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Abstract: This paper introduces a novel theoretical model of ternary nanoparticles for the improvement of heat transmission. Ternary nanoparticles in a heat conductor are shown in this model. Ternary nanoparticles consist of three types of nanoparticles with different physical properties, and they are suspended in a base fluid. Analytical solutions for the temperature and velocity fields are found by using the Laplace transform approach and are modeled by using a novel fractional operator. As a result, the ternary nanoparticles are identified, and an improved heat transfer feature is observed. Further experimental research on ternary nanoparticles is being carried out in anticipation of a faster rate of heat transmission. According to the graphed data, ternary nanoparticles have greater thermal conductivity than that of hybrid nanoparticles. Moreover, the fractional approach based on the Fourier law is a more reliable and efficient way of modeling the heat transfer problem than the artificial approach. The researchers were driven to create a concept of existing nanoparticles in order to boost heat transfer, since there is a strong demand in the industry for a cooling agent with improved heat transfer capabilities.

Keywords: ternary nanoparticles; hybrid nanoparticles; mono-nanoparticles; fourier's laws; Prabhakar fractional approach; channel flow

1. Introduction

Channel flow is crucial in a wide variety of industrial applications, such as in chemical reactors in the research industry and heat exchangers in power plants. There are numerous associated applications wherever the continuous fluid phase shows non-Newtonian stream properties, even though many procedures of real-world significance can also be characterized as two-phase flows through Newtonian behaviors in both phases. The biochemical, biomedical, and food processing industries all provide numerous examples [1]. On the scientific scale, Dippolito et al. [2] investigated the resistance of open channel flow caused by vegetation. The effects of a vortex generator's shape on liquids and the heat transition of hybrid nanofluids in a channel were studied by Zheng et al. [3]. Asjad et al. [4] discussed a hybrid nanoparticle analysis of fractional bioconvection in a channel flow.

Enhancing the rate of heat transmission of traditional base fluids is the main problem facing modern science and technology. To enhance heat performance and cooling systems, such as in the cooling of electronic devices, heat exchangers, and automotive cooling systems, with the greatest thermal performance, temperature reduction, precise working capability, and a long life span are required. As a result, scientists and researchers are intrigued the study of how solid particles transport heat in comparison to standard base fluids [5]. After conducting numerous studies, Choi and Eastman [6] found that adding a specific type of nano-sized particle suspension to the base fluid can speed up the rate of heat transfer. This fluid is referred to as a nanofluid. Moreover, it was found in this experiment that the base fluid's thermal transport capabilities were enhanced by a suspension of nanoparticles, which resulted in a higher stability than that in fluids containing milli-sized



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Copyright: © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). and micro-sized solid particles. Eastman et al. [7] showed that a normal fluid's thermal conductivity rises by 40 when ethylene glycol is mixed with 0.3% copper nanoparticles. Asjad et al. [8] explored advancements in generalized thermal processes and nanoparticle-based transport phenomena for vertical plates. Reddy et al. [9] discussed the performance of magnesium oxide and molybdenum disulfide nanoparticles in a micropolar thermal flux model. Izadi et al. [10] discussed a three-sided cavity and the characteristics of a porous material for the transient ordinary flow of energy transformation by a nanofluid. The extended Mittag–Leffler kernel and the impact of the MHD on a fractional Casson nanofluid with fixed boundary conditions were introduced by Saeed et al. [11].

Hybrid nanoparticles are combination of two different nanoparticles with a base fluid. Babazadeh et al. [12] studied hybrid nanofluids for free convective transportation within a porous medium in the presence of an externally supplied magnetic force. A base fluid that resulted in an exponentially extending bent surface was addressed by Nadeem et al. [13]. A study by Waini et al. [14] studied a continuous, fully established assorted convection stream on a longitudinally vertical surface embedded in a permeable medium with hybrid nanoparticles. Asadi et al. [15] addressed the topic of the effect of hybrid nanofluids on system stability. The work by Huminic et al. [16] explored different types of thermal structures intended for different boundary scenarios, and they included a summary of the effects of nanofluids and hybrid nanofluids on entropy formation. Asjad et al. [17] analyzed Prabhakar's fractional derivative and the advancement of non-Newtonian fluids that involved hybrid nanoparticles in turbulent channels.

Recently, researchers and scientists created a new class of nanoparticles by suspending three dissimilar types of nanoparticles in a pure fluid; this new class is known as ternary hybrid nanoparticles. Researchers have modified existing nanofluids in order to improve their thermal features, leading to the introduction of tri-hybrid nanoparticles, in response to the increased demand for cooling agents combined with the high thermal capabilities at the industrial level. As a result of this reasoning, more experimental studies have been carried out to improve the thermal properties of existing ternary nanoparticles by suspending three dissimilar types of solid nanoparticles in fluids [18,19]. Sahoo and Kumar [20] invented a novel correlation for evaluating the viscosity of ternary hybrid nanoparticles. The influences of temperature and particle volume concentration on the thermo-physical characteristics and rheological behaviors of aqueous ternary hybrid CuO/MgO/TiO2 nanoparticles were introduced by Mousavi et al. [21]. Raju et al. [22] discussed the nonlinear motions of isotropic ternary nanoparticles in thermally radiated Darcy walls of various forms and densities with extending or expanding permeability according to elementary linear regression. The stability of tri-hybrid nanoparticles in a water-ethylene glycol mixture was studied by Ramadhan et al. [23].

Fractional derivatives are essential in the mathematical modeling of practical events. It should be mentioned that fractional calculus is a topic from differentiation science, and L'Hopital introduced it in 1695. Fractional differential equations have recently gained much attention due to their numerous applications in the domains of engineering and physics. Therefore, learning how to generalize classical fluid models to fractional models is of interest for many analysts [24,25]. Some key findings on how to solve fractional differential equations were provided by Diethelm and Ford [26]. Sene [27] investigated a fractional derivative equation and the Caputo-Liouville component derivative to study the design of a second-grade fluid. The Caputo fractional derivative was used by Mozafarifarda et al. [28] to examine fractional thermal transfer equivalence for thin metallic sheets. Reyaz et al. [29] analyzed the Caputo-Fabrizio fractional derivative to assess the effects of thermal radiation and chemical reaction on MHD Casson fluid. An application of the Caputo-Fabrizio timefractional derivative by Hag et al. [30] revealed the impact of MHD on the channel flow of a fractionally viscous fluid through a porous medium. Thabet et al. [31] used a mathematical technique that connected the presence and constancy of ABC to study the numerical results of a unique disease, COVID-19. A Prabhakar fractional method based on the generalized Fourier law was used to study the convection flow of a Casson fluid through an oscillating

surface by Sarwar et al. [32]. Shah et al. [33] discussed Prabhakar-like fractional Maxwell fluids with generalized thermal transfer in natural convection.

An important class of nanoparticles, that of mono-, hybrid, and ternary nanoparticles on a two-sided vertical plate, has not been studied while using a fractional operator. To describe the channel flow problem, the Prabhakar fractional derivative was used, as it included mono-, hybrid, and ternary nanoparticles. As a result, the primary goal was to discover analytical solutions for the energy and momentum by using the Laplace transform method. The researchers were driven to create a concept of existing nanoparticles in order to boost heat transfer, since there is a strong demand in the industry for a cooling agent with improved heat transfer capabilities. Three types of nanoparticles with different physical properties were suspended as ternary nanoparticles. In order to support the experimental results, a theoretical model for ternary nanoparticles is presented in this study. The relationship between the thermo-physical properties of ternary nanoparticles is given in Table 1. The thermo-physical properties of nanoparticles and the base fluid are given in Table 2.

Ternary Nanoparticles				
$\mu_{mnf} = \mu_f (1 - (\phi_{Cu} + \phi_{Ag} + \phi_{TiO_2}))^{-2.5}$				
$\rho_{mnf} = (1 - (\phi_{mnf})\rho_f) + \phi_{Cu}\rho_{Cu} + \phi_{Ag}\rho_{Ag} + \phi_{TiO_2}\rho_{TiO_2}$				
$(\rho C_p)_{mnf} = (1 - (\phi_{mnf})(\rho C_p)_f + \phi_{Cu}(\rho C_p)_{Cu} + \phi_{Ag}(\rho C_p)_{Ag} + \phi_{TiO_2}(\rho C_p)_{TiO_2}$				
$(\rho\beta_T)_{mnf} = (1 - \phi_{mnf})(\rho\beta_T)_f + \phi_{Cu}(\rho\beta_T)_{Cu} + \phi_{Ag}(\rho\beta_T)_{Ag} + \phi_{TiO_2}(\rho\beta_T)_{TiO_2}$				
$\frac{\sigma_{mnf}}{\sigma_f} = 1 + \frac{3(\frac{\phi_{Cu}\sigma_{Cu}+\phi_{Ag}\sigma_{Ag}+\phi_{TiO_2}\sigma_{TiO_2}}{\sigma_f}-\phi_{mnf})}{(\frac{\phi_{Cu}\sigma_{Cu}+\phi_{Ag}\sigma_{Ag}+\phi_{TiO_2}\sigma_{TiO_2}}{\phi_{mnf}\sigma_f}+2)-(\frac{\phi_{Cu}\sigma_{Cu}+\phi_{Ag}\sigma_{Ag}+\phi_{TiO_2}\sigma_{TiO_2}}{\sigma_f}-\phi_{mnf})}$				
$\frac{k_{mnf}}{k_f} = \frac{\frac{\phi_{Cu}k_{Cu} + \phi_{Ag}k_{Ag} + \phi_{TiO_2}k_{TiO_2}}{\phi_{mnf}} + 2k_f + 2(\phi_{Cu}k_{Cu} + \phi_{Ag}k_{Ag} + \phi_{TiO_2}k_{TiO_2}) - 2k_f\phi_{mnf}}{\frac{\phi_{Cu}k_{Cu} + \phi_{Ag}k_{Ag} + \phi_{TiO_2}k_{TiO_2}}{\phi_{mnf}} + 2k_f + (\phi_{Cu}k_{Cu} + \phi_{Ag}k_{Ag} + \phi_{TiO_2}k_{TiO_2}) - k_f\phi_{mnf}}$				

Table 1. Thermo-physical properties of ternary nanoparticles [34].

Table 2. Thermo-physical properties of nanoparticles and the base fluid from [35,36].

Material	Base Fluid: Kerosene Oil	Silver (Ag)	Copper (Cu)	Titanium Dioxide (TiO ₂)
ρ (kg/m ³)	783	10500	8993	4250
C_p (J/kg·K)	2090	235	385	686.20
$k (W/m \cdot K)$	0.145	429	401	8.9538
σ (s/m)	$21 imes 10^{-6}$	$3.6 imes 10^7$	59.6×10^{6}	$2.6 imes 10^6$
$\beta imes 10^{-5} (1/K)$	99	1.89	1.67	0.90
Pr	21			

2. Mathematical Formulation for Fourier's Law

Let us consider an MHD convection flow through the microchannel of electrically conductive (Cu-Ag-TiO₂) tri-hybrid nanoparticles, as shown in Figure 1, under the following constraints. The microchannel length is infinite, with width *h*. The channel is along the *x*-axis and is normal to the *y*-axis. At t = 0, the temperature of the system is T_0 . After $t = 0^+$, the temperature increases from T_0 to T_1 . The fluid accelerates in the *x*-direction. A magnetic field of strength B_0 works transversely to the flow direction.

The flow of electrically conductive (Cu-Ag-TiO₂) tri-hybrid nanoparticles causes an electromotive force, which yields a current. Simultaneously, the induced magnetic field is ignored because of the hypothesis of a very small Reynolds number. Moreover, the electromagnetic force changes the intensity of the electric flux [17,18].

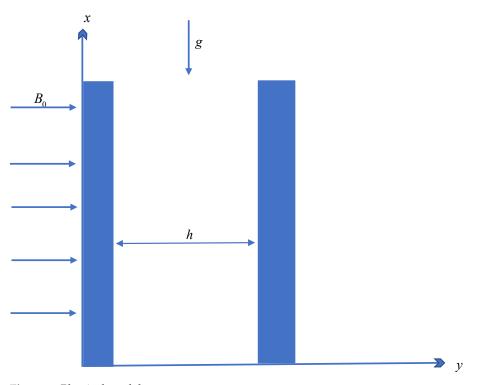


Figure 1. Physical model.

The momentum equation is:

$$\rho_{mnf}\left(\frac{\partial \breve{u}(y,t)}{\partial t} + \beta_{b^*}\breve{u}(y,t)\right) = \mu_{mnf}\frac{\partial^2 \breve{u}(y,t)}{\partial y^2} - \sigma_{mnf}B_0^2\breve{u}(y,t) + g(\rho\beta_T)_{mnf}[\breve{T}(y,t) - \breve{T}_0].$$
(1)

The energy equation is:

$$(\rho C_p)_{mnf} \frac{\partial \check{T}(y,t)}{\partial t} = -\frac{\partial \check{q}(y,t)}{\partial y}.$$
(2)

The generalized Fourier law for thermal flux is as follows:

$$\breve{q}(y,t) = -k_{mnf} \,^{C} D^{\gamma}_{\alpha,\beta,a} \, \frac{\partial \breve{T}(y,t)}{\partial y},\tag{3}$$

where the definition of the regularized Prabhakar derivative is ${}^{C}D_{\alpha,\beta,a}^{\gamma}$ and is defined as in [27,28].

For (1)–(3), we consider the following initial and boundary conditions [37]:

$$\breve{u}(0,t) = 0, \ \breve{T}(0,t) = T_0, \ as, \ t \ge 0,$$
(5)

By introducing dimensionless variables, we get

$$\tau = \frac{\nu_f}{h^2}t, \ Y = \frac{y}{h}, \ \breve{V} = \frac{h}{\nu_f}\breve{u}, \ \breve{q}_0 = \frac{\breve{k}_{mnf}(\breve{T}_1 - \breve{T}_0)\breve{u}_0}{\nu_{mnf}}, \ \breve{q}^* = \frac{\breve{q}}{\breve{q}_0}, \ \breve{T}^* = \frac{\breve{T} - \breve{T}_0}{\breve{T}_1 - \breve{T}_0}.$$
 (7)

The dimensionless fundamental equations are obtained by substituting (7) into (1)–(6) and ignoring the star documentation.

The dimensionless form of the momentum equation is as follows:

$$a_0^* \Big[\frac{\partial \breve{V}(Y,\tau)}{\partial \tau} + \beta_b^* \breve{V}(Y,\tau) \Big] = a_1^* \frac{\partial^2 \breve{V}(Y,\tau)}{\partial Y^2} - a_2^* M \breve{V}(Y,\tau) + a_3^* \mathrm{Gr} \breve{T}(Y,\tau).$$
(8)

The dimensionless form of the energy equation is as follows:

$$\frac{a_4^* \Pr}{\operatorname{Re}} \frac{\partial \check{T}(Y, \tau)}{\partial \tau} = -\frac{\partial \check{q}(Y, \tau)}{\partial Y}.$$
(9)

The dimensionless form of the generalized Fourier law for thermal flux [27,28] is as follows:

$$\breve{q}(Y,\tau) = -{}^{C}D^{\gamma}_{\alpha,\beta,a}\frac{1}{\operatorname{Re}}\frac{\partial \breve{T}(Y,\tau)}{\partial Y}.$$
(10)

The dimensionless forms of the associated conditions [37] are as follows:

$$\breve{V}(Y,0) = 0, \ \breve{T}(Y,0) = 0, \ as, \ Y \ge h,$$
(11)

$$\check{V}(0,\tau) = 0, \ \check{T}(0,\tau) = 0, \ as, \ \tau \ge 0,$$
 (12)

$$\breve{V}(1,\tau) = 0, \ \breve{T}(1,\tau) = 1.$$
 (13)

where the variables are as follows:

$$\begin{aligned} \Pr &= \frac{(\mu C_p)_f}{k_f}, \quad \beta_b^* = \frac{\beta_{b^*} h^2}{v_f}, \quad \operatorname{Gr} = \frac{g(\beta_T)_f h^3 (\check{T}_1 - \check{T}_0)}{v_f^2}, \quad \operatorname{M} = \frac{\sigma_f h^2 B_0^2}{\mu_f}, \quad \operatorname{Re} = \frac{\check{u}_0 h}{v_{mnf}}, \\ a_0^* &= 1 - (\phi_{mnf}) + \frac{\phi_{Cu}(\rho)_{Cu} + \phi_{Ag}(\rho)_{Ag} + \phi_{Tio_2}(\rho)_{Tio_2}}{\rho_f}, \\ a_2^* &= \frac{\sigma_{mnf}}{\sigma_f}, \quad a_3^* = 1 - (\phi_{mnf}) + \frac{\phi_{Cu}(\rho\beta_T)_{Cu} + \phi_{Ag}(\rho\beta_T)_{Ag} + \phi_{Tio_2}(\rho\beta_T)_{Tio_2}}{(\rho\beta_T)_f}, \\ a_4^* &= 1 - (\phi_{mnf}) + \frac{\phi_{Cu}(\rho C_p)_{Cu} + \phi_{Ag}(\rho C_p)_{Ag} + \phi_{Tio_2}(\rho C_p)_{Tio_2}}{(\rho C_p)_f}, \quad \lambda_{mnf} = \frac{k_{mnf}}{k_f}, \\ B_0 &= a_4^* \Pr, \quad B_1 = \frac{a_0^*}{a_1^*}, \quad B_2 = \frac{a_2^* M + a_0^* \beta_b^*}{a_1^*}, \quad B_3 = \frac{a_3^* \operatorname{Gr}}{a_1^*}, \quad B_4 = \frac{B_3}{B_2}. \end{aligned}$$

3. Results of the Problem for Fourier's Law

This section deals with the solution of the temperature and velocity fields with the Laplace transform method.

3.1. Outcome for the Temperature Field

By applying the Laplace transform to Equations (9) and (10) with conditions $(12)_2$ and $(13)_2$ and by utilizing the Prabhakar fractional derivative, for the temperature field, we get

$$\frac{B_0}{\operatorname{Re}}s\tilde{T}(Y,s) = -\frac{\partial\tilde{q}(Y,s)}{\partial Y},\tag{14}$$

and

$$\bar{\tilde{q}}(Y,s) = -(1 - as^{-\alpha})^{\gamma} s^{\beta} \frac{1}{\text{Re}} \frac{\partial \bar{\tilde{T}}(Y,s)}{\partial Y}.$$
(15)

By introducing Equation (15) into Equation (14), we get the following homogeneous differential equation:

$$\frac{\partial^2 \tilde{T}(Y,s)}{\partial Y^2} - \frac{B_0 s \tilde{T}(Y,s)}{(1 - a s^{-\alpha})^{\gamma} s^{\beta}} = 0,$$
(16)

which satisfies the following limitations:

$$\bar{\tilde{T}}(0,s) = 0, \quad \bar{\tilde{T}}(1,s) = \frac{1}{s}.$$
(17)

The general solution of Equation (16) with Equation (17) is as follows:

$$\bar{\tilde{T}}(Y,s) = \frac{1}{s} \left[\frac{sinhY \sqrt{\frac{B_0 s}{(1-a s^{-\alpha})^{\gamma} s^{\beta}}}}{sinh \sqrt{\frac{B_0 s}{(1-a s^{-\alpha})^{\gamma} s^{\beta}}}} \right].$$
(18)

It is important that Equation (18) can be written in the equivalent form:

$$\bar{\tilde{T}}(Y,s) = \frac{1}{s} \left[\sum_{m=0}^{\infty} e^{-(2m+1-Y)\sqrt{\frac{B_0s}{(1-as^{-\alpha})^{\gamma_s\beta}}}} - \sum_{m=0}^{\infty} e^{-(2m+1+Y)\sqrt{\frac{B_0s}{(1-as^{-\alpha})^{\gamma_s\beta}}}} \right].$$
(19)

The inverse Laplace transform cannot be found simply from the Laplace transform equation. As a result, Equation (19) is represented in the series as follows:

$$\bar{\tilde{T}}(Y,s) = \frac{1}{s} + \sum_{m=0}^{\infty} \sum_{n=1}^{\infty} \sum_{k=0}^{\infty} \frac{(Y-2m-1)^n (B_0)^{\frac{p}{2}}(a)^k}{n!k! \, s^{\alpha k + \frac{\beta n}{2} - \frac{n}{2} + 1}} \frac{\Gamma(\frac{\gamma n}{2} + k)}{\Gamma(\frac{\gamma n}{2})} + \sum_{m=0}^{\infty} \sum_{p=0}^{\infty} \sum_{l=0}^{\infty} \frac{(-Y-2m-1)^p (B_0)^{\frac{p}{2}}(a)^l}{p!l! \, s^{\alpha l + \frac{\beta p}{2} - \frac{p}{2} + 1}} \frac{\Gamma(\frac{\gamma p}{2} + l)}{\Gamma(\frac{\gamma p}{2})}.$$
(20)

Using the inverse Laplace transform of Equation (20), we have

$$\begin{split} \check{T}(Y,\tau) &= 1 + \sum_{m=0}^{\infty} \sum_{n=1}^{\infty} \sum_{k=0}^{\infty} \frac{(Y-2m-1)^n (B_0)^{\frac{n}{2}}(a)^k}{n!k!} \frac{t^{(\alpha k + \frac{\beta n}{2} - \frac{n}{2})}}{\Gamma(\alpha k + \frac{\beta n}{2} - \frac{n}{2} + 1)} \frac{\Gamma(\frac{\gamma n}{2} + k)}{\Gamma(\frac{\gamma n}{2})} + \\ &\sum_{m=0}^{\infty} \sum_{p=0}^{\infty} \sum_{l=0}^{\infty} \frac{(-Y-2m-1)^p (B_0)^{\frac{p}{2}}(a)^l}{p!l!} \frac{t^{\alpha l + \frac{\beta p}{2} - \frac{p}{2}}}{\Gamma(\alpha l + \frac{\beta p}{2} - \frac{p}{2} + 1)} \frac{\Gamma(\frac{\gamma p}{2} + l)}{\Gamma(\frac{\gamma p}{2})}. \end{split}$$
(21)

3.2. Outcome for the Velocity Field

By taking the Laplace transform of Equation (8) with constraints $(12)_1$ and $(13)_1$, we attain

$$\left[\frac{\partial^2}{\partial Y^2} - B_1 s - B_2\right] \tilde{\vec{V}}(Y,s) = -B_3 \tilde{\vec{T}}(Y,s),$$
(22)

which satisfies the following constraints:

$$\bar{V}(0,s) = 0, \quad \bar{V}(1,s) = 0.$$
(23)

From Equations (19), (22), and (23) we acquire the following results:

$$\bar{V}(Y,s) = -\frac{B_4}{s} \left[\frac{\sum_{m=0}^{\infty} e^{-(2m)\sqrt{\frac{B_0s}{s^{\beta}(1-as^{-\alpha})^{\gamma}}} - \sum_{m=0}^{\infty} e^{-(2m+2)\sqrt{\frac{B_0s}{s^{\beta}(1-as^{-\alpha})^{\gamma}}}}{[1 + (\frac{B_1s}{B_2} - \frac{B_0s}{B_2s^{\beta}(1-as^{-\alpha})^{\gamma}})]} \right] \\ \times \left[\sum_{n=0}^{\infty} e^{-(2n+1-Y)\sqrt{B_2+B_1s}} - \sum_{n=0}^{\infty} e^{-(2n+1+Y)\sqrt{B_2+B_1s}} \right] \\ + \frac{B_4}{s} \left[\frac{\sum_{m=0}^{\infty} e^{-(2m+1-Y)\sqrt{\frac{B_0s}{(1-as^{-\alpha})^{\gamma}s^{\beta}}}} - \sum_{m=0}^{\infty} e^{-(2m+1+Y)\sqrt{\frac{B_0s}{(1-as^{-\alpha})^{\gamma}s^{\beta}}}}}{[1 + (\frac{B_1s}{B_2} - \frac{B_0s}{B_2(1-as^{-\alpha})^{\gamma}s^{\beta}})]} \right].$$
(24)

The inverse Laplace of Equation (24) can be obtained numerically by using Tzou's and Stehfest's algorithms [38,39].

4. Mathematical Formulation of the Ternary Nanoparticles for Artificial Replacement

The momentum equation is:

$$\rho_{mnf}\left(\frac{\partial \breve{u}(y,t)}{\partial t} + \beta_{b^*}\breve{u}(y,t)\right) = \mu_{mnf}\frac{\partial^2 \breve{u}(y,t)}{\partial y^2} - \sigma_{mnf}B_0^2\breve{u}(y,t) + (g\beta_T)_{mnf}[\breve{T}(y,t) - \breve{T}_0].$$
(25)

The generalized Fourier law for thermal flux is as follows:

$$(\rho C_p)_{mnf} \frac{\partial \check{T}(y,t)}{\partial t} = k_{mnf} \,^C D^{\gamma}_{\alpha,\beta,a} \frac{\partial^2 \check{T}(y,t)}{\partial y^2}.$$
(26)

where the definition of the regularized Prabhakar derivative is ${}^{C}D_{\alpha,\beta,a}^{\gamma}$ and is defined as in [27,28].

We get the results for the temperature and velocity fields by using Equations (12) and (13). The dimensionless form of the momentum equation is:

$$a_0^* \begin{bmatrix} ^C D_{\alpha,\beta,a}^{\gamma} \frac{\partial \breve{V}(Y,\tau)}{\partial \tau} + \beta_b^* \breve{V}(Y,\tau) \end{bmatrix} = a_1^* \frac{\partial^2 \breve{V}(Y,\tau)}{\partial Y^2} - \mathrm{M}a_2^* \breve{V}(Y,\tau) + \mathrm{Gr}a_3^* \breve{T}(Y,\tau).$$
(27)

The dimensionless form of the generalized Fourier law for heat flux is:

$${}^{C}D^{\gamma}_{\alpha,\beta,a}A_{4}^{*}\Pr\frac{\partial \check{T}(Y,\tau)}{\partial \tau} = \frac{\partial^{2}\check{T}(Y,t)}{\partial Y^{2}}.$$
(28)

5. Results of the Problem for Artificial Replacement

This section deals with the solutions of the temperature and velocity fields with the Laplace transform method.

5.1. Outcome for the Temperature Field

By applying the Laplace transform to Equation (28) with conditions $(12)_2$ and $(13)_3$ and utilizing the Prabhakar fractional derivative, for the temperature field, we get

$$B_0(1 - as^{-\alpha})^{\gamma} s^{\beta} \bar{\tilde{T}}(Y, s) = \frac{\partial \tilde{T}(Y, s)}{\partial Y^2},$$
(29)

which satisfies the following limitations:

$$\tilde{\tilde{T}}(0,s) = 0, \quad \tilde{\tilde{T}}(1,s) = \frac{1}{s}.$$
(30)

The general solution of Equation (29) with Equation (30) is as follows:

$$\bar{\tilde{T}}(Y,s) = \frac{1}{s} \left[\frac{\sinh Y \sqrt{B_0 \, s^\beta (1 - as^{-\alpha})^\gamma}}{\sinh \sqrt{B_0 \, s^\beta (1 - as^{-\alpha})^\gamma}} \right].$$
(31)

It is important that previous Equation can be written in the equivalent form:

$$\bar{\tilde{T}}(Y,s) = \frac{1}{s} \left[\sum_{m=0}^{\infty} e^{-(2m+1-Y)\sqrt{B_0 s^\beta (1-as^{-\alpha})^\gamma}} - \sum_{m=0}^{\infty} e^{-(2m+1+Y)\sqrt{B_0 s^\beta (1-as^{-\alpha})^\gamma}} \right].$$
(32)

The inverse Laplace transform cannot be found simply from the Laplace transform equation. As a result, Equation (32) is represented in the series as follows:

$$\tilde{T}(Y,s) = \frac{1}{s} + \sum_{m=0}^{\infty} \sum_{l_1=1}^{\infty} \sum_{l_1=0}^{\infty} \frac{(Y-2m-1)^{l_1}(B_0)^{\frac{l_1}{2}}(a)^{l_2}}{l_1!l_2! \, s^{\alpha l_2 - \frac{\beta l_1}{2} + 1}} \frac{\Gamma(\frac{\gamma l_1}{2} + 1)}{\Gamma(\frac{\gamma l_1}{2} + 1 - l_2)} \\
+ \sum_{m=0}^{\infty} \sum_{l_3=0}^{\infty} \sum_{l_4=0}^{\infty} \frac{(-Y-2m-1)^{l_3}(B_0)^{\frac{l_3}{2}}(a)^{l_4}}{l_3!l_4! \, s^{\alpha l_4 - \frac{\beta l_3}{2} + 1}} \frac{\Gamma(\frac{\gamma l_3}{2} + 1)}{\Gamma(\frac{\gamma l_3}{2} + 1 - l_4)}.$$
(33)

Using the inverse Laplace transform of Equation (33), we have

$$\begin{split} \check{T}(Y,\tau) &= 1 + \sum_{m=0}^{\infty} \sum_{l_1=1}^{\infty} \sum_{l_1=0}^{\infty} \frac{(Y-2m-1)^{l_1} (B_0)^{\frac{l_1}{2}} (a)^{l_2}}{l_1! l_2!} \frac{t^{\alpha l_2 - \frac{\beta l_1}{2}}}{\Gamma(\alpha l_2 - \frac{\beta l_1}{2} + 1)} \frac{\Gamma(\frac{\gamma l_1}{2} + 1)}{\Gamma(\frac{\gamma l_1}{2} + 1 - l_2)} \\ &+ \sum_{m=0}^{\infty} \sum_{l_3=0}^{\infty} \sum_{l_4=0}^{\infty} \frac{(-Y-2m-1)^{l_3} (B_0)^{\frac{l_3}{2}} (a)^{l_4}}{l_3! l_4!} \frac{t^{\alpha l_4 - \frac{\beta l_3}{2}}}{\Gamma(\alpha l_4 - \frac{\beta l_3}{2} + 1)} \frac{\Gamma(\frac{\gamma l_3}{2} + 1)}{\Gamma(\frac{\gamma l_3}{2} + 1 - l_4)}. \end{split}$$
(34)

5.2. Outcome for the Velocity Field

By applying the Laplace transform to Equation (27) with constraints $(12)_1$ and $(13)_1$, we attain

$$\left[\frac{\partial^2}{\partial Y^2} - B_1 s^\beta (1 - a s^{-\alpha})^\gamma - B_2\right] \bar{V}(Y, s) = -B_3 \bar{T}(Y, s), \tag{35}$$

which satisfies the following constraints:

$$\bar{V}(0,s) = 0, \quad \bar{V}(1,s) = 0.$$
(36)

From Equations (32), (35), and (36), we acquire the following results:

$$\begin{split} \vec{\tilde{V}}(Y,s) &= -\frac{B_4}{s} \left[\frac{\sum_{m=0}^{\infty} e^{-(2m)\sqrt{B_0 s^{\beta}(1-as^{-\alpha})^{\gamma}}} - \sum_{m=0}^{\infty} e^{-(2m+2)\sqrt{B_0 s^{\beta}(1-as^{-\alpha})^{\gamma}}}}{[1 + \frac{(B_1 - B_0)s^{\beta}(1-as^{-\alpha})^{\gamma}}{B_2}]} \right] \\ &\times \left[\sum_{n=0}^{\infty} e^{(Y-2n-1)\sqrt{B_2 + B_1(1-as^{-\alpha})^{\gamma} s^{\beta}}} - \sum_{n=0}^{\infty} e^{(-Y-2n-1)\sqrt{B_2 + B_1(1-as^{-\alpha})^{\gamma} s^{\beta}}}} \right] \\ &+ \frac{B_4}{s} \left[\frac{\sum_{m=0}^{\infty} e^{-(2m+1-Y)\sqrt{B_0 s^{\beta}(1-as^{-\alpha})^{\gamma}}} - \sum_{m=0}^{\infty} e^{-(2m+1+Y)\sqrt{B_0 s^{\beta}(1-as^{-\alpha})^{\gamma}}}}{[1 + \frac{(B_1 - B_0)s^{\beta}(1-as^{-\alpha})^{\gamma}}{B_2}]} \right]. \end{split}$$
(37)

The inverse Laplace transform of Equation (37) can be obtained numerically by using Tzou's and Stehfest's algorithms [38,39].

6. Results and Discussion

Figures 2 and 3 present the behavior of the concentrations of the three types of nanoparticles for the temperature and velocity fields, respectively. It is clear in Figure 2 that the temperature can be enhanced to its maximum, unlike with hybrid and mono-nanoparticles. Due to the increase in the concentration of ternary nanoparticles, the thermal conductivity and, hence, the temperature increase. Figure 3 depicts the outcomes for the velocity to see the impact of the volume fraction ($\phi_1 = \phi_2 = \phi_3 = 0.02$). It is found that the velocity is a decreasing function of the concentration of the nanoparticles, and the maximum decline can be observed, unlike with hybrid and mono-nanoparticles. Physically, this is due to fact that increasing the concentration causes the fluid to become more thick; the space between the layers is reduced and, ultimately, the fluid flows slowly.

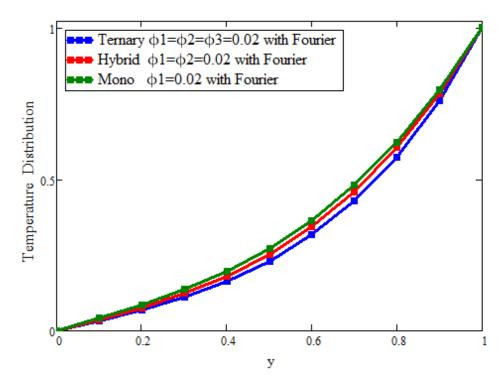
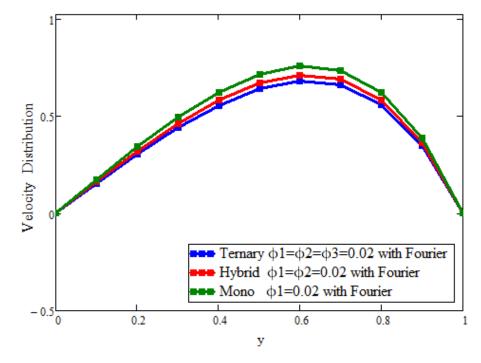


Figure 2. Comparison of temperature field assessments across y for the volumetric fraction of $\phi_1 = \phi_2 = \phi_3 = 0.02$, where $\alpha = \beta = \gamma = 0.5$, a = 0.02, t = 1.6, and Pr = 21.

Figure 4 presents the issue of modeling with the fractional derivative. This figure is plotted for the solutions that were obtained artificially and with the Fourier law. By fixing the flow parameters as constant and varying the values of the fractional parameters, it is evident that the solutions based on the Fourier law are efficient and exhibit more memory in comparison with the solutions obtained through replacement. A similar behavior is observed for velocity, as shown in Figure 5. Physically, the fractional operators are responsible for the memory of the fluid's properties for different values of the fractional parameters at different times.

Figure 6 shows only the effects of ternary nanoparticles with the Fourier law and replacement. Taking $\phi_1 = \phi_2 = \phi_3 = 0.01$ for the solutions, it was found that the ternary nanoparticles with the Fourier law predicted a greater enhancement in the temperature than that predicted in the artificial case. On the other hand, by increasing the concentration from 0.01 to 0.04, the temperature also increased, which supported the physical reasoning of the fluid temperature. Figure 7 plots only the effects of the ternary nanoparticles with the Fourier law and replacement. Taking $\phi_1 = \phi_2 = \phi_3 = 0.01$ for the solutions, it was found that the ternary nanoparticles with the Fourier law predicted a greater decline in the velocity than that predicted in the artificial case. On the other hand, by increasing the concentration



from 0.01 to 0.04, the velocity was also decreased, which supported the physical reasoning of the fluid velocity.

Figure 3. Comparison of velocity field assessments across y for the volumetric fraction of $\phi_1 = \phi_2 = \phi_3 = 0.02$, where $\alpha = \beta = \gamma = 0.5$, t = 1.1, Gr = 15, Pr = 21, a = 0.02, and M = 1.2.

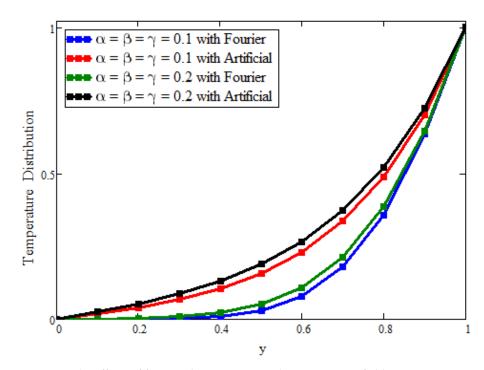


Figure 4. The effects of fractional parameters on the temperature field. Here, a = 0.02, t = 0.4, Pr = 21, $\phi_1 = 0.01$, $\phi_2 = 0.02$, and $\phi_3 = 0.03$.

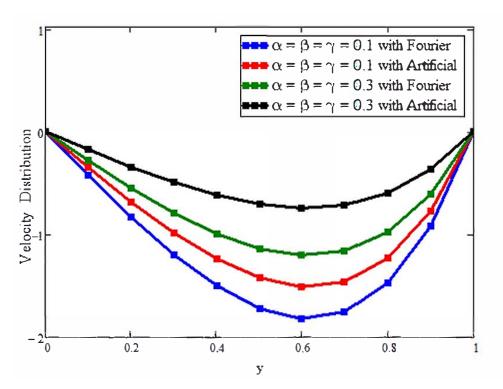


Figure 5. The effects of fractional parameters on the velocity field. Here, a = 0.02, t = 0.2, Pr = 21, Gr = 15, M = 1.2, $\phi_1 = 0.01$, $\phi_2 = 0.02$, and $\phi_3 = 0.03$.

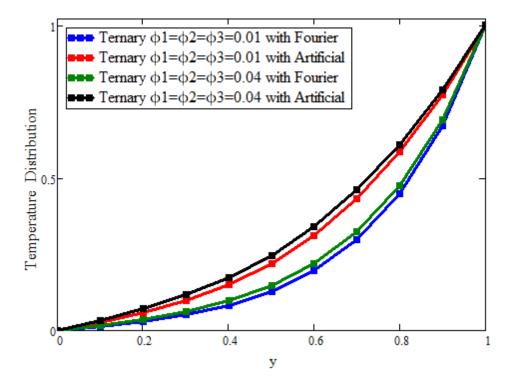


Figure 6. The effect of the volumetric fraction on the temperature field. Here, Pr = 21, $\gamma = 0.7$, $\alpha = 0.7$, $\beta = 0.7$, a = 0.02, and t = 0.3.

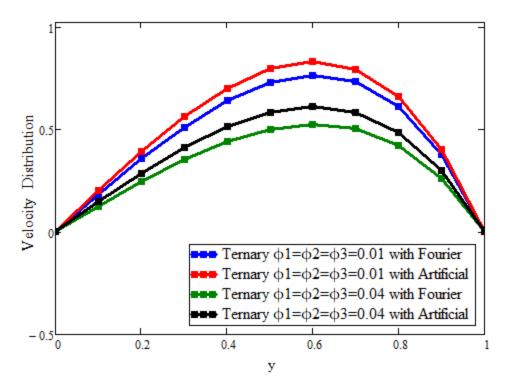


Figure 7. The effect of the volumetric fraction on the velocity field. Here, Pr = 21, a = 0.02, t = 2, $\alpha = 0.7$, $\beta = 0.7$, $\gamma = 0.7$, Gr = 15, and M = 1.2.

7. Conclusions

This study focuses on the numerical solutions of fractional partial differential equations that appear in phenomena. An approach that uses Prabhakar fractional models with a Laplace transform is used to investigate unsteady MHD convective streams of incompressible viscous fluids in a moving frame with a non-Newtonian fluid in a turbulent channel with ternary nanoparticles and Prabhakar fractional derivatives on the boundary. Therefore, the thermal transport model is based on the generalized fractional Fourier law of the thermal flux. By using the Mathcad software, some of the physical implications of the flow characteristics were examined. Graphical representations of two components, velocity and temperature, were created. It was discovered that the thermal transport's damping has a significant impact on the fluid's temperature and velocity.

- The heat transfer properties of ternary nanoparticles are superior to those of fluids, mono-nanoparticles, and hybrid nanoparticles.
- It is evident that fractional modeling based on the Fourier law is efficient and suitable in comparison with replacement.
- The Prabhakar fractional approach is responsible for the better memory of the function due to the generalized Mittag–Leffer kernel of the three parameters.

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Abbreviations

The following abbreviations are used in this manuscript:

- Pr Dimensionless Prandtl number
- Gr Dimensionless Groshof number
- Μ Magnetic field parameter
- Ř Thermal conductivity (m/WK)
- ĕ Dimensionless temperature
- Fluid density (kg/m^3) ρ
- Electrical conductivity σ
- Kinematic viscosity (m²/s) v
- t Time (s)
- Dynamic viscosity (kg/ms) μ
- C_p Specific heat (J/kg K)
- (ρC_p) \check{T} Heat capacitance $(J/kg m^3)$
- Temperature (K)
- Ť∞ Ambient temperature (K)
- Ťw Surface temperature (K)
- ŭ, ŭ Velocity component (m/s)
- α, β, γ Fractional parameters

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