

Article

Statistical Evaluation of Mechanical Properties of Slag Based Alkali-Activated Material

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Abstract: Slag is one of the by-products of the energy industry, which is suitable for secondary industrial processing. Although slag has been successfully used in industrial production for several decades, its use does not achieve the level of its potential. Today, to achieve a sustainable construction industry, alternative types of cement have been extensively investigated. Geopolymer is a kind of material which is obtained from the alkaline activator and it can be produced from the industrial wastes or by-products. In this study, $\text{SiO}_2/\text{Na}_2\text{O}$ ratio and the amount of Na_2O in activation solution parameters of alkali-activated materials were tested how they affect the strengths of hardened geopolymers from ground granulated blast furnace slag (GGBFS). Compressive and flexural strength tests were conducted, and the results were analyzed by analysis of variance (ANOVA). Strengths were tested after 7, 28, and 90 days.

Keywords: geopolymer; slag; compressive strength; flexural strength

1. Introduction

Portland cement is the most widely used binder in the concrete industry. Its annual worldwide production is expected to grow from approximately 2.54 billion tons in 2006 to 4.38 billion tons in 2050 based on 5% growth per year. Ordinary Portland cement (OPC)-based concrete is the most used construction. Portland cement contributes to about 5–6% of global CO_2 emission. Search for several alternatives—such as alkali-activated cement, calcium sulphoaluminate cement, etc.—are being made with the advantages of Portland cement [1,2]. In recent years, geopolymer has attracted considerable attention because of its early compressive strength, low permeability, good chemical resistance, and excellent fire resistance behavior [3,4]. Because of these advantageous properties, the geopolymer is a promising candidate as an alternative to ordinary Portland cement for developing various sustainable products in making building materials, concrete, fire-resistant coatings, fiber reinforced composites, and waste immobilization solutions for the chemical and nuclear industries. Geopolymers are emerging as a green alternative to Portland cement as they exhibit comparable mechanical properties and have significantly lower CO_2 emissions. During the past two decades, significant research has sought alternatives to OPC concrete, one of which is geopolymer concrete, which can be manufactured from industrial waste materials. As such geopolymer concretes have the potential to be the next generation of highly sustainable construction material [4–6].

Geopolymers are environmentally friendly specimens that can be made from an appropriate aluminosilicate source such as fly ash. The term geopolymer was first used by Joseph Davidovits. He defined the material that is formed in inorganic polycondensation called geopolymerization [7,8].

Geopolymers are synthetic alumino-silicate binders formed by the reaction between oxides and silicates of Si and Al. They are amorphous in nature and exhibit characteristic three-dimensional

frameworks of SiO_4 and AlO_4 tetrahedra like that of zeolite structure [9]. The mechanism for geopolymers is a polymerization process that involves a chemical reaction of alumina-silicate materials in the presence of an alkaline medium which results in the formation of three-dimensional polymeric chain [10]. For geopolymers, activation is required for the polymerization reaction which can be attained with alkaline compounds such as NaOH-based, KOH-based, or a mixture of Na_2O and SiO_2 -based. They have numerous advantages as binders because they can provide mechanical strength up to 100 MPa, better chemical resistance to sulphates and harmful acids, low creep and shrinkage, high early strength, and resistance to highly elevated temperatures [11–13].

Geopolymers can be used in many fields of industry such as transportation, metallurgy, emergency repairs, membrane materials and nuclear waste disposal. Regardless of important profitable and technological potential geopolymers character limits their widespread applications where excessive efforts are made to overcome such deficiencies. Many studies are devoted to optimizing the strength of geopolymer products and to comprehend the geopolymerization mechanism [14–17].

Bernal et al. [18] examined the development of binder structure in sodium silicate-activated slag-fly ash mixtures to determine the effects of slag addition on the final geopolymers strength. $\text{SiO}_2/\text{Al}_2\text{O}_3$ ratio, $\text{R}_2\text{O}/\text{Al}_2\text{O}_3$ ratio, $\text{SiO}_2/\text{R}_2\text{O}$ ratio ($\text{R} = \text{Na}^+$ or K^+) and liquid/solid ratio were the most significant factors which affected the properties of geopolymer binders. Therefore desired mechanical strength, amorphous structure of geopolymers is desirable as many research concluded. The association amongst the compressive strength and $\text{SiO}_2/\text{R}_2\text{O}$ ratio showed that an rise in alkali content or reduction in silicate content increases the mechanical strength of geopolymers indicates the formation of aluminosilicate network structures [19–22].

Naturally, the optimal geopolymer strength was described with the $\text{SiO}_2/\text{Al}_2\text{O}_3$ ratio in the range of 3.0–3.8 and $\text{Na}_2\text{O}/\text{Al}_2\text{O}_3$ ratio of ~ 1 [23]. Changes in $\text{SiO}_2/\text{Al}_2\text{O}_3$ ratio outside this range have been found to outcome in lower strength. The setting time of geopolymer binders increased with increasing $\text{SiO}_2/\text{Al}_2\text{O}_3$ ratio of the initial mixture. The same authors examined the $\text{Al}_2\text{O}_3/\text{SiO}_2$ ratio dependent on hardening and setting of the geopolymer system. This ratio proved the effects of setting time and final mechanical strength of the geopolymer [23].

On the other hand, the alkali reactant ratio can also be represented in term of $\text{SiO}_2/\text{Na}_2\text{O}$ molar ratio. Increasing $\text{SiO}_2/\text{Na}_2\text{O}$ ratio slower down the reaction and delays the setting of paste. A system with a Na-silicate solution has a slower rate of reaction than that of K-silicate solution. Davidovits suggested the $\text{SiO}_2/\text{Na}_2\text{O}$ ratio for alkaline reactant of 1.85 in order to achieve higher strength and durability [24].

Chindaprasirt examined the effect of $\text{SiO}_2/\text{Al}_2\text{O}_3$ and $\text{Na}_2\text{O}/\text{SiO}_2$ ratios on the setting time, workability, and the final mechanical strength of geopolymer system. It was recognized that the suitable ratios ranged between 2.87 to 4.79 for $\text{SiO}_2/\text{Al}_2\text{O}_3$ and within 1.2 to 1.4 for $\text{SiO}_2/\text{Na}_2\text{O}$ for geopolymer binder [25]. Bernal and Provis addressed used the accelerated degradation testing methods to determine the effects of increased concentrations of CO_2 , sulfates, and chlorides on the durability [26].

Davidovits recommended the composition of geopolymers should fall in order to obtain high-strength, durable products. Even so, he concluded the ideal $\text{Na}_2\text{O}/\text{Al}_2\text{O}_3$ and $\text{SiO}_2/\text{Al}_2\text{O}_3$ ratios are about 1.00 and 4.00, respectively [25].

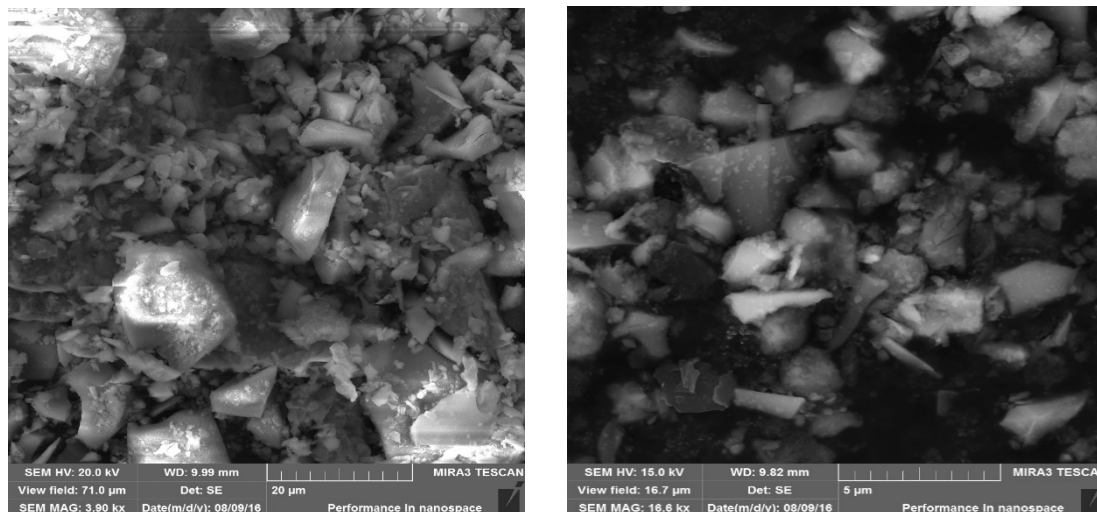
In this paper, we conducted several experiments based on our previous research with GGBFS.

2. Materials and Methods

The material used for alkali activation was ground granulated blast furnace slag (GGBFS) from which geopolymer samples were created. Chemical analysis of material is in Table 1. Because of slag lumps, it was necessary to grind material. Material was grinded in laboratory ball mill using steel balls with different diameter. After grinding stage d80 was 120 μm (80% of material was passing 120 μm sieve). The material was homogenized before alkali activation. No other treatment was applied to the material. SEM pictures of materials are in Figure 1.

Table 1. Chemical composition of material.

Material	SiO ₂	CaO	MgO	Al ₂ O ₃	Fe ₂ O ₃	Other
GGBFS (%)	40.3	37.01	12.1	8.51	0.3	1.78

**Figure 1.** SEM pictures of GGBFS.

The activation solution was prepared by mixing solid NaOH pellets with Na-water glass and water. Sodium water glass from the Kittfort Praha Co. with the density of 1.328–1.378 g/cm³ was used. It contains 36–38% Na₂SiO₃ and the molar ratio of SiO₂/Na₂O is 3.2–3.5. Solid NaOH with the density of 2.13 g/cm³ was obtained from Kittfort Praha Co. containing at least 97–99.5% of NaOH.

The effect of two main parameters was examined, amount of Na₂O (%) from slag weight (ratio of Na₂O in activation solution and amount of GGBFS) and SiO₂/Na₂O ratio (mol/mol) in activation solution on strengths of geopolymers. A selection of 28 different mixtures were designed in which the amount of Na₂O varied from 5 to 8 and with a varying SiO₂/Na₂O ratio from 0 to 1.4. The water-to-fly ash ratio (w) was adjusted to 0.25. GGBFS mixture was stirred with activation solution for 10 minutes until the creation of homogenous mixture. The mixture was then filled into prismatic molds with the dimensions 40 × 40 × 160 mm and compacted on the vibration table VSB-40. The pastes were cured in a hot air-drying chamber at 80 °C for 6 hours. Higher temperature in first hours was chosen to accelerate geopolymerization process and reduce cracking due to shrinkage. Thereafter, the samples were removed from the forms, marked, and stored in laboratory conditions until the moment of the strength test. The values of mechanical strength were determined according to the Slovak Standard STN EN 12390-3, which means after 7, 28, and 90 days were performed compressive and flexural strengths. The three same samples were broken into halves to determine flexural strength and six halves were tested for compressive strengths. The mechanical strengths of the hardened samples was determined using the hydraulic machine Form + Test MEGA 100-200-10D. Whole experiments designs with results are shown in Table 2.

Table 2. Experiment design with results.

Sample	Na ₂ O	SiO ₂ /Na ₂ O	W	Flex.	Compress.	Flex.	Compress.	Flex.	Compress.
	%	mol/mol		7 days		28 days		90 days	
1	5	0	0.25	3.3	9.4	4.6	11.4	3.3	16.6
2	6	0	0.25	4.7	9.2	4.6	10.9	4.1	16.2
3	7	0	0.25	5.2	8.5	4.6	10	5.3	15.3
4	8	0	0.25	4.5	8.4	5.9	11.1	5.2	17.9
5	5	0.25	0.25	2.8	11.8	3	13.3	2.5	22.9
6	6	0.25	0.25	2.7	7.6	3.4	9.3	3.4	16.7
7	7	0.25	0.25	2.8	6.6	4.2	6.7	4	12.7
8	8	0.25	0.25	4	7.7	4.9	7.9	3.8	12.7
9	5	0.5	0.25	3.3	18.5	3.3	22.1	4	29.8
10	6	0.5	0.25	3.5	17.3	4.1	19.5	4.6	28.1
11	7	0.5	0.25	5.5	20.8	6.3	24.4	3.6	30.9
12	8	0.5	0.25	4.7	15.7	6.6	15.8	4.9	24
13	5	0.75	0.25	4.9	32.6	5.3	38	4.5	33.3
14	6	0.75	0.25	4.8	25.7	4	32.9	4.9	32.9
15	7	0.75	0.25	3.3	14.9	3.4	21.5	3.5	18.4
16	8	0.75	0.25	2.3	9.7	2.2	15.1	1.9	15.3
17	5	1	0.25	4.2	37.6	4.3	40.2	2.5	34.3
18	6	1	0.25	3.3	32.9	5.6	36.6	4	37.8
19	7	1	0.25	3.5	31.6	2.1	37.2	2.8	34.9
20	8	1	0.25	4.6	28.6	2.6	33.2	3.2	31.4
21	5	1.2	0.25	5.2	44.2	6.2	44.7	5	45
22	6	1.2	0.25	5.4	42.7	5	44.6	3.9	44.2
23	7	1.2	0.25	4.3	39.3	5	41.6	5.2	39.7
24	8	1.2	0.25	5.7	21.5	5.4	23.5	5.7	23
25	5	1.4	0.25	4.1	49.4	3.6	51.2	3.2	48.7
26	6	1.4	0.25	4.5	52.5	3.5	52.7	4	52.2
27	7	1.4	0.25	3.9	47.5	4	51.9	3.9	50.5
28	8	1.4	0.25	2.2	39	2.7	43.3	1.5	40.1

3. Results

In this study, two parameters of alkali activated materials were tested how they affect the strengths of hardened geopolymers. From the design of experiments, 28 samples were tested after 7, 28, and 90 days, made them 84 tested samples. Compressive and flexural strengths tests were made and ANOVA was obtained and evaluated. Analysis of variance (ANOVA) is a collection of statistical models and their associated estimation procedures used to analyze the differences among group means in a samples. These results are presented in this section. The basic statistical parameters can be seen in the following Table 3.

Based on the conducted experiments, the effect of main parameters of geopolymerization, SiO₂/Na₂O ratio, and amount of Na₂O in activation solution on compressive and flexural strengths of geopolymers was examined. Showing the results by box plots (Figure 2a, and Figure 2b) of compressive and flexural strength, it can be seen that by increasing the hardening time, the compressive strength increases, and flexural strength reached a maximum at 28 days and at 90 days minimum. Changes in strength and pressure are statistically not significant.

From the results of the correlation analysis, it is clear that a high positive correlation is between the results of the compressive strength and the SiO₂/Na₂O ratio (Figure 3). As the SiO₂/Na₂O ratio increases, the compressive strength values also increase. This result is valid for each 7, 28, and 90 days hardening time as can be seen from the following table. Coefficients of the correlation between compressive strength and Na₂O show a low negative correlation and the results are not statistically significant, see Table 4.

Table 3. Statistical parameters of samples.

7 Days	Valid N	Mean	Median	Min.	Max.	Variance	Std. Dev
Na ₂ O (%)	28.00	6.50	6.50	5.00	8.00	1.30	1.14
SiO ₂ /Na ₂ O (-)	28.00	0.73	0.75	0.00	1.40	0.23	0.48
Flexural strength (MPa)	28.00	4.04	4.15	2.20	5.70	0.98	0.99
Compress. strength (MPa)	28.00	24.69	21.15	6.60	52.50	221.60	14.89
28 Days	Valid N	Mean	Median	Min.	Max.	Variance	Std. Dev
Na ₂ O (%)	28.00	6.50	6.50	5.00	8.00	1.30	1.14
SiO ₂ /Na ₂ O (-)	28.00	0.73	0.75	0.00	1.40	0.23	0.48
Flexural strength (MPa)	28.00	4.30	4.25	2.10	6.60	1.53	1.24
Compress. strength (MPa)	28.00	27.52	23.95	6.70	52.70	231.26	15.21
90 Days	Valid N	Mean	Median	Min.	Max.	Variance	Std. Dev
Na ₂ O (%)	28.00	6.50	6.50	5.00	8.00	1.30	1.14
SiO ₂ /Na ₂ O (-)	28.00	0.73	0.75	0.00	1.40	0.23	0.48
Flexural strength (MPa)	28.00	3.87	3.95	1.50	5.70	1.09	1.04
Compress. strength (MPa)	28.00	29.48	30.35	12.70	52.70	148.19	12.17

Notes: (-) means ratio (mol/mol), dimensionless number.

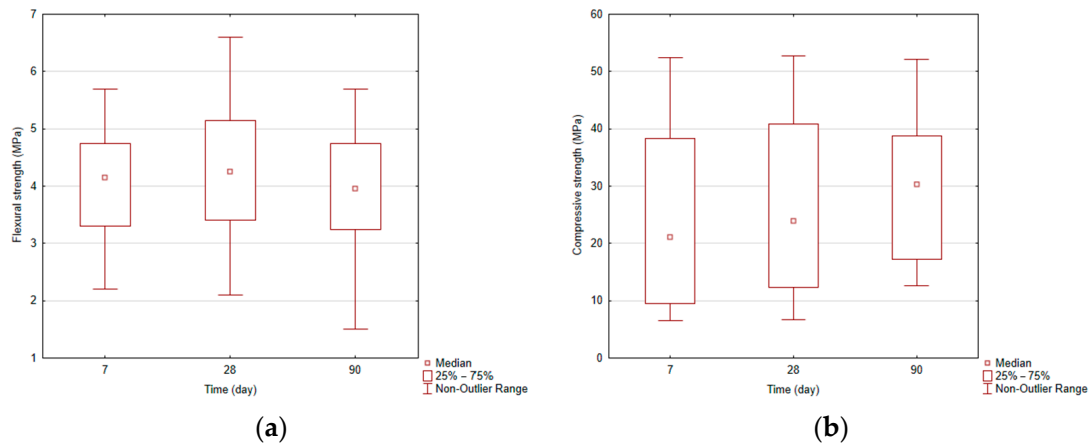
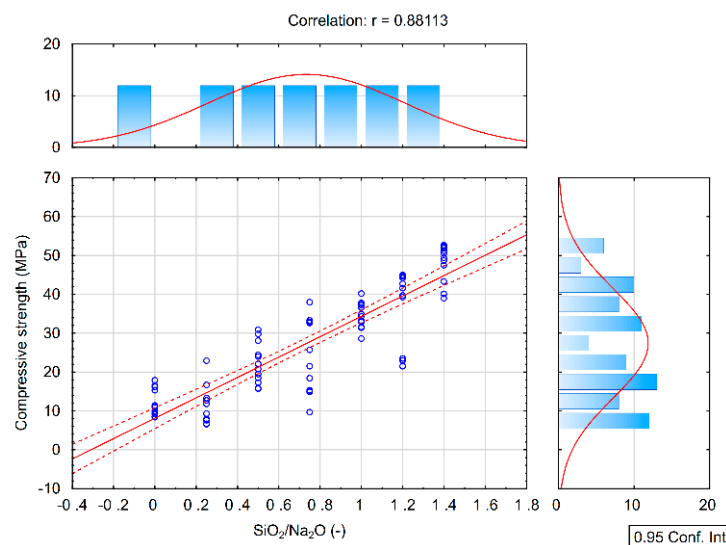
**Figure 2.** (a). Box plots—flexural strength. (b). Box plots—compressive strength.**Figure 3.** Correlation analysis of the compressive strength and the SiO₂/Na₂O ratio.

Table 4. Correlations analysis.

7 Days	Flexural Strenght (MPa)	Compressive Strength (MPa)
Na ₂ O (%)	0.003282	−0.259389
SiO ₂ /Na ₂ O (-)	0.114724	0.905184
28 Days	Flexural Strenght (MPa)	Compressive Strength (MPa)
Na ₂ O (%)	−0.007887	−0.241935
SiO ₂ /Na ₂ O (-)	−0.166900	0.915196
90 Days	Flexural Strenght (MPa)	Compressive Strength (MPa)
Na ₂ O (%)	0.046731	−0.299692
SiO ₂ /Na ₂ O (-)	−0.147759	0.854066

Notes: (-) means ratio (mol/mol), dimensionless number.

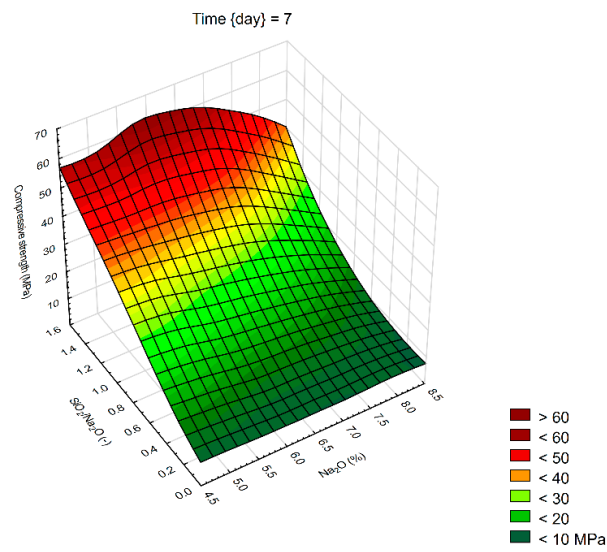
We created 3D surface charts to observe the compression strength and flexural strength of samples. Approximation of results was performed using the least squares of weighted distances. From the results obtained, it can be observed that the dependency patterns during the different hardening times are comparable and maximum compressive strengths are reached at the maximum values of SiO₂/Na₂O ratio 1.4 and Na₂O 6%. Minimum compressive strengths are achieved at the 6% of Na₂O and 0 value of SiO₂/Na₂O ratio. Figure 4 describes the effect of observed factors on compressive strengths of geopolymers. As the SiO₂/Na₂O ratio increases from 0, strengths increase to their maximum. After 7 days of hardening samples, best results in case of flexural strength were 8% of Na₂O and 1.2 SiO₂/Na₂O ratio. Compressive strength has best results in a sample with 5% of Na₂O and 1.4 SiO₂/Na₂O ratio. Twenty-eight days after alkali activation of samples results shown similar strengths, best was again 8% of Na₂O but only 0.5 SiO₂/Na₂O ratio, in case of compressive strengths it was 6% of Na₂O and 1.4 SiO₂/Na₂O ratio. Last samples hardened 90 days shows that in case of flexural strengths it is hard to make any prediction were should be best strengths, see Figure 5. Flexural strength of sample with 8% of Na₂O and 1.2 SiO₂/Na₂O ratio has the biggest strength. Compressive strength in our samples was as we predicted because it is very similar to another result, the best sample was with 6% of Na₂O and 1.4 SiO₂/Na₂O ratio same as at 28 days. Further increases of the SiO₂/Na₂O ratio should lead to more increased compressive strengths.

Methods of regression analysis and analysis of variance (ANOVA), a regression model was obtained and evaluated, which expresses the influence of compressive strength and flexural strength from the SiO₂/Na₂O ratio, amount of Na₂O and hardening time. The ANOVA result states that the regression model is appropriate and that all input parameters are statistically significant and affect the compressive strength results. The selected regression model explains the variability of parameters to the compressive strength of approximately 86%, see Table 5. R shows a high linear correlation among SiO₂/Na₂O ratio, Na₂O and compressive strength. R² shows how well terms (data points) fit a model (3D surface chart). The adjusted R² tells the percentage of variation explained by only the independent variables that actually affect the dependent variable. An extra 14% represents unexplained variability, the impact of random factors, and other unspecified impacts. Regression model is significant at the level of alpha 0.05 (*p*-value). The *p*-value is less than 0.05.

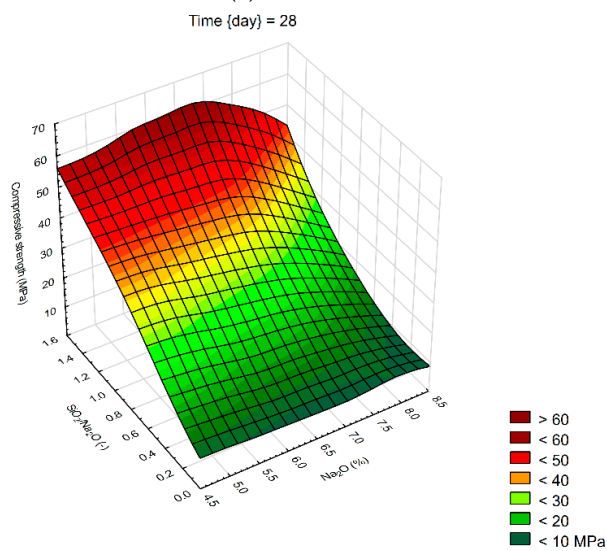
Table 5. ANOVA results.

Effect	Sums of Square	df	Mean Squares	F	<i>p</i> -value
Regress.	14259.00	3	4753.00	165.69737	0.0000000
Residual	2294.84	80	28.685		
Total	16553.84				

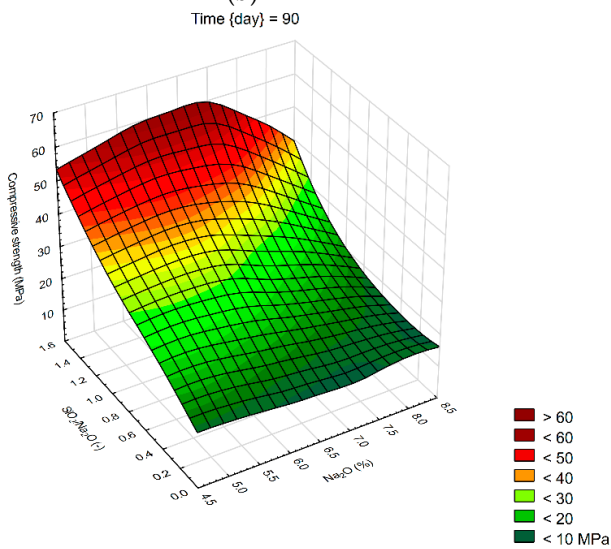
Notes: Regression Summary for Variable: Compressive Strength (ANOVA) R = 0.928100 R² = 0.86137 Adjusted R² = 0.856117.



(a)



(b)



(c)

Figure 4. Surface charts of compressive strengths—(a) 7 days; (b) 28 days; (c) 90 days.

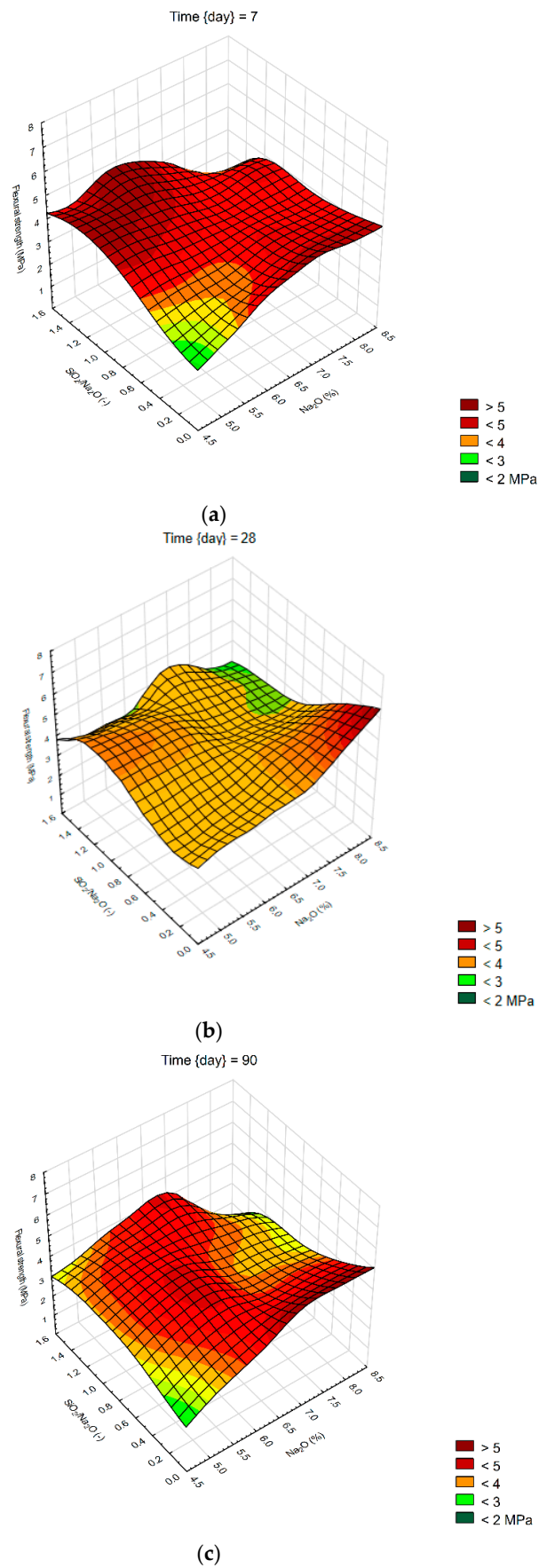


Figure 5. Surface charts of flexural strengths—(a) 7 days; (b) 28 days; (c) 90 days.

It is not possible to create a regression model with statistical significance and reliability from flexural strength data.

4. Discussion

Musaddiq et al. (2017) conducted tests with GGBS with the addition of fly ash and achieved similar strengths, but with more amount of FA, strengths were lowering down. Moreover, authors cured the specimens at ambient temperature in contrary to our experiments. However, in case of FA-based geopolymers, the elevated temperature is essential for SiO_2 and Al_2O_3 to form the geopolymerization products. Peyronnard et al. (2012) carried out a test with GGBS with addition others pozzolanic by-products such as waste glass (WG), copper slag (SC), and coal fly ash (CFS). Since their high reactivity, GGBFS allows the development of high mechanical strength. Their amount of binders could be adjusted to influence the strength. Authors also conducted the mechanical strengths test, but their maximum strengths were around 2.5 MPa with GGBS and even lower with addition another by-products. This can be due to their preparation method and curing temperature. Ye et al. (2017) performed tests using slag and calcined tailings mixture without any addition of water. Their samples reached in a period of 6 years compressive strengths over 75 MPa. The increase in strength with extended curing times proves the stability of the mechanical properties of the studied geopolymers. This increases the confidence in its durability. Geopolymers were stored in humidity chambers with relative humidity ranging from 40% to 80%. This continuous hydration helped created denser microstructure of geopolymers.

In future experiments, we would like to continue with our materials and work with different curing regimes at ambient temperature and enhanced temperature. We proved that pure GGBFS, with no addition of fly ash or any others suitable geopolymerization materials, is enough to create satisfactory geopolymers with high mechanical strengths [27–29].

5. Conclusions

For many purposes, there is an increasing demand for new materials that have low CO_2 emissions connected with their production. Alkali activated materials—geopolymers—are a new generation of inorganic binders. Any aluminosilicate materials can be used to prepare geopolymers, including fly ash and slag. Therefore, geopolymer concrete could possibly be utilized potentially as a replacement for OPC, however, this will only occur when both an efficient supply chain for raw materials and a supply network for the products are in place. In the present study, compressive and flexural strengths of GGBFS based geopolymers were investigated after 7, 28, and 90 days. From the results obtained, it can be observed that the dependency patterns during the different hardening times are comparable and maximum compressive strengths are reached at the maximum values of $\text{SiO}_2/\text{Na}_2\text{O}$ ratio 1.4 and Na_2O 6%. Compressive strengths were found to increase with increases in the $\text{SiO}_2/\text{Na}_2\text{O}$ ratio after all testing days. The ANOVA result states that the regression model is appropriate and that all input parameters are statistically significant and affect the compressive strength results.

Author Contributions: M.M., P.V., and T.H. carried out experiment. M.M., D.K., and M.S. wrote the manuscript. M.S. and D.K. supervise the experiment and conceived the original idea. D.K. processed the data. All authors discussed the results and contributed to the final manuscript.

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