

Supplementary Materials: UV-Assisted 3D Printing of Glass and Carbon Fiber-Reinforced Dual-Cure Polymer Composites

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The viscosity curves of all formulations investigated in this work were fitted by the power-law equation (Equation (1) in the main manuscript). The calculated values of the consistency index K and power-law index n are shown in Tables S1 and S2 and the consistency index K is plotted as a function of SiO_2 concentration in the blends in Figures S1 and S2.

Table S1. Values of the power-law index n and of the consistency index K for B33 formulations (dual-cure blend containing 33 wt. % of photocurable acrylic component).

SiO₂ wt. % in the Blend	K	n
0 (B33)	22.31	0.99
3	20.56	0.76
5	158.15	0.43
7	795.26	0.11

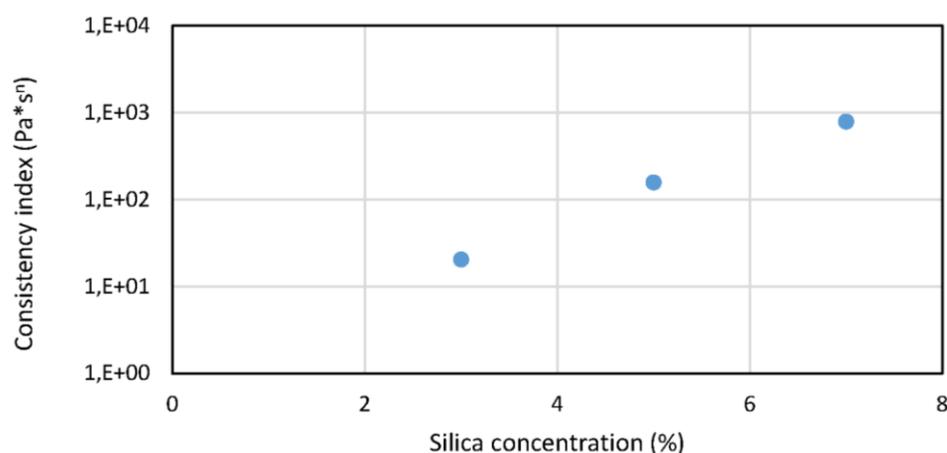


Figure S1. Consistency indexes K as a function of SiO_2 concentration for B33 formulations (dual-cure blend containing 33 wt. % of photocurable acrylic component).

Table S2. Values of the power-law index n and of the consistency index K for unfilled (B33 and B50) and CFR (B50C5) composite formulations. For comparison, CFR and GFR composite formulations without the addition of SiO_2 are also presented (B50C5-no SiO_2 and B33G5-no SiO_2 , respectively).

SiO₂ wt. % in the Blend	K	n
B33	919.16	0.14
B50	996.51	0.12
B50C5	803.33	0.20
B33G5-noSiO₂	4.67	0.97
B50C5-noSiO₂	3.46	1.00

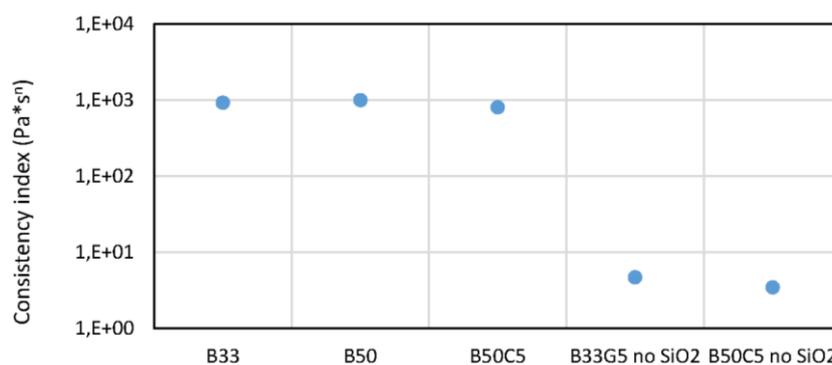


Figure S2. Consistency indexes K as a function of SiO₂ concentration for unfilled (B33 and B50) and CFR (B50C5) composite formulations. For comparison, CFR and GFR composite formulations without the addition of SiO₂ are also presented (B50C5-noSiO₂ and B33G5-noSiO₂, respectively).

A low-cost home-assembled 3Drag 1.2 benchtop printer (Futura Elettronica, Italy) incorporating a syringe dispenser with a 0.84 mm diameter nozzle was equipped with two 3W UV-A torches (WF-501B by Ultrafire Ltd., Shenzhen, China) on the printing head with light emission peaked at 405 nm (Figure S3).

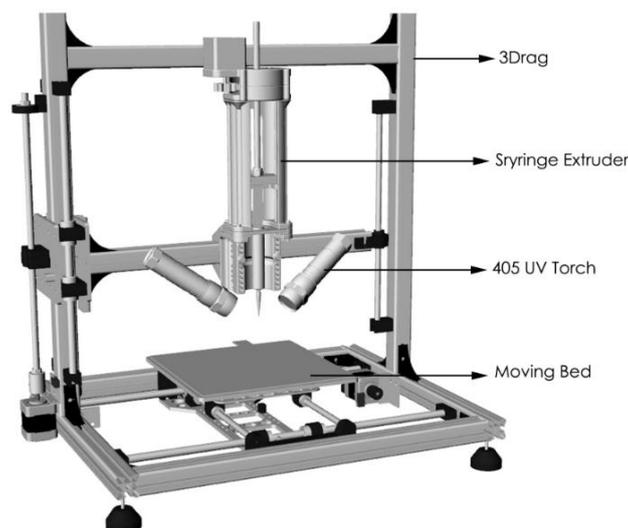


Figure S3. Schematic representation of the 3D printer equipped with UV-torches used in this work.

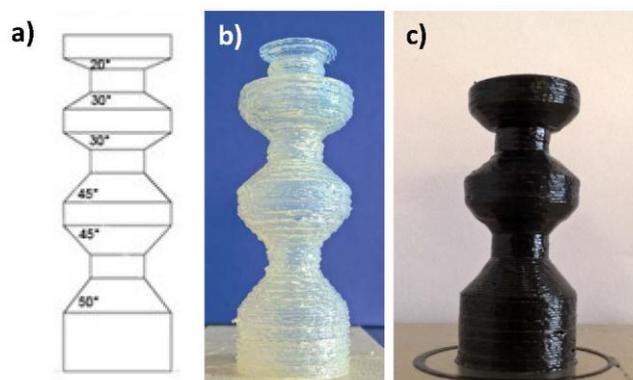


Figure S4. 3D digital model (a) and UV-3D printed reproductions of the object used to demonstrate the printability of the GFR (b) and CFR (c) composite formulations developed in this work.

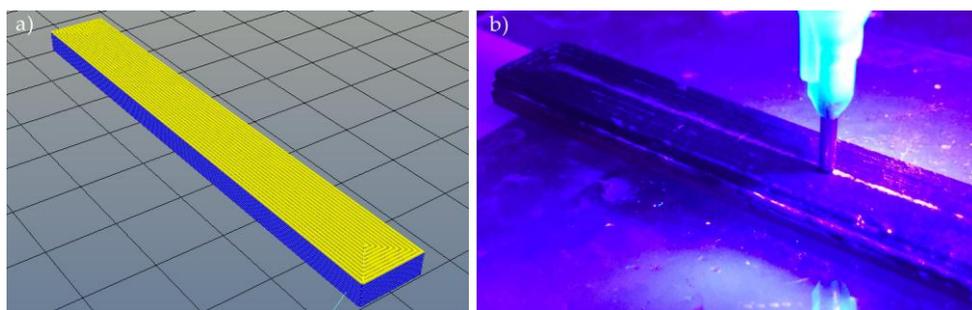


Figure S5. (a) 3D slicing model of a representative specimen (obtained using Cura, Ultimaker B.V.) and (b) detail of the UV-3D printing process of a CFR formulation.