



Article In Situ Grown 1D/2D Structure of Dy₃Si₂C₂ on SiC_w for Enhanced Electromagnetic Wave Absorption

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Abstract: To improve electromagnetic wave (EMW) absorption performance, a novel nano-laminated $Dy_3Si_2C_2$ coating was successfully in situ coated on the surface of SiC whisker (SiC_w/Dy₃Si₂C₂) using a molten salt approach. A labyrinthine three-dimensional (3D) net was constructed by the one-dimensional (1D) SiC_w coated with the two-dimensional (2D) Dy₃Si₂C₂ layer with a thickness of ~100 nm, which significantly improved the EMW absorption properties of SiC_w. Compared to pure SiC_w with the minimum reflection loss (RL_{min}) value of -10.64 dB and the effective absorption bandwidth (EAB) of 1.04 GHz for the sample with a thickness of 4.5 mm, SiC_w/Dy₃Si₂C₂ showed a significantly better EMW absorption performance with RL_{min} of -32.09 dB and wider EAB of 3.76 GHz for thinner samples with a thickness of 1.76 mm. The enhancement of the EMW absorption performance could be ascribed to the improvement of impedance matching, enhanced conductance loss, interfacial polarization as well as multiple scattering. The SiC_w/Dy₃Si₂C₂ can be a candidate for EMW absorber applications due to its excellent EMW absorption performance and wide EAB for relatively thin samples, light weight, as well as potential oxidation and corrosion resistance at high temperatures.

Keywords: SiC whisker; Dy₃Si₂C₂; electromagnetic wave absorption; molten salt method

1. Introduction

Electromagnetic wave (EMW) radiation pollution seriously endangers human health, as a consequence of the widespread applications of the high frequency electronic devices [1–5]. In recent years, numerous EMW absorption materials have been developed to solve these problems [6,7], including carbon-based materials [8,9], magnetic metal materials [10–12], ferrite and its composites [13–15], and polymer matrix composites [16–18]. However, the poor oxidation resistance of carbon-based materials and polymer matrix composites at high temperatures has impeded their applications, despite their excellent EMW absorption properties [19]. Magnetic materials also cannot be used at high temperatures due to the demagnetization [20]. Furthermore, a relatively high density of ferrite materials also hinders their applications in some special fields, such as aerospace. Therefore, the development of high performance EMW absorption materials with high absorption capability, broad effective absorption bandwidth (EAB), low density as well as small thickness, and excellent oxidation resistance at high temperatures is a critical challenge in this field to minimize EMW radiation pollution.

SiC has been considered a promising candidate for EMW absorbers because it has excellent dielectric properties, high temperature stability, as well as outstanding oxidation and corrosion resistance [21,22]. Most of the works on SiC-based EMW absorption materials



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Copyright: © 2023 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). have been focused on the SiC nanoparticles (SiCNP), SiC fibers (SiC_f), SiC nanowires (SiCNWs), and SiC whiskers (SiC_w) [23–28]. Among all of them, one-dimensional (1D) SiC_w or SiCNWs have drawn the most significant attention, since they have large aspect ratio, which is good for dissipating current by providing long transport paths, resulting in a strong conduction loss [29]. Furthermore, a three-dimensional (3D) network can be easily constructed, which is beneficial to improving the EMW absorption performance [27,30]. However, the EMW absorption properties of pure SiC_w cannot meet the strict requirements of a strong absorption and a broad EAB because of the poor impedance matching and single EMW loss mechanism [31–33]. Therefore, many research works have been conducted to improve the EMW absorption properties of SiC_w, including elemental doping, surface modification, and fabrication of SiC_w-based composites [34,35]. For example, Kuang et al. reported that the electrical conductivity of SiC_w was significantly enhanced by Al-doping. The lowest reflection loss (RL) value was –25.4 dB, and the EAB was 2 GHz when the Al/Si ratio was 0.03/0.97 [29]. In particular, surface modification of SiC_w has been demonstrated to be an efficient and feasible method for improving the EMW absorption [27,31,36].

Rare earth silicide carbides ($RE_3Si_2C_2$, where RE is a rare earth element) are a new group of ternary layered structure materials, which are similar to MAX phases (where M is an early transition metal, A is an A-group element, and X is either C or N) [37,38]. RE₃Si₂C₂ has been successfully used as the joining layer material and/or sintering additive for SiC-based ceramics and composites due to its ability to form a liquid phase by the eutectic reaction with SiC [39–46]. Furthermore, the addition of a second phase can significantly promote the EMW absorption properties of the resulting composites [47,48]. Our previous work indicated that the EMW absorption properties of SiC_f can be significantly improved by the incorporation of $Y_3Si_2C_2$ coating on the SiC_f surface [3]. The minimum RL of $SiC_{f}/Y_{3}Si_{2}C_{2}$ was -16.98 dB at a thin thickness of 2.19 mm. Furthermore, compared to the EAB of 1.92 GHz at the thickness of 3.38 mm for pure SiC fiber, $SiC_f/Y_3Si_2C_2$ shows significantly wider optimal EAB of 5.44 GHz at a much thinner thickness of 2.64 mm [3]. SiC_w whiskers have a larger aspect ratio compared to the chopped SiC fibers. It is relatively easy to form a 3D net, which is beneficial for increasing the heterogeneous interfaces and multiple reflections and scattering. Therefore, it is expected that $SiC_w/Dy_3Si_2C_2$ could show even better EMW absorption properties when compared to $SiC_f/Y_3Si_2C_2$.

In this work, the two-dimensional (2D) $Dy_3Si_2C_2$ coating is formed on the onedimensional (1D) SiC_w surface by the molten salt method to improve the EMW absorption properties. Combining $Dy_3Si_2C_2$ with SiC_w not only effectively improved the impedance matching but also provided a large number of heterogeneous interfaces as well as enhanced interface polarization loss. At the same time, the stacking effect of one-dimensional structures builds an efficient three-dimensional conductive network that enhances resistance loss. Furthermore, the two-dimensional layered structure of $Dy_3Si_2C_2$ can improve multiple reflections, which is beneficial to improving the EMW absorption properties. Microstructure, phase composition, dielectric, and EMW absorption properties of the as-obtained $SiC_w/Dy_3Si_2C_2$ coated whiskers were investigated. The possible EMW absorption mechanism of $SiC_w/Dy_3Si_2C_2$ was summarized. EMW absorption properties of the as-obtained $SiC_w/Dy_3Si_2C_2$ were compared to the previously reported materials.

2. Experimental Procedure

2.1. Materials and Experiments

DyH₂ powder with a purity of 99.9% and a mean particle size of ~75 μ m was purchased from Institute of Hunan rare earth metal materials Co., Ltd., Changsha, China. SiC whiskers (Union Materials Co., Daegu, Republic of Korea) with a diameter of 0.4–0.9 μ m and a length of 6–120 μ m; NaCl; and KCl powders (purity: 99.5%, mean particle size: 75 μ m; Sinopharm Chemical Reagent Co., Ltd., Shanghai, China) were used as the raw materials.

The DyH₂, SiC_w, NaCl, and KCl powders with the molar ratio of DyH₂: SiC_w =1:4 and NaCl:KCl = 1:1 were mixed for 30 min in an Ar atmosphere in a home-made glove box. The mixed DyH₂, SiC_w, NaCl, and KCl powders were heated to a target temperature of 1000 $^{\circ}$ C

in the molten salt furnace. The holding time was set 5 h. The heating and cooling rate was 5 °C/min. The as-obtained samples were washed and filtered using deionized water several times. The in situ coated $SiC_w/Dy_3Si_2C_2$ powder can be obtained after drying 12 h at 60 °C in a vacuum oven.

2.2. Characterizations

The phase compositions of the as-obtained $SiC_w/Dy_3Si_2C_2$ were detected using an X-ray diffractometer (XRD: D8 Advance, Bruker AXS, Karlsruhe, Germany) using Cu Kα radiation ($\lambda = 1.5406$ Å). The operating current and voltage were 40 mA and 40 kV, respectively. The step scan and step time was 0.02° 20 and 0.2 s, respectively. The microstructure of the $SiC_w/Dy_3Si_2C_2$ powders was observed using a scanning electron microscope (SEM, 8230, Hitachi, Tokyo, Japan). The microstructure and phase compositions of the $Dy_3Si_2C_2$ coating were further investigated using a transmission electron microscope (TEM, Talos F200X, Thermo Fisher Scientific, Waltham, MA, USA) equipped with an energy dispersive spectroscopy (EDS) system. The samples for TEM observations were prepared using the focused ion beam (FIB, Auriga, Carl Zeiss, Jena, Germany) technique. The complex permittivity and complex permeability were measured at a frequency range from 2 to 18 GHz using a Network Analyzer of Agilent N5230A. In order to measure the complex permittivity and complex permeability, SiC_w/Dy₃Si₂C₂ powder was mixed with 50 wt.% paraffin with a size of an inner and outer diameter of 3 and 7 mm as well as a thickness of 2 mm, respectively. For the sake of comparison, the electromagnetic properties of the pure SiC whiskers were detected using the same method.

3. Results and Discussion

3.1. Microstructure and Phase Composition of $SiC_w/Dy_3Si_2C_2$

Figure 1 presents the XRD patterns of the pure SiC whiskers and the as-obtained $SiC_w/Dy_3Si_2C_2$ whiskers.

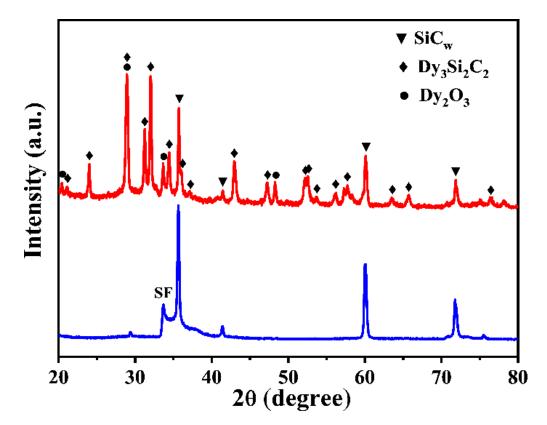


Figure 1. XRD patterns of pure SiC and $SiC_w/Dy_3Si_2C_2$ whiskers.

The XRD pattern of pure SiC whiskers indicated that they are formed by the 3C-SiC phase (JCPDS No. 75-0254). A small peak at approximately 33.5° corresponds to the stacking faults, which spontaneously formed during the growing process of SiC whiskers. The XRD pattern of the SiC_w / Dy₃Si₂C₂ powder revealed that besides SiC_w, it also contained characteristic peaks of Dy₃Si₂C₂ (JCPDS No. 97-005-1299) along with some impurities of Dy₂O₃ (JCPDS No. 97-018-5606). This confirmed that the Dy₃Si₂C₂ modification of SiC whiskers was successfully obtained.

Figure 2 shows the SEM images of both SiC_w and $SiC_w/Dy_3Si_2C_2$ whiskers.

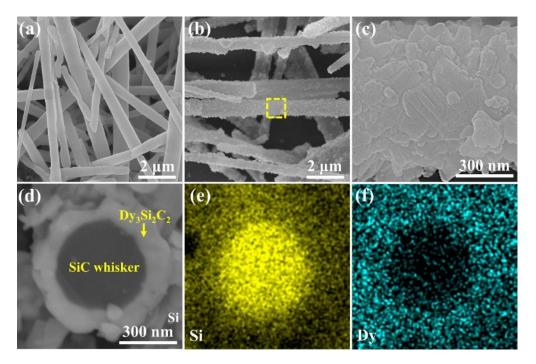


Figure 2. SEM images of pure SiC_w (**a**) and SiC_w/Dy₃Si₂C₂ (**b**,**c**), (**c**) is the high magnification SEM image of the yellow dashed area in (**b**), cross-section back scattered SEM image of SiC_w/Dy₃Si₂C₂ (**d**) and its corresponding EDS elemental distribution of Si (**e**) and Dy (**f**).

The diameter of the pure SiC whiskers was ~500 nm. A dense 2D structure $Dy_3Si_2C_2$ coating with a structure of randomly oriented nano-laminated sheets was in situ coated on the surface of SiC whiskers (Figure 2b,c). The thickness of $Dy_3Si_2C_2$ coating was around 100 nm, as shown in the SEM image of the fracture surface of the $SiC_w/Dy_3Si_2C_2$ whisker (Figure 2d). The corresponding elemental distribution of Si and Dy indicated that most of the $Dy_3Si_2C_2$ was homogenously coated on the surface of SiC whisker (Figure 2e,f).

To further confirm the microstructure and phase composition of the $Dy_3Si_2C_2$ coating, semi-quantitative EDS and high-resolution transmission electron microscope (HR-TEM) analysis along with selected-area electron diffraction (SAED) were performed. Figure 3 presents a high-angle annular dark-field (HAADF) image of the as-synthesized SiC_w/ $Dy_3Si_2C_2$ and the corresponding Dy, Si, C, and O elemental distributions, respectively.

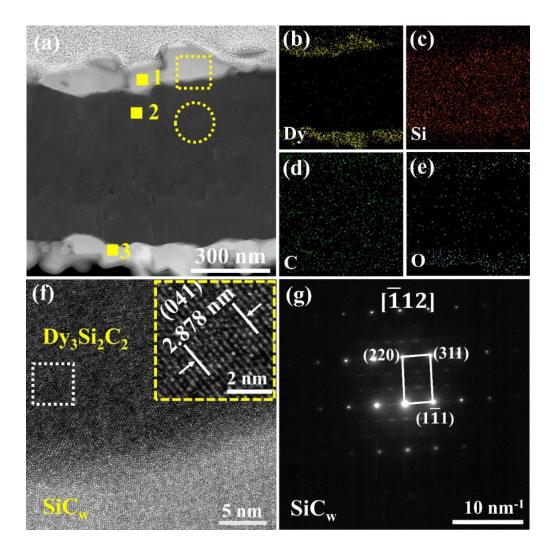


Figure 3. (a) HAADF image of the as-synthesized $SiC_w/Dy_3Si_2C_2$ and the corresponding EDS mapping of (b) Dy, (c) Si, (d) C, and (e) O, (f) HR–TEM image of the $Dy_3Si_2C_2$ coating, as highlighted by a yellow rectangle in (a), and (g) the SAED pattern taken from the area highlighted by the yellow circle in (a).

The semiquantitative EDS analysis results of areas 1–3 are shown in Table 1, suggesting the presence of SiC, $Dy_3Si_2C_2$, and/or Dy_2O_3 .

No.	Composition in Atomic %				Probable Phases
	Dy	Si	С	0	1100401011114505
1	45.92	23.11	15.72	15.25	Dy ₃ Si ₂ C ₂ , Dy ₂ O ₃
2	0.39	59.29	36.12	4.20	SiCw
3	42.11	22.98	16.99	17.93	$Dy_3Si_2C_2$, Dy_2O_3

 Table 1. EDS results collected from points 1–3 in Figure 3a.

Furthermore, the HR-TEM image of the interface between SiC_w and $Dy_3Si_2C_2$ coating is shown in Figure 3f. The lattice fringe spacing was 0.2878 nm, which can be assigned to the (041) planes of $Dy_3Si_2C_2$. Therefore, taking into account all the results obtained by XRD, EDS, and HR-TEM analysis, it can be concluded that a dense ~100 nm $Dy_3Si_2C_2$ coating was successfully fabricated on the surface of SiC_w using the molten salt approach.

The formation process of the $Dy_3Si_2C_2$ coating using the molten salt approach is similar to the formation mechanism of $Y_3Si_2C_2$ and $Pr_3Si_2C_2$ powders [45,48]. First, DyH_2

decomposed to Dy and released H_2 [49]. The Dy element diffused to the surface of SiC whiskers via the liquid molten salt, and then the $Dy_3Si_2C_2$ coating was formed. The main reactions can be summarized as follow:

$$DyH_2 \rightarrow Dy + H_2$$
 (1)

$$3Dy + 2SiC \rightarrow Dy_3Si_2C_2$$
 (2)

On the other hand, the potential formation barrier of the $Dy_3Si_2C_2$ could decline because the surface energy of both DyH_2 and SiC_w could be remarkably promoted by polarization effect of the molten salt [50,51]. In addition, the diffusion rate of the Dy, Si, and C atoms can be obviously promoted in the liquid molten salt reaction medium. Therefore, the $Dy_3Si_2C_2$ coating can be in situ formed on the surface of SiC whiskers at a relatively low temperature (1000 °C) and adhered well to the surface of SiC_w.

3.2. Dielectric Properties of $SiC_w/Dy_3Si_2C_2$

The EMW absorption property of materials is mainly confirmed by their complex permittivity and permeability. Meanwhile, good impedance matching between absorbing materials and free space can make EMW incident into materials with less reflection. While SiC_w and $SiC_w/Dy_3Si_2C_2$ are nonmagnetic materials, the real (μ') and imaginary (μ'') parts of the complex permeability is around 1 and 0, respectively (not shown here). Therefore, the EMW absorption capability of SiC_w and $SiC_w/Dy_3Si_2C_2$ is highly dependent on their complex permittivity. The real (ε') and imaginary (ε'') parts of complex permittivity of the pure SiC_w and $SiC_w/Dy_3Si_2C_2$ whiskers are shown in Figure 4.

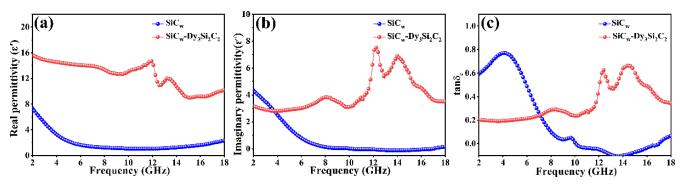


Figure 4. Real (**a**) and imaginary (**b**) parts of the complex permittivity, as well as the loss angle (**c**) of the pure SiC_w and $SiC_w/Dy_3Si_2C_2$ whiskers.

Most of the real (ε') and imaginary (ε'') parts of the complex permittivity of SiC_w/Dy₃Si₂C₂ were higher than that of pure SiC_w, indicating that the Dy₃Si₂C₂ coating could promote the dielectric properties of SiC_w.

According to the Debye theory, ε' and ε'' can be calculated by the following equations [52]:

$$\varepsilon' = \varepsilon_{\infty} + (\varepsilon_s - \varepsilon_{\infty}) / \left(1 + (\omega \tau)^2 \right)$$
(3)

$$\varepsilon'' = (\varepsilon_s - \varepsilon_{\infty}) / \left(1 + (\omega \tau)^2 \right) + \delta_{ac} / \omega \varepsilon_0 = \varepsilon_p'' + \varepsilon_c'' \tag{4}$$

where ε_0 , ε_s , and ε_∞ represent free space dielectric constant, the permittivity in static state, and light frequency, respectively. ω and τ are angular frequency and polarization relaxation time, respectively. σ is electric conductivity. ε_p'' and ε_c'' correspond to the contributions to ε'' from polarization loss and conductance loss, which are associated with σ . Generally, the real part of the permittivity signifies the storage capability of the dielectric energy, while the imaginary part of the permittivity stands for the loss of dielectric energy [53]. Thus, the improvement of ε' can be ascribed to the interfacial polarization caused by the improved heterogeneous interfaces in SiC_w / Dy₃Si₂C₂ whiskers, which were generated by the incorporation of nano-laminated (2D) Dy₃Si₂C₂ coating on the surface of SiC_w. The enhancement of ε'' was mainly decided by the increasing of the electrical conductivity (σ), where σ can be confirmed by the follow equation [54]:

$$\sigma = 2\pi\varepsilon_0\varepsilon\varepsilon'' \tag{5}$$

where ε_0 represents the permittivity in a vacuum.

The electrical conductivity of $SiC_w/Dy_3Si_2C_2$ was higher than that of pure SiC_w , as shown in Figure 5a.

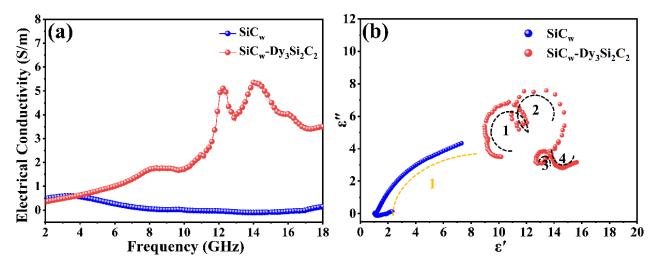


Figure 5. Electrical conductivity (a,b) Cole–Cole curves of the pure SiC_w and SiC_w / Dy₃Si₂C₂.

This can be mainly attributed to the metallic conductivity characteristic of the 2D structural Dy₃Si₂C₂ coating, as the coating formed a net structure, increasing the transmission channels of carriers [55]. In addition, both ε' and ε'' of SiC_w/Dy₃Si₂C₂ showed a fluctuation corresponding to the resonance, while this was not observed for the pure SiC_w. The permittivity of the SiC_w/Dy₃Si₂C₂ whiskers showed typical nonlinear resonant characteristics, indicating the existence of polarization and relaxation behavior, which implied better dielectric loss performance in the corresponding frequency range. The Cole–Cole semicircle was used to investigate the relaxation polarization process. According to the Debye theory, the relationship between ε' and ε'' can be expressed by Equation (6) [56]:

$$\left(\varepsilon'' - \left(\varepsilon_s + \varepsilon_{\infty}\right)/2\right)^2 + \varepsilon'' = \left(\varepsilon_s - \varepsilon_{\infty}\right)/2 \tag{6}$$

The Cole–Cole curves of pure SiC_w and SiC_w/Dy₃Si₂C₂ are shown in Figure 5b. Each Deby relaxation process is manifested by one Cole–Cloe semicircle [55,56]. There was only one Cole–Cole semicircle observed in pure SiC_w, indicating one relaxation process, while four semicircles were observed in SiC_w/Dy₃Si₂C₂, confirming the improvement of dielectric loss capacity in SiC_w/Dy₃Si₂C₂. The improvement of the relaxation process of SiC_w/Dy₃Si₂C₂ was mainly caused by the significantly increased interface relaxation, which resulted from the improved number of heterogeneous interfaces in SiC_w/Dy₃Si₂C₂.

3.3. Electromagnetic Wave Absorption Performance

Reflection loss (RL) and effective absorption bandwidth (EAB, the corresponding frequency range of RL < -10 dB, which presents more than 90% EMW energy absorbed) are usually used to evaluate the EMW absorption performance of materials. According to

the transmission line theory, the RL values of SiC_w and $SiC_w/Dy_3Si_2C_2$ can be calculated by the following equations [57–59]:

$$RL(dB) = 20\log|(Z_{in} - Z_0)/(Z_{in} + Z_0)|$$
(7)

$$Z_{in} = Z_0 \sqrt{\mu_r / \varepsilon_r} \tanh[j(2\pi f d/c) \sqrt{\mu_r \varepsilon_r}]$$
(8)

$$Z_0 = \sqrt{\mu_r / \varepsilon_r} \tag{9}$$

where Z_0 and Z_{in} is space free impedance and input impedance, respectively. c, d, and f are speed of light, thickness, and frequency, respectively. $\mu_r = \mu' - j\mu''$ and $\varepsilon_r = \varepsilon' - j\varepsilon''$ represent the complex permeability and permittivity of material.

Figure 6 shows the 3D and 2D plots of RL values at the frequency range of 2 to 18 GHz at different thicknesses of the SiC_w and $SiC_w/Dy_3Si_2C_2$ samples.

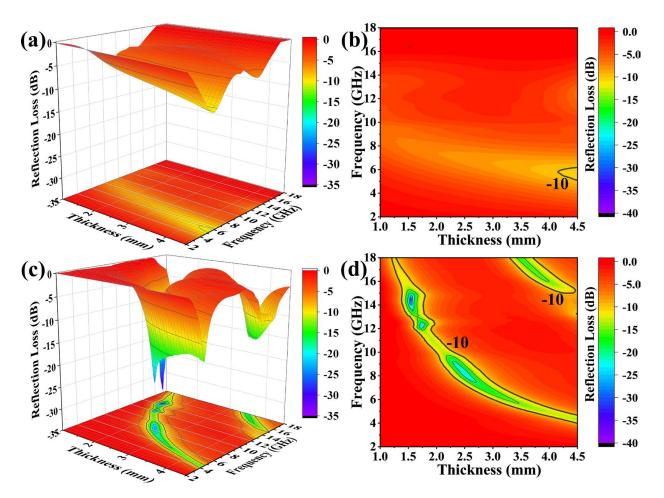


Figure 6. 3D and 2D patterns of RL values at the frequency range of 2 to 18 GHz for different thicknesses of SiC_w (**a**,**b**) and SiC_w -Dy₃Si₂C₂ samples (**c**,**d**).

The minimum RL (RL_{min}) value of the pure SiC_w is -10.64 dB at the frequency of 5.52 GHz with the 4.5 mm sample thickness. After coating of SiC_w with 2D Dy₃Si₂C₂ sheets, the RL_{min} value was improved to -32.09 dB at the frequency of 14.48 GHz for the 1.54 mm sample thickness. For convenience of comparison, the selected theoretical calculated RL of pure SiC_w and SiC_w/Dy₃Si₂C₂ with different thicknesses in the frequency range of 2 to 18 GHz is shown in Figure 7a,b.

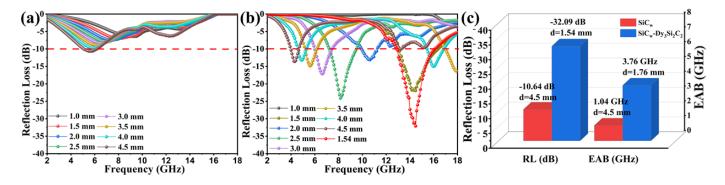


Figure 7. RE values at the frequency range of 2 to 18 GHz for different thicknesses of the SiC_w (a) and $SiC_w/Dy_3Si_2C_2$ samples (b), (c) comparison of the RL_{min} and EAB of the pure SiC_w and $SiC_w-Dy_3Si_2C_2$ samples.

It is obvious that the EAB of $SiC_w/Dy_3Si_2C_2$ is much wider than that of SiC_w for the samples with the thickness range of 1 to 4.5 mm at the frequency ranging from 2 to 18 GHz. The widest EAB can be as high as 3.76 GHz for thin $SiC_w/Dy_3Si_2C_2$ samples with the thickness of 1.76 mm (Figure 7c). However, the widest EAB of pure SiC_w is only 1.04 GHz for the sample with a thickness of 4.5 mm (Figure 7c). This indicates that the $Dy_3Si_2C_2$ coating can significantly improve the EMW absorption properties of SiC_w .

In order to reveal the intrinsic reason for the improved EMW absorption performance for $SiC_w/Dy_3Si_2C_2$, the impedance match (*Z*) as well as the attenuation constant (α) were calculated. *Z* was confirmed by the following equation [60]:

$$Z = |Z_{in}/Z_0| = \sqrt{\mu_r/\varepsilon_r \tanh[j(2\pi f d/c)\sqrt{\mu_r\varepsilon_r}]}$$
(10)

A favorable impedance match is the basic requirement to obtain an excellent EMW absorption performance, which ensures the EMW can enter materials instead of being reflected [61–64]. According to Equation (10), when the input impedance (Z_{in}) is infinitely close to the air impedance (Z_0), the ideal impedance matching can be obtained. Figure 8a,b presents the calculated Z values of the pure SiC_w and SiC_w/Dy₃Si₂C₂ samples with the thickness of 1–4.5 mm at the frequency ranging from 2 to 18 GHz.

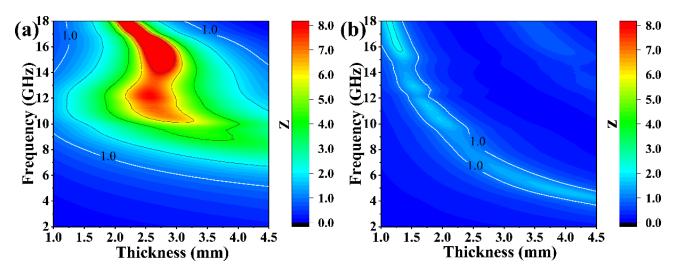


Figure 8. 2D patterns of Z value of SiC_w (**a**) and $SiC_w/Dy_3Si_2C_2$ (**b**).

The frequency range with good impedance match (Z-value is close to 1) of $SiC_w/Dy_3Si_2C_2$ was much larger than that of pure SiC_w , which indicates that the impedance match of the SiC_w was well improved by the $Dy_3Si_2C_2$ coating. Therefore, the EMW can enter the

Furthermore, to evaluate the attenuation ability of EMW energy of the samples, the α (Figure 9) was evaluated by the following formula [53]:

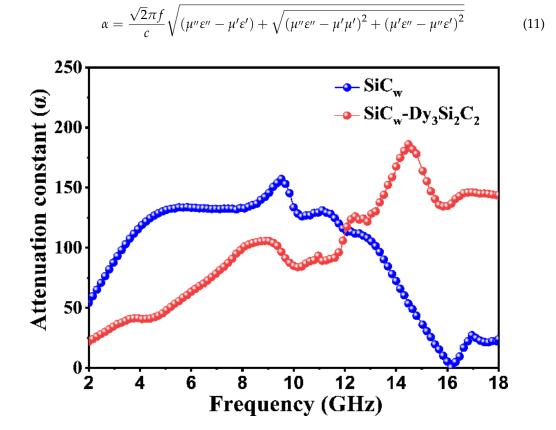
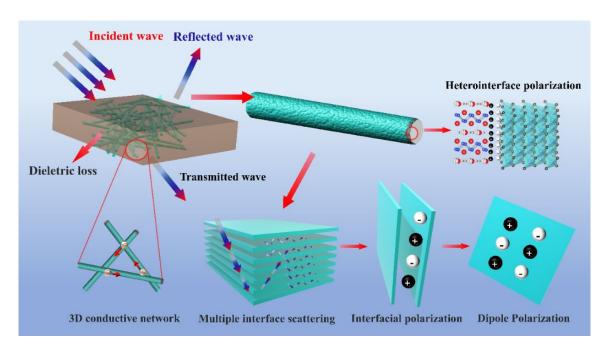


Figure 9. Attenuation constant of pure SiC_w and $SiC_w/Dy_3Si_2C_2$ at the frequency range from 2 to 18 GHz.

A larger value of α implies a stronger attenuation ability [65]. The sole high dielectric loss of SiC_w at a low frequency resulted in a high attenuation constant, which meant that most of the EMW was reflected. This is in good agreement with the poor impedance matching of the SiC_w sample. On the other hand, the introduction of the nano-laminated (2D) Dy₃Si₂C₂ coating significantly improved the impedance match as well as the attenuation ability of the SiC_w/Dy₃Si₂C₂. As a result, the EMW absorption property was significantly improved.

The possible EMW absorption mechanism of SiC_w/Dy₃Si₂C₂ is illustrated in Figure 10. Firstly, the favorable impedance matching suggests that the majority of the EMW can enter the SiC_w/Dy₃Si₂C₂ sample, while just a small part of the EMW is reflected. This is the premise of excellent EMW absorption performance of the material. Secondly, the metallic conductivity characteristic of Dy₃Si₂C₂ coating improved the electrical conductivity of SiC_w/Dy₃Si₂C₂, which enhanced the conductance loss by improving the electron transition channel in SiC_w/Dy₃Si₂C₂. Thirdly, a large number of heterogeneous interfaces in the SiC_w/Dy₃Si₂C₂ sample, such as Dy₃Si₂C₂/Dy₃Si₂C₂, SiC_w/Dy₃Si₂C₂, and SiC_w/SiC_w, significantly increased the interfacial polarization and hopping electrons between Dy₃Si₂C₂ nanosheets. This is beneficial for the improvement of the dielectric loss of the material. Finally, the high aspect ratio of SiC_w with the 2D nano-laminated Dy₃Si₂C₂ coating constructed a 3D microstructure and formed an effective conductive network, resulting in the enhancement of multiple scattering and reflections. Therefore, the excellent EMW absorption performance of SiC_w/Dy₃Si₂C₂ was attributed to the synergistic effect of fa-



vorable impedance matching, enhanced conductance loss, interfacial polarization, dipole polarization, and multiple scattering and reflections.

Figure 10. The EMW absorption mechanism of $SiC_w/Dy_3Si_2C_2$.

The EMW absorption property of $SiC_w/Dy_3Si_2C_2$ is better when compared to most of the previously reported materials, as shown in Figure 11.

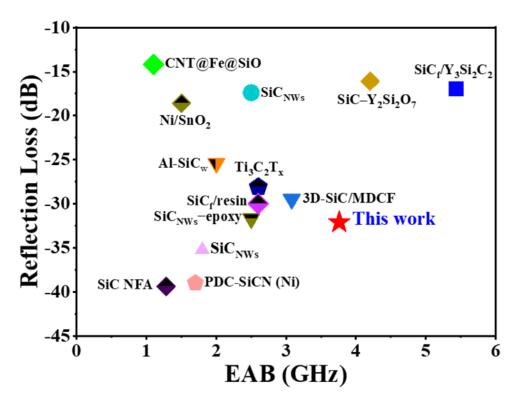


Figure 11. The comparison of EMW absorption properties of $SiC_w/Dy_3Si_2C_2$ with other materials [3,23,29,66–75].

It can be concluded that the as-obtained $SiC_w/Dy_3Si_2C_2$ whiskers could be a promising candidate for EMW absorbers for aerospace applications due to their excellent EMW absorption performance and wide EAB for thin samples, light weight, and potential oxidation resistance at high temperatures.

4. Conclusions

In summary, a novel nano-laminated $Dy_3Si_2C_2$ coating was in situ fabricated on the surface of SiC_w using the molten salt method to improve EMW absorption performance. A randomly stacked 2D $Dy_3Si_2C_2$ nanosheet coating with a thickness of ~100 nm was uniformly coated on the surface of 1D SiC_w, which further formed a 3D microstructure. The EMW absorption performance of the as-obtained 3D structural SiC_w/Dy₃Si₂C₂ sample was significantly improved when compared to the pure SiC_w sample. The minimum RL value increased from -10.64 dB for the pure SiC_w to -32.09 dB for the SiC_w/Dy₃Si₂C₂. At the same time, the corresponding thickness of 1.54 mm was much thinner than that of the pure SiC_w (4.5 mm). The possible EMW absorption mechanism of the as-obtained SiC_w/Dy₃Si₂C₂ sample was ascribed to the synergic effect of favorable impedance matching, enhanced conductance loss, interfacial polarization, dipole polarization, and multiple scattering. The as-obtained 3D structural SiC_w/Dy₃Si₂C₂ could be a candidate for EMW absorber applications due to its excellent EMW absorption performance and wide EAB for relatively thin samples, light weight, as well as potential oxidation and corrosion resistance at high temperatures.

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