



Article

Windthrow Dynamics in Boreal Ontario: A Simulation of the Vulnerability of Several Stand Types across a Range of Wind Speeds

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Abstract: In Boreal North America, management approaches inspired by the variability in natural disturbances are expected to produce more resilient forests. Wind storms are recurrent within Boreal Ontario. The objective of this study was to simulate wind damage for common Boreal forest types for regular as well as extreme wind speeds. The ForestGALES_BC windthrow prediction model was used for these simulations. Input tree-level data were derived from permanent sample plot (PSP) data provided by the Ontario Ministry of Natural Resources. PSPs were assigned to one of nine stand types: Balsam fir-, Jack pine-, Black spruce-, and hardwood-dominated stands, and, Jack pine-, spruce-, conifer-, hardwood-, and Red and White pine-mixed species stands. Morphological and biomechanical parameters for the major tree species were obtained from the literature. At 5 m/s, predicted windthrow ranged from 0 to 20%, with damage increasing to 2 to 90% for winds of 20 m/s and to 10 to 100% for winds of 40 m/s. Windthrow varied by forest stand type, with lower vulnerability within hardwoods. This is the first study to provide such broad simulations of windthrow vulnerability data for Boreal North America, and we believe this will benefit policy decisions regarding risk management and forest planning.

Keywords: ForestGALES_BC; Boreal; windthrow simulation; wind damage; forest disturbance

1. Introduction

Concepts like natural disturbance typing [1], the range of natural variability [2], and disturbance process domains [3] help researchers and managers consider and compare natural and human-induced disturbance regimes across landscapes. This is pertinent because across North America, forest management approaches inspired by natural disturbance dynamics are expected to lead to a more resilient landscape [4,5]. Implementing such an approach requires an understanding of disturbance processes and regimes at the tree, stand, and landscape scales [6,7]. Wind storms are a major disturbance process in North American forests [8].

Wind storm events in Boreal North America are driven by two major processes. First, extra-tropical cyclones produce moderate to high speed winds, over wide areas, primarily during the fall, winter, and early spring. These low pressure systems intensify over the Pacific and Atlantic oceans during winter months, and are driven by gradients in temperature between the tropical and polar oceans and resultant wind speeds can reach 30 m/s [9,10]. Inland Boreal regions with more continental

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climates experience intense thunderstorms in the late spring, summer, and early fall. These convective storms develop as a result of high surface heating and vertical temperature and pressure differentials. The resulting localized wind speeds are sometimes in excess of 40 m/s [11,12]. While wind speed is the main determinant of the severity of wind damage [13], other factors such as soil [14], stand demography [15,16], and management [17] could modify the impact.

Because wind storms are largely random, empirical studies are often only initiated after a windthrow event occurs. There are also approaches where hybrid-mechanistic windthrow prediction models have been developed for forest regions within windy climates [18,19]. Some of these models predict landscape-level susceptibility to windthrow [17], while others [18,19] simulate windthrow at the tree level. By simulating windthrow at the tree level, one is able to incorporate tree-specific traits and spatial arrangements [18], in addition to producing higher resolution characterization of post-storm stand conditions [19]. This is especially recommendable for regions with limited documentation of windthrow—as is the case for many inland Boreal regions in North America. However, by simulating at the tree scale, it becomes challenging to simulate a large number of stands across a broad and heterogeneous landscape. To circumvent this, one way would be to simulate a limited number of stand conditions and then develop relationships that could be applied at the landscape scale, thus, incorporating the local tree-level attributes.

In this study, ForestGALES_BC [19], a tree-level windthrow model was applied to study windthrow dynamics across a broad forest landscape in Boreal Ontario, a region that experiences recurrent thunderstorms. The goal of this work was to simulate windthrow for forest stands that are typical of Boreal Ontario. The key questions were (a) how does windthrow vulnerability vary across typical inland Boreal stand types, including hardwood, conifer, and mixed-species stands, and under regular as well as extreme wind speed scenarios [20] and; (b) how does this change with increasing stand development.

2. Methodology

2.1. Overview of Modelling and Simulation Steps

We commenced by acquiring tree-level data for forest types in the study region from a permanent sample plot (PSP) network. Basal area proportion by tree species was calculated and used to sort plots into forest stand types. Tree height modelling was carried out for trees with diameter at breast height (DBH) but missing height data. Based on the average tree height, plots were then assigned to height classes. Each forest stand type and height class is considered a simulation unit (space) to be run independently. A simulation space with several spatially-explicit set of individual trees belonging to a forest stand type and height class is hereafter called a 'treelist'. Treelists representative of each forest stand type and height class were loaded into the ForestGALES_BC model for simulation. For simulations to run smoothly, we needed to update ForestGALES_BC to include dendrometric and biomechanical equations for local species. Literature was reviewed for this purpose, and 17 published studies (Table S1) were retained which had the relevant data. With the treelists and the updated ForestGALES_BC, simulations were run for a series of increasing above-canopy wind speeds. Figure 1 illustrates the phases of this work.

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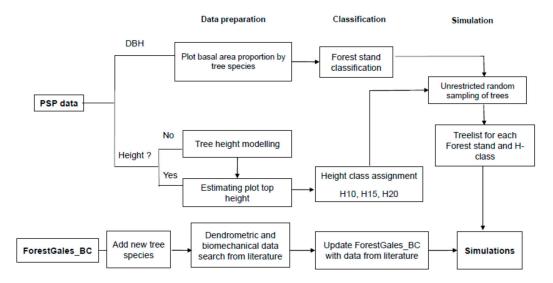


Figure 1. A schematic framework of the study methodological stages. H10, H15, H20 corresponds to height classes 10 m, 15 m, 20 m, respectively. PSP, permanent sample plot; DBH, diameter at breast height.

2.2. Data Acquisition

Tree and plot data for the study area was provided by the Ontario Ministry of Natural Resources (OMNR) from a PSP network [21] covering the Boreal forest region of western Ontario. These PSPs had been repeatedly measured between 1992 and 2005. For a given plot, only the most recent measurements were considered, yielding a database of 734 plots of 400 m² and composed of 13 tree species (Figure 2). A total of 731 plots were retained for further modelling work, as they represent the most common forest stand types of the study region.

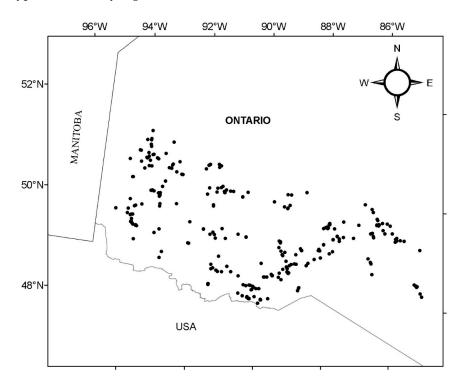


Figure 2. Study area map showing the distribution of the studied plots.

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2.3. Data Preparation

In order to allow windthrow simulations for the range of stand compositions that occur within the study region, basal area proportion was computed by species for each plot, with the resulting information used in identifying plots by stand type in the next phase.

Windthrow vulnerability typically increases with increasing stand height [19], and stand height is a surrogate of stand development and succession [22] and an important variable in growth and yield modelling. Also for predictive purposes, it is important to quantify the role of tree size (i.e., height and DBH) on windthrow [23]. Accordingly, each plot was assigned to one of three height classes. Across all species, there were trees in the database with DBH measurements but without height variable (Table S1), necessitating the development of predictive height models. In predicting tree heights, the modifier approach from [24] was followed, where the global average height (\overline{H}) across stand type and height classes is modified by DBH (f_{DBH}) and tree species (f_{syp}).

$$H = \overline{H} \times f_{DBH} \times f_{spp} \tag{1}$$

where f_{DBH} has a quadratic structure of the form:

$$f_{DBH} = 1 + \beta_l \left(\frac{\overline{DBH} - \overline{DBH}}{\overline{DBH}} \right) + \beta_q \left(\frac{\overline{DBH} - \overline{DBH}}{\overline{DBH}} \right)^2$$
 (2)

 β_l and β_q refer to the linear and quadratic correlates of DBH to the height variable. DBH refers to the tree-level DBH, \overline{DBH} is the global average DBH across stand type and height class.

 f_{spp} has a linear additive structure where the model variables are essentially binary:

$$f_{DBH} = 1 + \alpha_{B_{fir}} Z_{B_{fir}} + \alpha_{S_b} Z_{S_b} + \alpha_{S_w} Z_{S_w} + \alpha_{S_N} Z_{S_N} + \alpha_{C_w} Z_{C_w} + \alpha_{P_j} Z_{P_j} + \alpha_{P_W} Z_{P_W} + \alpha_{P_r} Z_{P_r} + \alpha_{L_a} Z_{L_a} + \alpha_{W_b} Z_{W_b} + \alpha_{A_W} Z_{A_W} + \alpha_{A_{WL}} Z_{A_{WL}} + \alpha_{B_p} Z_{B_p} + \alpha_{M_r} Z_{M_r}$$
(3)

 $Z_{B_{fir}}$, Z_{S_b} , Z_{S_w} , Z_{S_N} , Z_{C_w} , Z_{P_j} , Z_{P_w} , Z_{P_r} , Z_{La} , Z_{W_b} , Z_{A_w} , $Z_{A_{wL}}$, Z_{B_p} , Z_{M_r} are binary variables corresponding to Balsam fir (*Abies balsamea*), Black spruce (*Picea mariana*), White spruce (*Picea glauca*), Norway spruce (*Picea abies*), White cedar (*Thuja occidentalis*), Jack pine (*Pinus banskiana*), White pine (*Pinus strobus*), Red pine (*Pinus resinosa*), larch (*Larix laricina*), White birch (*Betula papyrifera*), trembling aspen (*Populus tremuloides*), large tooth aspen (*Populus grandidentata*), balsam poplar (*Populus balsamifera*), and Red maple (*Acer rubrum*), respectively.

 $\alpha_{B_{fir}}$, α_{S_b} , α_{S_w} , α_{S_N} , α_{C_w} , α_{P_j} , α_{P_w} , α_{P_r} , α_{La} , α_{W_b} , α_{A_w} , $\alpha_{A_{wL}}$, α_{B_p} , α_{M_r} are coefficients accounting for the differences in H = f(DBH) relationships by species, in the same order as above.

The predicted heights show a good fit with the actual heights (*R*-square = 0.87, Root Mean Square Error = 2.31, Figure S1). The predictive models (Table S3) were therefore used to estimate total heights for all trees with DBH and which did not have height.

2.4. Data Classification

2.4.1. Stand Type Grouping

Stand categorizations conform to the 'Forest Units' used in Ontario forest management planning [23] and were based on the computed percent basal area contributed by each tree species to the total plot basal area (Table 1).

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Table 1. Definition of stand types.

Name	Designation	Definition
Balsam fir dominated	BfDom	Balsam fir > 70
Jack pine dominated	PjDom	Jack pine > 70
Jack pine mixed stands	PjMx1	Red pine + Black spruce + Jack pine + White spruce + Balsam fir ≥ 70 AND Balsam fir ≤ 10 AND Poplar + White birch ≤ 20 AND Black spruce + White spruce < Jack pine
Black spruce dominated	SbDom	Black spruce > 70
Spruce mixed species	SbMx1	Red pine + Black spruce + Jack pine + White spruce + Balsam fir ≥ 70 AND Balsam fir ≤ 10 AND Poplar + White birch ≤ 20 AND Black spruce + White spruce > Jack pine
Conifer mixed species	ConMx	White pine + Red pine + Black spruce + White spruce + Balsam fir + Jack pine + White cedar + Larch \geq 50
Hardwood dominant	HrDom	Trembling aspen + White birch + Red maple + Balsam poplar ≥ 70
Hardwood-mixed species	HrdMx	Poplar + White birch + Red maple + Balsam poplar ≥ 50
Red and White pine mixed species	PrwMx	Red pine + White pine ≥ 40

2.4.2. Stand Height Classification

The average height of dominant trees within a plot corresponding to 100 top height trees/ha was calculated; for 400 m^2 plots, this means the average of four top height trees. Because we wanted to assign plots (not individual trees) to height classes, we used this plot-level metric, i.e., average of top height trees. Plots with top height < 13 m were placed in the '10 m' height class (H10). Plots with top height from 13 m to 18 m were placed in the '15 m' height class (H15), while stands with top height > 18 m were categorized as height class '20 m' (H20). The count of plots by stand type and height class can be found in Table 2.

Table 2. Plot distribution by stand type and height class.

Stand Type	Height Class			- Number of Plots	
Stand Type	H10	H15	H20	- Number of Flots	
Balsam fir dominated (BfDom)	6	0	0	6	
Jack pine dominated (PjDom)	122	70	15	207	
Jack pine mixed (PjMx1)	9	14	4	27	
Spruce dominated (SbDom)	87	29	5	121	
Spruce mixed (SbMx1)	23	8	2	33	
Conifer mixed (ConMx)	101	21	13	135	
Hardwood dominated (HrDom)	79	43	12	133	
Hardwood-mixed (HrdMx)	17	8	8	33	
Red and White pine (PrwMx)	12	12	12	36	
Total Plots	456	205	71	731	

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2.5. Simulation and Analysis

2.5.1. Model Framework

ForestGALES_BC was used for this modelling exercise [13,19]. This model includes five major components (i) an input dataset (treelist) and configuration; (ii) objects that calculate species-level dendrometrics (stem taper and tree characteristics objects); (iii) objects that model wind loading; (iv) a component that estimates tree resistance; and, (v) an output component (Flag tree object) where decisions are made as to whether a tree fails or stands. These objects are described in detail in Anyomi et al. [13].

First, dendrometric and drag data were added for tree species in the Ontario study area. Where there were no published critical turning moment or drag equations for a particular species, equations for surrogate species were used (Table S1). Surrogate species were selected in order of preference, first using data from the same species in the Boreal, or from elsewhere, then similar genus if available, and, if unavailable, a species whose properties would be comparable.

2.5.2. Simulation Space

To evaluate outcomes, a simulation space made up of five hundred $20 \text{ m} \times 20 \text{ m}$ cells was created for each stand type and height class combination. Using $20 \text{ m} \times 20 \text{ m}$ cells matches the 400 m^2 plot size of the OMNR sample plots. With 500 cells in the simulation space, wind fetch and damage propagation effects can be evaluated. Given that there are far fewer than 500 PSPs for each stand type and height class combination, we created additional plots for each combination in order to populate the simulation space. Starting with the treelist of all trees in the OMNR PSPs for a given stand type and height class, we applied unrestricted random sampling using the PROC SURVEYSELECT procedure (SAS v9.4, SAS Institute, Cary, NC, USA) to obtain a sufficient number of trees to populate additional individual cells, and then assembled these cells to make up a simulation space. The range of stand density of the underlying PSP plots in each of the stand types and height classes was the guiding rule, thus, only cells whose stems per hectare were within the range observed in the PSP plots were retained. These new cells were then randomly assigned to locations within the simulation space along with the original PSP plots. Figure S2 shows example simulation spaces for selected stand type and height class scenarios.

2.5.3. Estimating Resistive and Applied Moments

Dendrometric equations were used to convert DBH and height to stem shape, volume and mass, and tree crown breadth (width), depth (length), and mass for each tree in the treelist. These tree attributes were then used to estimate loading and resistance. Parameters for these dendrometric equations, along with modulus of rupture, stem density, drag, and critical turning moment equations were obtained from the literature (Table S1). For a given tree in the simulation space, when the applied moment due to the force of the wind is higher than the resistive moment of the tree to breakage or uprooting, the tree fails. Failed trees are marked as such in the treelist and are dropped from subsequent calculations of stand canopy density and within-canopy wind speed profiles. The model runs iteratively until such time when at the specified above-canopy wind speed, the resistive moment is higher than the applied moment for all surviving trees, or when the specified maximum number of iterations is reached.

2.5.4. Synthesizing Damage Outcomes

The wind damage level for a given cell within the simulation space was computed as the percentage of cell initial basal area that was uprooted or broken. Windthrow percentage was averaged for all cells within the simulation space to yield overall percent windthrow for a simulation run. Simulations for each stand type and height class were run for above-canopy wind speeds from 5 to 40 m/s in increments of 5 m/s. Smoothened curves were obtained from the raw simulated values and the smoothened data was then used in further analysis. Smoothing removes some of the variability introduced by using different groups of PSPs to create the input treelists for different height classes of the same stand type. Logistic equations were fit to produce families of curves. Examining the parameter values of the single global equation also facilitates comparison of species and height effects on vulnerability. When subsequently used in landscape-level simulations of wind disturbance patterns, these equations allow for interpolation of windthrow outcomes for stand heights and above-canopy wind speeds between those tested in our simulations:

$$W_{\%} = \alpha^{(-H_c)^{-\beta U}} \tag{4}$$

where $W_\%$ refers to the basal area proportion windthrown per plot, U is the above-canopy wind speed in m/s, α and β are the asymptote and rate parameters respectively. H_c adjusts the curve along the wind speed axis as a function of the stand height class. This model form was selected due to its sigmoid shape, providing a suitable fit for the shape of the windthrow vs. wind speed results. The fit statistics including the Akaike Information Criterion (AIC), the Root Mean Square Error (RMSE), and adjusted R-square were examined for goodness-of-fit. The logistic model predictions are hereafter called 'predicted estimates', while the ForestGALES_BC model simulations are called the 'simulated estimates'.

2.5.5. Evaluating Damage Outcomes

The ForestGALES_BC model was validated [19] and a similar adaptation in Quebec provided reasonable results [13]. For a complete validation of model simulations, windthrow data for different storms of known intensity and for a range of stand types would be required. In this study, we reviewed literature for published windthrow data from natural forests at known wind speeds. Model bias was computed as the difference between the expected or average prediction of our model and the observed or the average reported in literature.

3. Results

3.1. Windthrow Damage Outcomes

The level of windthrow varies with stand type, height class, and above-canopy wind speed. Curves are sigmoidal, with substantial increases in windthrow for above-canopy wind speeds over 15 m/s, reaching maximum levels of damage for winds over 25 m/s particularly for the tallest stands (Figure 3). In most cases, complete canopy failure occurs at wind speeds of 40 m/s.

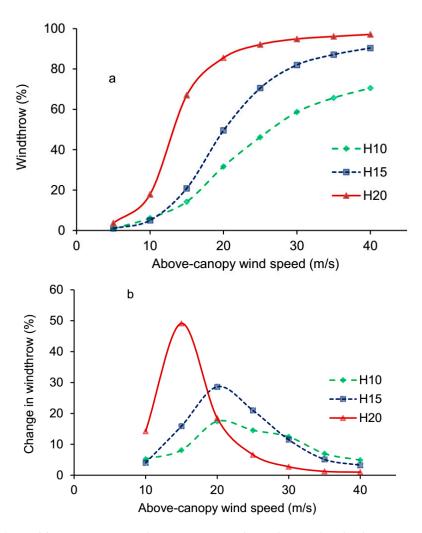


Figure 3. (a) Windthrow response to above-canopy wind speed across height classes. H10, H15, H20 correspond to 10 m, 15 m, and 20 m height classes, respectively. (b) Change in percent windthrow with increasing above-canopy wind speed across all stand types.

Percent windthrow varies by stand type (Figure 4 and 5, Table S4). Across a range of stand height classes, mixed stands of Red and White pine (Figure 4e) were more vulnerable to winds than other stand types. For the H10 height class and below 20 m/s, Balsam fir dominated stands (Bfir) were the most easily windthrown of all stand type and height class combinations. Hardwood dominated stands (Figure 4f) and mixed conifer-hardwood stands appear to be most resistant to windthrow across the range of wind speeds studied (Figure 4h). Among the taller stands (height class 20 m), Jack pine mixed stands (Figure 4c) and hardwood-mixed stands (Figure 4g) are the most resistant to windthrow.

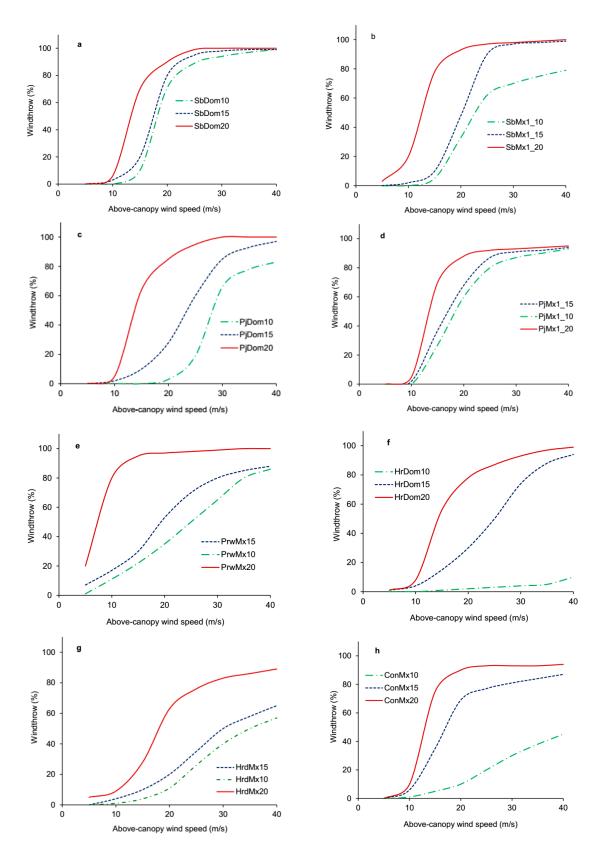


Figure 4. Proportion of plot total basal area windthrown at specific above-canopy wind speeds for the forest types: (a) spruce dominant; (b) spruce mixed stands; (c) Jack pine dominant; (d) Jack pine mixed; (e) Red and White pine mixed stands; (f) hardwood dominant stand type; (g) hardwood-mixed species stands; (h) Conifer mixed species stands, and by height class groups: 10 m, 15 m, and 20 m.

3.2. Generalizing Windthrow Simulations

Our analysis shows that wind speed explains most of the variability in the windthrow levels (Table 3). The logistic modelling to obtain a global model produces reasonable fits (Adjusted R-square = 0.75, RMSE = 0.10, AIC = -310.5; Figure 5).

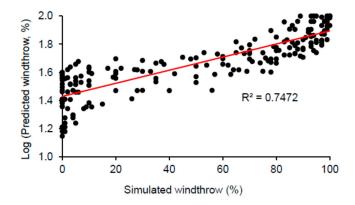


Figure 5. Scatter graph showing the fit between the simulated and predicted percent windthrow estimates.

Table 3.	Variability	in windthrov	v explained	by wind	speed, sta	ınd height clas	s, and stand type.

Source	Degrees of Freedom	Type III Sums of Square	Mean Square	F Value	<i>Pr</i> > <i>F</i>	Variance Explained
Wind speed	1	178,922.04	178,922.04	555.17	< 0.0001	60%
Height class	2	39,620.38	19,810.19	61.47	< 0.0001	13%
Stand type	8	22,900.97	2862.62	8.88	< 0.0001	8%
2.1						81%

Examining the parameters of the equations provides additional insights into stand type vulnerabilities. Based on the rate of change of windthrow with above-canopy wind speed, there appears to be two stand type clusters. The first cluster (β parameter) includes Balsam fir dominated stands, hardwood dominated stands, and hardwood-mixed species stands. A second cluster (α parameter) is made up of conifer mixed species stands, Jack pine dominated stands, Jack pine mixed species stands, Red and White pine mixed stands, Black spruce dominated stands, and spruce mixed stands. Hardwood dominant stand type and hardwood-mixed species stands have the lowest asymptote, while Jack pine mixed species stands, Red and White pine mixed species stands, and Black spruce dominated stands had the highest asymptote, albeit with similar values. The asymptote relates directly to the level of windthrow—the higher the asymptote the higher the overall level of windthrow for a given wind speed (Table 4, Table S4).

Table 4. Smoothed windthrow vs. windspeed model parameter estimates.

Stand Type	Designation	α	β	
Balsam fir	Bfir	29.304	0.003	
Conifer mix	ConMx	20.377	0.002	
Hardwood dominant	HrDom	12.058	0.003	
Hardwood mix	HrdMx	13.268	0.003	
Jack pine dominant	PjDom	20.106	0.002	
Jack pine mix	РјМх	32.013	0.002	
Red and White pine mix	PrwMx	32.926	0.002	
Black spruce dominant	SbDom	33.209	0.002	
Spruce mix	SbMx	26.769	0.002	

3.3. Evaluating Model Simulation Outcomes

Table 5 presents data on windthrow damage levels observed following storm events, and the corresponding simulated windthrow, showing that, overall, the model did better within the coniferous (Bias = +10%) stands relative to the hardwoods (+27%).

Species	Wind Speed (m/s)	Percent Windthrow Simulated, Min–Max (Average)	Percent Windthrow from Literature	Bias	Reference
Balsam fir	25	67	60	7	[13] #
Spruce	>53 >53 >20 33–44	71–100 (94)	$54.6 (S_b)$ $25.5 (S_w)$ $73.2 (S_n)$ $70 (S_r)$	38.2	[25] [25] [26] # [27]
Aspen	>20 >53	83–100 (93)	74.5 69.9	20.8	[26] [#] [25]
Birch	17 >20 33-44 >53	2–99 (54)	20 65.7 40 17.8	18.1	[28] # [26] # [27] [25]
Pine	>53 >53 55	1–99 (49)	82.4 (<i>P_j</i>) 77.1 (<i>P_r</i>) 33 (<i>P_m</i>)	-15.2	[25] [25] [29] #
White cedar	>53	10–99 (68)	12.4	55.6	[25]
Larch	21.1–32.5 9	2–97 (51) 4	2 (<i>L_e</i>) 11 (<i>L_k</i>)	49.7	[30] [#] [31]
Overall				22.8	

Table 5. Windthrow damage levels reported in literature by species.

4. Discussion

This is the first attempt at developing hybrid-empirical-mechanistic models for a region with a widely varying range of forest types and height classes, including conifer and hardwood species, and examining stand vulnerability across a wide range of wind speeds. A major challenge to windthrow model validation is that, often when there is field windthrow data, damage comes from a suite of storms of different intensities, and wind speed is rarely recorded. Also, topography and cutblock configuration could induce major variations in local wind speed, thus, the data from literature represent approximations of likely damage levels for the stand types and wind speed. The simulated windthrow compares well with published results for post-storm studies where wind speeds have been documented or estimated. Our results show three things: (a) the above-canopy wind speed is the primary determinant of the level of windthrow for any stand type; (b) the average stand height (stand development) is directly correlated with windthrow; and (c) that species composition affects the vulnerability to windthrow. These are consistent with earlier work that reported that 60% of the variability in windthrow damage is due to the wind speed, with species type and tree height explaining 9% and 6%, respectively, of the total variability [23]. Our simulations for Canadian Boreal forest types indicate that, on average, 30% of the forest canopy would be lost at above-canopy wind speeds of 72 km/h (20 m/s), similar to selection cut removals in the regions [13,24].

Our simulations suggested that hardwood dominated stand types and mixed conifer-hardwood stands are more resistant to windthrow for a given wind speed, supporting observations from North American forest systems [32]. Models have predicted hardwood expansion driven by climate change [33] and, given the lower susceptibility of hardwoods to wind storms, there could be a positive feedback into the disturbance regime such that windthrow damage would decline within hardwoods [34].

^{**} Stand-level, S_b —Black spruce, S_w —White spruce, S_n —Norway spruce, S_r —Red spruce, P_j —Jack pine, P_r —Red pine, P_m —Maritime pine, L_e —European larch, L_k —Japanese larch.

Stand types which experience high windthrow damage at relatively low wind speeds—in our case, Red and White pine mixed species stands and Balsam fir stands—are more likely to experience stand-replacing events. If these stands regenerate to the original species, in similar proportions, then cycles of recurrent damage and replacement are expected [35]. The duration of each cycle will depend upon species growth rates and site productivity. Stand types that experience partial damage (in our study, the mixed conifer-hardwood stands), even at high wind speeds are more likely to persist as multi-aged and mixed species stands, promoting structural diversity [36].

In Boreal North America, forest carbon stocks are simulated for both aboveground and belowground processes [37], as required under the Kyoto Protocol. However, owing to the non-availability of data on windthrow, windthrow related changes in carbon dynamics has yet to be incorporated into terrestrial ecosystem carbon budgeting for Boreal North America. In a similar work done in Europe, Fortin et al. [38] reported an 8% overestimation of ecosystem carbon as a result of not accounting for windstorm impacts on managed European beech stands. We believe our windthrow tables provide a starting point for integrating windthrow into ecosystem carbon simulation.

Our results represent stand-level simulations that could be incorporated into landscape-level simulators in studying forest landscape dynamics [39,40]. Wind-driven disturbances could be simulated concurrently and interactively with other landscape-scale disturbances such as wildfire. For example, our windthrow simulations can be integrated with the OMNR's BFOLDS (Boreal Forest Landscape Dynamics Simulator) fire disturbance and succession model [41]. Tree height as a class variable would impact the results of this integration, however, the fitted smoothed curves could be used for interpolating damage between height classes.

There are a number of ways of improving on our work. There is no winching or drag data for some local species and the relationship between their actual properties and those of the surrogate species we used is unknown. However, using winching data from other regions is standard within the global set of hybrid-mechanistic windthrow prediction models [42], and where these models have been validated, has been shown to be reasonable [43]. We also believe the use of surrogate species is reasonable since often species from the same genus show similar relationships [15,43–53] between stem mass and critical turning moment. However, as local data on windthrow outcomes become available, in particular data from thunderstorms (summer wind storms), simulated outcomes can be checked, parameter values updated, and the simulations re-run. By studying forest landscape by forest stand type and height classes, we believe site related variability in the resistance to windthrow was indirectly accounted for, however, we recommend that future work should verify the impact of soil on windthrow vulnerability.

5. Conclusions

ForestGALES is one of the most validated windthrow models [42]; the windthrow processes appear adequately represented and as demonstrated in this work, with the appropriate species parameters the model could be exported successfully. This simulation is the first study to explore windthrow vulnerability for a broad range of inland Boreal forest stands of North America and shows that irrespective of the forest cover type, the intensity of wind primarily drives windthrow severity, with lower and upper wind speed limits for partial and complete damage. Vulnerability to windthrow increases with stand development (height), and varies between stand types, with implications for forest management and succession in these recurrently wind disturbed landscapes. The simulation approach we have demonstrated could be integrated with fire disturbance modelling and incorporated into landscape succession models to examine long-term landscape dynamics under current and future climates.

Supplementary Materials: The following are available online at www.mdpi.com/1999-4907/8/7/233/s1, Figure S1: Observed vs. predicted heights and the distribution of the residuals; Figure S2: Simulation space for selected stand types (a) Conifer mixed stands, (b) Hardwood-mixed stands, (c) Hardwood dominant stand, (d) Spruce mixed stands; Table S1: Sources of data in adapting ForestGales_BC to Boreal Ontario; Table S2:

Characteristics of trees with and without height variable prior to tree height modelling; Table S3: Model [1] parameter estimates; Table S4: Variability in windthrow by stand type, height class, and above-canopy wind speed. *Height_Model.csv*; Tree-level data used in developing predictive height model. *Stand_Type.xls*; Plot-level data used in assigning stand type and height classes.

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