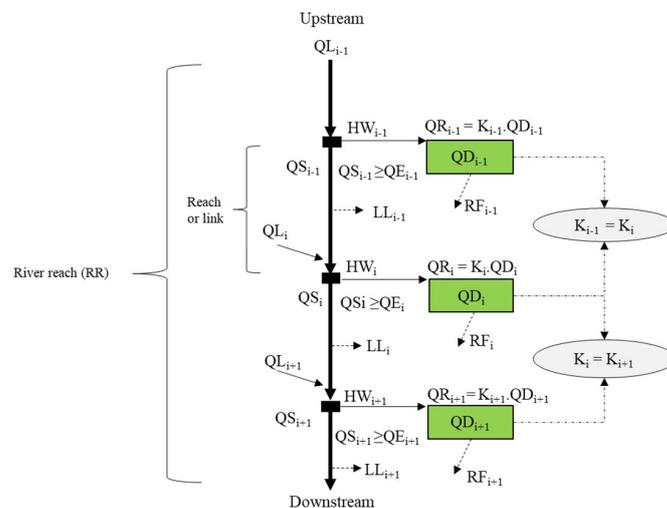


Figure 5. Variable in network-flow node trajectory.

The following MEQAA constraints will integrate: (a) sustainability, represented with ecosystem quota that has to be served from spill flow continuously; (b) efficiency, represented with a release \leq demand and K-factor as the index of water adequacy; and (c) equity, represented with a volumetric equality, being that the K-factor and C-factor of nodes must be equal in inter-time and space.

Constraint equations for linear optimization [10,33] according to water allocation concept in Figure 5 are:

1. Water Availability The total available water (QA) is described as local inflow (QL) and spill flow/contribution from upstream node (QS_{i-1}) is then:

$$QA_i = QL_i + QS_i \tag{3}$$

QL depends on hydrologic factors from the inter node catchment area.

2. Ecosystem Quota Sustainability of irrigation operations leads to food security and ecosystem sustainability has an impact on environmental stability. Both are important, so they must be integrated [6]. Spill flow in each node must meet the ecosystem water need for sustainable environment [7,34] or $QS_i \geq QE_i$ criteria. The environmental water requirements of rivers in Iran are 10% (October–March) and 30% (April–September) of water availability [6], while MEQAA is in line with regulations in Indonesia [35] as:

$$QE_i = 5\%.QA_i. \tag{4}$$

3. Efficiency The efficiency criterion is a release (QR_i) which is not exceeding demand (QD_i) or $0 \leq QR_i \leq QD_i$ [36]. If the elements $0 \leq QR_i \leq QD_i$ are divided by QD_i , then $0 \leq K_i \leq 100\%$ or release portion is:

$$K_i = \frac{QR_i}{QD_i} 100\%. \tag{5}$$

Equation (5) is identical to $QR = K. QD$ meanwhile $QR \leq (QA - QS)$. K will be classified according to Table 1 for operational information in the irrigation area. Criterion of utility of water available reviewed in the most downstream node. If $K < 100\%$ then $QS \approx QE$, and if $K = 100\%$ then $QS \geq QE$.

4. Reservoir Operation

- Reservoir operation rule is derived from mass balance in Equation (1) [10,22,37], which for each node is:

$$V_{cal} = V_{beg} + V_{in} - V_{loss} - V_{rel} - V_{spill} \tag{6}$$

with V_{cal} = calculation volume, V_{beg} and V_{end} denote the storage volume at the beginning and end, V_{in} = inflow, V_{loss} = losses, V_{rel} = release, V_{spill} = spill flow, and V_{eff} = effective capacity. Outflow in Equation (6) is based on boundary $0 \leq V_{end} \leq V_{eff}$; that is, if $0 \leq V_{cal} \leq V_{eff}$ (normal), then $V_{end} = V_{cal}$, and if $V_{cal} > V_{eff}$ (spill out), then $V_{end} = V_{eff}$.

- Based on Equation (6), future periods of operation need to anticipate volumes (V_{stock}) which is based on the reservoir rule curve. Storage portion (C-factor) in Equation (7) is an indicator of V_{end} achievement of V_{stock} . V_{stock} is the V_{end} which is expected to be achieved from the current operation. If water is limited, then $0 \leq C_i < 100\%$ ($V_{end} \leq V_{stock}$) and if it is at a surplus, then $C_i \geq 100\%$ ($V_{end} \geq V_{stock}$).

$$C_i = \frac{V_{end}}{V_{stock}} 100\% \tag{7}$$

- Rule curve operation is assumed to be cyclical to a certain pattern [38]. The rule curve pattern corresponds to a non-linear function that can be constructed through optimization-

simulation based on time series data [34]. This curve can be produced by using the regression method [39]. Rule curve can be transformed into a rule curve coefficient (CRC), such as a sinusoidal curve to facilitate the calculation of the mandatory V_{stock} period ($t + 1$). In this MEQAA experiment with single data, the boundary CRC is derived from $0 \leq V_{end} \leq V_{eff}$ which is divided by V_{eff} so that the stock portion becomes $0 \leq CRC \leq 100\%$, or:

$$V_{stock} = CRC_{t+1} \cdot V_{eff} \quad (8)$$

Where CRC is analog with K_{+1} . If $V_{stock} > V_{beg}$, then the volume anticipation will increase, or vice versa.

- Quoted from reservoir operation study in Pandanduri earth-filled dam in Lombok river basin, water loss coefficient from evaporation and seepage 0.7–1% towards V_{beg} was obtained [38]. In this MEQAA experiment, total water loss (V_{loss}) was estimated with 0.7% coefficient, as:

$$V_{loss} = 0.7\% \cdot V_{beg} \quad (9)$$

For another reservoir, the value of loss coefficient in Equation (9) can be re-adjusted depending on evaporation, storage, and dam construction.

5. Volumetric Equally

- To be quantitative, the equity is analogous to the equality of water allocation portion. The K-factor criterion equals inter-users in upstream (i) and downstream ($i + 1$) [36], that is:

$$K_i - K_{i+1} \leq \varepsilon \quad (10)$$

- C-factor criteria that equal inter-reservoir is:

$$C_i - C_{i+1} \leq \varepsilon \quad (11)$$

- Practically, Equations (5) and (7) are analogs of the supply/demand ratio. For the portion of the current QR release (K-factor) equals to the portion of anticipation volume V_{stock} for the coming period (C-factor), then both are equalized with this criterion: (a) if it is surplus then $K = 100\%$ (priority for storage or $C \geq K$); (b) if it is limited then $K_{min} \leq K < 100\%$ (priority for user equal with storage or $K \approx C$); and (c) if it is very limited then $K < K_{min}$ (priority for user or $K > C$). In Equation (10) the value of K is obtained from Equation (5).
 - In a river system with a suppletion channel/double estuary, the equalization will still review the K-factor and C-factor at each corresponding river reach. The water distribution in this system is controlled by the suppletion regulator towards the target which will be assisted.
6. Water Loss at Reach In the reach of inter-node, there can be a return flow (RF) from the irrigation area that may return to the original/other rivers and lateral loss (LL) due to evaporation/infiltration. Both are difficult to quantify, and LL is estimated by weighting factor per meter of reach length [10]. In MEQAA, RF and LL are assumed to cancel each other (zero).
 7. Intake Capacity Intake capacity of each node (QC) is assumed to be able to drain $QR \leq QD$ maximum or $QC \geq QD_{max}$.

Systems with “n nodes” in “N trajectory” will produce “N.n set equation”, for optimization-simulation from node to node. If the equation is large, then it is impossible to apply an analytical solution, so a simulation is used with iteration [13,14]. Simulation is a technique in the model for the study of system behavior by using a computer, according to mathematical descriptions and decision policy so that output is able to be received [24]. To get around inter-time equalization, K-factor and C-factor is used according to V_{stock} from CRC_{t+1} by using Equation (8). Simulations with progressive

iteration solutions as Figure 6, with the inter-node concept at each reach (i) in trajectory at a number of river reach (N), are iterated until the K and C are convergent. The simulation will end at the termination status, meaning K, K and C, and C are in the tolerance gap ($\epsilon \leq 1\%$) [40], and the fulfillment of the constraint criteria with decision variable is nonnegative [30]. Comparison of water allocation solutions utilizes the first-come-first-serve (FCFS) method that is familiar to irrigation practices in Indonesia. The FCFS method prioritizes services in the upstream node, then in downstream [41]. MEQAA will be functionalized to simulate FCFS, by modifying the decision policy according to FCFS characters in Equations (10)–(12).

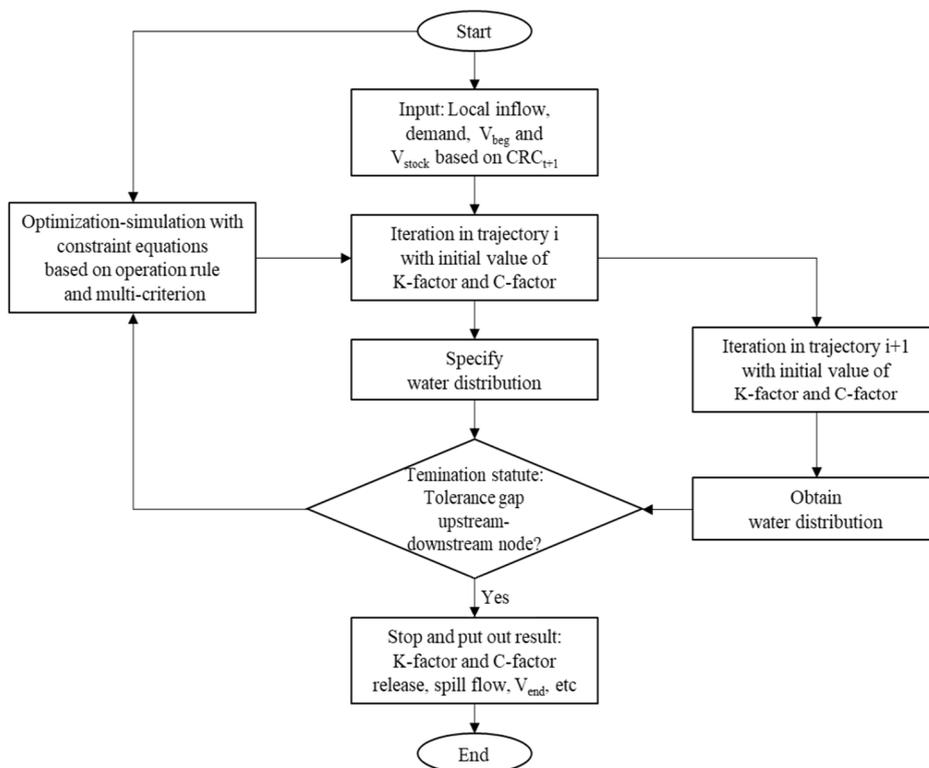


Figure 6. Progressive iteration algorithm in network equation table.

2.5. Tracking of River Scheme for Network Equation

The software packages of modeling systems use watershed-based water system configurations, with a Graphical User Interface (GUI) [10,42]. The GUI is a facility of interaction between users and computers, with one of its features being direct manipulation for applications and data functions. Studies have shown that the GUI does not guarantee effective usability, but if it well-designed then it can be more effective than without a GUI [42]. MEQAA is categorized as “semi-GUI” because it uses MS Excel and user intervention.

There is a difference in building a river scheme between software package and MEQAA: if the package software uses GUI facilities to overlay watershed maps, then MEQAA is manual without map overlay. GUI facilities on MEQAA are uses for running process buttons and other instruction buttons, such as nodes tracking in river scheme to be converted to become a network-flow node configuration. In order to be tracked, each node and river reach are coded accordingly Table 2. Furthermore, based on the configuration, MEQAA will formulate a specific model containing the network equation (NE) structure in table form. NE structure uses a dynamic system approach, so it can accommodate system components as a discrete objects collection, to describe the behavior of complex systems [43].

NE structure connects variables between cells in MS Excel according to network-flow node configuration in dynamic systems [10], with the procedure shown in the Figure 7.

Table 2. The coding guidelines for the network-flow node in river scheme.

Code	Usefulness	Description
100	Main river	Written above the main river
200, 300, etc.	Tributary	Written above the tributary of the node
1, 2, 3, etc.	River junction	Written on the junction, with formula $\{(tributary\ code - 100)/100\} - 1$
0	Main river estuary	Written below the main river estuary
B	The initial name for diversion	Written in front of the node/object name
BD	The initial name for reservoir	Written in front of the node/object name
BS	The initial name for extern suppletion channel	Written in front of the node/object name

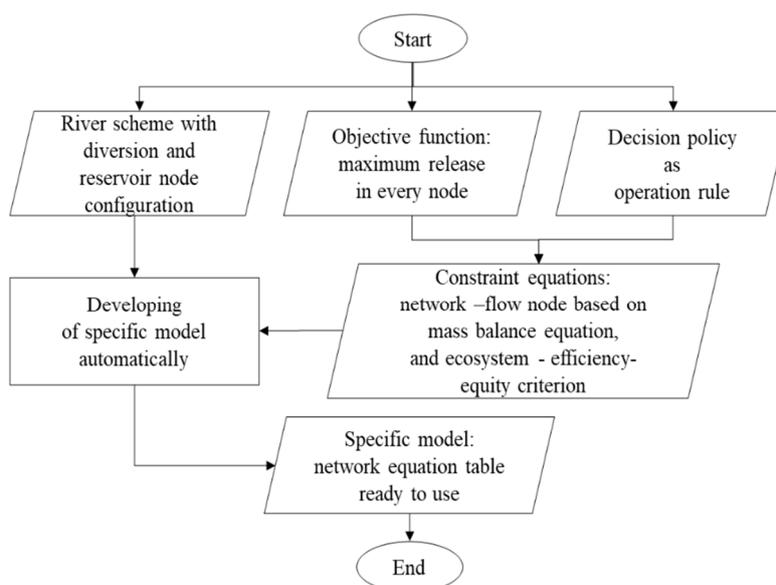


Figure 7. Procedures for the arrangement of the network equation structure.

2.6. The Criterion of Verification and Validation for the Model

Referring to [3,44], verification and validation can be arranged according to the modeling concept and the criteria for termination status on Table 3:

1. The syntax code of verification criteria are: (a) configuration of network-flow nodes mapped in domino effect in every river reach; (b) NE structure according to dynamic system and accommodate constraints criteria; and (c) the iteration simulation being able to run to reach the termination status of K-factor, C-factor, and the flow contribution in the suppletion regulator.
2. The criteria of output validation are: (a) maximum QR total; (b) the downstream node having a minimum QS value which is its QE value; (c) K-factor, K-factor and C-factor, and C-factor as the portion indicator must reach the maximum-equal value; (d) decision variable is nonnegative (noneg); and e) water balance (WB) control is null.

Table 3. Criteria for termination status.

Item	Key Indicator	Related Components	Function
K_draft	-	QR, QD	K iteration, from 100% to 0 with step $\leq 1\%$
Noneg	1	$QA \geq 0, QR \geq 0, QS \geq QE, QE \geq 0$	Criteria indicator for decision variables without containing negative values.
Stor_key	1	DR_key include V_{cal}, QA, QD, QR, QE towards KC_{key} .	Criteria indicator for decision variables.

Table 3. Cont.

Item	Key Indicator	Related Components	Function
C_draft	-	$V_{end}, V_{stock}, V_{eff}$	C iteration, from C_max to 0 with step $\leq 1\%$.
WB	0	$V_{beg}, V_{loss}, V_{end}, QA, QR, QS$	Criteria indicator for water balance (input-output on mass balance equation)
C_max	-	$V_{cal}, V_{stock}, V_{eff}$	Maximum value of C iteration. ($0 \leq C_{max} \leq 100\%$)
CK_key	1	$QS, QE, K, C, V_{end}, V_{eff}$	Criteria indicator for decision variables.
K_key	1	QR, QD, K	Criteria indicator for decision variables.

3. Experimental

3.1. Operation Procedure

In Figure 8 on the left side there are (a) a black box containing buttons that can be selected according to their functions, (b) DAR meter (demand/available ratio) as a global water balance indicator, as surplus (<100%), balance (100%) or deficit (>100%), (c) RDR meter (release/demand ratio) as an indicator of global water allocation reliability (0–100%), and (d) iteration box (located below RDR meter) as an indicator of the total of iterations until it reaches the termination status in the tolerance gap. The movement of DAR meter indicator is according to input data, while RDR meter and number of iterations are according to the result of simulation optimization at each data input.

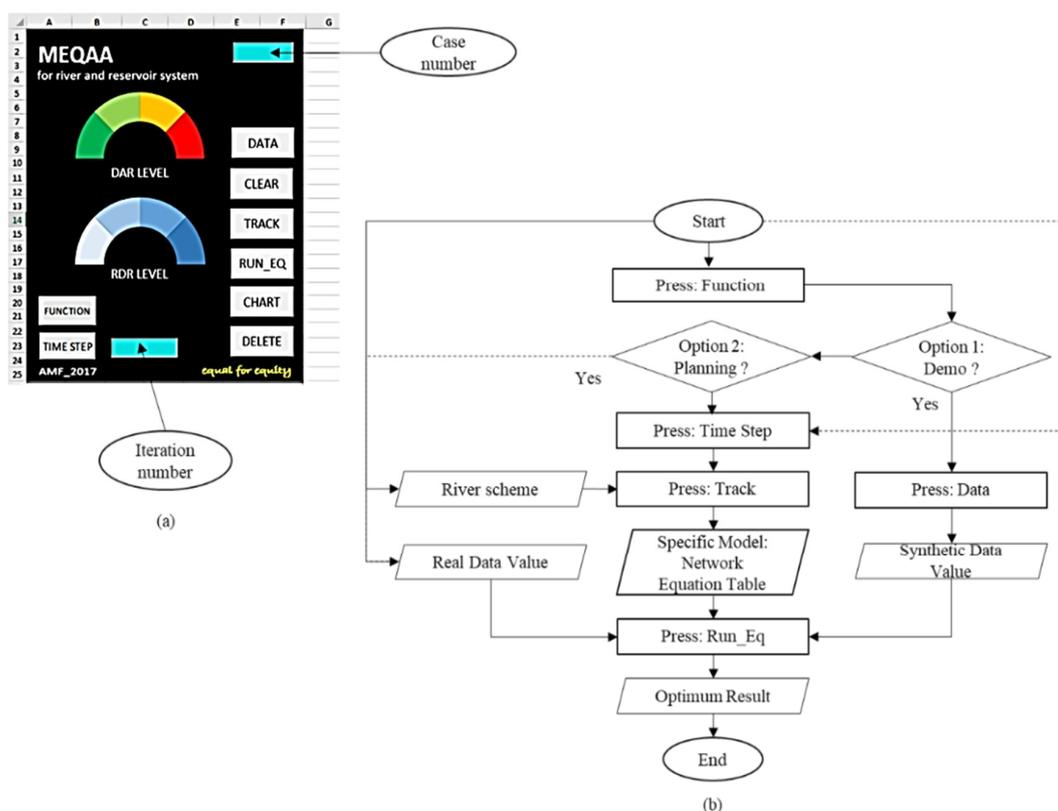


Figure 8. (a) MEQAA user interface facility with instruction buttons; (b) Standard operating procedures of MEQAA.

The MEQAA operating procedure that is shown in Figure 8 is (a) create or copy the schemas available in the spreadsheet manually according to MS Excel procedures, and (b) choosing the process

buttons, include: (i) FUNCTION for selecting DEMO (with synthetic data) or PLANNING (with real data), (ii) TRACK to determine the network-flow node configuration in the river scheme and to get the NE table, (iii) RUN_EQ for optimization-simulation, (iv) CLEAR for removing the NE table, (v) DELETE for deleting the entire format, (vi) DATA for inputting data in each case period—this button is only active when the DEMO button is selected, (vii) CHART for showing output information graphically, and (viii) TIME STEP for options for time step in each case (period 1, 5, 10, 15, and 30 each day). This experiment uses time step for 10 each day. Meanwhile, software packages of other modeling systems also have time step options such as hourly, daily, half-monthly, and monthly [10,16].

If a K-factor is less than K_{min} , then MEQAA will display the on-off rotation option information. If the user agrees to on-off rotation, it is necessary to specify nodes that are not given water. Choosing a closed gate at a certain node in a river scheme is done using the “Format Painter” feature in MS Excel based on the standard color of “closed” (gray). The choice of the target location for water distributed is according to priority scale, based on the critical period of the plant. Then, RUN_EQ is selected again to get a larger K-factor.

3.2. Data Input

Experiments using a synthetic river scheme (Figure 9) combine 5 types of schemes in Figure 2, with diversion, multi-reservoir and suppletion regulator. The schemes are system-dependent because there is a supply channel of river reach (RR) 500 in the XYZ River flows to RR 600 in another river. In the scheme, the input has been coded according to the guidelines in Table 2. In the scheme there are 6 river reaches (RR 100–600), 5 junctions, 1 suppletion channel, 1 main estuary (0), 1 s estuary, 7 diversions (B6, B8, B4, B9, B15, B12, and B13), 6 reservoirs (BD1, BD5, BD7, BD2, BD10, and BD14) and 2 suppletion regulators (BS 3 and BS 11). All water users are irrigations.

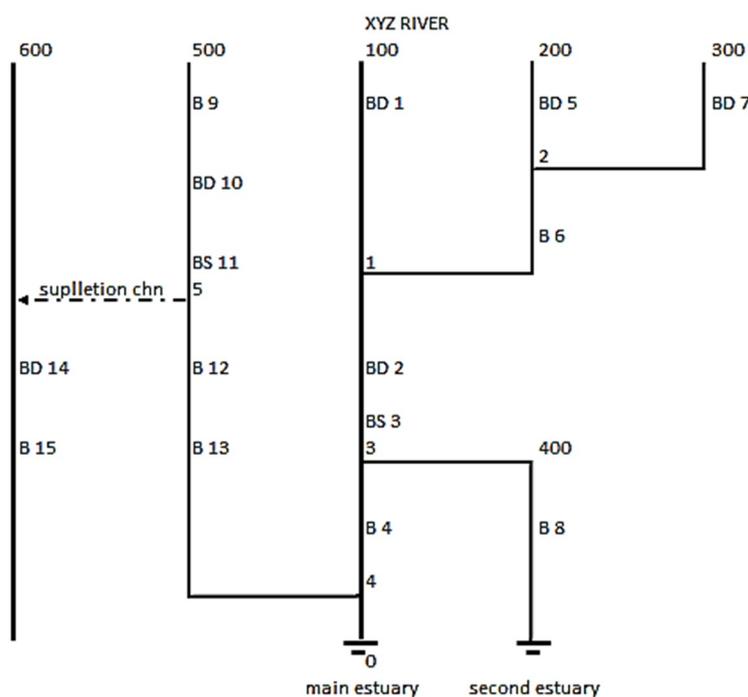


Figure 9. Synthetic river scheme.

The data value is random within ranges: (a) QL 0–2.094 L/s; (b) QD 0–6.381 L/s; (c) V_{eff} 11,000,000–26,000,000 m^3 ; (d) V_{beg} 9,720,000–21,320,000 m^3 ; and (e) V_{stock} 4,420,000–20,000,000, based on the characteristics of the Lombok river basin. The value of V_{stock} is determined from the CRC of each reservoir; BD1, BD5, BD7, BD2, BD10, and BD14 are respectively 77%, 59%, 63%, 43%, 40%, and 67% towards V_{eff} . The CRC portion is a random value contained in the MEQAA syntax code and is not

shown in the NE table. In this case, these generally occur: (a) increased water demand in operation in future periods ($V_{stock} > V_{beg}$) in BD7 and BD2, whereas other reservoirs are the opposite ($V_{stock} < V_{beg}$), and (b) global water balance is surplus-fluctuating with 53% of DAR. By using the same data value, the output of methods with and without equalization will be comprised.

4. Results and Discussion

4.1. Network Equation Table

The NE structure connects Equation (1) to (12) according to the network-flow node configuration as exemplified by some NE tables in Figure 10, with the explanation of notation in Figure 11. For the scheme in, MEQAA forms a trajectory according to the sequence of hydraulic in every headwork node printed on the U column in each river reach on the AU column. AT column informs the location of the node located at the most upstream in each river reach. As long as no changes are made to the nodes in the system, each river scheme will have only one specific NE table.

J	T	U	V	W	X	Y	Z	AA	AB	AC	AD	AE	AF	AG	AH	AI	AJ	AK	AL	AM	AN	AO	AP	AQ	AR	AS	AT	AU	
1		MEQAA																											
2		XYZ RIVER								CLASS OF K-FACTOR STANDARD																			
3		RIV=6								K1	100-80%	K4	40-20%																
4		J=5								K2	80-60%	E	20-0%																
5		RES=6								K3	60-40%		Closed/Zero dem.																
6		HW=15																											
7																													
8	No	HW	Veff	Vbeg	Vloss	Vcal	Vend	Vstock	QL	QA	QD	K_draft	QR	QS	QE	K	Noneg	C	Stor_key	DR_key	C_draft	WB	C_max	Ok_key	K_key	DAR	HW_first	Riv_rch	
9	1	BD 1	0	0	0	0	0	0	0	0	0	0	0	0	0	FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00	BD 1	100	
10	2	BD 5	0	0	0	0	0	0	0	0	0	0	0	0	0	FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00	BD 5	200	
11	3	BD 7	0	0	0	0	0	0	0	0	0	0	0	0	0	FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00	BD 7	300	
12	4	B 6														FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00		200	
13	5	BD 2		0	0	0	0	0	0	0	0	0	0	0	0	FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00		100	
14	6	BS 3														FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00		100	
15	7	B 8														FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00		400	
16	8	B 4														FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00		100	
17	9	B 9														FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00	B 9	500	
18	10	BD 10		0	0	0	0	0	0	0	0	0	0	0	0	FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00		500	
19	11	BS 11														FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00		500	
20	12	BD 14		0	0	0	0	0	0	0	0	0	0	0	0	FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00		600	
21	13	B 15														FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00		600	
22	14	B 12														FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00		500	
23	15	B 13														FALSE	1.00	FALSE	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00		500	

Figure 10. Some network equation tables for optimization-simulation.

Case_1		Sum_QL_12222 l/s		Sum_Vbeg_69125000 m3		Sum_QD_48833 l/s		DAR_53%									
It_4193801		Sum_Veff_119000000 m3		Sum_Vend_51624146 m3		Sum_QR_31369 l/s		RDR_64%									
No	HW	Veff	Vbeg	Vloss	Vend	Vstock	QL	QA	QD	QR	QS	QE	K	Class	K	C	Qsup*
1	BD 1	26000000	21320000	42640	16200000	20000000	2094	2094	5381	4359	3612	107	81%	K1	81%		
2	BD 5	17000000	11220000	22440	8000000	10000000	1314	1314	4933	3946	1068	67	80%	K1	80%		
3	BD 7	24000000	14880000	29760	12000000	15000000	1943	1943	2113	1690	3551	99	80%	K1	80%		
4	B 6						281	4901	5874	4656	245	245	80%	K1			
5	BD 2	26000000	10860000	21720	9055800	11180000	0	3857	1911	1567	4353	194	82%	K1	81%		
6	BS 3						0	4353	0	0	218	218					4135
7	B 8						1329	5464	6381	5191	273	273	81%	K1			
8	B 4						1302	1520	1002	1002	518	76	100%	K1			
9	B 9						2020	2020	5076	1919	101	101	38%	K4			
10	BD 10	11000000	9720000	19440	1906346	4420000	1500	1601	0	0	10622	81				43%	
11	BS 11						0	10622	0	0	3395	531					7228
12	BD 14	15000000	1125000	2250	4462000	10000000	0	7228	5219	2296	1066	362	44%	K3	45%		
13	B 15						0	1066	2358	1013	53	53	44%	K3			
14	B 12						0	3395	3981	1752	1643	170	44%	K3			
15	B 13						439	2082	4604	1978	104	104	44%	K3			

Figure 11. Computation output with equalization method.

On the tracking scheme (Figure 9), the total trajectory obtained are river reach (RIV) = 6, junctions (J) = 5, reservoirs (RES) = 6, and headwork node (HW) = 15 with information presented in the top left corner of the NE table. The format and load on the NE table are always dynamic, following the network-flow node configuration and type of node. The NE table format in the configuration with diversion will be simpler and shorter since there is no storage function. If there is a reservoir in the system, the NE table format will be wider, because there is a storage function. Table 4 will be at maximum if the system contains a complete mix of diversions, reservoirs, and suppletion channel/double estuary as shown in Figure 9. The illustration in Figure 10 is an example of NE table in maximum capacity, due to the case with complex river scheme configuration.

Table 4. Notation in NE table.

No	Notation	Acronym	Description	Equation
1	No	Node number	Output from tracking	-
2	HW	Headwork configuration	Output from tracking	-
3	V_{eff}	Effective volume	Input data	-
4	V_{beg}	Beginning volume	Input data	-
5	V_{loss}	Losses volume	Calculated	(9)
6	V_{end}	End volume	Calculated from V_{cal} (boundary operation)	(6)
7	V_{stock}	Stock volume anticipation for next operation period	Calculated	(8)
8	QL	Local inflow	Input data	-
9	QA	Water available (total inflow)	Calculated	(3)
10	QD	Water demand	Input data	-
11	QR	Intake release	Calculated	Connected
12	QS	Spill flow /contribution	Calculated	Connected
13	QE	Ecosystem water need	Calculated	(4)
14	K_{draft}, K	K iteration and optimum	Calculated	(5), (10), (12)
15	Class_K	Class of K	From Table 1	-
16	C_{draft}, C	C iteration and optimum	Calculated	(7), (11), (12)
17	$Stor_{key},$ $DR_{key},$ CK_{key}, K_{key}	Termination status indicator at iteration process	Calculated	Connected
18	Noneg, WB	Control indicator at optimization criterion	Calculated	Connected

In Figure 10 there are empty cells, which (a) in columns V, W, AA, QL , and QD will be filled by input data such as V_{eff} and others, (b) in column AW will be filled with K_{draft} iteration (100%–0) with a certain $step_K$ (1%), (c) in column AN will be filled with C_{draft} iteration ($\geq 100\%$ –0) based on C_{max} in AP column, with $step_C$ synchronized with $step_K$, and (d) in column US will be filled with local DAR values according to QD and QL input data in each node. C_{max} is a storage portion potential calculated from Equation (7). As in the columns with cells that have been filled/printed, a formula is automatically loaded describing objective function and constraint equations, which (a) in column X, cells $X9 = W9 \times 0.002$ are Equation (9) with $X9 = V_{loss}$ and $W9 = V_{beg}$ and (b) in column K, cells $K9 = AF9/AD9$ are Equation (5) with $K9 = K$ -factor optimum, $AF9 =$ optimum release, and $AD9 =$ demand. These values will remain after the simulation reaches the termination state. Meanwhile, in cells with numbers of 1 or 0, the columns X, Y, Z, AC, AF AG, AH, AI, and AK will automatically change according to the iteration simulation until it reaches the termination state. If all cells in the AJ, AL, AM, AO, AQ, and AR columns contain constants with code 1 or 0 values, according to the constraint equations criteria, then the termination status has been reached.

4.2. Output with Equalization

Verification and validation based on criteria on point 2.7 are done to fit the modeling purpose. It is done gradually and repeatedly, starting from simple river scheme to complex river scheme along with the data value of each node. MEQAA forms the NE table automatically and quickly; overall it is less than 10 s after clicking the "TRACK" button. The duration of the calculation depends on the type of node, the complexity of the river scheme, and the data variability (in this case it takes 2174 s to complete). Verification of syntax code found that: (a) network-flow node configuration matches trajectory in RR 100RR 600, with a domino effect at 15 nodes; (b) The table contains the NE structure according to Equation (1) to (11) which link up inter-variables and internodes; and (c) iteration always leads to the convergence of K, C, and the contribution of the flow in the suppletion regulator to achieve the termination state. Output validation at each node generates: (a) maximum release; (b) the ecosystem water need met from spill flow; (c) as long as water can be shared, equal value on K, K and C, and C including contaminant contribution in supplement; (d) non-negative variable; and (e) null

water balance control. All the output of this method is to satisfy the sustainability-efficiency-equity criteria as the main constraint of MEQAA. All decision variables fit Equations (1) to (11).

In the equalization method of water allocation, available water is released proportionally according to demand, by considering the downstream water requirements and anticipated volumes for the upcoming operating period. The MEQAA output illustrates water distribution in Figure 11, based on data input at point 3.2. In general, the total remaining storage is 51,624,146 m³, the total release is 31,369 L/s, total supply is 11,362 L/s, RDR average is 64%, and ecosystem water need is filled from spill flow at each node.

Since the equalization method of water allocation is emphasizing the water distribution, the K has been equal at 44–100% (K_1 , K_2 , K_3 , and K_4). Downstream K equals upstream K , there is no emergency (E), and release is more than demand. The achievement of the C has been equal at 44–81%; it means each reservoir prepares V_{stock} for future operational needs.

In RR 100, 200, 300, and 400, regarding BD1, BD5, BD7, and BD2, these are multi-reservoirs (cascade-parallel type) with V_{beg} less than V_{eff} . BD5 and BD7 have to share the water to B6, so the K is equal at 80–81% (from Table 1 obtained K_1) and C is equal at 80–81%. The achievement of C is less than 100% because local inflow and V_{beg} are limited so it is difficult to meet the load factor. Contribution from BD 1 to BD 2 with K is 81–82% and C is 81%, proceeding to the double estuary through suppletion regulator of BS3 at 4135 L/s, so B8 reaches 81% of its K . B4 does not need supply from BS3, because reach BS3-B4 have local inflow in the amount of 1302 L/s, so the water availability (1520 L/s) is greater than demand (1002 L/s). As a result of a surplus in B4, the K in B4 reaches 100% and spill flow is 518 L/s, which is greater than the ecosystem water need (76 L/s). While spill flow in B 8 for ecosystem water need is 273 L/s, it complies with the criteria of minimizing spill flow.

RR 500 and 600 have BD10 as reservoir regulator (without demand) and BD 14. Both are a cascade, but among them, there is a suppletion regulator BS11 as a contribution towards RR 600. RR 500 ends at downstream B4, while RR 600 is the dry river with the most downstream node in B15. B9 has 38% of K since the local inflow is only 2020 L/s which must be shared with 5076 L/s of demand and 101 L/s of ecosystem water need. Meanwhile, BD10 which has no demand is in the downstream of B9, so 10,622 L/s of spill flow is used to assist downstream needs and 7288 L/s of supply to RR 600 through BS11. Because the water is limited in RR, the K achievement is 44% (from Table 1: water distribution in irrigation area by using rotation-2/medium/ K_3) and C achievement is 43–45%; both of them are equal. Spill flow at the downstream nodes B13 and B15 are equal to their own ecosystem water need, according to the efficiency criterion

RR 100-400 and RR 500-600 achieved K and C with the same value, which was 80–81% for RR 100-400 and 43–45% for RR 500-600. In this case, in each reservoir, V_{stock} for the next period is only partially fulfilled from the current V_{end} or $V_{end} < V_{stock}$, so $C < 100\%$; however, the current supply/demand is the same as the next period ($K \approx C$). It can be said that supply/demand inter-time are equal. In conditions of limited water availability ($K < 100\%$) MEQAA can be designed to enhance the current release but it may endanger the next operation; conversely, decreasing the current release will give a benefit to the next period of operation. Both of these conditions do not pay attention to the sustainability of the operation, including the storage portion inter-reservoir, so the K decision policy being equal to C is reasonable. If the condition is surplus ($K = 100\%$), then the reservoir will store water limited to V_{eff} in order to reach $V_{end} \geq V_{stock}$ or $C \geq K$. Meanwhile, there is no drought condition ($K < K_{min}$ or emergency) in this case, so MEQAA does not show the information option of on-off rotation. On-off rotation is recommended during a drought in real-time operation.

In the iteration of K and C, it has a tolerance gap of error $\varepsilon = 1\%$, so it can be categorized as the smallest error for the solution of water allocation. The simulation based on data input at point 3.2 takes 4,193,801 iterations. The number of iterations depends on the complexity of the system or trajectory, the characteristics of the data value or the water balance at each reach, and the iteration step. An increasingly complex system requires a long duration of iteration, including when deficit in reach occurs.

4.3. Output without Equalization

Calculations are performed using NE table on equalization method, with a decision policy that does not follow objective function in Equation (2) and sustainability-efficiency-equity criteria on constraint equations. Decision policy includes: (a) water available in the upstream node will be used as a release as much as demand or greater and (b) the downstream needs will be given after the fulfillment of upstream needs [20]. Another policy is to prioritize the use of water in the reservoir for the present rather than operations in a later period. MEQAA is modified in such a way so that it can emulate the behavior of FCFS. Based on the decision policy and the input data in point 3.2 the results are 57,061,200 m³ of total remaining storage, 25,790 L/s of total release, 7270 L/s of total suppletion, mean of RDR is 53%, and ecosystem water need is not fulfilled at B6, BS3, B8, B9, B15, B12, and B13. The calculation results are presented in Figures 12 and 13b.

No	HW	Case_1 It_54448			Sum_QL_12222 l/s Sum_Veff_119000000 m3			Sum_Vbeg_69125000 m3 Sum_Vend_57061200 m3			Sum_QD_48833 l/s Sum_QR_25790 l/s			DAR_53% RDR_53%		
		Veff	Vbeg	Vloss	Vend	Vstock	QL	QA	QD	QR	QS	QE	K	Class_K	C	Qsup*
1	BD 1	26000000	21320000	42640	18200000	20000000	2094	2094	5381	5381	275	107	100%	K1	91%	
2	BD 5	17000000	11220000	22440	8000000	10000000	1314	1314	4933	4933	82	67	100%	K1	80%	
3	BD 7	24000000	14880000	29760	14550000	15000000	1943	1943	2113	2113	178	99	100%	K1	97%	
4	B 6						281	541	5874	541	0	27	9%	E		
5	BD 2	26000000	10860000	21720	9391200	11180000	0	275	1911	1911	39	15	100%	K1	84%	
6	BS 3						0	39	0	0	0	2				39
7	B 8						1329	1368	6381	1368	0	68	21%	K4		
8	B 4						1302	1302	1002	1067	235	65	107%	K1		
9	B 9						2020	2020	5076	2020	0	101	40%	K3		
10	BD 10	11000000	9720000	19440	4420000	4420000	1500	1500	0	0	7612	76			100%	
11	BS 11						0	7612	0	0	381	381				7231
12	BD 14	15000000	1125000	2250	2500000	10000000	0	7231	5219	5219	418	362	100%	K1	25%	
13	B 15						0	418	2358	418	0	21	18%	E		
14	B 12						0	381	3981	381	0	19	10%	E		
15	B 13						439	439	4604	439	0	22	10%	E		

Figure 12. Computation output with FCFS method.

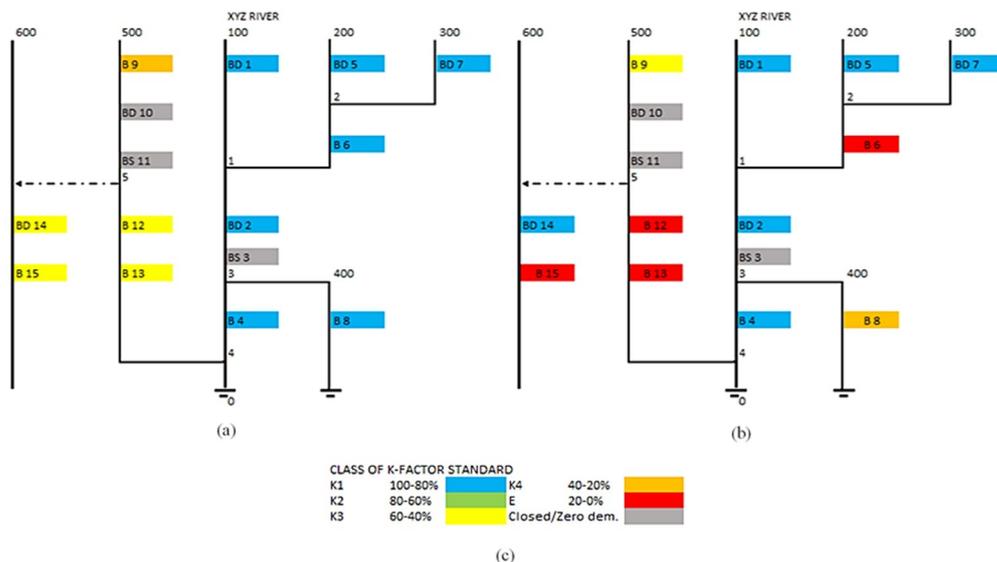


Figure 13. Class of K-factor comparison in the scheme. (a) With equalization; (b) Without equalization (FCFS method); (c) Class of K-factor standard.

The FCFS method results in an uneven distribution of Ks between 9–107% (K1, K3, K4, and E). K in downstream nodes that contain much water will be difficult to be optimized, and even emergency (E) happens as in B6. Inefficiency (K > 100%) of water withdrawal occurs in B4 with K reaching 107%, because the release is greater than demand. In addition, the uneven distribution of C between 25% and 100%, because in each reservoir competes to fill the storage than the water distribution to downstream. Water available is prioritized for current operational needs rather than for a later period. From Figure 3 it appears that this method which is selfish user-oriented does not anticipate volume for

future operations across all reservoirs ($C < K$). Application of FCFS method will decrease available volume in the reservoir before the end of operation cycle according to plan.

4.4. Output Comparison

From the output of the two water allocation methods, the class of K-factor comparisons in the river scheme is presented in Figure 13 and K-factor and C-factor are presented in graph form in Figure 14. Figure 14 is a bar chart that displays node-based output information, as a correlation between K-factor and C-factor at each node. From the chart, there are significant differences between K-factor and C-factor in each node due to the application of the equalization and first-come-first-serve (FCFS) methods. In the Prop method, in each reservoir, there are K-factor and C-factor that reach equality, as well as K-factor internodes which reach equality. In contrast, FCFS experiences unequal conditions that become disadvantageous to the water allocation in interspace and time, including ecosystem water need.

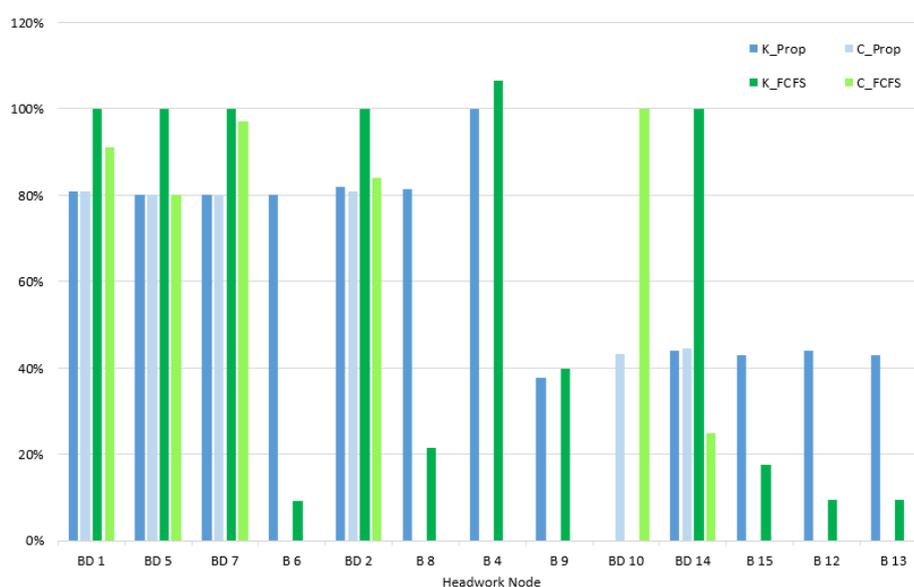


Figure 14. K-factor and C-factor comparison.

The FCFS method generates more release than demand, and thus it is inefficient, as it does not consider downstream needs including the ecosystem water need, and it does not anticipate operations in upcoming periods in the reservoir. The practice of water allocation with this method will be prone to conflict because it is self-oriented. If it is unequal, then there will be protests by downstream users, because the threat of drought. All output of FCFS method does not satisfy the sustainability-efficiency-equity criteria as the main constraint of MEQAA and does not according with the criteria for termination status. Additional water to downstream can be provided through difficult negotiations with results determined by upstream users. Otherwise, conducive and productive conditions will occur when applying water allocation by using the equalization method.

5. Conclusions

From the results and discussion, it can be concluded that:

1. MEQAA can track network-flow node configuration in independent river systems to create a network equation structure as the main equation of computational model, with input single data and output based on operation rule and the sustainability-efficiency-equity criteria.

2. Number of iterations in the simulation of water allocation depends on the iteration step, network-flow node configuration, local inflow, water demand, and the beginning volume of the reservoir.
3. Based on experiments using complex synthetic river schemes and containing many diversions and multi-reservoirs, suppletion channels and double estuaries that are described from the complexity of the system in Lombok river basin, MEQAA as a dynamic system-based deterministic model can work according to its function and the result is in accordance with the constraint.
4. The output of MEQAA satisfied the sustainability-efficiency-equity criteria, being that spill flow/contribution flow is adequate with ecosystem quota on downstream nodes; the release is efficient since it does not exceed demand with the K-factor minimum of 40%, and water allocation portion in internode is equal.
5. The practice of water allocation by equalization method according to the sustainability-efficiency-equity criteria will simultaneously integrate inter-user benefit and ecosystem quota, release, demand and water availability, upstream-downstream, and wet-dry river, storage portion in multi-reservoirs for current and future periods. In contrast, the first-come-first-serve method will cause a conflict, because of unsustainability-inefficiency-inequity.

MEQAA is potentially developed for (a) water allocation solution in the interdependent system with the multi-river interconnection, and (b) water allocation plan based on time series data in reservoir system, in order to make K-factor and C-factor equal or decreasing gradually from period to period. Spill flow as MEQAA output requires travel time model, for water delivery calculation of travel time in real-time operation.

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References

1. Fulazzaky, M.A. Review—Challenges of integrated water resources management in Indonesia. *Water* **2014**, *6*, 2000–2020. [[CrossRef](#)]
2. Strauß, S. Water conflicts among different user groups in South Bali, Indonesia. *Hum. Ecol.* **2011**, *39*, 69–79. [[CrossRef](#)]
3. Eriyatno. *Ilmu Sistem-Meningkatkan Mutu dan Efektivitas Manajemen*; Guna Widya: Surabaya, Indonesia, 2012.
4. Roozbahani, R.; Abbasi, B.; Schreider, S.; Ardakani, A. A multi-objective approach for transboundary river water allocation. *Water Resour. Manag.* **2014**, *28*, 5447–5463. [[CrossRef](#)]
5. Peraturan Pemerintah Republik Indonesia No. 121 Tahun 2015 tentang Pengusahaan Sumber Daya Air. Available online: <http://ditjenpp.kemenkumham.go.id/arsip/ln/2015/pp121-2015bt.pdf> (accessed on 18 July 2018).
6. UN Water. *The United Nations World Water Development Report 2015 “Water for a Sustainable World”*; UNESCO: Paris, France, 2015.
7. Roozbahani, R.; Abbasi, B.; Schreider, S. Optimal allocation of water to competing stakeholders in a shared watershed. *Ann. Oper. Res.* **2015**, *229*, 657–676. [[CrossRef](#)]
8. Perera, B.J.C.; James, B.; Kularathna, M.D.U. Computer software tool REALM for sustainable water allocation and management. *J. Environ. Manag.* **2005**, *77*, 291–300. [[CrossRef](#)] [[PubMed](#)]
9. Sulis, A.; Sechi, G.M. Comparison of generic simulation models for water resource systems. *Environ. Model. Softw.* **2013**, *40*, 214–225. [[CrossRef](#)]
10. Wurbs, R.A. *Comparative Evaluation of Generalized Reservoir/River System Models—Technical Report No. 282*; Texas Water Resources Institute the Texas A&M University System: College Station, TX, USA, 2005.

11. Hatmoko, W.; Triweko, W.; Yudianto, D. Sistem pendukung keputusan untuk perencanaan alokasi air secara partisipatoris pada suatu wilayah sungai. *Jurnal Teknik Hidraulik Puslitbang Sumber Daya Air-Departemen Pekerjaan Umum Republik Indonesia* **2012**, *3*, 71–86.
12. Farriansyah, A.M.; Juwono, P.T.; Suhartanto, E.; Dermawan, V.; Alyaminy, R.S.Z. The Performance of Equalization Model of Water Allocation Inter Irrigation Areas in River System. In Proceedings of the Third International Conference on Sustainable Infrastructure and Built Environment, ITB, Bandung, Indonesia, 26–27 September 2017.
13. Farriansyah, A.M.; Corsel, A.R.; Novelia, G.R. Rekayasa model alokasi air tahunan Wilayah Sungai Lombok (Studi DAS Jangkok). In Proceedings of the 31st Indonesian Association of Hydraulic Engineers Annual Conference (PIT HATHI), Padang, Indonesia, 22–24 August 2014.
14. Farriansyah, A.M.; Novelia, G.R.; Husnan, B. Alokasi air real time (kasus: Sungai Jangkok). In Proceedings of the 32nd Indonesian Association of Hydraulic Engineers Annual Conference (PIT HATHI), Malang, Indonesia, 6–8 November 2015.
15. Mensik, P.; Sary, M.; Marton, D. Water Management Software for Controlling the Water Supply Function of Many Reservoirs in a Watershed. *Water Resour.* **2015**, *42*, 133–145. [[CrossRef](#)]
16. Kim, T.J.; Wurbs, R.A. Modeling river/reservoir system management with the expanded WRAP. *KSCE J. Civ. Eng.* **2011**, *15*, 1457–1467. [[CrossRef](#)]
17. Li, H.; Shao, D.; Xu, B.; Chen, S.; Gu, W.; Tan, X. Failure Analysis of a New Irrigation Water Allocation Mode Based on Copula Approaches in the Zhanghe Irrigation District, China. *Water* **2016**, *8*, 251. [[CrossRef](#)]
18. Farriansyah, A.M.; Aribowo, G.G. Adaptasi alokasi air akibat indikasi perubahan iklim dan kompleksitas sistem sumber daya air di Wilayah Sungai Pulau Lombok. In Proceedings of the 26th Indonesian Association of Hydraulic Engineers Annual Conference (PIT HATHI), Banjarmasin, Indonesia, 23–25 October 2009.
19. Kartabrata, M.; Marjanto, W.D. Penggunaan computer model untuk distribusi air dan alokasi air pada Water Operation Centre (WOC) Unit—Dinas Pekerjaan Umum Provinsi Nusa Tenggara Barat (NTB). *Jurnal Informasi Teknik, Direktorat Jenderal Pengairan—Departemen Pekerjaan Umum Republik Indonesia* **1994**, *14*, 46–60.
20. Hatmoko, W. Indeks kelangkaan air irigasi. In Proceedings of the Paper Conference of Indonesia's INACID, Palembang, Indonesia, 16–18 May 2014; Volume 1.
21. *Rencana Alokasi Air Tahunan 2016/2017 dan Rencana Alokasi Air Tahunan 2017/2018 Wilayah Sungai Lombok*; Balai Wilayah Sungai Nusa Tenggara I (BWS-NT I): Mataram, Lombok, Indonesia, 2016/2017.
22. Yazdeli, Y.B.; Haddad, O.B.; Mehdipour, E.F.; Mariño, M.A. Evaluation of real time operation rules in reservoir systems operation. *Water Resour. Manag.* **2014**, *28*, 715–729. [[CrossRef](#)]
23. Singh, A. Review: Computer-based models for managing the water-resource problems of irrigated agriculture. *Hydrogeol. J.* **2015**, *23*, 1217–1227. [[CrossRef](#)]
24. Guo, S.; Chen, J.; Li, Y.; Liu, P.; Li, T. Joint operation of the multi-reservoir system of the Three Gorges and the Qingjiang cascade reservoirs. *J. Energies* **2011**, *4*, 1036–1050. [[CrossRef](#)]
25. Haro, D.; Paredes, J.; Solera, A.; Andreu, J. A model for solving the optimal water allocation problem in river basins with network flow programming when introducing non-linearities. *Water Resour. Manag.* **2012**, *26*, 4059–4071. [[CrossRef](#)]
26. Koch, H.; Grunewald, U. A comparison of modelling systems for the development and revision of water resources management plans. *Water Resour. Manag.* **2008**, *23*, 1403–1422. [[CrossRef](#)]
27. Wegerich, K. A critical review of the concept of equity to support water allocation at various scales in the Amu Darya Basin. *Irrig. Drain. Syst.* **2007**, *21*, 185–195. [[CrossRef](#)]
28. Gorantiwar, S.D.; Smout, I.K. *Performance Assessment of Irrigation Water Management of Heterogeneous Irrigation Schemes: 1. A Framework for Evaluation*. Irrigation and Drainage Systems; Loughborough University's Institutional Repository: Leicestershire, UK, 2005.
29. Kundzewicz, Z.W.; Kindler, J. Multiple criteria for evaluation of reliability aspects of water resource systems. In Proceedings of the Modelling and Management of Sustainable Basin-scale Water Resource Systems (Proceedings of a Boulder Symposium), Boulder, CO, USA, 1–6 July 1995; IAHS Publ, No. 231. pp. 217–224.
30. Kelley, T.; Johnson, S.H., III. Technical Communication: Use of Factor-K Water Allocation System in Irrigation Management: Theory and Application in Indonesia. *Water Resour. Manag.* **1989**, *3*, 49–71. [[CrossRef](#)]
31. Peraturan Menteri Pekerjaan Umum dan Perumahan Rakyat Republik Indonesia No.12/PRT/M/2015 tentang Eksploitasi dan Pemeliharaan Jaringan Irigasi. Available online: <http://birohukum.pu.go.id/uploads/DPU/2015/PermenPUPR12-2015.pdf> (accessed on 18 July 2018).

32. Dutta, D.; Kima, S.; Vazea, J.; Hughesa, J.; Yanga, A. Water accounting for sustainable water resources management—Role of hydrological modelling. In Proceedings of the 21st International Congress on Modelling and Simulation, Canberra, Australia, 29 November–4 December 2015; A CSIRO Land and Water. pp. 2040–2046.
33. Gonzalez, J.F.; Decker, C.A.; Hall, J.W. A linear programming approach to water allocation during a drought. *Water* **2018**, *10*, 363. [[CrossRef](#)]
34. Meijer, K.S.; Krogt van der, W.N.M.; Beek van, E. A new approach to incorporating environmental flow requirements in water allocation modeling. *Water Resour. Manag.* **2012**, *26*, 1271–1286. [[CrossRef](#)]
35. *Kriteria Perencanaan Irigasi KP-02*; Direktorat Jenderal Sumber Daya Air, Departemen Pekerjaan Umum: Jakarta, Indonesia, 2013.
36. Farriansyah, A.M.; Novelia, G.R.; Husnan, B. The Development of Equalization Model of Water Allocation. In Proceedings of the 5th International Seminar HATHI, Bali, Indonesia, 29–31 July 2016.
37. Fayaed, S.S.; El-Shafie, A.; Jaafar, O. Reservoir-system simulation and optimization techniques. *Stoch. Environ. Res. Risk Assess.* **2013**, *27*, 1751–1772. [[CrossRef](#)]
38. Kafiansyah, M.Y. *Simulasi Pola Operasi Waduk Pandanduri dengan Optimasi Faktor-K Irigasi*. Skripsi; Departement of Water Resources Engineering-Universitas Brawijaya: Malang, Indonesia, 2017.
39. Shamim, M.A.; Hassan, M.; Ahmad, S.; Zeeshan, M. A comparison of artificial neuron network (ANN) and local linear regression (LLR) techniques for predicting monthly reservoir levels. *KSCE J. Civ. Eng.* **2015**, *20*, 971–977. [[CrossRef](#)]
40. Wang, T.; Fang, G.; Xie, X.; Liu, Y.; Ma, Z. A multi-dimensional equilibrium allocation model of water resources based on a groundwater multiple loop iteration technique. *Water* **2017**, *9*, 718. [[CrossRef](#)]
41. Hatmoko, W. Modeling of real time water allocation planning in Indonesia. In Proceedings of the 3rd Asian Regional Conference-ICID, Kuala Lumpur, Malaysia, 10–15 September 2006.
42. Hoff, H.; Bonzi, C.; Joyce, B.; Tielbörger, K. A water resources planning tool for the Jordan River Basin. *Water* **2011**, *3*, 718–736. [[CrossRef](#)]
43. Elmahdi, A.; Malano, H.; Etchells, T. Using system dynamics to model water-reallocation. *Environmentalist* **2007**, *27*, 3–12. [[CrossRef](#)]
44. Sargent, R.G. Verifying and validating simulation models. In Proceedings of the 2014 Winter Simulation Conference, Savannah, GA, USA, 7–10 December 2014.



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