



Article Mapping of Peat Thickness Using a Multi-Receiver Electromagnetic Induction Instrument

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Received: 29 June 2020; Accepted: 30 July 2020 ; Published: 31 July 2020



Abstract: Peatlands constitute extremely valuable areas because of their ability to store large amounts of soil organic carbon (SOC). Investigating different key peat soil properties, such as the extent, thickness (or depth to mineral soil) and bulk density, is highly relevant for the precise calculation of the amount of stored SOC at the field scale. However, conventional peat coring surveys are both labor-intensive and time-consuming, and indirect mapping methods based on proximal sensors appear as a powerful supplement to traditional surveys. The aim of the present study was to assess the use of a non-invasive electromagnetic induction (EMI) technique as an augmentation to a traditional peat coring survey that provides localized and discrete measurements. In particular, a DUALEM-421S instrument was used to measure the apparent electrical conductivity (EC_a) over a 10-ha field located in Jutland, Denmark. In the study area, the peat thickness varied notably from north to south, with a range from 3 to 730 cm. Simple and multiple linear regressions with soil observations from 110 sites were used to predict peat thickness from (a) raw EC_a measurements (i.e., single and multiple-coil predictions), (b) true electrical conductivity (σ) estimates calculated using a quasi-three-dimensional inversion algorithm and (c) different combinations of ECa data with environmental covariates (i.e., light detection and ranging (LiDAR)-based elevation and derived terrain attributes). The results indicated that raw EC_a data can already constitute relevant predictors for peat thickness in the study area, with single-coil predictions yielding substantial accuracies with coefficients of determination (R²) ranging from 0.63 to 0.86 and root mean square error (RMSE) values between 74 and 122 cm, depending on the measuring DUALEM-421S coil configuration. While the combinations of EC_a data (both single and multiple-coil) with elevation generally provided slightly higher accuracies, the uncertainty estimates for single-coil predictions were smaller (i.e., smaller 95% confidence intervals). The present study demonstrates a high potential for EMI data to be used for peat thickness mapping.

Keywords: digital soil mapping; proximal soil sensing; peat thickness; apparent electrical conductivity; electromagnetic induction; quasi-3D inversion

1. Introduction

Under natural conditions, peatlands constitute carbon sinks. However, they have been used both for fuel mining and agriculture for over 1000 years. Climate change and rapid land use change have turned peatlands into carbon sources. Within the European Union 2030 climate and energy framework, all member states have to report on the emissions and removals of greenhouse gases from wetlands, including peatlands [1]. The assessment of key peat soil properties, such as the extent, thickness (or depth to mineral soil) and bulk density, is highly relevant for the precise calculation of the amount of stored soil organic carbon (SOC) at the field scale. Several methods have been used to measure peat thickness (or depth to mineral layer) in the field. Conventional measurements using hand augers are still commonly used, although this process is labor-intensive and time-consuming and only provides depth observations at single point locations. In different Digital Soil Mapping (DSM) studies, models were derived to predict peat thickness using conventional field observations and environmental data. Considering environmental data, a few studies mostly used terrain attributes, including elevation and slope [2,3], only elevation [4] or the distance to a river [5]. More recently, machine learning models have also been used [6-8] as well as regression kriging [9]. Rudiyanto et al. [6] (2016) and Young et al. [9] (2018) built models using a relatively limited amount of environmental data (i.e., elevation, slope, aspect, System of Automated Geoscientific Analyses Wetness Index (SAGAWI) and nearest distance to river for the first study, and elevation, slope, aspect, vegetation type and soil for the latter). Rudiyanto et al. [8] (2018) and Aitkenhead [7] (2017) used a wide array of environmental covariates: topography (i.e., elevation, vegetation-corrected elevation, and two derived terrain attributes—the Multi-Resolution Index of Valley Bottom Flatness (MRVBF) and SAGAWI-Euclidean distances to rivers, seas and combined rivers and seas, radar images (i.e., Sentinal-1A and ALOS-PALSAR) and vegetation (i.e., seven Landsat raw bands and the normalized difference vegetation index) in Rudiyanto et al. [8] (2018), and topography (i.e., elevation and seven derived terrain attributes), climate (i.e., 24 different meteorological layers), soil (i.e., land cover, geology and soil maps) and vegetation (i.e., Landsat raw bands and derived vegetation indices) in Aitkenhead [7] (2017).

Within soil sensing, geophysical techniques constitute a powerful supplement to traditional coring in the attempt to map peat properties at different scales. These methods cannot represent a complete alternative to field coring although they can significantly reduce costs by limiting the dependency on the latter only for calibration purposes. Peat displays particular electric properties, making geoelectric methods more suitable for mapping its thickness or extent. Its electrical conductivity depends mainly on the water content and amount of dissolved ions [10-12]). Peat also presents a high relative dielectric permittivity due to its generally high water content, which allows it to be distinguished from mineral soils with lower permittivity values [13]. Remote sensing and airborne geophysical techniques represent the most suitable means to investigate peatlands at a large scale (>10 km²). Several recent studies have successfully used airborne electromagnetic (AEM) methods to estimate peatland thickness and extent [14-17]. Likewise, different proximal or ground-based geophysical sensors have been accurately applied to map peat properties at smaller scales. Ground-penetrating radar (GPR) and electrical conductivity or resistivity surveys have been predominantly used to map peatlands [12]. In particular, GPR, which detects the contrast in dielectric permittivity, has been extensively used to map peat thickness for the last three decades [18–22]. Other studies have used complex electrical conductivity surveys [23] and electrical resistivity surveys [24] to explore the stratigraphy of peat. Electrical conductivity surveys based on electromagnetic induction (EMI) measure the apparent electrical conductivity (EC_a) for a volume of soil. Recent advances in EMI technology have resulted in the advent of on-the-go sensing systems, making it possible to determine EC_a for varying depths. EC_a can further be used to determine true electrical conductivity (σ) estimates from quasi-three-dimensional (quasi-3D) inversion models [25,26], thereby enabling the variation of soil properties in 3D to be inferred [27–29]. To our knowledge, EMI surveys have only been implemented in a few studies on peatlands: Theimer et al. [19] (1994) studied peat thickness, Slater and Reeve [21] (2002) investigated peatland stratigraphy and hydrology, Comas et al. [30] (2011) focused on peat basin morphology, and Koszinski et al. [31] (2015) and Altdorff et al. [32] (2016) estimated bulk density, SOC content and stock. Furthermore, a recent study by Boaga et al. [33] (2020) hypothesized that the combination of proximal and airborne electromagnetic data could be successfully used in a joint inversion scheme with the aim of enhancing the AEM survey resolution where ground-based EMI data are available and extending the results to larger areas where only AEM data might be available.

The aim of the present case study is to assess the use of data collected from a single-frequency multi-receiver EMI instrument—namely a DUALEM-421S—for the prediction of peat thickness. Soil observations were used for calibration and validation purposes. Linear regression (LR) and

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multiple linear regression (MLR) were used to investigate the spatial variability of peat thickness over a 10 ha field area located in Jutland, Denmark. This was done solely from EC_a measurements (i.e., single and multiple-coil predictions) or from σ estimates calculated using a quasi-3D inversion algorithm and from the combination of EC_a data with environmental covariates (i.e., topography variables comprising elevation and derived terrain attributes).

2. Materials and Methods

2.1. Study Area

The study area is a 10 ha agricultural field with a high peat thickness gradient (3–730 cm), located in the Nørre Å valley in central Jutland, Denmark (Figure 1). The field mainly comprises organic soil areas and small zones with mineral soils (coarse sand). This site is considered as a riparian fen peatland [34] where vascular plants such as reeds and sedges dominate [12]. As will be discussed later, and similar to Walter et al. [12] (2015), its specific configuration, underlain by sandy soils characterized by low electrical conductivity, ensured a contrast with the peat layers, which generally present higher electrical conductivity. The field belongs to the East Jutland glacial landscape and borders a young moraine landscape to the West [35]. The originally uneven tunnel-valley bottom has been covered by sea and organic sediments deposited after the last glaciation [36]. The study area is characterized by a temperate oceanic climate with a winter mean temperature of 0 °C and a summer mean temperature of 17 °C. The annual precipitation ranges from 650 to 750 mm [37]. The field is tile-drained and currently used as extensive grassland.



Figure 1. Location of soil observations collected during two sampling survey campaigns within the study area (orthophoto from the spring 2006 as background [38]).

2.2. Soil Observations and Sampling Design

Soil observations were collected during two sampling survey campaigns in June 2017 and May 2019 (Figure 1). The thickness of peat deposits (or depth to the mineral layer) was investigated using a peat probe including a 120 cm main part and 94 cm extension rods. During the 2017 campaign, 76 soil observations were carried out following five pseudo-transects roughly in a southwest–northeast

orientation. These first observations were restricted to the southern half of the study area as a plot experiment was running in the northern part. The locations were selected directly in the field using the results from a DUALEM-21S survey carried out at the same time. Preliminary EC_a maps were generated using kriging within ArcMap [39]. During the 2019 campaign, 34 soil observations were carried out following three transects in a northwest–southeast orientation. Their locations were selected using preliminary kriged EC_a maps from a recent DUALEM-421S survey (i.e., from April 2019). In total, 110 soil observations were used as calibration and validation data within the predictive modeling of peat thickness. The sampling approach can be compared to that recommended by Rudiyanto et al. [6] (2016), which was based on (1) stratifying the study area by elevation (in our case, kriged EC_a data) and (2) sampling locations along transects crossing all strata or random locations within each stratum (in our case, along transects). The precise location of each soil observation was determined in the field using a conventional portable GPS system (Trimble SPS851 Global Navigation Satellite System, Trimble Navigation Limited, Sunnyvale, CA, USA).

2.3. DUALEM-421S Data Collection

An EMI instrument typically comprises a transmitter (Tx) and a receiver (Rx) coil. A primary magnetic field is generated by powering the Tx coil with an alternating current. This primary field creates eddy currents in the conductive media present in the subsurface inducing a secondary magnetic field. Both the primary and secondary fields are detected at the Rx coil. Since the primary field is known depending on the Tx–Rx configuration, the secondary field can be calculated in relation to the response to the actual subsurface properties [40]. The quadrature-phase and in-phase signal response of an EMI instrument are representative of the EC_a and magnetic susceptibility of the soil [41].

In our study, the EC_a data were collected using a single-frequency multi-receiver DUALEM-421S instrument. The instrument operates at a low frequency (9 kHz) and comprises three pairs of perpendicular (PRP) and horizontal coplanar (HCP) coil arrays. The Tx coil is located at one end and is shared by all Rx coils. The distances from the Tx to the PRP and HCP Rx coils are 1.1, 2.1 and 4.1 m, and 1, 2 and 4 m, respectively. The depth of exploration (DOE) is the depth at which the signal accumulates 70% of its total sensitivity [41]. At low induction numbers, the DOE is a function of the coil spacing (*S*) and orientation, and the DOEs for the PRP and HCP configurations are 0.5 *S* and 1.6 *S*, respectively, when the instrument is placed on the ground [42]. As such, the DOE sfor the different coil configurations are as follows: for the 1 m Rx coils, 0–50 cm (1mPRP), 0–160 cm (1mHCP); for the 2 m Rx coils, 0–100 cm (2mPRP) and 0–320 cm (2mHCP); and for the 4 m Rx coils, 0–200 cm (4mPRP) and 0–640 cm (4mHCP).

The DUALEM-421S survey consisted of crossing the field in about 60 roughly parallel transects in a southwest–northeast orientation (Figure 2). The transects were spaced approximately 5–6 m apart with the instrument held 0.3 m above the surface of the ground. Notably, two small zones in the northwestern part of the study area could not be surveyed because of the prohibitively dense vegetation due to the former plot experiment (Figure 2). A total of 48,150 EC_a measurements were collected and georeferenced using a real-time kinematic (RTK) Trimble SPS851 global navigation satellite system (GNSS, Trimble Navigation Limited, Sunnyvale, CA, USA) installed on the top of the Tx coil. The RTK/GNSS georeferencing and EC_a data were logged using an ALGIZ 10X data logger and StarPal HGIS Professional logging software.



Figure 2. Location of the DUALEM-421S survey transects within the study area.

2.4. DUALEM-421S Data Processing and Inversion

Aarhus Workbench software [43] was used for dedicated data processing and inversion. Firstly, data processing was performed using both automatic and manual steps. In the automatic data processing, the negative EC_a values were removed and the measurements from different channels were corrected for the offset between the RTK/GNSS and the center of the Tx–Rx arrays. An average sounding distance of 1 m was chosen, and the data from all channels were averaged using a running mean width of 3 m to improve the signal-to-noise ratio. An appropriate choice of the sounding distance and running mean width was necessary in order not to smear the data generated by the soil variability at hand and to discard the redundant information to reduce the computation time for performing inversions. Later, a manual inspection of the raw data was performed to remove the potential noise due to anthropogenic coupling; for example, this relates to buried cables, field monitoring installations or the proximity of the instrument to the ATV when making turns. The changes made in the raw data were integrated back into the averaged data generated through the automatic processing step.

After data processing, the inversions were performed using a fully nonlinear inversion routine (AarhusInv code) with a quasi-3D spatially constrained algorithm that applied constraints in both in-line and cross-line directions using Delaunay triangulation [25,26]. The inversions were executed using two-layered, three-layered, four-layered, smooth, blocky and sharp models with an initial σ estimate of 25 mS/m. Later, the σ estimates were retrieved using a depth interval of 50 cm starting from 0 to 750 cm (i.e., 15 layers for each model). As a final step, quality control was accomplished by plotting the total residual, data residuals and depth of investigation (DOI) to assess the quality of inversions. We refer to a report [44] for a detailed explanation on the regularization schemes employed and Christiansen et al. [45] (2016) for a more comprehensive overview of the data processing and inversion of a DUALEM instrument using the Aarhus Workbench software.

2.5. Environmental Covariates

In addition to the six EC_a and six σ -based variables (i.e., 1mPRP, 1mHCP, 2mPRP, 2mHCP, 4mPRP, and 4mHCP, and $\sigma_{2-layered}$, $\sigma_{3-layered}$, $\sigma_{4-layered}$, σ_{blocky} , σ_{smooth} , and σ_{sharp}), we tested a few environmental covariates (i.e., topography variables) as predictors for the peat thickness modeling: (a) a Digital Elevation Model (DEM) derived from the national 1.6 m resolution airborne LiDAR data and (b) terrain attributes derived from the DEM using ArcGIS [31] or SAGAGIS [36]. The different

terrain attributes were as follows: slope gradient, MRVBF (an indicator of depositional areas to identify valley bottoms), SAGAWI (a topographic wetness index calculated from the slope gradient and modified catchment area), profile curvature (curvature parallel to the maximum slope) and plan curvature (curvature perpendicular to the maximum slope) and the sine and cosine of the surface aspect (see Figure 3 for examples). Depending on the topography and peat formation, different terrain attributes can display different prediction capacities [13].



Figure 3. Examples of environmental covariates tested for the prediction of peat thickness: (**a**) Digital Elevation Model (DEM), (**b**) slope gradient, (**c**) Multi-Resolution Index of Valley Bottom Flatness (MRVBF), and (**d**) System of Automated Geoscientific Analyses Wetness Index (SAGAWI).

2.6. Predictive Modelling of Peat Thickness

Linear regression (LR) was used in order to predict peat thickness from the raw EC_a measured by the different coils of the DUALEM-421S (i.e., single-coil predictions) and also from the σ estimates calculated using quasi-3D inversion models. Multiple linear regressions (MLR) enabled the prediction of peat thickness from different combinations of EC_a (i.e., multiple-coil predictions) and of EC_a and environmental covariates (i.e., elevation and derived terrain attributes). Leave-one-out cross validation (LOOCV) enabled the assessment of the performance of LR and MLR models for the calibration and prediction of peat thickness. The metrics used were the coefficient of determination (R²), root mean square error (RMSE) and Lin's concordance correlation coefficient (CCC). In the present study, all maps were generated at a 1.6 m spatial resolution with UTM zone 32N, ETRS 1989 as the projected coordinate system.

3. Results and Discussion

3.1. Preliminary Analysis of EC_a Data

Table 1 shows the summary statistics for EC_a measured by the DUALEM-421S for the whole survey area and at the soil observation sites. As expected in a typical fen [12], EC_a values were relatively low, ranging from 1.6 to 65.9 mS/m when considering all the coil arrays (Table 1). Considering the

mean and maximal values, EC_a generally increased with the theoretical DOE of the measuring coil configurations. On average, 4mPRP and 4mHCP coil configurations (27.1 and 25.6 mS/m, respectively) were higher than 2mPRP and 2mHCP (23.7 and 24.7 mS/m, respectively), followed by 1mPRP and 1mHCP (17.1 and 20.9 mS/m, respectively).

The summary statistics of the EC_a values for the 110 soil observation sites were slightly lower compared to the entirety of the survey data. This was mainly because we had relatively few soil observations in areas in which thick peat layers were expected. Nevertheless, as the sampling was done with consideration to the coverage of the areas representing EC_a variability from low to high, the soil observations can be approximated to provide a relatively accurate representation of the survey data.

EC _a (mS/m)							
Data Source	n	Min.	Mean	Median	Max.	Skewness	CV (%)
Survey data							
1mPRP	48,150	3.7	17.1	17.5	43.6	0.17	37.4
1mHCP	48,150	1.6	20.9	21.8	56.4	0.09	47.8
2mPRP	48,150	5.1	23.7	24.5	58	0.07	39
2mHCP	48,150	4.3	24.7	25.5	62.6	0.14	45.9
4mPRP	48,150	6.2	27.1	28.1	65.9	0.12	41.4
4mHCP	48,150	8.1	25.6	25.1	60.8	0.29	41.6
Soil observation sites							
1mPRP	110	2.5	14.1	13.4	39.2	0.47	52.4
1mHCP	110	0.6	15.5	14.3	47.2	0.46	68.7
2mPRP	110	4.2	18.9	17.9	53.7	0.54	54.5
2mHCP	110	4.2	18.2	16.1	50.1	0.59	61.2
4mPRP	110	6.1	20.8	19	56.5	0.60	55.3
4mHCP	110	7.1	19.4	16.2	44.3	0.76	48.5

Table 1. Summary statistics for the apparent electrical conductivity (EC_a —mS/m) measured by a DUALEM-421S for the whole survey area and at the soil observation sites.

n: number of measurements/observations; Min.: minimum; Max.: maximum; CV: coefficient of variation; PRP: perpendicular coplanar coil array; HCP: horizontal coplanar coil array.

3.2. Spatial Distribution of Peat Thickness and EC_a

Figure 4 represents the peat thickness measured at the soil observation sites. It shows that the peat thickness mainly decreases from north to south over the study area. The maximal value of 730 cm was measured in the northwest corner of the study area, while minimal values, close to zero, were recorded in the southeast border area (Table 2). In general, relatively large peat thicknesses (i.e., >250 cm) were observed to the northern half of the study area, while small peat thicknesses (i.e., <250 cm) to no peat layer were observed in the southern half.

A preliminary map representing EC_a (Figure 5) was generated using ordinary kriging within ArcMap [39]. The interpolated EC_a contour plots (Figure 5) all indicate the same general pattern with a decrease from north to south over the study area. The maximal EC_a values (>40 mS/m) were measured in the northwest corner of the study area, while the minimal values (<10 mS/m) were recorded in the southeast border area (Figure 5). Again, EC_a values generally increased with the theoretical DOE of the measuring coil configurations.



Figure 4. Peat thickness (cm) measured at soil observation points and locations of cross-sections S1 and S2.

 Table 2. Summary statistics for peat thickness at the soil observation sites.

Soil Observation Sites	n	Min.	Mean	Median	Max.	Skewness	CV (%)
Peat thickness (cm)	110	3	230	210	730	0.91	89.7

n: number of measurements/observations; Min.: minimum; Max.: maximum; CV: coefficient of variation.



Figure 5. Contour plots of the interpolated apparent electrical conductivity (EC_a —mS/m) collected using the six different coils configurations of a DUALEM-421S instrument: (**a**) 1mPRP, (**b**) 1mHCP, (**c**) 2mPRP, (**d**) 2mHCP, (**e**) 4mPRP and (**f**) 4mHCP.

3.3. Direct Correlation between Peat Thickness and Predictor Variables

Table 3 shows the zero-order correlations (Pearson's *r* correlation coefficient) of the different predictor variables to the target variable. The EC_a-based variables correlated best with peat thickness, with *r* values ranging from 0.80 to 0.93. The DEM and σ -based predictor variables were also highly correlated with peat thickness, with *r* values of -0.69 and a range from 0.70 to 0.72, respectively. MRVBF and SAGAWI were moderately correlated (*r* values of 0.41 and 0.31, respectively), while the remaining topography-based variables were not correlated significantly with the target variable (*r* values ranging from -0.19 to 0.16). Subsequently, DEM and MRVBF were used to build the models in combination with single or multiple-coil EC_a measurements.

Table 3. Pearson's *r* correlation coefficient between the target variable (i.e., peat thickness) and the EC_a, σ and topography-based predictor variables.

1mPRP	1mHCP	2mPRP	2mHCP	4mPRP	4mHCP		
0.80	0.86	0.84	0.90	0.88	0.93		
$\sigma_{2\text{-layered}}$	$\sigma_{3\text{-layered}}$	$\sigma_{4\text{-layered}}$	$\sigma_{ m blocky}$	σ_{sharp}	σ_{smooth}		
0.71	0.72	0.71	0.70	0.71	0.71		
DEM	slope	MRVBF	SAGAWI	plan curv	prof curv	cos aps	sin asp
-0.69	-0.19	0.41	0.31	-0.15	-0.04	0.16	-0.04

DEM: Digital Elevation Model; MRVBF: Multi-Resolution Index of Valley Bottom Flatness; SAGAWI: System of Automated Geoscientific Analyses Wetness Index; prof curv: profile curvature; plan curv: plan curvature; cos asp and sin asp: cosine and sine of aspect.

3.4. Predicting Peat Thickness with EC_a Data from Single-Coil Configurations

Figure 6 shows the measured peat thickness versus the measured EC_a collected using the six different coil configurations of the DUALEM-421S instrument, including the corresponding LR equations and R². R² values ranged between 0.63 and 0.86. The highest R² (0.86) was recorded for 4mHCP, while the lowest (0.63) was for 1mPRP. This finding is coherent as the peat thickness ranged from 3 to 730 cm and was thus best represented by the 4mHCP coil configuration, which presents the largest DOE (0–640 cm), in contrast to the 1mPRP coil configuration with the smallest DOE (0–50 cm).

Figure 7 shows the measured peat thickness versus that predicted by the LR models for each coil configuration including the LR equations and LOOCV performance metrics. From Figure 7, it is evident that peat thickness is clearly underestimated for values larger than 500 cm, especially in the shallow measuring channels (1mPRP, 2mPRP, and 1mHCP) due to their limited DOE. The underestimation becomes less prominent with an increase in DOE, with the 4mHCP providing the most accurate predictions for the larger (i.e., >500 cm) peat thicknesses. Table 4 summarizes the LOOCV performance metrics (R², RMSE, and CCC) for the different LR models. RMSE and CCC values ranged between 74 and 122 cm and 0.77 and 0.92, respectively. In accordance with the R² variation previously described, the lowest RMSE and highest CCC were found for 4mHCP, while the highest RMSE and lowest CCC were recorded for 1mPRP. The RMSE variation represented about 7% of the measured peat thickness range. CCC was ranked excellent (i.e., >0.75) for all predictions using the Fleiss interpretation [46]. In accordance with Altdorff et al. [32] (2016), we suggest that these particularly good prediction results demonstrate the suitability of EMI surveys for soils with high variability.



Figure 6. Measured peat thickness (cm) vs. measured apparent electrical conductivity (EC_a —mS/m) collected using the six different coil configurations of a DUALEM-421S instrument: (a) 1mPRP, (b) 2mPRP, (c) 4mPRP, (d) 1mHCP, (e) 2mHCP and (f) 4mHCP (fitted regression line represented on each plot).



Figure 7. Measured vs. predicted peat thickness (cm) using leave-one-out cross validation (LOOCV) for EC_a collected from the six different coil configurations of a DUALEM-421S instrument: (**a**) 1mPRP, (**b**) 2mPRP, (**c**) 4mPRP, (**d**) 1mHCP, (**e**) 2mHCP and (**f**) 4mHCP (1:1 identity line represented on each plot).

	_ ^		_
	R ²	RMSE (cm)	CCC
Single-coil EC _a			
1mPRP	0.63	103	0.84
1mHCP	0.74	122	0.77
2mPRP	0.70	89	0.89
2mHCP	0.81	111	0.82
4mPRP	0.78	74	0.92
4mHCP	0.86	94	0.87
Multiple-coil EC _a			
1m coils	0.80	90	0.88
2m coils	0.85	78	0.91
4m coils	0.87	73	0.92
PRP coils	0.85	78	0.91
HCP coils	0.87	72	0.92
All coils	0.87	72	0.92
Single-coil EC ₂ + DEM			
1mPRP + DEM	0.74	103	0.84
1mHCP + DEM	0.80	89	0.88
2mPRP + DEM	0.78	93	0.87
2mHCP + DEM	0.85	78	0.91
4mPRP + DEM	0.84	81	0.90
4mHCP + DEM	0.89	67	0.93
Multiple-coil EC ₂ + DEM			
1^{m} coils + DEM	0.85	79	0.91
2m coils + DEM	0.88	70	0.93
4m coils + DEM	0.89	66	0.93
PRP coils + DEM	0.88	70	0.93
HCP coils + DEM	0.89	66	0.94
All coils + DEM	0.90	65	0.94
Single-coil EC ₂ + DEM + MRVBF			
1mPRP + DEM + MRVBF	074	102	0.85
1 mHCP + DEM + MRVBF	0.81	88	0.89
2mPRP + DFM + MRVBF	0.01	93	0.87
2mHCP + DEM + MRVBF	0.75	78	0.07
4mPRP + DEM + MRVBE	0.83	81	0.91
4mHCP + DEM + MRVBF	0.89	67	0.90
Multiple-coil EC + DEM + MRVBE			
1m coils + DFM + MRVBF	0.85	79	0.91
2m coils + DEW + MRVRE	0.05	79	0.91
2 In CONS + DEW + WIXVDP 4 m coils + DEM + MPVPP	0.00	66	0.93
$\frac{1}{2} \frac{1}{2} \frac{1}$	0.09	70	0.93
r Kr COHS + DEIVI + WIKV DF	0.00	10	0.93
IICF COIIS + DEN(+ MEXVDF	0.09	00	0.94
All colls + DEM + MKVBF	0.90	65	0.94
Average σ	0.50	140	0.65
U2-layered	0.50	142	0.67
$\sigma_{3 ext{-layered}}$	0.51	141	0.68
$\sigma_{ ext{4-layered}}$	0.51	141	0.67
$\sigma_{ m blocky}$	0.48	145	0.65
$\sigma_{ m sharp}$	0.50	143	0.66
$\sigma_{\rm emosth}$	0.50	143	0.66

Table 4. LOOCV performance metrics for models predicting peat thickness from single-coil EC_a data (LR), different combinations of EC_a data (i.e., multiple-coil predictions) and environmental covariates (MLR), and from the average σ calculated using different inversion models (LR).

R²: coefficient of determination; RMSE: root mean square error; CCC: Lin's concordance correlation coefficient.

3.5. Predicting Peat Thickness with Combinations of EC_a Data and Environmental Covariates

From Table 4, we can compare the results of all models predicting peat thickness. Multiple-coil EC_a MLR models yielded better predictions than single-coil EC_a LR models: while R² values were comparable or higher, RMSE and CCC were consistently lower and higher, respectively. Moreover, considering the MLR models built with different combinations of EC_a data and environmental covariates, the addition of elevation data (i.e., DEM) improved the single and multiple-coil predictions. The R^2 value did not increase drastically (with gains ranging from 0.02 to 0.11), which indicates that the MLR models comprising the DEM explained between 2% and 11% more variation than the LR models. While RMSE generally decreased (variation between -33 and +7 cm), CCC mostly increased (with a variation between -0.02 and +0.11). However, the addition of other terrain attributes only provided small improvements to some of the single-coil predictions and did not generate any upgrade for the multiple-coil predictions. According to Nathans et al. [47] (2012), a predictor variable displaying no or a very weak correlation to a target variable can still contribute significantly to a MLR model. Acting as a noise suppressor, the predictor variable removes irrelevant variance from other predictors within the regression [47]. In contrast to Altdorff et al. [32] (2016), the prediction accuracy was not impacted by the use of additional topography-based variables, which did not act as noise suppressors in our study. Table 4 displays the results obtained with the addition of MRVBF for illustration. Here, R^2 and CCC increased by 0.01 and RMSE decreased by 1 cm for only three different combinations.

Figure 8 shows the measured peat thickness versus that predicted by the models yielding the best performances in the categories of single-coil or multiple-coil EC_a models and their respective combinations with the DEM (i.e., 4mHCP, all coils, 4mHCP plus DEM and all coils plus DEM). For these selected models, R² values ranged from 0.86 to 0.90, while RMSE values ranged from 65 to 94 cm. In particular, the predictions were more accurate for the larger (i.e., >500 cm) peat thicknesses when compared to the single-coil configurations. These results can be compared with previous DSM studies. Using elevation and slope data, Holden and Connolly [2] (2011) and Parry et al. [3] (2012) obtained lower R^2 values ranging from 0.58 to 0.63 for the former and a value of 0.53 (with a RMSE of 14 cm) for the latter. Similar to Altdorff et al. [32] (2016), Parry et al. [3] (2012) suggested that the predictions were worsened in the case of shallow peat and a lesser variation in peat thickness. Several studies by Rudiyanto et al. [4,6,8] reported predictions with similar performances. Using LR or an empirical peat thickness model with elevation data, Rudiyanto et al. [4] (2015) obtained R² values of 0.90 and 0.93 and RMSE values of 69 and 58 cm, respectively. A study by Rudiyanto et al. [6] (2016) compared four machine learning algorithms (i.e., cubist, random forest, quantile regression forest and artificial neural networks) using several environmental covariates (i.e., elevation, slope, aspect, SAGAWI and nearest distance to river). The best models yielded R^2 values ranging from 0.67 to 0.92 and RMSE values ranging from 60 to 110 cm. Finally, Rudiyanto et al. [8] (2018) compared an array of machine learning algorithms (e.g., partial least squares regression, cubist, random forest, quantile regression forest, artificial neural networks and support vector machines) using many environmental covariates (i.e., DEM and derived terrain attributes, Euclidean distances to water bodies and radar and optical satellite images). The best models demonstrated better performance for calibration data (R² from 0.95 to 0.99, and RMSE from 28 to 110 cm) than for validation data (with all models presenting similar mean values of R^2 and RMSE of 0.6 and 250 cm, respectively). Notably, the predictions of these studies were carried out on larger study areas (ranging from 1000 to 100,000 ha).



Figure 8. Measured vs. predicted peat thickness (cm) using (**a**) 4mHCP, (**b**) the combination of all six coils, (**c**) the combination of 4mHCP and DEM and (**d**) the combination of all six coils and DEM (1:1 identity line represented on each plot).

3.6. Predicting Peat Thickness from Average σ Calculated Using a Quasi-3D Inversion Algorithm

For each soil observation site, we calculated the average value from the σ estimates for the range corresponding to the peat thickness measured at the specific point. For instance, for the soil observation site with the maximum measured thickness of 730 cm, we calculated the average value from 15 σ estimates derived for each 50 cm layer corresponding to the depth interval from 0 down to 750 cm. Table 4 summarizes the LOOCV performance metrics for the LR models between peat thickness and the different average σ estimates. The three metrics were similar for the six different inversion models. In comparison with the predictions obtained from single-coil EC_a, σ -based predictions were poorer for all metrics: R² and CCC values were lower (ranging between 0.48 and 0.51, and 0.65 and 0.68, respectively) while RMSE values were higher (ranging between 141 and 145 cm). R² values indicate that the σ -based models explain between 12% and 38% less variation, and CCC values were ranked as fair to good [46]. Altdorff et al. [32] (2016) reported that inversion did not provide substantial estimates of peat thickness. However, they associated these weak results to the narrow range of peat thickness in their study area, among others, which is not the case in the present investigation. While σ represents the true electrical conductivity estimated at different depth intervals for a specific location, the peat thickness corresponds to a sole measurement at a precise location. It is therefore difficult to predict peat thickness directly from σ estimates. We attempted to avoid this pitfall by calculating the average σ separately for each soil observation site; unfortunately, this still resulted in poor predictions in comparison with the predictions made directly from EC_a. One explanation lies in the DOI. Figure 9 shows the DOI for σ_{smooth} , which provided the lowest total residual of 0.88 out of all models: two-layered (1.73), three-layered (1.43), four-layered (1.20), blocky (0.91) and sharp (0.98). The smooth model was selected for illustration as it requires the least strict assumptions regarding the subsurface architecture and provides reasonable σ estimates in most cases. From Figure 9, areas with expected peat layers located in the northern half of the study area presented a shallow DOI (generally smaller than 400 cm, which is the average DOI value considering the whole study area). These shallow DOIs could explain the poor predictions for areas with peat layers thicker than 400 cm.



Figure 9. Depth of investigation (DOI) for the calculated true electrical conductivity (σ_{smooth}) estimates over the study area.

Although the inversions yielded poorer predictions, they can be advantageous to understand the conductivity distribution with depth. This is particularly important as the electrical conductivity of peat is highly dependent on the water content [10–12]. After inverting the data, we have derived the distribution of σ_{smooth} estimates at the 110 observation points (Figure 10) to determine if there was a contrast between the peat and underlying layers. We observed that the transition is more gradual; however, overall, it can be deduced that the peat presents a conductive overburden on resistive sandy soils.



Figure 10. Distribution of the calculated average true electrical conductivity (σ_{smooth}) estimates over the study area for peat and the underlying layers.

Two cross-sections (i.e., S1 and S2, represented in Figure 4) showing the calculated σ_{smooth} estimates are used for further interpretation (Figure 11). S1 is approximately oriented in the west–east direction and S2 in the north-.south direction (Figure 4). S1 is located in the northern half of the study area; accordingly, the soil observation sites along this cross-section mostly present relatively large peat thicknesses (i.e., >250 cm). Along S1 (Figure 11a), the correlations between σ and peat thickness were not evident. For example, large peat thicknesses occur to the eastern side (i.e., 170–290 m in the profile) even though σ values were low (i.e., <25 mS/m) in the topsoil (i.e., 0–2 m). Likewise, the σ values were generally high to the western side (i.e., 0–90 m in the profile) where the observed peat thicknesses

were small. Interestingly, the expected relationship (i.e., high σ at large peat thickness locations) was only observed at the center of the profile (i.e., within 100–160 m). These σ variations could result from variations in water content or cation exchange capacity within the soil, which are associated with peat properties such as bulk density, SOC content and degree of decomposition [32]. However, the expected patterns were evidently observed along S2—a cross-section along which high variability in peat thicknesses was observed (Figure 4). Along S2 (Figure 11b), the section to the northern side showed higher σ values where relatively large peat thicknesses (i.e., >250 cm) occur, in comparison to the southern side with shallow or no peat. In both cross-sections, it can be seen that the DOI does not reach the bottom of peat layers at the locations where the σ values were high, thereby limiting our capability for interpretation.



Figure 11. Cross-sections S1 (**a**) and S2 (**b**) showing the calculated σ_{smooth} estimates (for each soil observation site, peat layers are represented in red and underlying layers in green).

3.7. Predictive Maps for Peat Thickness

Predictive maps for peat thickness were generated using ordinary kriging within ArcMap [39]. Figure 12 displays the interpolated contour plots for peat thickness predicted by the single-coil EC_a LR models. All six predictive maps show the same general pattern with a decrease of peat thickness from north to south over the study area, which is consistent with Figure 4. The main variation is in the size of the area, with a predicted peat thickness larger than 500 cm in the northern part of the study area. This area increases with the theoretical DOE of the measuring coil arrays. Figure 13 presents the predictions from the four best models selected previously (i.e., 4mHCP, all coils, 4mHCP plus DEM and all coils plus DEM). These four models show the same general patterns, with the only clear variation being the extent of the predicted areas with the largest and smallest peat thicknesses in the northern and southern parts of the study area, respectively.



Figure 12. Contour plots of the interpolated peat thickness (cm) predicted from the apparent electrical conductivity (EC_a —mS/m) collected using the six different coil configurations of a DUALEM-421S instrument: (a) 1mPRP, (b) 1mHCP, (c) 2mPRP, (d) 2mHCP, (e) 4mPRP and (f) 4mHCP.

3.8. Uncertainty Assessment

Figure 14 shows the 95% confidence interval (CI) for each selected model over the study area. The northwestern part of the study area presents both the largest predicted peat thickness values and the largest CIs in all four models. The large CIs in this particular area can be explained by (a) a relative under-sampling in comparison with the middle/southern areas (Figure 1); (b) the limitation due to the DOE for 4mHCP (i.e., 0 to 640 cm) when the largest peat thickness recorded in the area was 730 cm and (c) the fact that the DUALEM-421S could not be used to survey two small areas covered by overly dense vegetation resulting from the former plot experiment (Figure 2). The other area with large CIs in three models (i.e., 4mHCP plus DEM, all coils and all coils plus DEM) is located in the southwestern part of the study area and presents small predicted peat thickness values (Figure 13b–d). The large CIs in this specific area can be attributed to the lack of soil observations (Figure 1). Notably, the CIs for peat thickness predictions are much smaller for 4mHCP and 4mHCP plus DEM models (Figure 14a,c) than for all coils plus DEM models (Figure 14b,d). These results suggest that the single-coil predictions, using 4mHCP with or without the DEM as an additional predictor, provided the most reliable results (i.e., high accuracy and low uncertainty) in our case, which can be further used for decision-making; for example, in the case of peatland restoration.



Figure 13. Contour plots of the interpolated peat thickness (cm) predicted from (**a**) 4mHCP, (**b**) the combination of all six coils, (**c**) the combination of 4mHCP and the DEM and (**d**) the combination of all six coils and the DEM.



Figure 14. Plots of 95% confidence intervals for the peat thickness (cm) predicted from (**a**) 4mHCP, (**b**) the combination of all six coils, (**c**) the combination of 4mHCP and the DEM and (**d**) the combination of all six coils and the DEM.

4. Conclusions

The present case study demonstrated that data collected with a single-frequency multi-receiver electromagnetic induction (EMI) instrument enabled the non-invasive and reliable prediction of peat thickness over a 10 ha field. The results indicated that raw EC_a data can already constitute valuable predictors for peat thickness (i.e., within single-coil predictions). The use of σ estimates calculated from quasi-3D inversion resulted in poor predictions for this case study. This outcome can be explained by the shallow depths of investigation obtained in areas with thick peat layers after the inversion of the EC_a measurements. Peat thickness could also be predicted with multiple linear regression based on the combination of EC_a data (i.e., multiple-coil predictions), and further with the addition of environmental covariates (i.e., elevation and different derived terrain attributes). While multiple-coil predictions and the addition of elevation data generally provided slightly higher accuracies than single-coil predictions, their corresponding uncertainty estimates calculated from 95% confidence intervals were larger. Therefore, we suggest that for our case study, the single-coil predictions—in particular using 4mHCP with or without elevation as an additional predictor—provided the most reliable results (i.e., high accuracy and low uncertainty) for use in decision-making; for example, in the case of peatland restoration. Notably, the significant results obtained in this study can be explained by the high variability in peat thickness of the selected field area. Finally, this study demonstrates the considerable potential of EMI data for use in peat thickness mapping.

A future development of the present study will aim at the intensive investigation of the spatial variability of different key peat soil properties, such as soil organic carbon content, bulk density and soil organic carbon stock. This subsequent study would greatly benefit from inversion modeling and the use of an EMI instrument which can reach a larger DOI over the whole field, yielding more detailed information on the peat and underlying layers. To achieve this, a comprehensive soil sampling procedure guided by a more appropriate soil sampling design (for example, from a conditioned Latin hypercube sampling approach; the procedure in [48] can be adopted to measure different soil properties at consistent depth intervals). Furthermore, this study can greatly benefit from the use of a combination of complementary techniques such as visible near-infrared (vis–NIR) spectroscopy for a more accurate representation of peat and the underlying layers. Fusing EMI and vis–NIR data will allow the SOC content to be mapped at different depths and enable the further assessment of the SOC stocks over the study area.

Author Contributions: Conceptualization: A.B. and T.K.; data curation: A.B. and T.K.; visualization: A.B.; supervision and funding: M.H.G. and B.V.I.; writing—original draft preparation: A.B. and T.K.; writing—review and editing: M.H.G. and B.V.I.; methodology, software, and validation: A.B. and T.K. All authors have read and agreed to the published version of the manuscript.

Funding: This research received no external funding.

Acknowledgments: The authors would like to thank Henrik No rgaard for assisting with the collection of DUALEM data and Jesper Bjergsted Pedersen for help with the Aarhus Workbench software.

Conflicts of Interest: The authors declare no conflict of interest.

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