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# Fabrication and Characterization of $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ Composite Channel Metamorphic HEMTs (mHEMTs) on a GaAs Substrate

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**Abstract:** In this work, we successfully demonstrated  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  composite channel metamorphic high electron mobility transistors (mHEMTs) on a GaAs substrate. The fabricated mHEMTs with a 100 nm gate length exhibited excellent DC and logic characteristics such as  $V_T = -0.13$  V,  $g_{m,max} = 949$  mS/mm, subthreshold swing (SS) = 84 mV/dec, drain-induced barrier lowering (DIBL) = 89 mV/V, and  $I_{on}/I_{off}$  ratio =  $9.8 \times 10^3$  at a drain-source voltage ( $V_{DS}$ ) = 0.5 V. In addition, the device exhibited excellent high-frequency characteristics, such as  $f_T/f_{max} = 261/304$  GHz for the measured result and well-matched modeled  $f_T/f_{max} = 258/309$  GHz at  $V_{DS} = 0.5$  V, which is less power consumption compared to other material systems. These high-frequency characteristics are a well-balanced demonstration of  $f_T$  and  $f_{max}$  in the mHEMT structure on a GaAs substrate.

**Keywords:** mHEMT; HEMT; InAs HEMT; InGaAs HEMT; Mo-based Ohmic contact;  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  composite channel; GaAs; InGaAs/InAs/InGaAs composite channel



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## 1. Introduction

High electron mobility transistors (HEMTs) based on indium-rich  $\text{In}_x\text{Ga}_{1-x}\text{As}$  channel materials on an InP substrate have demonstrated excellent high-frequency and logic characteristics. In terms of high-frequency characteristics of the InGaAs channel HEMT, H. -B. Jo et al. demonstrated 738 GHz unity current gain cutoff frequency ( $f_T$ ) in a 19 nm  $\text{In}_{0.8}\text{Ga}_{0.2}\text{As}$  composite-channel HEMT on a InP substrate [1], D. -H. Kim et al. showed excellent logic performance and a  $f_T$  of 644 GHz in 30 nm InAs Pseudomorphic HEMTs (pHEMTs) [2], and Northrop Grumman Corporation exhibited an  $f_T$  of 610 GHz/ $f_{max}$  of 1.5 THz by using an  $\text{In}_{0.53}\text{GaAs}/\text{InAs}/\text{In}_{0.53}\text{GaAs}$  composite channel with a  $L_g$  of 25 nm [3]. These remarkable performances have been achieved through downscaling of device feature size, an optimized fabrication process, and optimized InGaAs channel materials for excellent transport properties. In addition, InGaAs channel MOSFETs have shown outstanding logic performance on various substrates, such as InP and flexible substrates, with extensive efforts to enhance their capability in new device structures, S/D Ohmic contacts, and optimization of the gate stack [4–7]. Meanwhile, large-size and cheaper-cost substrates will be essential for large-volume manufacturing from a mass production point of view, but an InP substrate is more expensive than a GaAs substrate, and the size to date is limited to 6 inches. To overcome these limitations of the InP substrate, many groups have demonstrated many outstanding results for mHEMTs on a GaAs substrate [8–11]. In particular, Teledyne demonstrated excellent results of a 688 GHz  $f_T$  by utilizing an  $\text{In}_{0.7}\text{GaAs}$  mHEMT structure with dual Si  $\delta$ -doping and an InAs-rich  $\text{In}_{0.7}\text{Al}_{0.3}\text{As}$  spacer on a GaAs substrate in 2011 [9]. Fraunhofer

showed a maximum oscillation frequency ( $f_{max}$ ) exceeding 1000 GHz by using an  $\text{In}_{0.8}\text{GaAs}$  mHEMT structure on a GaAs substrate in 2013 [11]. Among various HEMT structures, an  $\text{InGaAs}/\text{InAs}/\text{InGaAs}$  composite channel was used to enhance high-frequency characteristics in HEMT structures because of its excellent electron transport properties, such as electron velocity and mobility [2,3,12]. However, an  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  composite channel structure on a GaAs substrate has not been demonstrated yet. In this work, we fabricated an  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  composite channel HEMT on a GaAs substrate incorporating a molybdenum (Mo)-based Ohmic contact using blanket Mo deposition and investigated its electrical performance, such as DC, logic, and RF characteristics, with an  $L_g$  of 100 nm.

## 2. Layer Structure and Experiments

The mHEMT heterostructures consisted of a 500 nm  $\text{In}_{0.52}\text{Al}_{0.48}\text{As}$  buffer, a 12 nm  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  (4/5/3 nm) channel, a 3 nm  $\text{In}_{0.52}\text{Al}_{0.48}\text{As}$  spacer, Si  $\delta$ -doping ( $4.1 \times 10^{12} \text{ cm}^{-2}$ ), an 8 nm  $\text{In}_{0.52}\text{Al}_{0.48}\text{As}$  barrier, a 4 nm InP etch stop layer, and a 35 nm heavily doped  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{In}_{0.52}\text{Al}_{0.48}\text{As}$  multi-layer cap from the bottom to the top as shown in Figure 1a. The energy band diagram of the epitaxial structure is shown in Figure 1b. From this structure, sheet carrier density and electron hall mobility were measured to be  $2.92 \times 10^{12} \text{ cm}^{-2}$  and  $10,000 \text{ cm}^2/\text{V}\cdot\text{s}$  at room temperature, respectively, with four-point probe measurement methods (Van der Pauw measurement method). Device fabrication began with a 30 nm blanket molybdenum (Mo) deposition for ohmic contact to prevent surface contamination and improve the contact resistance ( $R_c$ ), then mesa isolation down to an InAlAs buffer layer by Mo dry etching and wet etching. After Ti/Au/Ni (20/150/30 nm) metallization for source and drain, dry etching in an  $\text{SF}_6/\text{Ar}$  plasma was performed to etch Mo in the gate region using the Ni metal etch mask of the source and drain [13]. A 30 nm thick layer of  $\text{SiO}_2$  was deposited by plasma-enhanced chemical vapor deposition (PECVD), and then the pad patterns with Ti/Au (20/300 nm) were defined for ground-signal-ground probing. After e-beam exposure, the defined e-beam resist pattern was transferred to define the T-gate by using reactive ion etching based on  $\text{CF}_4$  plasma. Gate recessing was performed in two different step stages, followed by anisotropic reactive ion etching of the InP etch stop layer in an Ar-based plasma [14]. After InP etching, Schottky gate metallization of Ti/Pt/Au (20/30/300 nm) was deposited on top of the InAlAs layer. Finally, the mHEMT with a width of  $2 \times 50 \mu\text{m}$  was fabricated, and a schematic of the fabricated mHEMT is shown in Figure 1c. Figure 1d shows the SEM image of the fabricated T-gate, whose foot and head sizes are 100 nm and 470 nm, respectively.

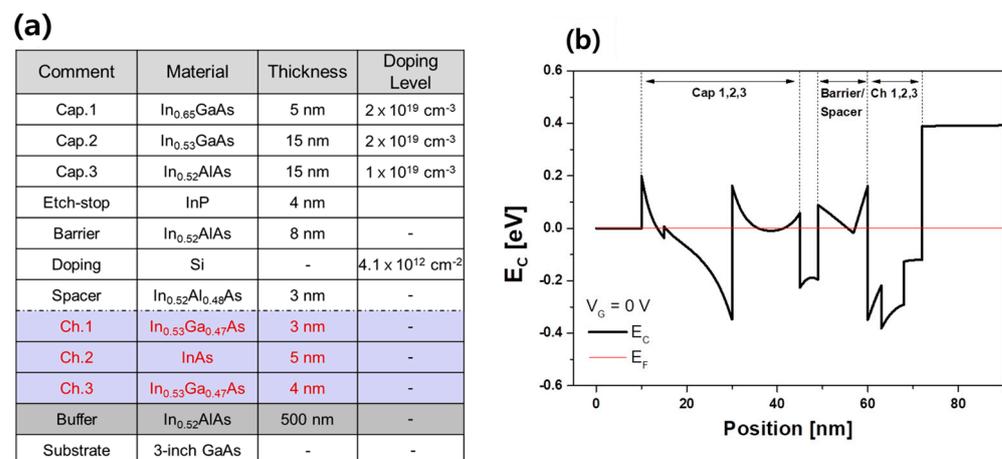
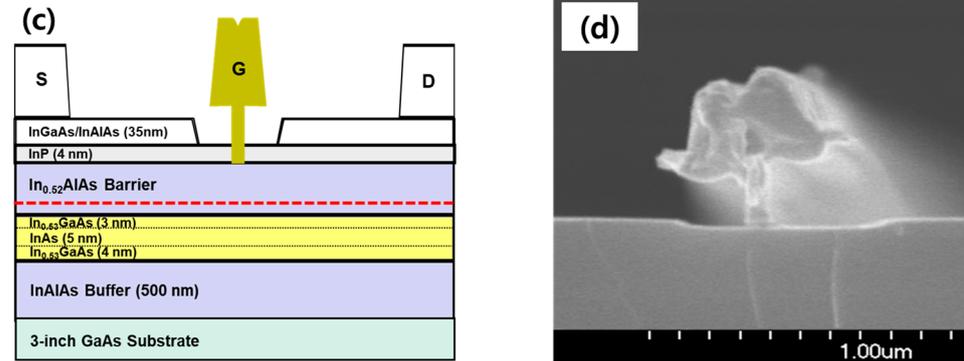


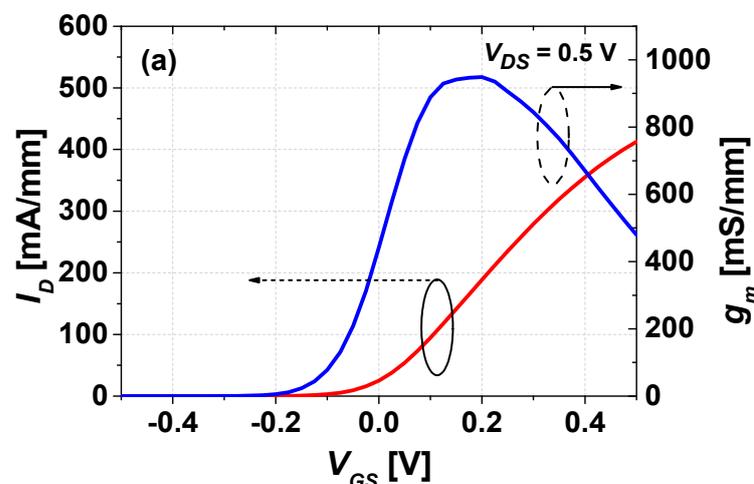
Figure 1. Cont.



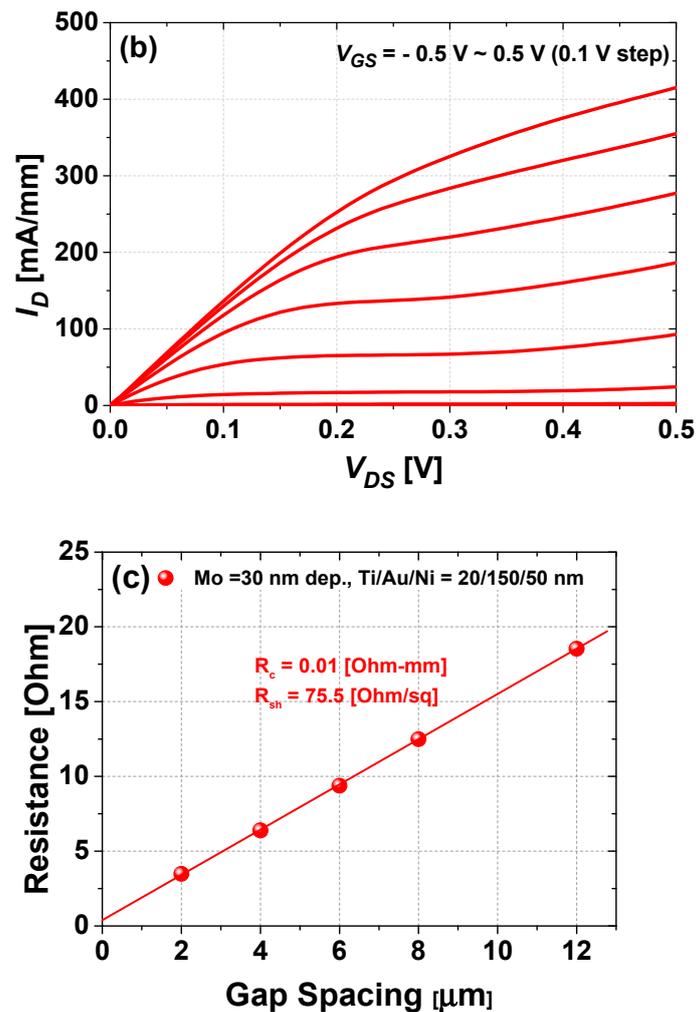
**Figure 1.** (a) Epitaxial structure of the  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  composite channel HEMT structure on a GaAs substrate. (b) Energy band diagram of the epitaxial structure (c) Schematic of the  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  composite channel HEMT on a GaAs substrate (d) SEM image of the fabricated T-gate.

### 3. Results and Discussion

The transfer characteristic and output characteristic of the mHEMTs are shown in Figure 2. The maximum transconductance ( $g_{m,max}$ ) and maximum drain current density ( $I_{D,max}$ ) were 949 mS/mm and 413 mA/mm at  $V_{DS} = 0.5$  V, respectively. The output characteristics presented in Figure 2b show good pinch-off characteristics, but the measured  $R_{on}$  was 733  $\Omega\text{-}\mu\text{m}$ , which is a higher value than the lift-off Mo/Ti/Mo/Au metal scheme with an InAs rich InAlAs barrier spacer [15]. The ohmic contact resistance ( $R_c$ ) and sheet resistance ( $R_{sh}$ ) measured by the transmission line method (TLM) was as low as 0.01  $\Omega\text{-mm}$  and 75.5  $\Omega/\text{sq}$  as shown in Figure 2c. When compared to the lift-off method using a Mo/Ti//Mo/Au scheme (30/20/20/150 nm) on the same multi-cap layer, the blanket Mo method shows a higher  $R_{sh}$  value of 75.5  $\Omega/\text{sq}$  than the lift-off method of 69.2  $\Omega/\text{sq}$  because of  $\text{SF}_6/\text{Ar}$  plasma damage in the active region during Mo etching to define the active gate region. However, the blanket Mo method shows a  $R_c$  of 0.011 Ohm-mm, which is lower than that of 0.026 Ohm-mm with the lift-off method because it is beneficial to protect the surface underneath the metal contact region from contaminants during the device process. Due to the lower  $R_c$  of the Mo blanket method, a lower  $R_{on}$  value could be achieved if the S/D distance was reduced, as in the self-aligned gate scheme.



**Figure 2.** Cont.



**Figure 2.** (a) Typical transfer characteristics of the mHEMTs measured at  $V_{DS} = 0.5$  V. (b) Typical output characteristics of the mHEMTs ( $V_{GS} = -0.5$  V  $\sim$  0.5 V). (c) TLM result of the Mo-based Ohmic contact.

Figure 3 shows the subthreshold characteristics at  $V_{DS} = 0.5$  V and 0.05 V, respectively. At  $V_{DS} = 0.5$  V, the threshold voltage ( $V_T$ ) is  $-0.13$  V, defined as the value of  $V_{GS}$  that yields at  $I_D = 1$  mA/mm, and a  $V_T$  of  $-0.13$  V indicates that the fabricated mHEMT operated in depletion mode (D-mode). The fabricated device shows excellent electrostatic integrity, such as the subthreshold swing (SS) of 84 mV/dec, the drain-induced barrier lowering (DIBL) of 89 mV/V, and the  $I_{on}/I_{off}$  ratio of  $9.8 \times 10^3$ , respectively. Additionally, the gate leakage current of the fabricated mHEMT was measured at  $V_{DS} = 0.5$  V and shows that the gate Schottky metallization is in good contact with the  $\text{In}_{0.52}\text{Al}_{0.48}\text{As}$  barrier layer. These outstanding logic performances are due to the well-designed heterostructure and optimized fabrication process on the GaAs substrate.

To verify the high-frequency RF characteristics of the mHEMT, S-parameters were measured from 0.5 to 40 GHz using a vector network analyzer (VNA). In addition, small-signal modeling was performed by using a small-signal equivalent circuit [16], and we found that small-signal modeling and measured S-parameters are well matched, as shown in Figure 4a. Figure 4b shows the unity current gain cutoff frequency ( $f_T$ ), maximum oscillation frequency ( $f_{max}$ ), and maximum stable gain (MSG)/maximum available gain (MAG) against frequency for the measured results (symbols) and modeled results (solid lines) at  $V_{DS} = 0.5$  V and  $V_{GS} = 0.2$  V with a  $L_g$  of 100 nm mHEMT device. The de-embedding method was done by using open and short patterns to extract parasitic pad capacitance and inductance. We obtained 261 GHz/304 GHz for  $f_T/f_{max}$  by extrapolation (dashed lines)

and 258 GHz/309 GHz for  $f_T/f_{max}$  by small-signal modeling, respectively. This excellent high-frequency response is due to the high value of the intrinsic transconductance ( $g_{mi}$ ) of 2.0 mS/ $\mu\text{m}$ . The extracted intrinsic parameters of the mHEMT are summarized in Table 1 and are well-matched to the measured results. The difference between  $g_{m,ext}$  (0.95 mS/ $\mu\text{m}$ ) and  $g_{mi}$  (2.0 mS/ $\mu\text{m}$ ) is due to the  $R_s$  and  $g_o$  values according to equation (1) [17].

$$g_{m,ext} = g_{mi}(1 - 2R_s \cdot g_o)/(1 + R_s \cdot g_{mi}) \tag{1}$$

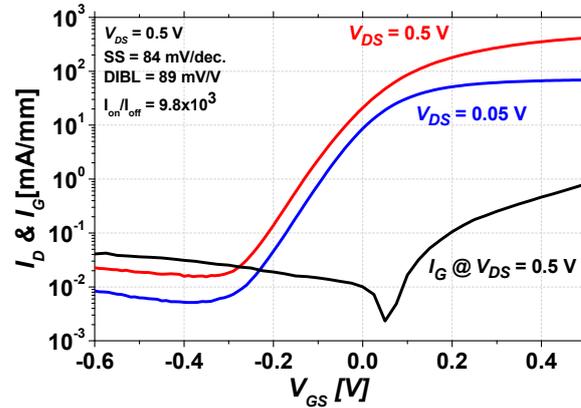


Figure 3. Subthreshold characteristics of the mHEMT were measured at  $V_{DS} = 0.5 \text{ V}$  and  $V_{DS} = 0.05 \text{ V}$ , and the gate leakage current was measured at  $V_{DS} = 0.5 \text{ V}$ , respectively.

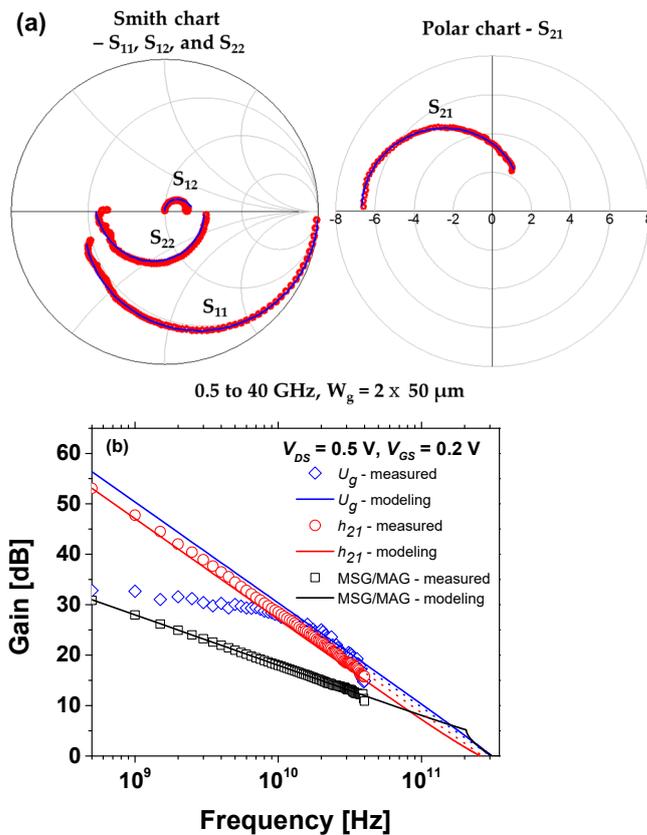


Figure 4. (a) Comparison of small-signal modeling and measured S-parameters at  $V_{DS} = 0.5 \text{ V}$  and  $V_{GS} = 0.2 \text{ V}$ . A Smith chart of  $S_{11}$ ,  $S_{12}$ , and  $S_{22}$  (left) and a polar chart of  $S_{12}$  (right). (b) Measured (symbols) and modeled (solid lines) of RF gains-Maximum oscillation frequency ( $f_{max}$ ), maximum stable gain (MSG)/maximum available gain (MAG), and unity current gain cutoff frequency ( $f_T$ ) of the mHEMTs at  $V_{DS} = 0.5 \text{ V}$  and  $V_{GS} = 0.2 \text{ V}$ .

**Table 1.** Extracted intrinsic small-signal parameters.

Intrinsic Parameters	Measured $f_T$	Modeling $f_T$
$g_{mi} = 2.0 \text{ mS}/\mu\text{m}$	261 GHz	258 GHz
$g_{ds} = 0.22 \text{ mS}/\mu\text{m}$		
$R_g = 70 \Omega\text{-}\mu\text{m}$		
$R_s = 360 \Omega\text{-}\mu\text{m}$		
$R_d = 360 \Omega\text{-}\mu\text{m}$	Measured $f_{max}$	Modeling $f_{max}$
$R_i = 100 \Omega\text{-}\mu\text{m}$	304 GHz	309 GHz
$C_{gs} = 0.65 \text{ fF}/\mu\text{m}$		

Figure 5 shows  $f_T$  and  $f_{max}$  as functions of  $I_D$  at  $V_{DS} = 0.5 \text{ V}$  and  $0.4 \text{ V}$ . Around an  $I_D$  of  $75 \text{ mA}/\text{mm}$ , our device had already exhibited an  $f_T$  and  $f_{max}$  value of over  $200 \text{ GHz}$  and was confirmed to operate stably for the fabricated mHEMT.

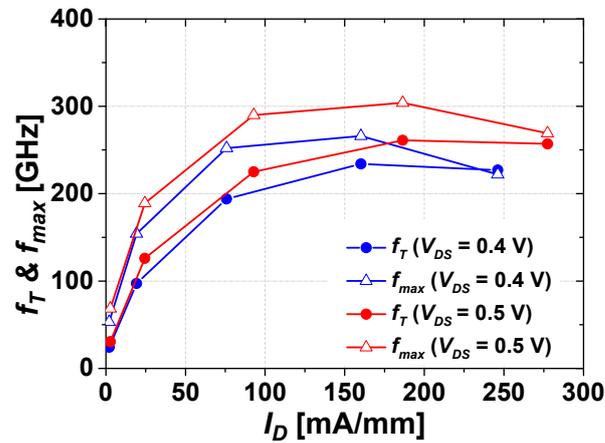
**Figure 5.** Maximum oscillation frequency ( $f_{max}$ ) and unity current gain cutoff frequency ( $f_T$ ) of the mHEMTs against drain current density ( $I_D$ ) at a  $V_{DS} = 0.5$  and  $0.4 \text{ V}$ , respectively.

Table 2 shows the benchmark high-frequency characteristics of the published state-of-the-art pHEMT and mHEMT results with an  $L_g$  of  $100 \text{ nm}$ . Among various HEMT structures, the  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  composite channel HEMT on an InP substrate shows excellent high-frequency characteristics such as an  $f_T$  of  $421 \text{ GHz}$  and an  $f_{max}$  of  $620 \text{ GHz}$  because of the well-optimized fabrication process and improved carrier transport properties of the  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  composite channel [18]. Our fabricated mHEMT exhibits an excellent  $L_g f_T$  of  $26.1 \text{ GHz}\text{-}\mu\text{m}$ , which is related to carrier transport properties [19], and an outstanding  $f_T/f_{max}$  of  $261/304 \text{ GHz}$  with a  $L_g$  of  $100 \text{ nm}$  at a  $V_{DS} = 0.5 \text{ V}$ . Although the performance of the fabricated mHEMT is not comparable to that of the  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  composite channel HEMT on an InP substrate, our fabricated mHEMT shows outstanding high-frequency characteristics compared to a single InGaAs channel HEMT on an InP substrate and other mHEMT structures because of the excellent transport properties of the composite channel on a GaAs substrate. Additionally, our fabricated device is operated at a  $V_{DS} = 0.5 \text{ V}$ , which has a lower power consumption than other group devices' operational voltage. These excellent performances are mainly attributed to the well-grown  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  composite channel structure by using an  $\text{In}_{0.52}\text{AlAs}$  buffer layer on a GaAs substrate, and a fabricated mHEMT would be a good candidate for the high-frequency device in both  $5\text{G}$  and  $6\text{G}$  communications through further scaling-down of device feature size.

**Table 2.** Performance parameters of the pHEMTs and mHEMTs with a  $L_g$  of 100 nm.

	[20]	[18]	[21]	[22]	This Work
Substrate	InP	InP	GaAs	GaAs	GaAs
Channel	$\text{In}_{0.68}\text{Ga}_{0.32}\text{As}$	$\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ / InAs/ $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$	$\text{In}_{0.65}\text{Ga}_{0.35}\text{As}$ / $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$	$\text{In}_{0.6}\text{Ga}_{0.4}\text{As}$	$\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ / InAs/ $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$
Buffer layer	InAlAs buffer	InAlAs buffer	Linear $\text{In}_x\text{Al}_{0.48}\text{Ga}_{0.52-x}\text{As}$	Graded InAlAs	500 nm $\text{In}_{0.52}\text{AlAs}$
$L_g$ [nm]	100	100	100	100	100
$f_T$ [GHz]	183	421	220	210	261
$f_{max}$ [GHz]	230	620	300	252	304
$L_g f_T$ [GHz- $\mu\text{m}$ ]	18.3	42.1	22.0	21.0	26.1
$V_{DS}$ [V]	0.5	0.7	1	1	0.5
Passivation	100 nm $\text{SiN}_x$	-	250 nm $\text{SiN}_x$	50 nm $\text{SiN}_x$	-

#### 4. Conclusions

The 100 nm  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  composite channel metamorphic high electron mobility transistors (mHEMTs) on a GaAs substrate exhibited excellent logic characteristics as well as high-frequency RF performances. These outstanding performances are due to the excellent carrier transport properties of the well-grown  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{InAs}/\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  composite channel mHEMT structure on a GaAs substrate and an optimized fabrication process. The proposed mHEMT structure on a GaAs substrate, together with optimized source/drain and gate technologies, will potentially improve logic and high-frequency characteristics. Furthermore, the proposed mHEMT structure grown on a large-size GaAs substrate could be indispensable for large-volume manufacturing.

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