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Wood Density Determination by Drilling Chips Extraction in Ten Softwood and Hardwood Species

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Abstract: *Research Highlights:* The novelty of this study is the development of an accurate wood density estimation method based on a relatively brand new semi-destructive testing technique (drilling chips extraction). This method is especially crucial in the assessment of existing timber structures. *Background and Objectives:* Probing, drilling, and coring are non-destructive and semi-destructive techniques commonly used for timber density estimation in existing timber structures. Most of these techniques show poor or medium accuracy or are so expensive or destructive. This paper aims to obtain accurate estimation models for wood density in existing structures using the easy to use drilling chips extraction technique. *Materials and Methods:* 300 specimens ($95 \times 65 \times 200$ mm³) from ten softwood and hardwood species covering a wide range of density (from 350 to 980 kg·m⁻³) were tested after conditioning. The Wood Extractor device based on the drilling chips extraction technique was used in the radial and the tangential direction. Mass of the chips collected (drilling residue) from each drill was recorded. *Results:* Density obtained from drilling residue was not statistically significantly different between radial and tangential directions avoiding take into account direction when measuring. The density obtained in the whole specimens is slightly higher than the density obtained by drilling residue being this difference uniformly through the range of densities studied. Two different estimation models were presented with high determination coefficients (96% and 97%) and low standard errors. These results were similar to those obtained by other authors using core drilling but causing less damage. *Conclusions:* Drilling chips extractor is a simple, reliable and inexpensive method to estimate density in existing structures with accuracy.

Keywords: Non-destructive testing; semi-destructive testing timber structures assessment; Wood Extractor

1. Introduction

To retrofit the existing timber structures with renovation and restoration works, it is previously necessary the characterization of wood singularities (knots, cracks, *etc.*), biologic degradation, and the estimation of the mechanical properties [1–6]. Non-destructive and semi-destructive testing (NDT/SDT) includes accurate, dependable and easy to use techniques for estimation of timber mechanical properties in the assessment of existing timber structures [7–11].

Many researchers combine several NDT techniques results to increase accuracy and safety in the evaluation of timber structures [12–16]. Density is probably the essential property estimated because it is closely correlated with other wood mechanical properties [17,18], and it has been traditionally

considered a fundamental parameter as a wood quality indicator [19]. Furthermore, combining wood density with other NDT results, as the velocity of acoustic wave propagation, dynamic modulus of elasticity is calculated [20–25].

There are several NDT techniques, sometimes considered SDT, to estimate wood density [26–28]. However, its application over existing timber structures sometimes is difficult, and these local measurements show medium correlation with the real densities.

The pullout resistance technique using the commercial device Screw Withdrawal Resistance Meter (Fakopp, Sopron, Hungary), has been extensively used to estimate density over existing timber structures for a long time. However, low determination coefficients (r^2) with values from 50% to 67% [29–31] are achieved by this technique. The needle penetration resistance technique, which relates the wood resistance to insert a needle with a constant force to wood density, has been used initially on forest works to estimate the density on standing trees, with a commercial tool as Pilodyn (Proceq, Schwerzenbach, Switzerland) [32,33]. This technique was also used on timber structures, though its results showed scattered r^2 , from 50% to 61% achieved on softwoods [34,35], to values from 0.75 to 0.84 reported on hardwoods [36].

Another NDT technique less commonly used to estimate wood density is the infrared thermography. Nevertheless, some parameters, as the influence of knots or fissures, are still not well defined; this technique achieves over clean wood values of r^2 upper to 90% [37].

This r^2 scattered in results has generated new investigations to achieve and develop more reliable tools to estimate wood density. Resistograph techniques show as the most accurate tool to estimate local wood density, with a value of r^2 in a range from 80% to 90% [38–40]. This complex, and expensive, the equipment uses a small drill that penetrates inside the wood with a constant speed, recording the wood resistance to the penetration allowing density estimation [41,42]. The core drilling technique (CDT) is an inexpensive method based on the obtention of wood samples making a small hollow drill. This technique has been widely used on standing trees to determine differences in physical and mechanical properties as density or moisture content (MC) with good results [43–45]. The r^2 of this technique achieves values upper to 80% [2,39] and in some assessment of softwood timber structures an r^2 of 89% was reported [46,47].

In the present study, a relatively brand new SDT device to estimate wood density using the drilling residue is analyzed. The Wood Extractor [48] not only estimates density from duster residue collected from drilling but also estimates MC. Previous studies using pine species showed an r^2 of 84% [49,50].

There are currently no simple, economical, reliable and accurate NDT or SDT methods that can estimate wood density in a wide range of density values. The drilling residue technique meets these parameters, but there are no data available for very low or high wood densities.

Besides, this drilling chips extraction technique has a potential application in forestry to estimate the density of standing trees. Current device has been developed to estimate wood density under conditions of wood MC below the fiber saturation point. However, with a little adaptation, this device could also be used to measure on greenwood (trees). Our preliminary tests showed promising results [51]. This paper aims to obtain reference values to estimate wood density in existing structures using the drilling chips extraction technique. Being able to use in the entire spectrum of densities used in construction and without species identification.

2. Materials and Methods

2.1. Drilling Residue Collection Device

The Wood Extractor device developed and patented by Martínez, and Bobadilla [48] has been used to estimate the density of wood. This device was designed to be coupled to a commercial power drill to collect all the waste that is produced during drilling in a single-use paper bag filter [50]. This device involves setting drill diameter (8 mm) and depth (47.7 mm), giving a known removed volume of wood (2.4 cm³). After drilling and the collection of residues in the filter, the sample is weighed to estimate wood density according to Equation 1. The operation of the device is based on harnessing

the movement of air produced by the turbine of a conventional drill to suck up the chips produced by drilling a hole and encapsulating them in a one-use filter (0.22g constant mass of filter)(Figure 1).

$$\rho = m/v \quad (1)$$

Because the chips and dust generated during drilling are absorbed and stored in the filter bag, the worker doesn't need special protective equipment, unlike what is stated in the CDT [52].

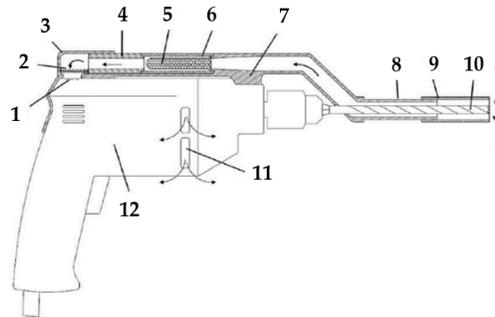


Figure 1. Cross-section view of the Wood Extractor device. Main components: 1 air intake, 2 spring, 3 enveloping structure, 4 telescopic tube, 5 paper filter bag, 6 cartridge, 7 clamp, 8 coaxial pipes, 9 telescopic system, 10 drill bit, 11 side holes, 12 power drill. The arrows indicate airflow.

2.2. Wood Specimens

Density estimation was carried out on 300 pieces from ten softwoods and hardwoods commonly used in construction in Spain with an extensive density distribution (350 to $980 \text{ kg}\cdot\text{m}^{-3}$), (Table 1). 30 specimens were tested per species with dimensions of $95 \times 65 \times 200 \text{ mm}^3$.

Table 1. Common and Botanical names of wood species tested.

Number	Common Name	Botanical Name
1	Western red cedar	<i>Thuja plicata</i> Donn ex D. Don
2	Black poplar	<i>Populus x euroamericana</i> (Dade) Guinier
3	Radiata pine	<i>Pinus radiata</i> D. Don
4	Maritime pine	<i>Pinus pinaster</i> Ait. ssp. <i>mesogeensis</i> Fieschi & Gaussen
5	Scots pine	<i>Pinus sylvestris</i> L.
6	Salzmann pine	<i>Pinus nigra</i> Arnold. ssp. <i>salzmannii</i> (Dunal) Franco
7	Sweet chestnut	<i>Castanea sativa</i> Mill.
8	European oak	<i>Quercus robur</i> L.
9	Iroko	<i>Milicia excelsa</i> (Welw.) C.C. Berg.
10	Missanda	<i>Erythrophleum</i> Afzel ex G. Don Sp.

2.3. Density Estimation

Conditioned specimens, in a climatic chamber at $20 \pm 2^\circ\text{C}$ and $65 \pm 5\%$ relative humidity (approx. 12% equilibrium moisture content), were sized with a resolution of 0.01mm and weighed with a resolution of 0.01g to obtain their density according to Equation 1; where ρ is the density in $\text{kg}\cdot\text{m}^{-3}$, m is the mass in kg and v is the volume in m^3 .

Two tests per specimen were performed following the methodology described in Martínez et al. [51], one in radial direction and another in tangential direction. The location of the tests is shown in Figure 2. Each extraction was weighed with a resolution of 0.01g, and the diameter and depth of each hole were measured with a resolution of 0.01mm. For each sample, the density of the wood extracted in each of the holes was calculated according to Equation 1, using the nominal volume of the hole and the mass of the chips removed, discounting the mass of the filter.

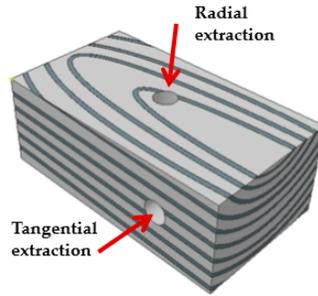


Figure 2. Specimen and sampling locations.

3. Results and Discussions

The mean density values (ρ) of the specimens and drilling residue and their coefficients of variation (COV) are listed in Table 2. A higher COV for pine species (around 9%) than for the other species (about 4%) was reported. This higher COV may be due to the significant differences between sapwood and heartwood proportions in the pine specimens and the high resin content typical of maritime pine.

Table 2. Average densities of specimens and drilling residue.

Sp.	Specimens Density (ρ)		Drilling Residue Density (ρ)					
			ρ radial		ρ tangential		ρ mean	
	Mean ($\text{kg}\cdot\text{m}^{-3}$)	COV (%)	Mean ($\text{kg}\cdot\text{m}^{-3}$)	CO V (%)	Mean ($\text{kg}\cdot\text{m}^{-3}$)	CO V (%)	Mean ($\text{kg}\cdot\text{m}^{-3}$)	CO V (%)
Western red cedar	347	1.7	336	5.5	352	3.7	344	2.5
Black poplar	504	2.4	485	3.6	497	4.9	491	3.5
Radiata pine	476	8.9	465	9.9	455	11.8	461	9.7
Maritime pine	543	9.6	507	10.0	516	9.9	511	9.6
Scots pine	573	6.3	533	9.6	542	11.9	538	9.7
Salzmann pine	585	12.1	567	13.2	562	12.6	565	12.7
Sweet chestnut	615	7.7	580	9.1	590	8.4	585	8.5
European oak	672	3.5	664	5.0	681	4.3	673	4.2
Iroko	617	5.0	558	6.0	544	6.4	551	5.7
Missanda	975	1.2	937	1.9	935	2.3	936	1.9
Average of all	593	27.1	561	27.6	568	27.1	566	27.2

Normality was verified for each variable. No significant differences between radial and tangential drilling residue densities at 95% confidence level (ANOVA P value = 0.9245) were found (Figure 3). Martínez et al. (2018) declared similar findings in the case of pine species. CDT, pullout resistance and needle penetration resistance measurements also showed no differences [29,46,52,53].

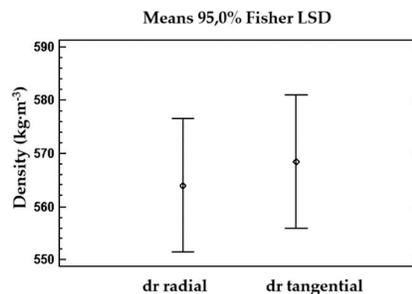


Figure 3. Means plot of density of drilling residues(dr) from radial and tangential holes.

Since there was no statistically significant difference between the densities of the residues in the radial and tangential direction, from now on, the study was carried out with the average of both values.

Table 2 and Figure 4 show slightly lower drilling residues densities than specimen densities except for European oak. Drilling residue density was on average 4% lower than specimen density, and there was not a statistically significant difference between the two values measured (ANOVA P value = 0.0525), with a level of confidence of 95%. Similar behaviour was reported by Martínez et al. [50] whose explanation was: “This may be mainly due to three reasons: first, there is a possible loss of material (wood dust) during drilling; second, moisture is lost from drilling residue due to the increased temperature caused by friction between the bit and wood; and finally, when a hole is drilled in wood the bit produces a transversal embedment compression perpendicular to the grain in the inner walls of the hole, so the extracted volume of wood is less than the volume of the hole”.

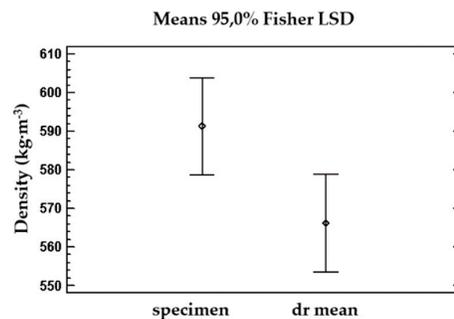


Figure 4. Means plot of density obtained by specimens and by drilling residues.

As is shown in Figure 5, the centre of the distribution of variation of the density (around 0.96) between the drilling residues and the specimens is uniformly distributed throughout all the densities studied. It can be concluded that the loss of mass during the extraction of the drilling residues is constant and does not depend on the density of the specimen.

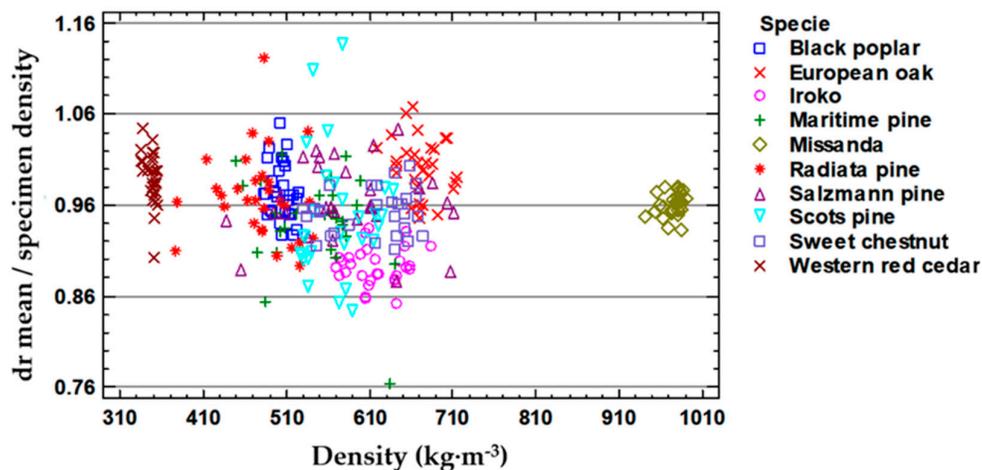


Figure 5. Distribution plot of the ratio of dr density/specimen density depending on the specimen's density.

Taking into account that the volume used to calculate the drilling residue density is constant (nominal volume of the hollow), the authors propose a regression model to correlate the mass of the chips collected during drilling including the filter bag and the specimen density. A robust statistical relationship between the average of radial and tangential drilling residue mass and the specimen

mass was found (P -value < 0.002). Therefore, a linear regression model to estimate specimen density using drilling residue mass as a predictor variable was developed.

The assumptions of normality, homoscedasticity and linearity were tested. The resulting model is shown in Equation (2) and Figure 6.

$$\rho = 433.372 \cdot dr_{\text{mean}} - 105.816 \quad r^2 97.38\%, \text{StE } 26.07 \text{ kg}\cdot\text{m}^{-3} \quad (2)$$

Where “ ρ ” is the specimen density in $\text{kg}\cdot\text{m}^{-3}$ and “ dr_{mean} ” is the drilling residue mean mass in g (including the filter bag). StE is the standard error. The relation is significant at a confidence level of 95%.

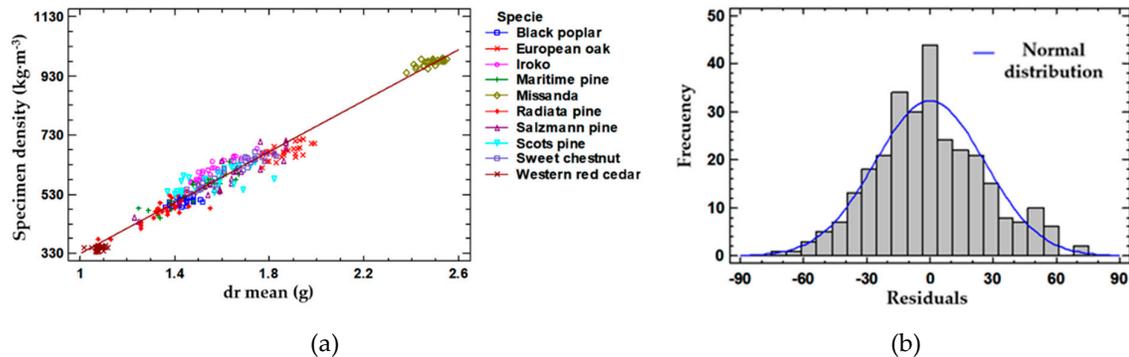


Figure 6. Linear regression between specimen density and drill residue mass mean of radial and tangential results. (a) Plot of the fitted model; (b) Frequency histogram of the model residuals.

In the previous model, two measurements in radial and tangential direction are needed. In the assessment of existing timber structures, the test direction is usually unknown, and it is difficult to have access to more than one face of the timber element. As no statistically significant differences between radial and tangential direction were found, a new estimation model using all mass values without taking into account the test direction was developed.

The assumptions of normality, homoscedasticity and linearity were tested. The resulting model is shown in Equation (3) and Figure 7.

$$\rho = 428.66 \cdot dr - 97.593 \quad r^2 96.26\%, \text{StE } 31.01 \text{ kg}\cdot\text{m}^{-3} \quad (3)$$

Where “ ρ ” is the specimen density in $\text{kg}\cdot\text{m}^{-3}$ and “ dr ” is the drilling residue mass in g (including the filter bag). StE is the standard error. The relation is significant at a confidence level of 95%.

The exposed models present almost the same accuracy and standard error as the CDT (r^2 98%, StE $22\text{kg}\cdot\text{m}^{-3}$) [52] but producing a hole (2.4 cm^3) equivalent to one-eighth of the volume generated in core extraction (18.8 cm^3).

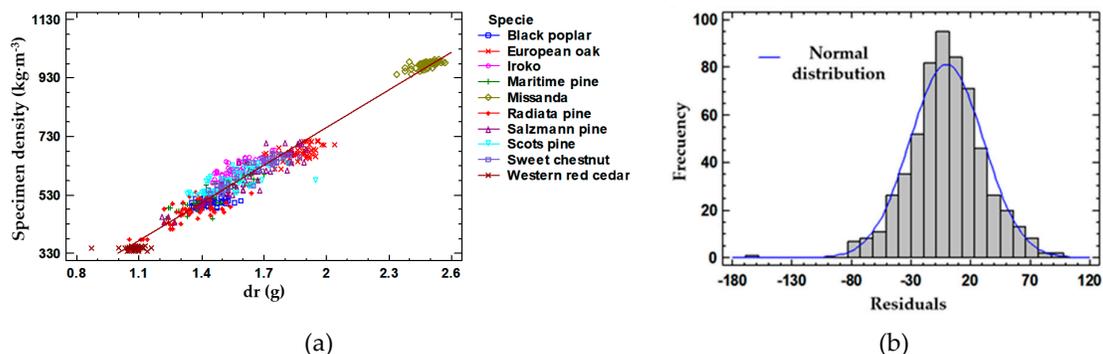


Figure 7. Linear regression between specimen density and drill residue mass. (a) Plot of the fitted model; (b) Frequency histogram of the model residuals.

Finally, two linear regression models to estimate softwood and hardwood specimen density separately using drilling residue mass as a predictor variable were developed. In both models, the assumptions of normality, homoscedasticity and linearity were tested. The resulting models are shown in Equation 4 and Equation 5. Where “ ρ ” is the specimen density in kg m^{-3} and “ d_{rmean} ” is the drilling residue mean mass in g (including the filter bag). StE is the standard error. The relation is significant at a confidence level of 95%.

Softwood model (Western red cedar, Radiata pine, Maritime pine, Scots pine and Salzmann pine).

$$\rho = 433.037 \cdot d_{\text{rmean}} - 109.546 \quad r^2 92.78\%, \text{StE } 26.70 \text{ kg}\cdot\text{m}^{-3} \quad (4)$$

Hardwood model (Black poplar, Sweet chestnut, European oak, Iroko and Missanda)

$$\rho = 423.696 \cdot d_{\text{rmean}} - 86.149 \quad r^2 97.06\%, \text{StE } 27.84 \text{ kg}\cdot\text{m}^{-3} \quad (5)$$

As can be seen, the models for softwood and hardwood (equations 4 and 5) present an r^2 and a StE similar to the model obtained with the ten species (equation 2).

For density estimation in large timber pieces, the author recommends several measurements in different areas due to the variability of wood density within the same piece.

The number of measurements will depend on the overall dimensions of the piece. Bobadilla et al. [29] proposed a measure per meter, and if possible, in different faces. For structural timber members, Osuna-Sequera et al. [54] recommended to carry out a minimum number of three or four measurements using Wood Extractor, commencing readings in the central one-third of the piece (the area of the maximum bending moment)

It is strongly recommended to seal drill holes left in the tested wood by wooden dowels to avoid the laying of xylophagous insect eggs, the penetration of fungi and for aesthetic reasons.

4. Conclusions

Wood density estimation models using drilling residue mass as a predictor were developed using ten softwood and hardwood species with a wide range of densities (from 350 to 960 $\text{kg}\cdot\text{m}^{-3}$). The first model considered average sawdust and filter mass as well as radial and tangential directions. It gives a 97.38% determination coefficient. As no statistically significant difference was found between radial and tangential results, a second model considering sawdust and filter mass while omitting direction was developed, resulting in a determination coefficient of 96.26%.

Given the very high coefficients of determination obtained (97 and 96%) and the low associated standard errors (26 and 31 $\text{kg}\cdot\text{m}^{-3}$), the drilling chips extraction method can be considered as a determination of wood density rather than an estimation.

The drilling chips extraction technique is as accurate as the core drilling technique for wood density determination but producing eight times less damage.

In summary, drill residue collection is a simple, reliable, accurate, and inexpensive semi-destructive method for wood density estimation and the holes left in the wood do not have a significant effect on the mechanical properties.

5. Patents

Martínez R, Bobadilla I (2013) Extractor de muestras de madera mediante taladro (Wood sample extractor using a conventional drill). Spain, ES2525504. (B27C 3/00) (2006.01), 16 Nov 2015. Appl. 201330890, 14 Jul 2013.

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