

Supplementary Material

The Promoting Effect of Ni on Glycerol Hydrogenolysis to 1,2-Propanediol with *in situ* Hydrogen from Methanol Steam Reforming Using a Cu/ZnO/Al₂O₃ Catalyst

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Deceased November 2, 2018, this paper is dedicated to the memory of Professor Garry L. Rempel

A1. Calculation of methanol content in crude glycerol

Estimation of Methanol Content in Crude Glycerol before Methanol Recovery:

Triolein + 3Methanol \rightleftharpoons 3FAME + Glycerol

885.43 96.12 889.51 92.04

Assume Every 100g of Triolein and 100% Conversion:

If Methanol/Triolein Molar Ratio = 6:1

Unreacted Methanol = $100 \times 96.12 / 885.43 = 10.86\text{g}$

FAME Produced = $100 \times 889.51 / 885.43 = 100.46\text{g}$

Glycerol Produced = $100 \times 92.04 / 885.43 = 10.39\text{g}$

Distribution Coefficient = 0.2 [1], assume glycerol and FAME are not soluble.

Mass of methanol in glycerol is x, mass of methanol in FAME is y:

$$x + y = 10.86$$

$$\{y/(y+100.46)\} / \{x/(x+10.39)\} = 0.2$$

By Matlab 'solve' function: $x = 4.45$; $y = 6.41$

Methanol% in crude glycerol = $4.45 / (4.45 + 10.86) \times 100\% = 29.07\%$

If Methanol/Triolein Molar Ratio = 12:1

Unreacted Methanol = $100 \times 96.12 / 885.43 \times 3 = 32.58\text{g}$

$$x + y = 32.58$$

$$\{y/(y+100.46)\} / \{x/(x+10.39)\} = 0.2$$

By Matlab 'solve' function: $x = 17.99$, $y = 14.59$

Methanol% in crude glycerol = $17.99 / (17.99 + 10.86) \times 100\% = 62.36\%$



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Shandong Ding-yu Biotech Energy Co Ltd Laboratory Test Report

Methanol/Oil Feed Ratio: 6:1 (25wt% of methanol with respect to oil)

Methanol Content in Crude Glycerol before Methanol Recovery:

37.10%

Methanol/Oil Feed Ratio: 9:1 (35wt% of methanol with respect to oil)

Methanol Content in Crude Glycerol before Methanol Recovery:

51.35%

Methanol/Oil Feed Ratio: 12:1 (45wt% of methanol with respect to oil)

Methanol Content in Crude Glycerol before Methanol Recovery:

56.40%



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A2. Calculation of P value [2]

$$P = \beta S_0 / FC_0$$

Where,

$$\beta = \text{heat rate} = 0.083 \text{ K/s}$$

$$F = \text{flow rate} = 0.5 \text{ cm}^3/\text{s}$$

$$C_0 = \text{initial H}_2 \text{ concentration} = 2.23 \mu\text{mol}/\text{cm}^3$$

For CuO/ZnO/Al₂O₃-OA catalyst:

$$S_0 = \text{amount of CuO} = 0.000244 \text{ mol} = 244 \mu\text{mol}$$

$$P = 18.16 \text{ molH}_2/\text{molCuO}$$

For NiO/CuO/ZnO/Al₂O₃-OA catalyst:

$$S_0 = \text{amount of CuO and NiO} = 0.000262 \text{ mol} = 262 \mu\text{mol}$$

$$P = 18.82 \text{ molH}_2/\text{molCuO}$$

For NiO catalyst:

$$S_0 = \text{amount of NiO} = 0.000267 \text{ mol} = 267 \mu\text{mol}$$

$$P = 19.88 \text{ molH}_2/\text{molNiO}$$

Based on the calculation of characteristic P value, they are all below 20K. As suggested by Bravo-Suarez et al., the experiments were carried out with the absence of significant reducing gas concentration gradients along the sample bed [2].

A3. Verification for absence of mass transfer limitation

Weisz-Prater Criterion for Internal Diffusion

The Weisz-Prater criterion was used to determine if internal diffusion is limiting the reaction. This criterion was calculated by the equation below:

$$C_{WP} = \frac{-r'_{G(OBS)} \rho_c R^2}{D_e C_{As}}$$

Where,

$$r'_{B(OBS)} = \text{observed reaction rate} = -6.085 \times 10^{-6} \text{ mol.g}_{\text{cat}}^{-1}.\text{s}^{-1}$$

$$\rho = 2.21 \text{ g}_{\text{cat}}/\text{cm}^3$$

$$R = 100 \mu\text{m} = 0.01 \text{ cm}$$

$$C_{AS} = 1.0 \times 10^{-3} \text{ mol/cm}^3_{\text{cat}}$$

D_e – Effective Diffusivity (cm^2/s)

$$D_e = \frac{D_{AB} \phi_p \sigma_c}{\tau}$$

Typical Values of the constriction factor $\sigma_c = 0.8$, tortuosity $\tau = 3.0$ and porosity $\phi_p = 0.40$ suggested by Fogler Elements of Chemical Reaction Engineering (p. 815-p.816) [3].

The diffusion coefficient was calculated using the WILKE – CHANG equation:

$$D_{AB} = 1.48 \times 10^{-4} \text{ cm}^2/\text{s} \text{ for the diffusion coefficient of glycerol to water at } 220^\circ\text{C} (493.15\text{K})$$

$$D_e = 1.579 \times 10^{-5} \text{ cm}^2/\text{s}$$

$$C_{WP} = 0.039 \ll 1$$

According to the Weisz-Prater criterion, the calculated C_{PW} is significantly smaller than the criterion 1, therefore, it is verified that the reaction is with absence of internal mass transfer limitation.

Verification of Absence of Liquid to Solid Mass Transfer Limitations

$$P = \frac{-r_G}{k_s a_p B^*}$$

Where,

$$-r_G = \text{volumetric reaction rate} = 1.8255 \times 10^{-7} \text{ mol.}(\text{cm}^3)^{-1}.\text{s}^{-1}$$

$$a_p = \text{external area of particles per unit volume of reactor, cm}^2/\text{cm}^3 = 5640 \text{ cm}^2/\text{cm}^3$$

$$B^* = \text{concentration of glycerol in the liquid, mol/cm}^3 = 0.00217 \text{ mol/cm}^3$$

$$k_s = \text{mass transfer coefficient estimated from Frössling Correlation (Fogler, p.774-p.777)}^1$$

$$\text{Reynolds number: } Re = \frac{U \rho d_p}{\mu}$$

$$U = 0.785 \text{ m/s}$$

$$\rho = \text{density of the mixture at } 220^\circ\text{C} = 908.95 \text{ kg/m}^3$$

$$d_p = 1 \times 10^{-4} \text{ m}$$

$$\mu = \text{dynamic viscosity of mixture at } 220^\circ\text{C} = 0.00017056 \text{ kg.s}^{-1}\text{m}^{-1}$$

$$Re = 418.34$$

$$\text{Schmidt number: } Sc = \nu/D_{AB} = 12.679$$

$$\text{Sherwood number} = Sh = 2 + 0.6Re^{1/2}Sc^{1/3} = 30.618$$

$$Sh = \frac{k_s d_p}{D_{AB}} \Rightarrow k_s = \frac{Sh \cdot D_{AB}}{d_p} = 0.453 \text{ cm/s}$$

$$P = 3.293e^{-8} \ll 0.3$$

According to Hu et al. reported on 2010 [4] as well as the criteria defined by Ramachandran and Chaudhari [5], the calculated parameter is far smaller than the criteria 0.3, it is believed that the reaction system is with absence of external mass transfer limitation.

The space time conversion (STC) of glycerol and space time yield (STY) of 1,2-PD are calculated using the following equations:

$$STC_{Glycerol} = \frac{n_{Glycerol_{in}} * Conversion_{Glycerol}}{Reaction Time * Catalyst Weight}$$

$$STY_{1,2-PD} = \frac{n_{Glycerol_{in}} * Yield_{1,2-PD}}{Reaction Time * Catalyst Weight}$$

Where,

$$Yield_{1,2-PD} = Conversion_{Glycerol} * Selectivity_{1,2-PD}$$

Table S1 Space Time Yields for glycerol hydrogenolysis with *in situ* H₂ from methanol steam reforming over Cu/ZnO/Al₂O₃-Na catalysts¹

Time	Glycerol Conversion	1,2-PD Selectivity	1,2-PD Space Time Yield	Glycerol Space Time Conversion
hour	%	%	mol.gcat ⁻¹ .hr ⁻¹	mol.gcat ⁻¹ .hr ⁻¹
0	0.0	N/A	0.0	0.0
2	16.0	16.7	0.00097	0.00581
4	42.2	31.7	0.00243	0.00764
8	60.3	29.1	0.00159	0.00546

¹Reaction Conditions: 220°C, 1.5MPa N₂, 100g feedstock mixture, 20wt% glycerol, 32.2wt% of water and 47.8wt% methanol (water/methanol molar ratio = 1.2), 3g catalyst, 500RPM, Cu/Zn/Al (molar) = 35/35/30.

Table S2 Space Time Yields for glycerol hydrogenolysis with *in situ* H₂ from methanol steam reforming over Cu/ZnO/Al₂O₃-OA catalysts¹

Time	Glycerol Conversion	1,2-PD Selectivity	1,2-PD Space Time Yield	Glycerol Space Time Conversion
hour	%	%	mol.gcat ⁻¹ .hr ⁻¹	mol.gcat ⁻¹ .hr ⁻¹
0	0.0	N/A	0.0	0.0
1	30.3	53.9	0.0118	0.0219
2	47.6	57.2	0.0099	0.0173
4	70.2	65.7	0.0084	0.0127
6	80.1	67.0	0.0065	0.0097
8	87.1	70.7	0.0056	0.0079

¹Reaction Conditions: 220°C, 1.5MPa N₂, 100g feedstock mixture, 20wt% glycerol, 32.2wt% of water and 47.8wt% methanol (water/methanol molar ratio = 1.2), 3g catalyst, 500RPM, 500RPM, Cu/Zn/Al (molar) = 35/35/30.

Table S3 Space Time Yields for glycerol hydrogenolysis with *in situ* H₂ from methanol steam reforming over Cu/ZnO/Al₂O₃-OA catalysts¹

Time	Glycerol Conversion	1,2-PD Selectivity	1,2-PD Space Time Yield	Glycerol Space Time Conversion
	%	%	mol.gcat ⁻¹ .hr ⁻¹	mol.gcat ⁻¹ .hr ⁻¹
0	0.0	N/A	0.0	0.0
2	43.9	62.3	0.00991	0.01591
4	63.9	66.2	0.00766	0.01157
6	77.7	68.4	0.00642	0.00939
8	82.7	69.9	0.00524	0.00749

¹Reaction Conditions: 220°C, 1.5MPa N₂, 100g feedstock mixture, 20wt% glycerol, 32.2wt% of water and 47.8wt% methanol (water/methanol molar ratio = 1.2), 3g catalyst, 500RPM, Cu/Zn/Al (molar) = 25/25/50.

Table S4 Space Time Yields for glycerol hydrogenolysis with *in situ* H₂ from methanol steam reforming over Cu/ZnO/Al₂O₃-OA catalysts¹

Time	Glycerol Conversion	1,2-PD Selectivity	1,2-PD Space Time Yield	Glycerol Space Time Conversion
	%	%	mol.gcat ⁻¹ .hr ⁻¹	mol.gcat ⁻¹ .hr ⁻¹
0	0.0	N/A	0.0	0.0
2	35.2	54.9	0.00700	0.01275
4	56.4	62.1	0.00635	0.01022
6	70.6	63.7	0.00544	0.00853
8	80.2	65.7	0.00477	0.00726

¹Reaction Conditions: 220°C, 1.5MPa N₂, 100g feedstock mixture, 20wt% glycerol, 32.2wt% of water and 47.8wt% methanol (water/methanol molar ratio = 1.2), 3g catalyst, 500RPM, Cu/Zn/Al (molar) = 45/45/10.

Table S5 Space Time Yields for glycerol hydrogenolysis with *in situ* H₂ from methanol steam reforming over Ni/Cu/ZnO/Al₂O₃-OA catalysts¹

Time	Glycerol Conversion	1,2-PD Selectivity	1,2-PD Space Time Yield	Glycerol Space Time Conversion
hour	%	%	mol.gcat ⁻¹ .hr ⁻¹	mol.gcat ⁻¹ .hr ⁻¹
0	0.0	N/A	0.0	0.0
1	20.6	73.7	0.0110	0.0149
2	38.3	77.9	0.0108	0.0139
4	57.2	81.3	0.0084	0.0104
6	67.4	83.3	0.0068	0.0081
8	70.0	85.5	0.0054	0.0063

¹Reaction Conditions: 220°C, 1.5MPa N₂, 100g feedstock mixture, 20wt% glycerol, 32.2wt% of water and 47.8wt% methanol (water/methanol molar ratio = 1.2), 3g catalyst, 500RPM, Ni/Cu/Zn/Al (molar) = 5/32.5/32.5/30.

Table S6 Space Time Yields for glycerol hydrogenolysis with *in situ* H₂ from methanol steam reforming over Ni/Cu/ZnO/Al₂O₃-OA catalysts¹

Time	Glycerol Conversion	1,2-PD Selectivity	1,2-PD Space Time Yield	Glycerol Space Time Conversion
hour	%	%	mol.gcat ⁻¹ .hr ⁻¹	mol.gcat ⁻¹ .hr ⁻¹
0	0.0	N/A	0.0	0.0
1	22.7	66.2	0.0109	0.0165
2	41.0	72.7	0.0108	0.0149
4	61.3	78.5	0.0087	0.0111
6	72.3	81.6	0.0071	0.0087
8	77.4	82.8	0.0058	0.0070

¹Reaction Conditions: 220°C, 1.5MPa N₂, 100g feedstock mixture, 20wt% glycerol, 32.2wt% of water and 47.8wt% methanol (water/methanol molar ratio = 1.2), 3g catalyst, 500RPM, Ni/Cu/Zn/Al (molar) = 3/33.5/33.5/30.

Table S7 Space Time Yields for glycerol hydrogenolysis with *in situ* H₂ from methanol steam reforming over Ni/Cu/ZnO/Al₂O₃-OA catalysts¹

Time	Glycerol Conversion	1,2-PD Selectivity	1,2-PD Space Time Yield	Glycerol Space Time Conversion
hour	%	%	mol.gcat ⁻¹ .hr ⁻¹	mol.gcat ⁻¹ .hr ⁻¹
0	0.0	N/A	0.0	0.0
1	24.4	57.3	0.0101	0.0177
2	46.4	63.5	0.0107	0.0168
4	66.3	66.6	0.0080	0.0120
6	76.9	69.6	0.0065	0.0093
8	85.5	76.7	0.0059	0.0077

¹Reaction Conditions: 220°C, 1.5MPa N₂, 100g feedstock mixture, 20wt% glycerol, 32.2wt% of water and 47.8wt% methanol (water/methanol molar ratio = 1.2), 3g catalyst, 500RPM, Ni/Cu/Zn/Al (molar) = 1/34.5/34.5/30.

Table S8 Space Time Yields for acetol hydrogenation over Cu/ZnO/Al₂O₃-OA catalyst¹

Time	Acetol Conversion	1,2-PD Selectivity	1,2-PD Space Time Yield	Acetol Space Time Conversion
hour	%	%	mol.gcat ⁻¹ .hr ⁻¹	mol.gcat ⁻¹ .hr ⁻¹
0	0.0	N/A	0.0	0.0
0.5	12.8	57.3	0.0107	0.0692
1	29.8	63.5	0.0318	0.0806
2	65.3	66.6	0.0430	0.0882
4	81.0	69.6	0.0290	0.0548
6	92.0	76.7	0.0230	0.0414
8	97.7	63.1	0.0208	0.0330

¹Reaction Conditions: : 200°C, 500RPM, 100g feedstock mixture, 20wt% aqueous acetol, 1g catalyst, H₂ pressure 2.8PMa, Cu/Zn/Al (molar) = 35/35/30.

Table S9 Space Time Yields for acetol hydrogenation over Ni/Cu/ZnO/Al₂O₃-OA catalyst¹

Time	Acetol Conversion	1,2-PD Selectivity	1,2-PD Space Time Yield	Acetol Space Time Conversion
hour	%	%	mol.gcat ⁻¹ .hr ⁻¹	mol.gcat ⁻¹ .hr ⁻¹
0	0	0	0.0	0.0
0.5	60.0	66.0	0.2141	0.3243
1	79.7	69.6	0.1498	0.2153
2	87.4	69.5	0.0822	0.1182
3	93.3	68.4	0.0575	0.0840
4	97.8	71.1	0.0470	0.0661
6	100.0	72.6	0.0327	0.0450
8	100.0	75.1	0.0254	0.0338

¹Reaction Conditions: : 200°C, 500RPM, 100g feedstock mixture, 20wt% aqueous acetol, 1g catalyst, H₂ pressure 2.8PMa, Ni/Cu/Zn/Al (molar) =5/32.5/32.5/30.

References:

1. de Sousa Maia, A.C.; e Silva, I.S.; Stragevitch, L. *Int. J. Chem. Eng. Appl.* **2013**, *4*, 285-289.
2. J. Bravo-Suarez, B. Subramaniam, and R. Chaudhari. *J. Phys. Chem. C* 2012, *116*, 18207–18221
3. H. Scott. Fogler, *Elements Of Chemical Reaction Engineering*. Upper Saddle River, N.J. :Prentice Hall PTR, 1999. Print.
4. W. Hu, D. Knight, B. Lowry, and A. Varma, *Ind. Eng. Chem. Res.* **2010**, *49*, 10876–10882
5. P. A. Ramachandran, R. V. Chaudhari. *Three-phase catalytic reactors*. Gordon and Breach Science Publishers, 1983 – Science.